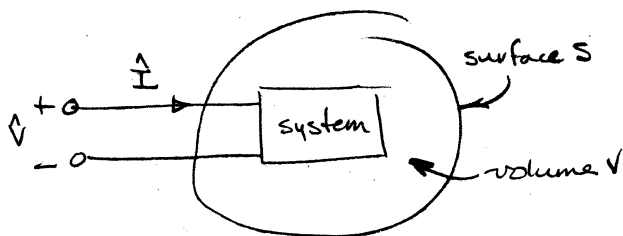


1. (a) Using complex Poynting's theorem find the complex admittance of a system. Use an equivalent parallel RLC circuit as a model.

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$$-\nabla \cdot \hat{\mathbf{P}} = \frac{1}{2} \hat{\mathbf{E}} \cdot \hat{\mathbf{J}}^* + 2j\omega \left[\frac{1}{4} \mu |\hat{\mathbf{H}}|^2 - \frac{1}{4} \epsilon |\hat{\mathbf{E}}|^2 \right] \quad (1)$$



$$Y = \frac{\hat{\mathbf{I}}}{\hat{\mathbf{V}}} = \frac{\hat{\mathbf{I}} \hat{\mathbf{V}}^*}{|\hat{\mathbf{V}}|^2} = 2 \frac{\frac{1}{2} \hat{\mathbf{I}} \hat{\mathbf{V}}^*}{|\hat{\mathbf{V}}|^2} = 2 \frac{\left(- \oint_S \hat{\mathbf{P}} \cdot d\hat{\mathbf{S}} \right)^*}{|\hat{\mathbf{V}}|^2} \quad (2)$$

complex power input to the system

integrating eq (1) over the volume V and using Gauss' theorem

$$- \oint_S \hat{\mathbf{P}} \cdot d\hat{\mathbf{S}} = \int_{vol} \frac{\hat{\mathbf{E}} \cdot \hat{\mathbf{J}}^*}{2} dV + 2j\omega \int_{vol} \left[\frac{1}{4} \mu |\hat{\mathbf{H}}|^2 - \frac{1}{4} \epsilon |\hat{\mathbf{E}}|^2 \right] dV \quad (3)$$

$$\left(\frac{1}{2} \hat{\mathbf{I}} \hat{\mathbf{V}}^* \right) = \langle P_d \rangle + 2j\omega [\langle u_m \rangle - \langle u_e \rangle] \quad (4)$$

where $\langle P_d \rangle \triangleq \int_{vol} \frac{\hat{\mathbf{E}} \cdot \hat{\mathbf{J}}^*}{2} dV$ average power dissipated (5)

$\langle u_m \rangle \triangleq \int_{vol} \frac{1}{4} \mu |\hat{\mathbf{H}}|^2$ average stored magnetic energy (6)

$\langle u_e \rangle \triangleq$ average stored electric energy (7)

Note that $-\oint_S \hat{\mathbf{P}} \cdot d\hat{\mathbf{S}} = \frac{1}{2} \hat{\mathbf{I}} \hat{\mathbf{V}}^*$ (8)

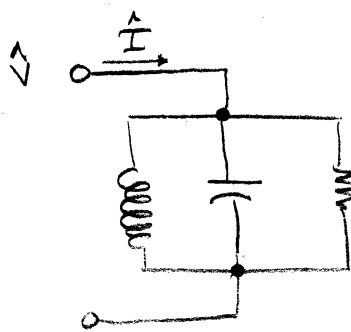
$$\frac{1}{2} \hat{\mathbf{I}} \hat{\mathbf{V}}^* = \left(\frac{1}{2} \hat{\mathbf{V}} \hat{\mathbf{I}}^* \right)^* = \left\{ \langle P_d \rangle + 2j\omega [\langle u_m \rangle - \langle u_e \rangle] \right\}^* \quad (9)$$

$$= \langle P_d \rangle + 2j\omega [\langle u_e \rangle - \langle u_m \rangle] \quad \checkmark \text{ good} \quad (10)$$

Substituting eq (10) into eq (2) we obtain

$$Y = \frac{2}{|\hat{\mathbf{V}}|^2} \left[\langle P_d \rangle + 2j\omega [\langle u_e \rangle - \langle u_m \rangle] \right]$$

u - energy density
 $\int u dV$
 V - energy (11)



$$\langle u_m \rangle = \frac{V V^*}{4\omega^2 L} \quad (12) \quad \langle u_e \rangle = \frac{C V V^*}{4} \quad (13) \quad \langle P_d \rangle = \frac{V V^*}{2R} \quad (14)$$

Using (12)(13)(14) in (11) we obtain

$$Y = \frac{2}{|V|^2} \left[\frac{|V|^2}{2R} + 2j\omega \left[\frac{C|V|^2}{4} - \frac{|V|^2}{4\omega^2 L} \right] \right] \quad (15)$$

(b) Find an equation for the admittance near the resonant frequency and determine the Q.

resonance occurs when $\frac{C|V|^2}{4} - \frac{|V|^2}{4\omega^2 L} = 0 \quad (16)$

$$\omega_0^2 = \frac{1}{LC} \quad (17)$$

$$Y = Y(\omega_0) + (\omega - \omega_0) \left. \frac{\partial Y}{\partial \omega} \right|_{\omega = \omega_0} \quad (18)$$

$$= \frac{2}{|V|^2} \left[\frac{|V|^2}{2R} + 2j\omega_0 \left[\frac{C|V|^2}{4} - \frac{|V|^2}{4\omega_0^2 L} \right] \right] + (\omega - \omega_0) \frac{4j}{|V|^2} \left[\frac{C|V|^2}{4} + \frac{|V|^2}{4\omega^2 L} \right] \quad (19)$$

$$Y = \frac{2}{|V|^2} \left[\frac{|V|^2}{2R} \right] + (\omega - \omega_0) \frac{4j}{|V|^2} \left[\frac{C|V|^2}{4} + \frac{|V|^2}{4\omega_0^2 L} \right] \quad (20)$$

$$Y \approx \frac{2}{|V|^2} \left[\frac{|V|^2}{2R} + 2j(\omega - \omega_0) \left\{ \frac{C|V|^2}{4} + \frac{|V|^2}{4\omega_0^2 L} \right\} \right] \quad (21)$$

$$\frac{|V|^2}{2R} + 2j(\omega - \omega_0) \left[\frac{C|V|^2}{4} + \frac{|V|^2}{4\omega_0^2 L} \right] = 0 \quad (22)$$

$$\Delta\omega = 2(\omega - \omega_0) = \frac{\frac{|V|^2}{2R}}{\frac{C|V|^2}{4} + \frac{|V|^2}{4\omega_0^2 L}} \quad (23)$$

$$Q = \frac{\omega_0}{\Delta\omega} = \frac{\omega_0}{\frac{1}{2R}} \left[\frac{C\omega_0^2}{4} + \frac{1}{4\omega_0^2 L} \right] \quad (24)$$

$$= 2R\omega_0 \left[\frac{C}{4} + \frac{1}{4\omega_0^2 L} \right] = RC\omega_0 \quad (25)$$

$\omega_0^2 = \frac{1}{LC}$

$$Q = \frac{\omega_0 RC}{2} + \frac{R}{2\omega_0 L} \quad (26)$$

(c) Determine the change in resonant frequency for a small change in the magnetic permeability. Hint: Consider the equivalent inductance to be proportional to the permeability.

i.e. I wish to determine $\frac{\partial\omega_0}{\partial L}$

differentiating eq. (17) with respect to ω_0

$$2\omega_0 \frac{\partial\omega_0}{\partial L} = \frac{1}{C} \left(-\frac{1}{L^2} \right)$$

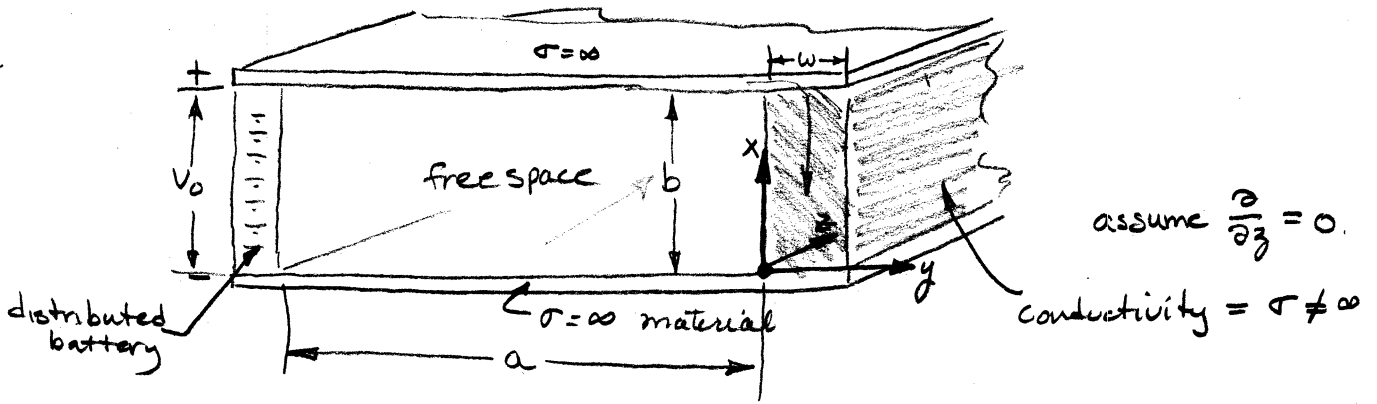
$$\frac{\partial\omega_0}{\partial L} = \frac{1}{2\omega_0} \left(-\frac{1}{L^2} \right) = -\frac{1}{2\omega_0 L^2}$$

See solution

$$\Delta Y = \frac{\partial Y}{\partial \omega} \Big|_{\omega_0} (\omega - \omega_0) + \left(\frac{\partial Y}{\partial L} \frac{\partial L}{\partial \mu} \right)_{\omega_0} \Delta \mu \quad \text{which is set } = 0$$

$\Delta Y = 0$ since we change ω from ω_0 to return to the resonant condition i.e. $Y_0 + \Delta Y = 0$

2.



Note: Work the problem per unit length in the z -direction.

a) Determine the electric & magnetic fields in the resistor (surrounding region has zero conductivity)

Neglecting fringing fields.



$$\phi = - \int \mathbf{E} \cdot d\mathbf{l}$$

but in $\sigma = \infty$ material there can be no electric fields

assume $\vec{E} = -E_x \vec{u}_x$

$$\phi = V_0 = - \int_b^0 (-E_x \vec{u}_x) \cdot (-\vec{u}_x dx) = \int_0^b E_x dx$$

$$V_0 = E_x b$$

$$E_x = \frac{V_0}{b}$$

$$\vec{E} = - \frac{V_0}{b} \vec{u}_x$$

As this is a static problem

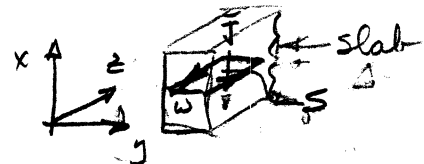


$$\oint_C \mathbf{H} \cdot d\mathbf{l} = \int_S \mathbf{J} \cdot d\mathbf{S}$$

pick a surface $S \perp (\vec{u}_z \times \vec{u}_y)$

$$\vec{J} = \sigma \vec{E} = -\sigma \frac{V_0}{b} \vec{u}_x$$

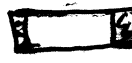
$$d\mathbf{S} = w dz \vec{u}_x$$



$$\int_S \mathbf{J} \cdot d\mathbf{S} = \int_0^{\Delta z} -\sigma \frac{V_0}{b} \vec{u}_x \cdot w dz \vec{u}_x = -\sigma \frac{V_0 w \Delta z}{b}$$

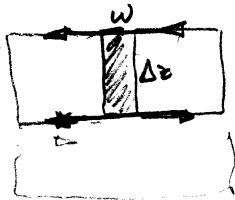
However, pick a new coordinate y' such that $y' = y - \frac{w}{2}$

$$\text{then } \int_S \mathbf{J} \cdot d\mathbf{S} = f(y) = -\sigma \frac{V_0 w \Delta z}{b} \quad |k| \leq \frac{w}{2}$$

Because of the symmetry of the problem there can be no y component of H . Furthermore $|H_z|$ must be the same on both sides of the resistor. (No!) 

$$\therefore \oint_C \vec{H} \cdot d\vec{l} = 2 H_z \Delta z$$

this is an entirely closed loop of current (like a solenoid) and the field is only inside its interior only - outside $E=H=0$

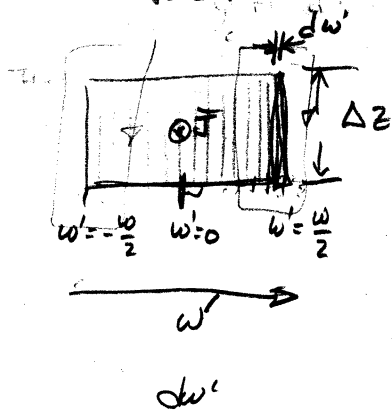


$$2 H_z \Delta z = - \frac{\sigma V_0 w \Delta z}{b}$$

$$H_z = - \frac{\sigma V_0 w}{2b}$$

good toy

Now H_{tan} must be discontinuous by the amount of surface current. Pick the surface of length Δz .



for each surface of thickness dw' the discontinuity in H_z is:

$$|\vec{J}| \frac{dw' \Delta z}{\Delta z} = |\vec{J}| dw'$$

$$\text{or } dH = |\vec{J}| \frac{dw'}{b} = - \frac{\sigma V_0}{b} dw'$$

$$\frac{dH}{dw'} = - \frac{\sigma V_0}{b}$$

$$H = - \frac{\sigma V_0}{b} w'^2$$

\Rightarrow the magnetic field in the resistor is given by

$$\vec{H} = - \frac{\sigma V_0}{b} \left(y - \frac{w}{2} \right) \vec{a}_z \quad 0 \leq y \leq w$$

(b) Show the solution for the potential within the space between the battery and the resistor is a solution of Laplace's equation.

$$\vec{E} \triangleq -\nabla\phi$$

$$\nabla \cdot \vec{E} = -\nabla \cdot \nabla\phi = -\nabla^2\phi$$

but $\nabla \cdot \epsilon\vec{E} = \rho$

$$\text{or } \nabla \cdot \vec{E} = \frac{\rho}{\epsilon}$$

$$\therefore \frac{\rho}{\epsilon} = -\nabla^2\phi$$

$\nabla^2\phi = -\frac{\rho}{\epsilon}$ but there are no charges in this region of space, i.e. $\rho=0$

$\Rightarrow \nabla^2\phi = 0$ (Laplace's equation) describes this region.

(c) Find and sketch the solution for potential and electric field within the space.

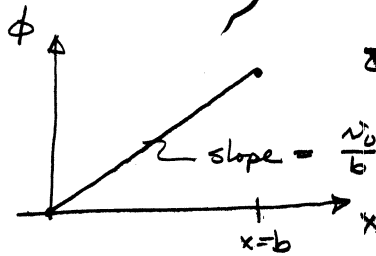
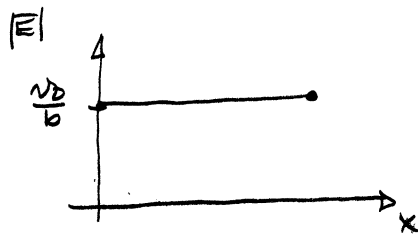
Because \vec{E} is continuous across the boundary of the resistor

$$\vec{E} = -\frac{V_0}{b} \vec{a}_x \quad \text{in the space}$$

$$\phi = -\int_0^x \vec{E} \cdot d\vec{l} = -\int_0^x -\frac{V_0}{b} \vec{a}_x \cdot x' \vec{a}_x = \int_0^x \frac{V_0}{b} dx'$$

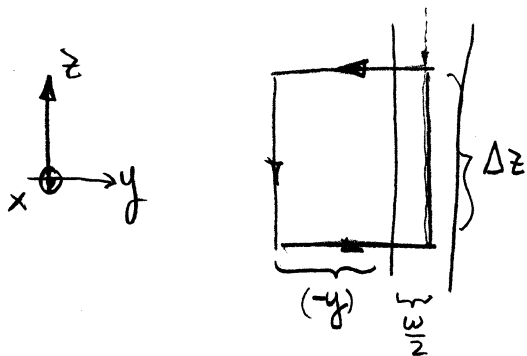
$$\phi = \frac{V_0 x}{b} \quad ; \quad \begin{cases} \phi(0) = 0 \\ \phi(b) = V_0 \end{cases}$$

\therefore Laplace's equation is satisfied. why is it satisfied within the free space region? It is with your solution but you only assumed the \vec{E} -field. In a more complicated problem you could not have done this.



Note: E_y and $E_z \equiv 0$

(d) Find and sketch the magnetic field within the space.



$$\oint \mathbf{H} \cdot d\mathbf{l} = \int_S \mathbf{J} \cdot d\mathbf{S}$$

because of symmetry and the choice of the contour

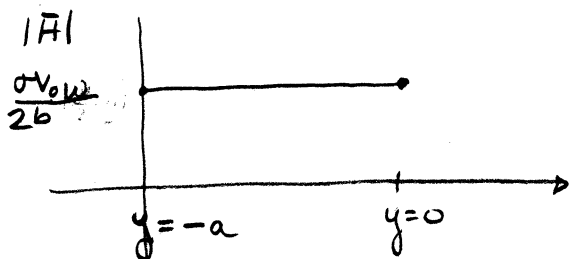
$$\oint \mathbf{H} \cdot d\mathbf{l} = -H_z \Delta z$$

$$\oint_S \mathbf{J} \cdot d\mathbf{S} = -\sigma \frac{V_0}{b} \hat{i}_x \cdot \left(\frac{\omega}{2}\right) \Delta z \hat{a}_x$$

$$\Leftrightarrow -H_z \Delta z = -\frac{\sigma V_0}{b} \left(\frac{\omega}{2}\right) \Delta z$$

$$H_z = \frac{\sigma V_0}{b} \left(\frac{\omega}{2}\right)$$

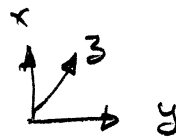
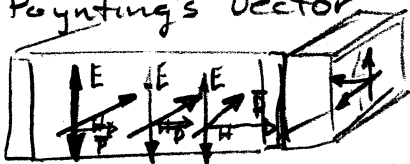
\Rightarrow The H field is constant throughout the resistive slab.



Δy
 z
 x

(e)

Sketch Poynting's vector



$$\begin{aligned} \vec{P} &= \vec{E} \times \vec{H} = \left(-\frac{V_0}{b} \hat{a}_x\right) \times \left(\frac{\sigma V_0 \omega}{2b} \hat{a}_y\right) \hat{a}_z \\ &= +\frac{\sigma V_0^2 \omega}{2b^2} \hat{a}_z \end{aligned}$$

(f) Show that Poynting's Theorem is satisfied by your results by investigating it in integral form on the resistor.

$$\oint_{\Sigma} \vec{P} \cdot d\vec{S} \stackrel{?}{=} - \int_V \vec{J} \cdot \vec{E} \, dV - \int_V \left[E \frac{\partial D}{\partial t} + H \cdot \frac{\partial B}{\partial t} \right] dV$$

FAKE! \int_V

The $\frac{1}{2}$ factor only enters in time varying problems.

$$\int_V \frac{\vec{J} \cdot \vec{E}}{2} dV \stackrel{NO}{=} \left(\frac{1}{2} - \frac{\sigma V_0 \bar{a}_x}{b} \right) \cdot -\frac{V_0}{b} \bar{a}_x \, w b \Delta z$$

$$= \frac{\sigma V_0^2 w}{2b} \Delta z$$

If you had used the correct Poynting's theorem you would have found a factor of $\frac{1}{2}$ error which resulted from your improper solution for \vec{H} !

$$\oint_{\Sigma} \vec{P} \cdot d\vec{S} = \frac{1}{2} \left(\frac{\sigma V_0^2 w}{2b^2} \bar{a}_y \right) \cdot \Delta z b (-\bar{a}_y) + \left(\frac{\sigma V_0^2 w}{2b^2} \bar{a}_y \right) \cdot \Delta z b \bar{a}_y$$

2 terms because at the $y=w$ plane there is an E field from

$$\oint_{\Sigma} \vec{P} \cdot d\vec{S} = -\frac{\sigma V_0^2 w}{4b} \Delta z - \frac{\sigma V_0^2 w}{4b} \Delta z$$

$$= -\frac{\sigma V_0^2 w}{2b} \Delta z$$

$$\Leftrightarrow \oint_{\Sigma} \vec{P} \cdot d\vec{S} = - \int_V \vec{J} \cdot \vec{E} \, dV$$

(g) From Ohm's law we would expect

$$P = \frac{V^2}{2R} \quad \text{or} \quad P = \frac{V_0^2}{2R} = \frac{V_0^2}{2 \rho \frac{L}{A}} = \frac{V_0^2}{2 \frac{L}{\sigma A}}$$

$$P = \frac{\sigma V_0^2 A}{2L}$$

$$= \frac{\sigma V_0^2 w \Delta z}{2b}$$

∴ the field concept does explain power flow.

3. Find Poynting's vector, electric and magnetic energy density for a uniform plane wave.

$$\text{let } \underline{\hat{E}} = \underline{\hat{E}}_0 e^{-jk_0 \underline{n} \cdot \underline{r}} \quad k_0 = \frac{\omega}{c} : \text{the wave number}$$

where $\underline{n} \cdot \underline{r}$ defines a plane perpendicular to \underline{n}
 \underline{n} is the direction of propagation of the wave
 $\underline{\hat{E}}_0$ is a constant vector.

Assume in free space. i.e. $B = \mu_0 H$

$$\text{Then } \nabla \times \underline{\hat{E}} = -j\omega\mu_0 \underline{\hat{H}}$$

$$\begin{aligned} \underline{\hat{H}} &= \frac{j}{\omega\mu_0} \nabla \times \underline{\hat{E}} = \frac{j}{\omega\mu_0} \nabla \times \underline{\hat{E}}_0 e^{-jk_0 \underline{n} \cdot \underline{r}} \\ &= \frac{j}{\omega\mu_0} \underline{\hat{E}}_0 \times \nabla e^{-jk_0 \underline{n} \cdot \underline{r}} = \frac{j}{\omega\mu_0} \underline{\hat{E}}_0 \times \underline{n} -jk_0 e^{-jk_0 \underline{n} \cdot \underline{r}} \\ \underline{\hat{H}} &= + \frac{k_0}{\omega\mu_0} \underline{\hat{E}}_0 \times \underline{n} e^{-jk_0 \underline{n} \cdot \underline{r}} \end{aligned}$$

$$\begin{aligned} \underline{\hat{P}} &= \frac{1}{2} \underline{\hat{E}} \times \underline{\hat{H}}^* = \frac{1}{2} \underline{\hat{E}}_0 e^{-jk_0 \underline{n} \cdot \underline{r}} \times \frac{k_0}{\omega\mu_0} \underline{\hat{E}}_0^* \times \underline{n} e^{+jk_0 \underline{n} \cdot \underline{r}} = \frac{k_0}{2\omega\mu_0} \left[\underline{\hat{E}}_0 \times \underline{\hat{E}}_0^* \times \underline{n} \right] \\ &= \frac{k_0}{2\omega\mu_0} \left[(\underline{\hat{E}}_0 \cdot \underline{n}) \underline{\hat{E}}_0^* - (\underline{\hat{E}}_0 \cdot \underline{\hat{E}}_0^*) \underline{n} \right] \end{aligned}$$

$$\text{but } \underline{\hat{E}}_0 \cdot \underline{n} = 0 \quad \text{why } \nabla \cdot \underline{\hat{E}} = \nabla \cdot \underline{\hat{E}}_0 e^{-jk_0 \underline{n} \cdot \underline{r}} = \underline{\hat{E}}_0 \cdot \nabla e^{-jk_0 \underline{n} \cdot \underline{r}} = \underline{\hat{E}}_0 \cdot (-jk_0 \underline{n}) e^{-jk_0 \underline{n} \cdot \underline{r}}$$

$$\text{but } \nabla \cdot \underline{\hat{E}} = 0 \text{ in free space } \Rightarrow \underline{\hat{E}}_0 \cdot \underline{n} = 0$$

$$\underline{\hat{P}} = + \frac{k_0}{2\omega\mu_0} |\underline{\hat{E}}_0|^2 \underline{n}$$

i.e. power is transported along the direction of travel of the wave.

$$\begin{aligned}
\langle u_m \rangle &= \frac{1}{4} \mu_0 |\hat{H}|^2 = \frac{1}{4} \mu_0 \hat{H} \cdot \hat{H}^* \\
&= \frac{1}{4} \mu_0 \left(\frac{-k_0}{\omega \mu_0} \right) (\hat{E}_0 \times \underline{n}) \cdot \left(\frac{-k_0}{\omega \mu_0} \right) (\hat{E}_0^* \times \underline{n}) e^{+jk_0 \underline{n} \cdot \underline{r}} \\
&= \frac{k_0^2}{4\omega^2 \mu_0} (\hat{E}_0 \times \underline{n}) \cdot (\hat{E}_0^* \times \underline{n}) \\
&= \frac{k_0^2}{4\omega^2 \mu_0} \left[(\hat{E}_0 \cdot \hat{E}_0^*) (\underline{n} \cdot \underline{n}) - (\hat{E}_0 \cdot \underline{n}) (\underline{n} \cdot \hat{E}_0^*) \right] \\
&= \frac{k_0^2}{4\omega^2 \mu_0} (\hat{E}_0 \cdot \hat{E}_0^*)
\end{aligned}$$

$$\langle u_e \rangle = \frac{1}{4} \epsilon_0 \hat{E} \cdot \hat{E}^* = \frac{1}{4} \epsilon_0 \hat{E}_0 e^{-jk_0 \underline{n} \cdot \underline{r}} \cdot \hat{E}_0^* e^{+jk_0 \underline{n} \cdot \underline{r}}$$

$$\langle u_e \rangle = \frac{\epsilon_0}{4} (\hat{E}_0 \cdot \hat{E}_0^*)$$

4. assume a solution of the form $\underline{H} = -\nabla\psi$

$$\nabla \cdot \underline{H} = -\nabla \cdot \nabla \psi$$

$$\text{but } \nabla \cdot \underline{H} = 0$$

$$\therefore \nabla^2 \psi = 0$$

in spherical coordinates \Rightarrow

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial \psi}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial \psi}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 \psi}{\partial \phi^2} = 0$$

Assume $\psi \neq f(\phi)$ because of the symmetry of the problem. Furthermore assume $\psi = R(r) \Theta(\theta)$

then

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial R \Theta}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial R \Theta}{\partial \theta} \right) = 0$$

when reduced

$$\frac{1}{R} \left[2r \frac{\partial R}{\partial r} + r^2 \frac{\partial^2 R}{\partial r^2} \right] + \frac{1}{\Theta \sin \theta} \left[\cos \theta \frac{\partial \Theta}{\partial \theta} + \sin \theta \frac{\partial^2 \Theta}{\partial \theta^2} \right] = 0$$

From Fano Chu & Adler solution is

$$\left. \begin{aligned} R(r) &= A_1 r^n + A_2 r^{-(n+1)} \\ \Theta(\theta) &= C P_n^m(\cos \theta) \end{aligned} \right\} \text{with } n=m=1$$

$$R(r) = A_1 r + \frac{A_2}{r^2}$$

$$\Theta(\theta) = C \cos \theta$$

$$\psi = A_1 C \frac{\cos \theta}{r} + \frac{A_2 C \cos \theta}{r^2}$$

$$H = -\nabla\psi = -a_r \frac{\partial\psi}{\partial r} - a_\theta \frac{1}{r} \frac{\partial\psi}{\partial\theta}$$

$$H_1 = \ominus A_1 \cos\theta \bar{a}_r + A_2 \sin\theta \bar{a}_\theta \quad r < R$$

$$H_2 = \frac{2A_3}{r^3} \cos\theta \bar{a}_r + \frac{A_4}{r^3} \sin\theta \bar{a}_\theta \quad r > R$$

now with these two equations for H

$$\text{Set } H_{1r}|_{r=R} = H_{2r}|_{r=R}$$

$$\frac{1}{r^2} \frac{\partial}{\partial r} (r^2 A_1 \cos\theta) + \frac{1}{r \sin\theta} \frac{\partial}{\partial\theta} (A_2 \sin^2\theta) = 0$$

and $\nabla \cdot H = 0$

$H_{1\theta} - H_{2\theta} = K_0$
for 2 eqns
2 unknowns
 A_1, A_2

$$\frac{1}{r^2} 2r A_1 \cos\theta + \frac{1}{r \sin\theta} A_2 2 \sin\theta \cos\theta = 0$$

$$\therefore A_1 = -A_2$$

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(\frac{A_3}{r} \cos\theta \right) + \frac{1}{r \sin\theta} \frac{\partial}{\partial\theta} \left(\frac{A_4}{r^3} \sin^2\theta \right) = 0$$

$$\frac{1}{r^2} - \frac{A_3}{r^2} \cos\theta + \frac{A_4}{r^3} \frac{2 \sin\theta \cos\theta}{r \sin\theta} = 0$$

All this work is unnecessary

$$A_3 = 2A_4$$

$$\therefore A_3 = -A_1 R^3$$

$$A_2 = \frac{A_4}{R^3} - K_0$$

$$A_1 = -A_2$$

$$A_3 = 2A_4$$

$$A_3 = A_2 R^3 \quad \therefore A_2 = \frac{A_3}{R^3}$$

$$A_2 = \frac{A_3}{2R^3} - K_0$$

$$\frac{A_3}{R^3} = \frac{A_3}{2R^3} - K_0$$

$$-K_0 = \frac{A_3}{2R^3} \quad A_3 = -2R^3 K_0$$

NOTE: You must remember the coefficients A_1 & A_2 are the same and A_3 & A_4 are identical otherwise you cannot satisfy $\nabla \cdot H = 0$

$$-A_1 = \frac{2A_3}{R^3}$$

$$\text{and } \left(\frac{A_3}{R^3} - A_1 \right) \sin\theta = K_0$$

$$\text{so } \frac{3A_3}{R^3} = K_0$$

$$A_3 = \frac{K_0 R^3}{3}$$

$$\text{so } A_1 = -\frac{2K_0}{3}$$

$$\underline{H} = -\nabla\tau = -\frac{\partial\tau}{\partial r}\bar{a}_r - \frac{1}{r}\frac{\partial\tau}{\partial\theta}\bar{a}_\theta$$

$$\begin{aligned}\underline{H} &= -\left(+A_1\cos\theta - A_2\frac{\cos\theta}{r^3}\right)\bar{a}_r + \frac{1}{r}\left(\frac{A_1 r}{r} + \frac{A_2}{r^2}\right)\sin\theta\bar{a}_\theta \\ &= -\left(A_1 + \frac{A_2}{r^3}\right)\bar{a}_r\cos\theta + \left(A_1 + \frac{A_2}{r^3}\right)\sin\theta\bar{a}_\theta\end{aligned}$$

1) require \underline{H} to be finite everywhere

says that $A_2 = 0$

i.e. $\underline{H}_1 = -A_1\cos\theta\bar{a}_r + A_2\sin\theta\bar{a}_\theta$ inside the sphere

1) require \underline{H} to tend to 0 as $r \rightarrow \infty$

says that $A_1 = 0$

i.e. $\underline{H}_2 = +\frac{A_3}{r^3}\cos\theta\bar{a}_r + \frac{A_4}{r^3}\sin\theta\bar{a}_\theta$

require H_r to be continuous at $r=R$

$$\Rightarrow -A_1\cos\theta = +\frac{A_3}{R^3}\cos\theta \quad A_3 = +A_1R^3$$

Furthermore

$$\nabla \times (\underline{H}_1 - \underline{H}_2) = \underline{K}$$

$$\bar{a}_r \times (\underline{H}_1 - \underline{H}_2)_\theta = \frac{K_0 \sin\theta}{r} \bar{a}_\phi$$

$$\Rightarrow H_{1\theta} - H_{2\theta} = K_0 \sin\theta$$

$$+ A_2 \sin\theta + \frac{A_4}{R^3} \sin\theta = K_0 \sin\theta$$

$$-A_1 - A_2 + \frac{A_4}{R^3} = K_0$$

$$\mathbb{H} = \begin{cases} +\frac{k_0}{2} \cos\theta \bar{a}_r - \frac{k_0}{2} \sin\theta \bar{a}_\theta \\ +\frac{k_0}{2} \left(\frac{R}{r}\right)^3 \cos\theta \bar{a}_r + k_0 \left(\frac{R}{r}\right)^3 \sin\theta \bar{a}_\theta \end{cases}$$

$$\mathbb{H} = \begin{cases} \frac{k_0}{2} \left\{ \begin{array}{l} \cos\theta \bar{a}_r - \sin\theta \bar{a}_\theta \\ \left(\frac{R}{r}\right)^3 \cos\theta \bar{a}_r + \sin\theta \bar{a}_\theta \end{array} \right. & \begin{array}{l} r < R \\ r > R \end{array} \end{cases}$$

I know the result is incorrect
but I can't find the error.

try again with the correction

#2

(1) in general

$$-\underline{a}_z \times \nabla_t \hat{e}_z - \gamma \underline{a}_z \times \hat{e}_t = -j\omega\mu \hat{h}_t$$

$$\nabla_t \times \hat{e}_t = -j\omega\mu \hat{h}_z$$

9/10

$$-\underline{a}_z \times \nabla_t \hat{h}_z - \gamma \underline{a}_z \times \hat{h}_t = j\omega\epsilon \hat{e}_t$$

$$\nabla_t \times \hat{h}_t = j\omega\epsilon \hat{e}_z$$

$$\nabla_t \cdot \hat{e}_t = \gamma \hat{e}_z$$

$$\nabla_t \cdot \hat{h}_t = \gamma \hat{h}_z$$

for a TE wave $e_z = 0$

$$-\gamma \underline{a}_z \times \hat{e}_t = -j\omega\mu \hat{h}_t$$

$$\nabla_t \times \hat{e}_t = -j\omega\mu \hat{h}_z$$

$$-\underline{a}_z \times \nabla_t \hat{h}_z - \gamma \underline{a}_z \times \hat{h}_t = j\omega\epsilon \hat{e}_t$$

$$\nabla_t \times \hat{h}_t = 0$$

$$\nabla_t \cdot \hat{e}_t = 0$$

$$\nabla_t \cdot \hat{h}_t = \gamma \hat{h}_z$$

these waves must obey the Helmholtz equation

$$\nabla^2 H + \omega^2\mu\epsilon H = 0$$

$$(\nabla_t^2 + \gamma^2) \hat{h}_t + \omega^2\mu\epsilon \hat{h}_t = 0$$

$$(\nabla_t^2 + \gamma^2) \hat{h}_z + \omega^2\mu\epsilon \hat{h}_z = 0$$

$$\nabla_t^2 \hat{h}_t + (\gamma^2 + \omega^2\mu\epsilon) \hat{h}_t = 0$$

$$\nabla_t^2 \hat{h}_z + (\gamma^2 + \omega^2\mu\epsilon) \hat{h}_z = 0$$

$$\nabla_t^2 \underline{h}_z + (\gamma^2 + \omega^2 \mu \epsilon) \underline{h}_z = 0$$

$$\nabla_t^2 = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2}{\partial \phi^2}$$

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial \underline{h}_z}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 \underline{h}_z}{\partial \phi^2} + (\gamma^2 + \omega^2 \mu \epsilon) \underline{h}_z = 0$$

$$\text{let } \underline{h}_z = h_z a_z$$

then

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial h_z}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 h_z}{\partial \phi^2} + (r^2 + \omega^2 \mu \epsilon) h_z = 0 \quad \checkmark$$

(b)

$$\text{let } h_z = f(r) g(\phi)$$

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r g \frac{\partial f}{\partial r} \right) + \frac{1}{r^2} f \frac{\partial^2 g}{\partial \phi^2} + (\gamma^2 + \omega^2 \mu \epsilon) f g = 0$$

$$\frac{g}{r} \frac{\partial^2 f}{\partial r^2} + \frac{g}{r} \frac{\partial f}{\partial r} + \frac{1}{r^2} f \frac{\partial^2 g}{\partial \phi^2} + (\gamma^2 + \omega^2 \mu \epsilon) f g = 0$$

$$\frac{1}{f(r)} \frac{\partial^2 f(r)}{\partial r^2} + \frac{1}{r f(r)} \frac{\partial f(r)}{\partial r} + \frac{1}{r^2 g(\phi)} \frac{\partial^2 g(\phi)}{\partial \phi^2} + (\gamma^2 + \omega^2 \mu \epsilon) = 0$$

$$\frac{r^2}{f(r)} \frac{d^2 f(r)}{dr^2} + \frac{r}{f(r)} \frac{df(r)}{dr} + r^2 (\gamma^2 + \omega^2 \mu \epsilon) + \frac{1}{g(\phi)} \frac{d^2 g(\phi)}{d\phi^2} = 0$$

$$\frac{1}{g(\phi)} \frac{d^2 g(\phi)}{d\phi^2} = -n^2 \quad \checkmark$$

$$\frac{d^2 g(\phi)}{d\phi^2} = -n^2 g(\phi)$$

n must be an integer
for ϕ to have periodicity of 2π

$$\Rightarrow g(\phi) = A_1 \cos n\phi + A_2 \sin n\phi$$

$$\Leftrightarrow \frac{r^2}{f(r)} \frac{d^2 f(r)}{dr^2} + \frac{r}{f(r)} \frac{df(r)}{dr} + r^2 (\gamma^2 + \omega^2 \mu \epsilon) = n^2$$

$$\frac{d^2 f(r)}{dr^2} + \frac{1}{r} \frac{df(r)}{dr} + \left(\gamma^2 + \omega^2 \mu \epsilon - \frac{n^2}{r^2} \right) f(r) = 0$$

$$k_c^2 \triangleq \gamma^2 + \omega^2 \mu \epsilon$$

$$\frac{d^2 f(r)}{dr^2} + \frac{1}{r} \frac{df(r)}{dr} + \left(k_c^2 - \frac{n^2}{r^2} \right) f(r) = 0$$

from p. 207-208 of Ramo, Whinnery, & Van Duzer

$$f(r) = B_1 J_n(k_c r) + B_2 Y_n(k_c r)$$

because $f(r)$ must be finite at the origin $B_2 = 0$

$$\therefore f(r) = B_1 J_n(k_c r)$$

(4) and (5)

$$h_z = J_n(k_c r) [C_1 \cos n\phi + C_2 \sin n\phi]$$

the because there are no fields in the interior of a perfect conductor

$$n \cdot B = 0 \iff n \cdot H = 0$$

$$\text{as } n \times H = J_s - K$$

$$\text{but } n \cdot H = 0 \quad \text{but } k = \underline{h}_t + \underline{h}_z$$

$$n \cdot (\underline{h}_t + \underline{h}_z) = 0$$

$$n \cdot \underline{h}_t = 0$$

$$\text{but } \underline{h}_t = - \frac{\nabla_t (\gamma h_z)}{\gamma^2 + \omega^2 \mu \epsilon}$$

Proof:

$$\nabla_t \times \underline{h}_t = 0$$

$$\nabla_t \times (\nabla_t \times \underline{h}_t) = \nabla_t \nabla_t \cdot \underline{h}_t - \nabla_t^2 \underline{h}_t = 0$$

$$\text{but } \nabla_t^2 \underline{h}_z = -(\gamma^2 + \omega^2 \mu \epsilon) \underline{h}_z$$

$$\underline{h}_t = - \frac{\gamma \nabla_t h_z}{\gamma^2 + \omega^2 \mu \epsilon}$$

$$\Rightarrow n \cdot \left(- \frac{\nabla_{\perp} (Y h_z)}{\delta^2 + \omega^2 \mu \epsilon} \right) = 0$$

$$\underline{n} \cdot \nabla_{\perp} h_z = 0$$

$$\text{but } \nabla_{\perp} = \underline{a}_r \frac{\partial}{\partial r} + \underline{a}_{\phi} \frac{1}{r} \frac{\partial}{\partial \phi}$$

$$h_z = J_n(k_c r) [C_1 \cos n\phi + C_2 \sin n\phi]$$

$$\underline{n} = \underline{a}_r$$

$$\underline{n} \cdot \nabla_{\perp} = \frac{\partial}{\partial r}$$

$$\Leftrightarrow \frac{\partial}{\partial r} h_z = \frac{\partial}{\partial r} [f(r)g(\phi)] = 0$$

$$\Leftrightarrow \frac{\partial f(r)}{\partial r} = 0$$

$$\text{but } f(r) = J_n(k_c r)$$

$$\therefore \left. \frac{dJ_n(k_c r)}{dr} \right|_{r=a} = 0 \quad \checkmark$$

and given the boundary conditions of the system we can examine the dispersion relation of the system.

Consider p_{mn} as that value of $k_c r$ which is the m -th zero of the derivative of the n -th order Bessel function J_n ✓

$$\text{i.e. for all } p_{mn} \quad \left. \frac{dJ_n(k_c r)}{dr} \right|_{k_c r = p_{mn}} = 0$$

in general $P_{mn} = k_c r$

$$\text{or } k_c = \frac{P_{mn}}{r}$$

but P_{mn} is only defined for $r=a$
i.e. the boundary condition

$$k_c = \frac{P_{mn}}{a}$$

$$\text{but } -k_c^2 = \omega^2 \mu \epsilon + \gamma^2$$

$$\therefore \gamma^2 + \omega^2 \mu \epsilon = \frac{P_{mn}^2}{a^2}$$

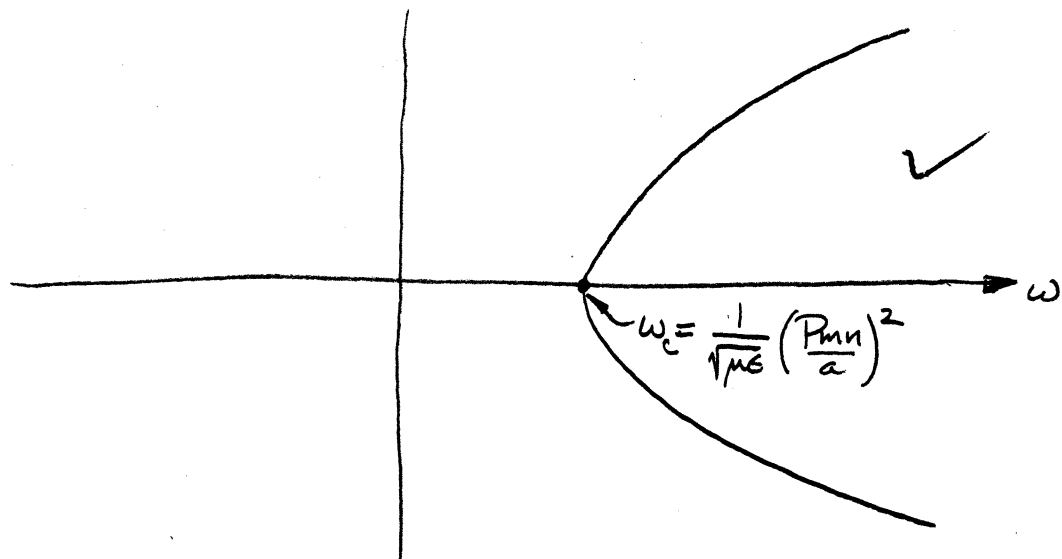
$$\gamma = \alpha + j\beta$$

assume $\alpha=0$ in this case.

$$-\beta^2 + \omega^2 \mu \epsilon = \frac{P_{mn}^2}{a^2}$$

$$\beta^2 = \omega^2 \mu \epsilon - \frac{P_{mn}^2}{a^2}$$

$$\beta = \sqrt{\omega^2 \mu \epsilon - \left(\frac{P_{mn}}{a}\right)^2}$$



(6)

TE₀₁ mode

1. no azimuthal variation
2. $\frac{1}{2}$ cycle variation of h_z in the radial direction from the axis to the wall

corresponds to the first zero of the zero-order Bessel function

i.e. $\hat{h}_z = J_0(k_c r)$

$$\nabla_t \times \hat{h}_t = 0$$

$$\nabla_t \times (\nabla_t \times \hat{h}_t) = \nabla_t \nabla_t \cdot \hat{h}_t - \nabla_t^2 \hat{h}_t = 0$$

$$= \nabla_t (\gamma \hat{h}_z) - \nabla_t^2 \hat{h}_t = 0$$

$$\nabla_t \cdot \hat{h}_t = \gamma \hat{h}_z$$

but these waves must obey the Helmholtz equation

$$\nabla^2 \underline{H} + \omega^2 \mu \epsilon \underline{H} = 0$$

$$(\nabla_t^2 + \gamma^2) \underline{h}_t + \omega^2 \mu \epsilon \underline{h}_t = 0$$

$$\nabla_t^2 \underline{h}_t = -(\gamma^2 + \omega^2 \mu \epsilon) \underline{h}_t$$

$$\therefore \nabla_t (\gamma \hat{h}_z) - \nabla_t^2 \hat{h}_t = \nabla_t (\gamma \hat{h}_z) + (\gamma^2 + \omega^2 \mu \epsilon) \hat{h}_t = 0$$

$$\therefore \hat{h}_t = -\frac{\gamma}{\gamma^2 + \omega^2 \mu \epsilon} \nabla_t (\hat{h}_z)$$

$$\nabla_t = \underline{a}_r \frac{\partial}{\partial r} + \underline{a}_\theta \frac{1}{r} \frac{\partial}{\partial \theta} + \frac{\underline{a}_\phi}{r \sin \theta} \frac{\partial}{\partial \phi}$$

if $\hat{h}_z = c_1 J_0(k_c r)$

knowing $\frac{dJ_0(k_c r)}{d(k_c r)} = -J_1(k_c r)$ ✓

$$\nabla_t \hat{h}_z = \underline{a}_r \frac{d}{dr} (J_0(k_c r)) = k_c \underline{a}_r \frac{dJ_0(k_c r)}{d(k_c r)}$$

$$\nabla_t \hat{h}_z = -\underline{a}_r k_c J_1(k_c r)$$

$$\underline{\hat{h}}_+ = + \frac{\gamma}{\gamma^2 + \omega^2 \mu \epsilon} \underline{a}_r k_c J_1(k_c r)$$

$$= \frac{\gamma}{k_c^2} \underline{a}_r k_c J_1(k_c r)$$

$$= \frac{\gamma}{k_c} J_1(k_c r) \underline{a}_r$$
 ✓

2 \hat{e}_+ \hat{h}_+ \hat{r}

$$-\gamma \underline{a}_z \times \underline{\hat{e}}_+ = -j\omega \mu \underline{\hat{h}}_+$$

$$-\gamma [\underline{a}_z \times \underline{a}_z \times \underline{\hat{e}}_+] = -j\omega \mu [\underline{a}_z \times \underline{\hat{h}}_+]$$

$$\gamma \underline{\hat{e}}_+ = -j\omega \mu [\underline{a}_z \times \underline{\hat{h}}_+]$$

$$\underline{\hat{e}}_+ = -\frac{j\omega \mu}{\gamma} [\underline{a}_z \times \underline{\hat{h}}_+]$$

$$= -\frac{j\omega \mu}{\gamma} \left[\frac{\gamma}{k_c} J_1(k_c r) \underline{a}_\phi \right] = -\frac{j\omega \mu}{k_c} J_1(k_c r) \underline{a}_\phi$$

in summary:

$$\hat{h}_z = c_1 J_0(k_c r) e^{-\gamma z} \underline{a}_z$$

$$\hat{h}_t = c_1 \frac{\gamma}{k_c} J_1(k_c r) e^{-\gamma z} \underline{a}_r$$

$$\hat{e}_t = -\frac{j\omega\mu}{k_c} J_1(k_c r) e^{-\gamma z} \underline{a}_\phi$$

the lower case fields \underline{e} don't contain $e^{-\gamma z}$ factors

$$\lambda_c = \frac{2\pi}{k_c} = \frac{2\pi}{p_{mn}/a} = \frac{2\pi a}{p_{mn}}$$

$a = 1 \text{ cm}$ given

$p_{mn} = 3.832$

Xerox notes p. 111

$$\omega_{ce} = \left(\frac{p_{mn}}{a} \right) c$$

$$\lambda_c = \frac{2\pi (1 \text{ cm})}{3.832} = \frac{2\pi}{3.832} \text{ cm}$$

$$f_c = \frac{2\pi}{3.832 \sqrt{\mu\epsilon}}$$

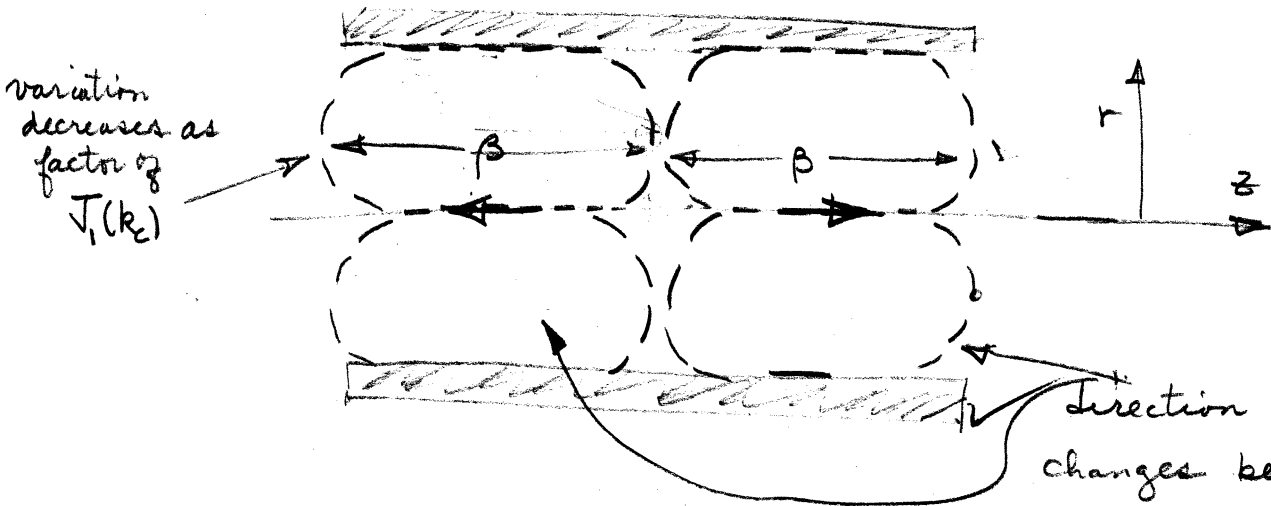
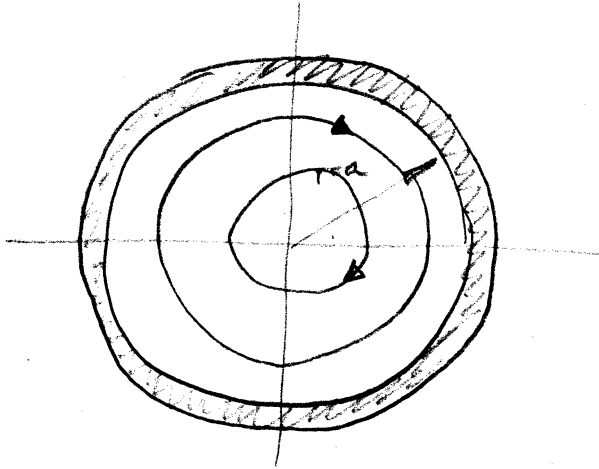
assume the center of the waveguide is free space.

$$c = \frac{1}{\sqrt{\mu\epsilon}} = 3 \times 10^{10} \text{ cm/sec.}$$

$$f_c = \frac{2\pi}{3.832} (3 \times 10^{10} / \text{sec}) = 4.92 \times 10^{10} \text{ Hz.}$$

$$f_c = 49.2 \text{ kHz.}$$

(7)



variation
decreases as
factor of
 $J_1(kr)$

Direction of rotation
changes because

of $e^{-\gamma z}$ factor
which becomes
$$e^{-\gamma z + j\omega t} = e^{-j\beta z + j\omega t} = e^{j(\omega t - \beta z)}$$

periodic in z

10/10

4.12 e

Eq. 4.12(2)

$$\nabla \times \underline{H} = \sigma \underline{E} + \frac{\partial \underline{D}}{\partial t}$$

$$\nabla \cdot (\nabla \times \underline{H}) = \sigma \nabla \cdot \underline{E} + \frac{\partial}{\partial t} \nabla \cdot \underline{D}$$

good work

$$\text{but } \nabla \cdot (\nabla \times \underline{H}) \equiv 0$$

$$\text{furthermore } \nabla \cdot \underline{D} = \rho$$

$$0 = \sigma \nabla \cdot \underline{E} + \frac{\partial \rho}{\partial t}$$

$$\text{but } \underline{D} = \epsilon \underline{E} \quad \text{or} \quad \nabla \cdot \underline{E} = \frac{1}{\epsilon} \nabla \cdot \underline{D} = \frac{\rho}{\epsilon}$$

$$\Rightarrow \frac{\partial \rho}{\partial t} + \frac{\sigma}{\epsilon} \rho = 0$$

solution is $\rho = c_1 e^{-\frac{\sigma}{\epsilon} t} + c_2 e^{+\frac{\sigma}{\epsilon} t}$ this couldn't possibly be a solution

obviously $c_2 \equiv 0$

$$\rho = \rho(0) e^{-\frac{\sigma}{\epsilon} t}$$

notice how it won't work by replacing it in the equation

where $\rho(0)$ is the initial charge density.

this implies that free charge cannot exist in the interior of a good conductor for a long period of time.

If we put excess charge q at the center of a solid conducting sphere of radius $r = 1 \text{ cm}$. This charge would rapidly move to the surface of the sphere.

this says that if we put total charge q at the center of the sphere $\frac{1}{\epsilon}$ of this charge would be on the surface of the sphere after $\frac{\epsilon}{\sigma}$ seconds.

$$\langle \text{velocity} \rangle = \frac{1 \text{ cm}}{\left(\frac{\epsilon}{\sigma}\right) \text{ sec}} = \frac{\sigma}{\epsilon} \frac{\text{cm}}{\text{sec}}$$

$$\frac{\sigma}{\epsilon} = \frac{5.8 \times 10^7}{\frac{1}{36\pi} \times 10^{-9}} = (36\pi)(5.8) \times 10^{16} = 656 \times 10^{16}$$

$$\frac{\sigma}{\epsilon} = 6.56 \times 10^{18} \frac{\text{cm}}{\text{sec}}$$

$$\langle \text{velocity} \rangle = 6.56 \times 10^{18} \frac{\text{cm}}{\text{sec}}$$

a speed vastly in excess of that of light.

our fundamental assumptions were that the material be linear, homogeneous and isotropic I believe that the material continues to be homogeneous and isotropic and that such large current flows (a few electrons at such a high speed constitute a very short very large current, i.e. current = $\frac{\text{charge}}{\text{second}}$)

$$= \frac{\# \text{ of electrons} \times \text{average velocity}}{\text{distance travelled}}$$

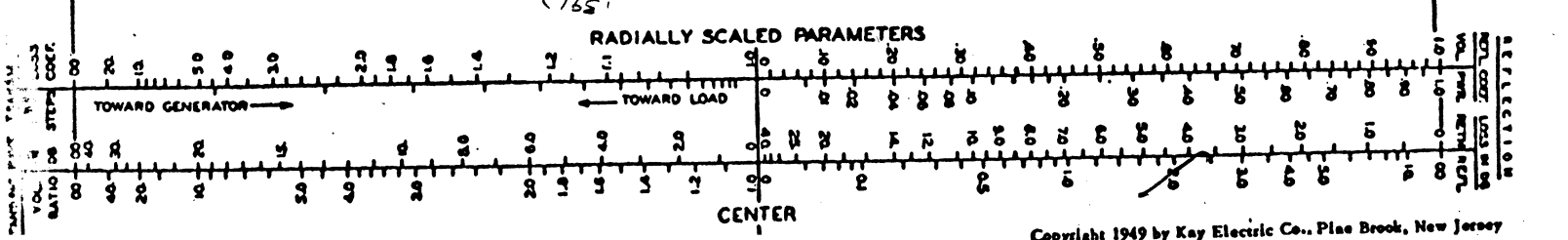
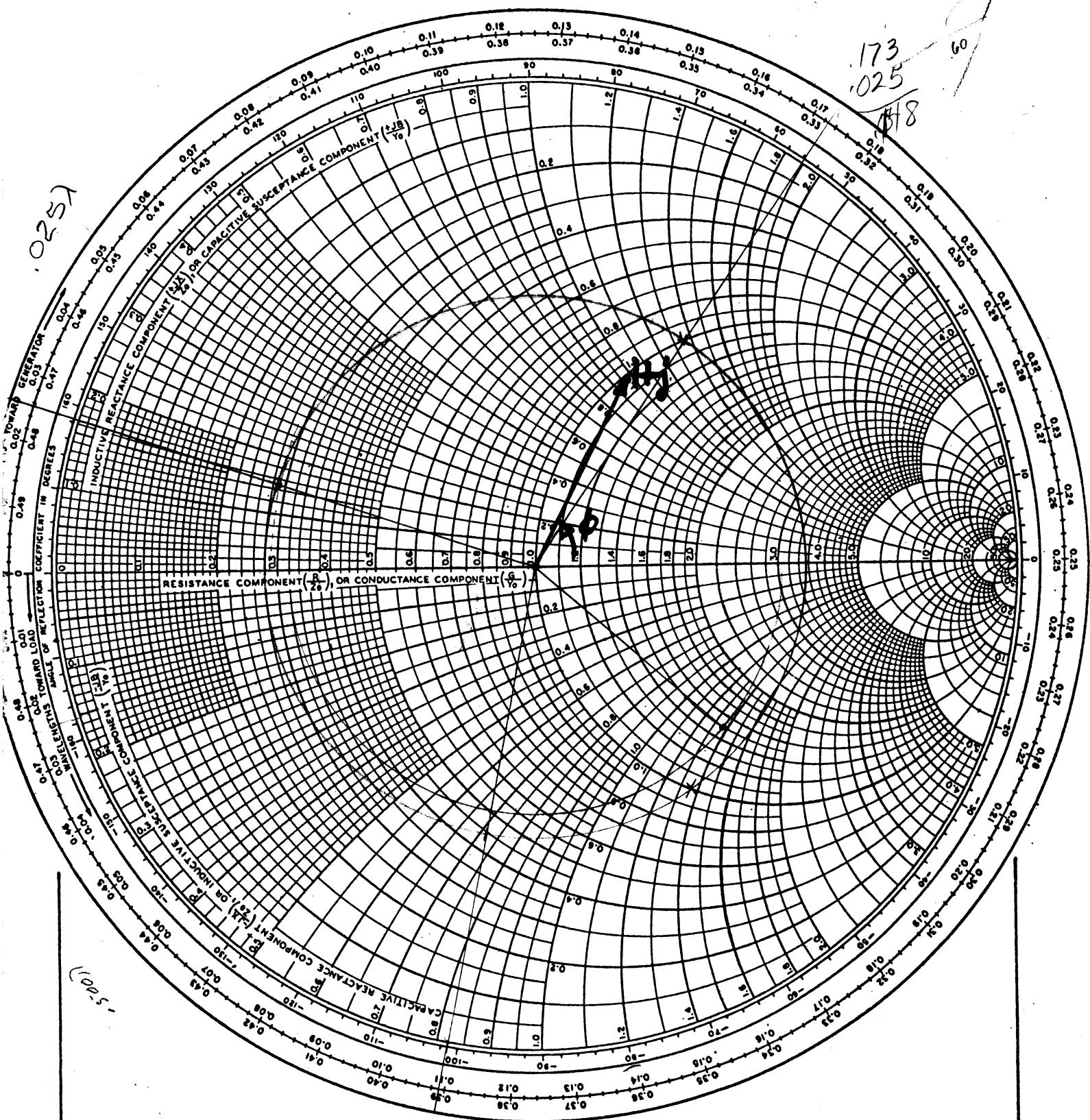
Because of this it would seem that $\underline{J} \neq \underline{\sigma E}$ and perhaps $\underline{D} \neq \underline{\epsilon E}$

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IMPEDANCE OR ADMITTANCE COORDINATES



1.16a

$$\rho = \frac{R_L - Z_0}{R_L + Z_0} = \frac{V_-}{V_+} = \frac{\frac{V_-}{Z_0}}{\frac{V_+}{Z_0}} = \frac{I_-}{I_+}$$

8/10

$$\frac{P_{ref}}{P_{inc}} = \frac{I_- V_-}{I_+ V_+} = \left(\frac{I_-}{I_+}\right) \left(\frac{V_-}{V_+}\right) = \rho^2$$

$$\frac{P_{trans}}{P_{inc}} = \frac{V_L I_L}{V_+ I_+} = \tau \frac{I_L}{I_+} = \tau^2 \frac{Z_0}{R_L}$$

because $\frac{I_L}{I_+} = \frac{I_L Z_0 R_L}{I_+ Z_0 R_L} = \frac{Z_0 V_+}{V_+ R_L} = \frac{Z_0}{R_L} \tau$

furthermore $\frac{V_+ + V_-}{V_+} = \frac{V_L}{V_+}$
 $1 + \rho = \tau$

$$\frac{P_{trans}}{P_{inc}} = \frac{Z_0}{R_L} (1 + \rho)^2$$

1.16b

$$R_L = 0 \quad \rho = -1$$

$$R_L = \frac{1}{2} Z_0 \quad \rho = -\frac{1}{3}$$

$$R_L = Z_0 \quad \rho = 0$$

$$R_L = 2Z_0 \quad \rho = \frac{1}{3}$$

$$R_L = \infty \quad \rho = 1$$

$$\frac{P_{ref}}{P_{inc}} = \rho^2$$

$$\frac{P_{trans}}{P_{inc}} = \frac{Z_0}{R_L} \rho^2$$

0 ✓

 $\frac{8}{9}$ ✓

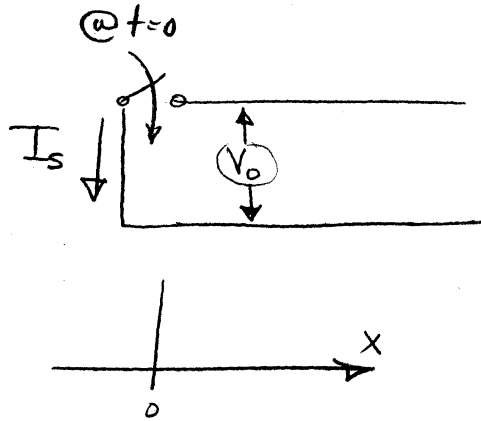
1 ✓

 $\frac{8}{9}$ ✓

0 ✓

$$\lim_{R_L \rightarrow 0} \frac{4R_L^2}{R_L (R_L + Z_0)^2} = \lim_{R_L \rightarrow 0} \frac{4R_L}{R_L (R_L + Z_0) (R_L + Z_0)^2} = 0$$

1.17a



The current flowing into the short circuit is the negative of the current associated with the positively traveling wave, i.e. $I_s = -\frac{V_+}{Z_0}$.

Zero voltage at the short requires that $V_+ = -V_0$.

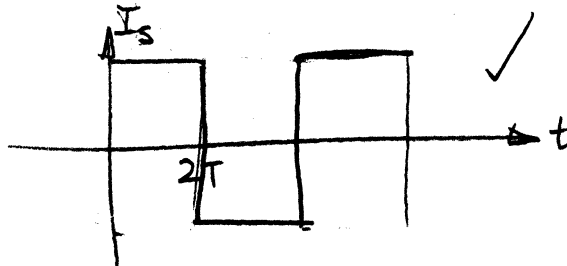
At the open end we require a reflected wave at the open end so that the total current is zero, so the current associated with the reflected wave is $-I_+$ or $\frac{V_0}{Z_0}$ ($I_+ = \frac{V_+}{Z_0} = -\frac{V_0}{Z_0}$).

The voltage associated with this negatively traveling wave satisfies $I_- = -\frac{V_-}{Z_0}$.

$$\therefore V_- = -I_- Z_0 = -(-I_+) Z_0 = I_+ Z_0 = V_0.$$

This current reaches the short requiring a new voltage wave propagated in the $+x$ direction. This new wave has associated with it a voltage of $V_+ = V_0$ volts, and an $I_s = -\frac{V_+}{Z_0} = -\frac{V_0}{Z_0}$.

$$T = \frac{l}{v}$$



1.18.

$$\beta = \frac{2\pi}{\lambda}$$

$$y \quad z = -\frac{\lambda}{3}$$

$$\beta z = -\frac{2\pi}{3}$$

$$Z_0 = 100 \Omega$$

$$Z_L = 100 + j100$$

$$Z_L = \frac{V}{I} \Big|_{e^{z=0}} = \frac{V_+ + V_-}{\frac{1}{Z_0}(V_+ - V_-)} = 100 + j100$$

$$\frac{V_+ + V_-}{V_+ - V_-} = \frac{100 + j100}{Z_0} = \frac{100 + j100}{100} = 1 + j$$

$$V_+ + V_- = (1 + j)(V_+ - V_-)$$

$$\frac{V_-}{V_+} = \frac{j}{2 + j} = \frac{1 + j^2}{5}$$

$$\begin{aligned} Z_i &= \frac{V}{I} \Big|_{e^{z=-l}} = \frac{V_+ e^{j\frac{2\pi}{3}} + V_- e^{-j\frac{2\pi}{3}}}{\frac{1}{Z_0}(V_+ e^{j\frac{2\pi}{3}} - V_- e^{-j\frac{2\pi}{3}})} \\ &= \frac{e^{j\frac{2\pi}{3}} + \frac{V_-}{V_+} e^{-j\frac{2\pi}{3}}}{e^{j\frac{2\pi}{3}} - \frac{V_-}{V_+} e^{-j\frac{2\pi}{3}}} Z_0 \end{aligned}$$

$$e^{j\frac{2\pi}{3}} = -\frac{1}{2} + j\frac{\sqrt{3}}{2}$$

$$e^{-j\frac{2\pi}{3}} = -\frac{1}{2} - j\frac{\sqrt{3}}{2}$$

$$z_i = \frac{(-\frac{1}{2} + j\frac{\sqrt{3}}{2}) + (2 + j.4)(-\frac{1}{2} - j\frac{\sqrt{3}}{2})}{(-\frac{1}{2} + j\frac{\sqrt{3}}{2}) - (2 + j.4)(-\frac{1}{2} - j\frac{\sqrt{3}}{2})} z_0$$

$$z_i = \frac{-\frac{1}{2} + j\frac{\sqrt{3}}{2} + 2(-\frac{1}{2}) - j(2)\frac{\sqrt{3}}{2} - (.4)\frac{1}{2}j + (.4)\frac{\sqrt{3}}{2}}{-\frac{1}{2} + j\frac{\sqrt{3}}{2} + 2(\frac{1}{2}) + (.4)\frac{1}{2}j + j(2)\frac{\sqrt{3}}{2} - (.4)\frac{\sqrt{3}}{2}} z_0$$

$$z_i = \frac{(-1 - .2 + .4\sqrt{3}) + j(\sqrt{3} - .2\sqrt{3} - .4)}{(-1 + .2 - .4\sqrt{3}) + j(\sqrt{3} + .4 + .2\sqrt{3})} z_0$$

$$z_i = \frac{(-1.2 + .4\sqrt{3}) + j(.8\sqrt{3} - .4)}{(-.8 - .4\sqrt{3}) + j(1.2\sqrt{3} + .4)} z_0$$

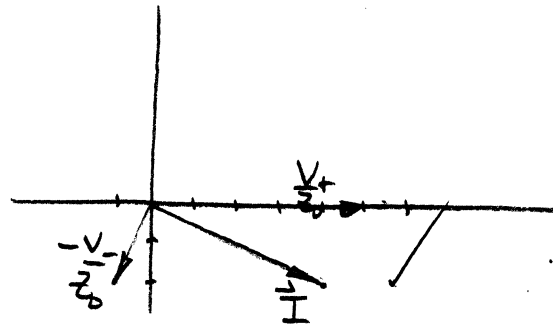
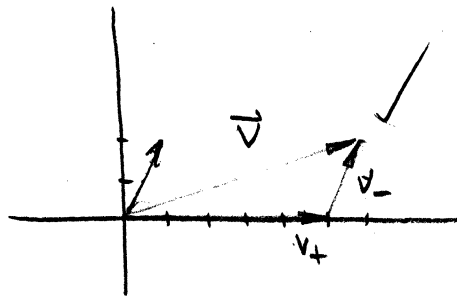
$$z_i = \frac{(-3 + \sqrt{3}) + j(2\sqrt{3} - 1)}{(-2 - \sqrt{3}) + j(3\sqrt{3} + 1)} z_0$$

$$z_i = \frac{20 + j(5\sqrt{3} - 10)}{35 + 10\sqrt{3}} z_0$$

$$z_i = \frac{4 + j(\sqrt{3} - 2)}{7 + 2\sqrt{3}} z_0$$

$$z_i = \frac{4 - j(2 - \sqrt{3})}{7 + 2\sqrt{3}} (100)$$

Phasor diagram for z_L



$$V_- = (1.2 + j.4) V_+$$

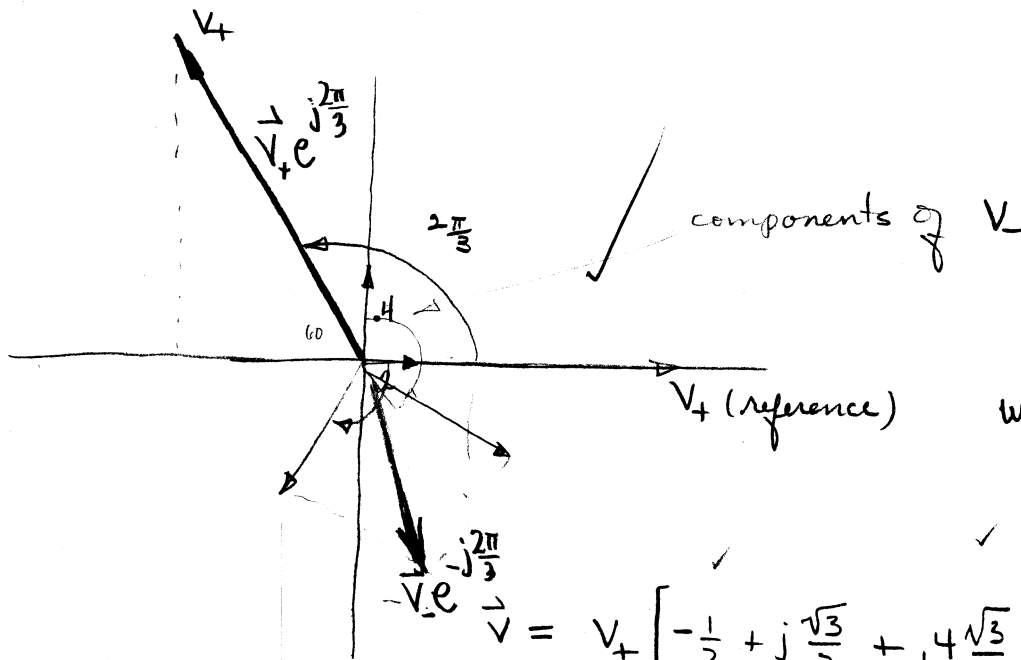
$$\vec{V} = (1.2 + .4j) V_+$$

$$I = \frac{V_+}{z_0} (.8 - .4j)$$

$$z_L = \frac{1.2 + .4j}{.8 - .4j} z_0 = \frac{3 + j}{2 - j} z_0 = \frac{5 + 5j}{5} z_0$$

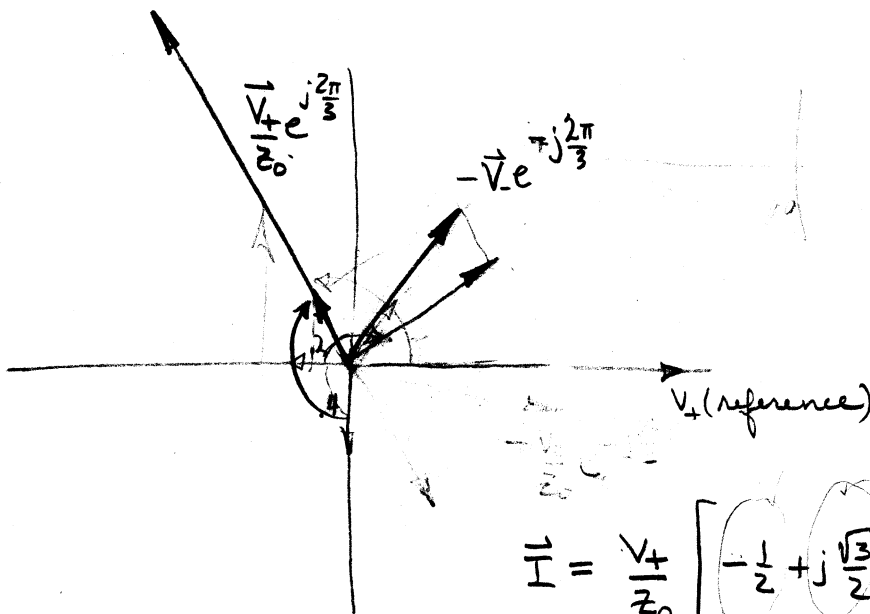
$$z_L = (1 + j) z_0 = (1 + j) 100 = 100 + j100$$

phasor diagram for Z_i



$$\vec{V} = V_+ \left[-\frac{1}{2} + j\frac{\sqrt{3}}{2} + .4\frac{\sqrt{3}}{2} - j\frac{.4}{2} - .2\frac{1}{2} - j(.2)\frac{\sqrt{3}}{2} \right]$$

$$= \frac{V_+}{2} \left[(-1 + .4\sqrt{3}) + j(\sqrt{3} - .4 - .2\sqrt{3}) \right]$$



$$\vec{I} = \frac{V_+}{Z_0} \left[-\frac{1}{2} + j\frac{\sqrt{3}}{2} + j(.4)\frac{1}{2} + \frac{\sqrt{3}}{2}(.4) + (.2)\frac{1}{2} - j(.2)\frac{\sqrt{3}}{2} \right]$$

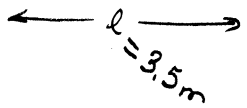
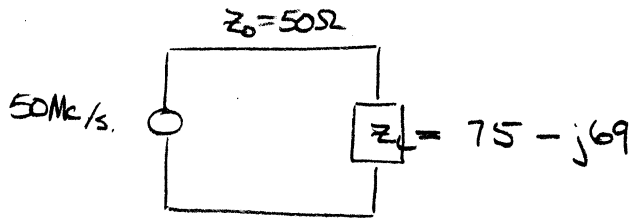
$$= \frac{V_+}{2Z_0} \left[(-1 + .4\sqrt{3} + .2) + j(\sqrt{3} + .4 + .2\sqrt{3}) \right]$$

and $Z_i = Z_0 \left[\frac{(-1.2 + .4\sqrt{3}) + j(.8\sqrt{3} - .4)}{(-.8 + .4\sqrt{3}) + j(1.2\sqrt{3} + .4)} \right]$

1.20 a.

FRANCIS MERAT
ENGR 336

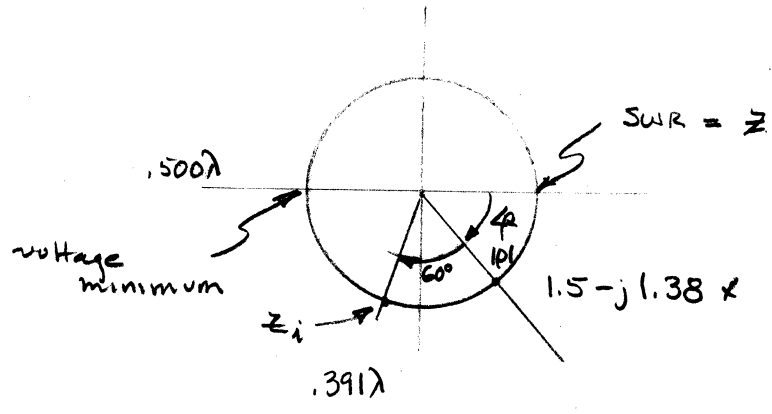
6.5/20



$$v_p = 3 \times 10^8 \text{ m/sec.}$$

$$Z_n = \frac{75 - j69}{50} = 1.5 - j1.38$$

to find Z_i



$$\beta l = \left(\frac{\omega}{v_p}\right) l = \left(\frac{2\pi f}{v_p}\right) l = \frac{2\pi \cdot 50 \times 10^6}{3 \times 10^8} = \frac{\pi}{3} = 30^\circ \text{ (toward generator)}$$

$$2\beta l = 60^\circ$$

$$Z_{i_n} = 0.5 - j0.77$$

$$Z_i = (0.5 - j0.77) 50 = \boxed{25 + j38.5 \Omega}$$

$$|p| = \sqrt{(1.5)^2 + (1.38)^2} = \sqrt{2.25 + 1.90} = \sqrt{4.15}$$

$|p| = 1.72$ X read $|p|$ from subsidiary scale or calculate it, but you've calculated

$$\phi = -41^\circ$$

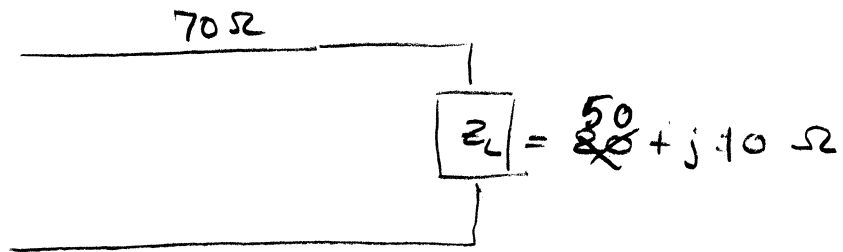
$$\text{SWR} = 3.05$$

12 n/20

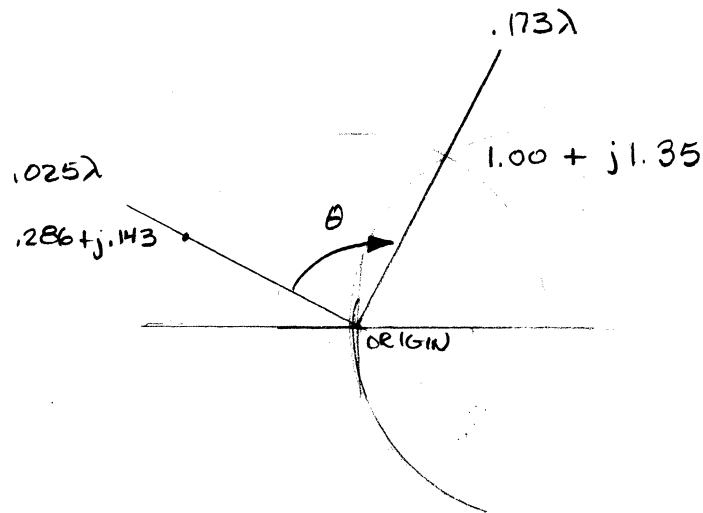
voltage minimum occurs at $(0.500 - 0.391)\lambda$ toward generator

$$.109\lambda = .109 \frac{v_p}{f} = .109 \frac{3 \times 10^8 \text{ m/sec}}{.50 \times 10^8 \text{ m/sec}} = \boxed{.654 \text{ m toward generator}}$$

1.20 d.



$$Z_{in} = \frac{20 + j10}{70} = .286 + j.143$$



$$\theta = .173\lambda - .025\lambda = .148\lambda$$

matching can be done by putting a capacitive reactance ($X_c = 1.35$) 0.148λ from the load.

right idea ✓

$$\begin{aligned} \text{consider } (A+jB)^{\frac{1}{2}} &= A^{\frac{1}{2}} + \frac{1}{2} A^{-\frac{1}{2}} (jB) + \frac{1}{2} \left(-\frac{1}{2}\right) A^{-\frac{3}{2}} (jB)^2 + \dots \\ &= \sqrt{A} + \frac{j}{2} \frac{B}{\sqrt{A}} + \frac{1}{4} \frac{B^2}{(\sqrt{A})^3} - \dots \end{aligned}$$

$$\text{if } Z = R + j\omega L \quad Y = G + j\omega C$$

$$Y^2 = ZY = RG + j\omega LG + j\omega RC - \omega^2 LC$$

$$Y^2 = (RG - \omega^2 LC) + j(\omega LG + \omega RC)$$

$$\therefore Y = \left[(RG - \omega^2 LC) + j(\omega LG + \omega RC) \right]^{\frac{1}{2}}$$

$$\text{identify } A = (RG - \omega^2 LC)$$

$$B = (\omega LG + \omega RC)$$

retaining upto 1st order terms.

$$\sqrt{A} = \sqrt{RG - \omega^2 LC} \approx \sqrt{-\omega^2 LC} = j\omega\sqrt{LC}$$

$$\frac{j}{2} \frac{B}{\sqrt{A}} = \frac{j}{2} \frac{\omega(LG + RC)}{j\omega\sqrt{LC}} = \frac{1}{2} \frac{LG}{\sqrt{LC}} + \frac{1}{2} \frac{RC}{\sqrt{LC}}$$

$$= \frac{1}{2} G \sqrt{\frac{L}{C}} + \frac{1}{2} R \sqrt{\frac{C}{L}}$$

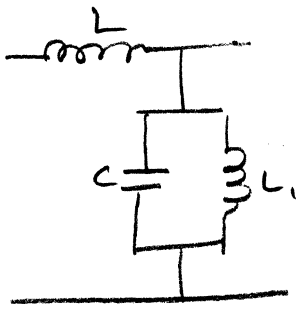
$$= \frac{1}{2} G Z_0 + \frac{1}{2} \frac{R}{Z_0} \quad \text{where } Z_0 = \sqrt{\frac{L}{C}}$$

$$Y \approx \frac{1}{2} G Z_0 + \frac{1}{2} \frac{R}{Z_0} + j\omega\sqrt{LC} \quad \checkmark$$

$$\text{if } Y = \alpha + j\beta$$

$$\text{identify } \alpha = \frac{1}{2} G Z_0 + \frac{1}{2} \frac{R}{Z_0} ; \beta = \omega\sqrt{LC}$$

4.



$$z = j\omega L$$

$$Y = j\omega C + \frac{1}{j\omega L_1}$$

$$\delta^2 = zY = j\omega L \left(j\omega C + \frac{1}{j\omega L_1} \right)$$

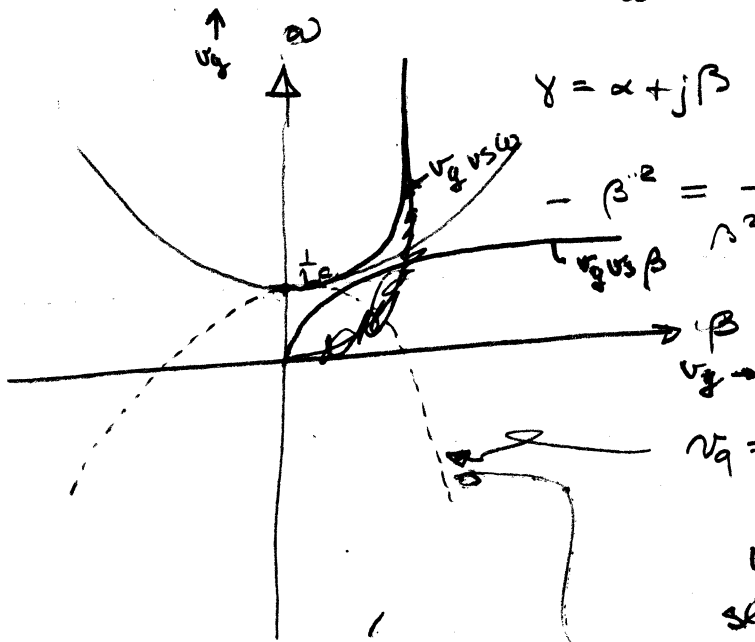
$$= -\omega^2 LC + \frac{L}{L_1}$$

$$Y = \alpha + j\beta \quad \text{assume } \alpha = 0$$

$$-\beta^2 = -\omega^2 LC + \frac{L}{L_1}$$

$$\beta^2 = \omega^2 LC - \frac{L}{L_1}$$

$$\omega^2 = \frac{\beta^2}{LC} + \frac{1}{L_1 C}$$



$$\nu_g = \frac{d\omega}{d\beta}$$

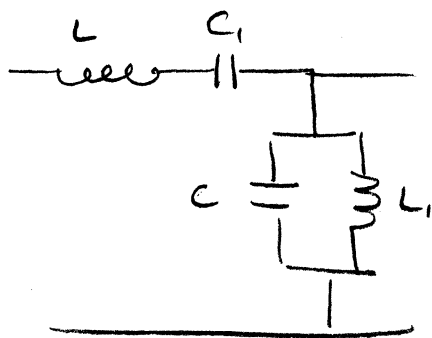
Why do you think the slope becomes negative here?

(or are you plotting ν_g vs β)

It's important to label your plot.

In any case it's wrong.

(b)



$$LC_1 > LC$$

$$Z = j\omega L + \frac{1}{j\omega C_1}$$

$$Y = j\omega C + \frac{1}{j\omega L_1}$$

$$Y^2 = ZY = -\omega^2 LC + \frac{C}{C_1} + \frac{L}{L_1} + \frac{1}{-\omega^2 L_1 C_1}$$

$$-\beta^2 = -\omega^2 LC - \frac{1}{\omega^2 L_1 C_1} + \left(\frac{C}{C_1} + \frac{L}{L_1}\right)$$

$$\beta^2 = \omega^2 LC + \frac{1}{\omega^2 L_1 C_1} - \left(\frac{C}{C_1} + \frac{L}{L_1}\right)$$

$$\beta^2 = \left(\omega^2 LC - \frac{C}{C_1}\right) + \left(\frac{1}{\omega^2 L_1 C_1} - \frac{L}{L_1}\right)$$

$$= \frac{C(\omega^2 LC_1 - 1)}{C_1} + \frac{1 - \omega^2 C}{\omega^2 L_1 C_1}$$

-1.5

$$\beta^2 = \omega^2 LC + \frac{1}{\omega^2 L_1 C_1} - \left(\frac{C}{C_1} + \frac{L}{L_1} \right)$$

$$\beta^2 \omega^2 L_1 C_1 = \omega^4 L C L_1 C_1 - \left(\frac{C}{C_1} + \frac{L}{L_1} \right) \omega^2 L_1 C_1 + 1$$

$$\omega^4 L C L_1 C_1 - \left(\frac{C}{C_1} + \frac{L}{L_1} \right) \omega^2 L_1 C_1 - \beta^2 \omega^2 L_1 C_1 + 1 = 0$$

$$\omega^4 L C L_1 C_1 - \omega^2 L_1 C - \omega^2 L C_1 - \beta^2 \omega^2 L_1 C_1 + 1 = 0$$

$$\omega^4 (L C L_1 C_1) + \omega^2 (L_1 C + L C_1 + L_1 C_1 \beta^2) + 1 = 0$$

$$\omega^2 = \frac{L_1 C + L C_1 + L_1 C_1 \beta^2 \pm \sqrt{(L_1 C + L C_1 + L_1 C_1 \beta^2)^2 - 4 L C L_1 C_1}}{2 L C L_1 C_1}$$

$$\omega^2 LC + \frac{1}{\omega^2 L_1 C_1} = \beta^2 + \left(\frac{C}{C_1} + \frac{L}{L_1} \right)$$

$$\frac{\omega^4 L C L_1 C_1 + 1}{\omega^2 L_1 C_1} = \beta^2 + \left(\frac{C}{C_1} + \frac{L}{L_1} \right)$$

$$\omega^4 L C L_1 C_1 + 1 = \beta^2 \omega^2 L_1 C_1 + \omega^2 L_1 C + \omega^2 L C_1$$

I cannot come up with a reasonable equation to plot.

$$\beta_0 \sqrt{\frac{\omega_p^2}{(\omega - \beta v_0)^2 - \omega_c^2} - 1}$$

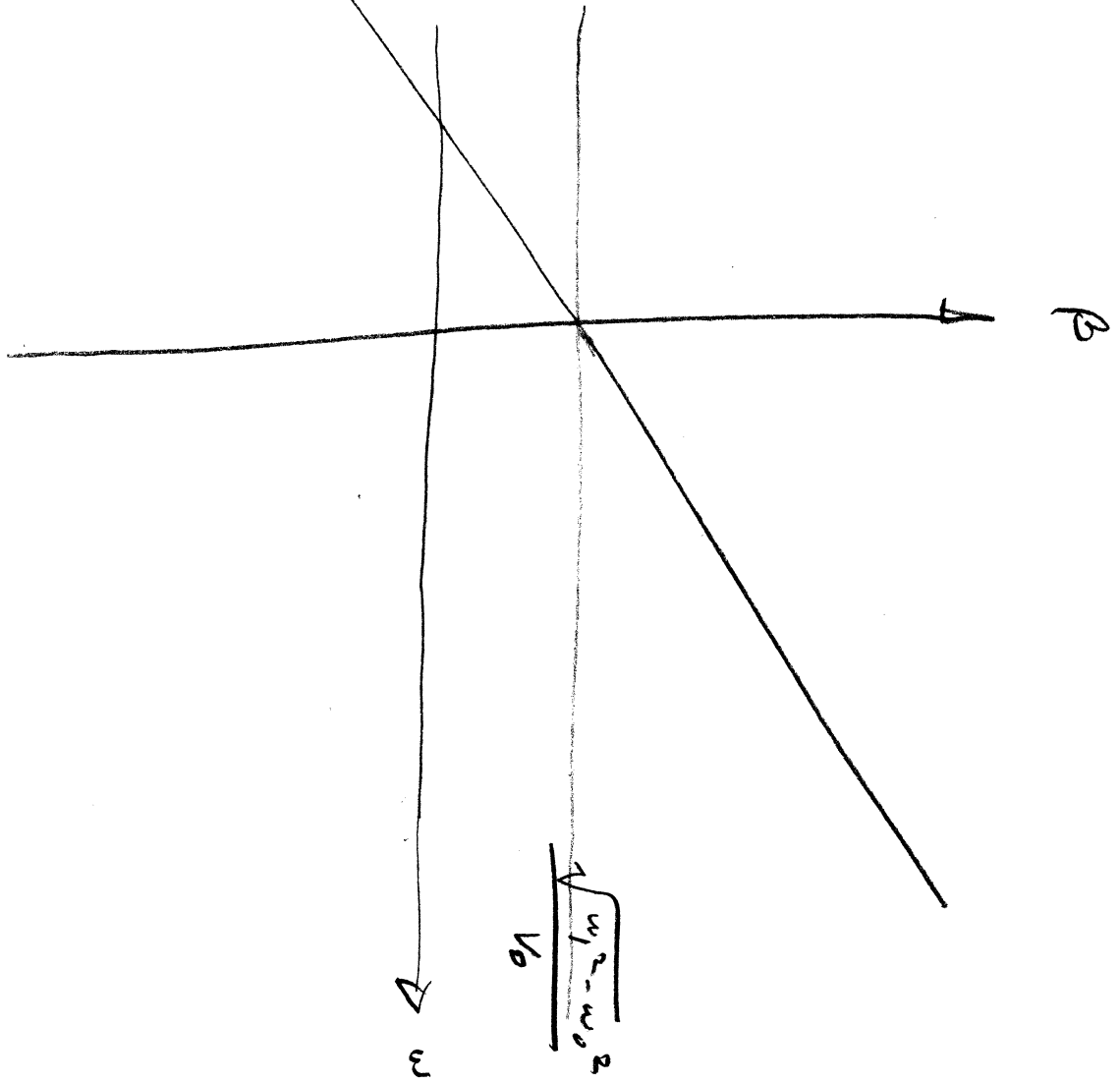
$$\omega_p \geq (\omega - \beta v_0)^2 - \omega_c^2$$

$$\beta_0 \omega_p^2 - \omega_c^2 \geq (\omega - \beta v_0)^2$$

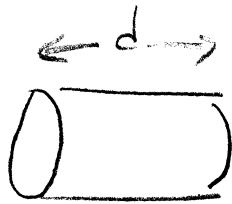
$$\omega - \beta v_0 \geq \sqrt{\omega_p^2 - \omega_c^2} - 1$$

$$\omega \geq \sqrt{\omega_p^2 + \omega_c^2} + \beta v_0$$

$$\frac{\omega + \sqrt{\omega_p^2 - \omega_c^2}}{v_0} \geq \beta$$



6.



$$\hat{h}_z = H_0 J_0 \left(\frac{3.832}{a} r \right) \underline{a}_z$$

$$\hat{h}_t = \frac{H_0 \gamma}{k_c^2} \left(\frac{3.832}{a} \right) J_1 \left(\frac{3.832}{a} r \right) \underline{a}_r$$

$$\hat{e}_t = -\frac{H_0}{j\omega\epsilon_0} \left(\frac{3.832}{a} \right) J_1 \left(\frac{3.832}{a} r \right) \underline{a}_\phi$$

boundary condition is that

$$\underline{a}_z \cdot \nabla H_z = 0 \quad \text{at } z=0 \quad z=L$$

$$\frac{\partial}{\partial z} \left(H_0 J_0 \left(\frac{3.832}{a} r \right) e^{-j\beta z} \right) = 0$$

$$-j\beta H_0 J_0 \left(\frac{3.832}{a} r \right) e^{-j\beta z} = 0$$

$$\therefore \text{require } \operatorname{Re} -j e^{-j\beta z} = 0 \quad \text{at } z=0 \quad z=L$$

$$-j (\cos \beta z - j \sin \beta z) = 0$$

$$-j \cos \beta z - \sin \beta z = 0$$

$$\therefore \beta d = n\pi$$

$$\beta = \frac{n\pi}{d}$$

$$U = \frac{\epsilon_0}{2} \int_0^d \int_0^{2\pi} \int_0^a \frac{H_0^2}{\omega^2 \epsilon_0^2} \left(\frac{3.832}{a} \right)^2 J_1^2 \left(\frac{3.832}{a} r \right) r \, dr \, d\phi \, dz$$

$$= \frac{\epsilon_0}{2} \int_0^d \int_0^{2\pi} \frac{H_0^2}{\omega^2 \epsilon_0^2} \left(\frac{3.832}{a} \right)^2 \frac{a^2}{2} J_0^2(3.832) \, d\phi \, dz$$

$$= \frac{d\pi H_0^2}{2\omega^2 \epsilon_0} (3.832)^2 J_0^2(3.832)$$

$$W_L = \frac{1}{2} R_s \int |H_{tan}|^2 \, dS$$

loss in walls
from homework #1

$$= \frac{R_s}{2} \left[\frac{H_0^2}{2} J_0^2(3.832) 2\pi a d \right] + \frac{R_s}{2} \cdot 2 \int_0^a \frac{H_0^2 \gamma^2}{k_c^2} \left(\frac{3.832}{a} \right)^2 J_1^2 \left(\frac{3.832}{a} r \right) 2\pi r \, dr$$

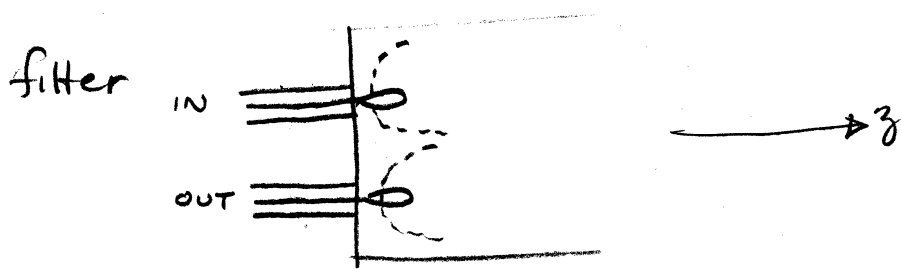
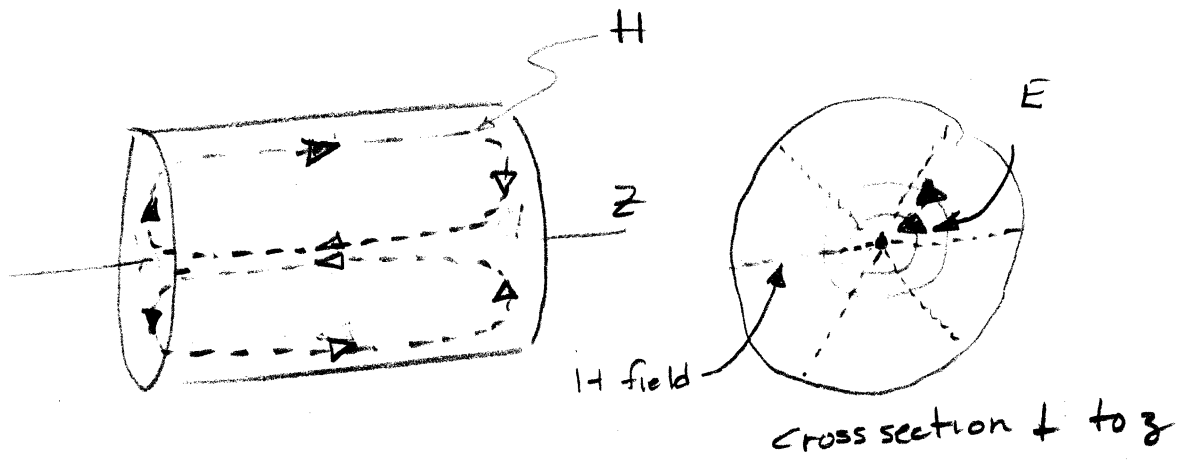
$$= \frac{R_s}{2} \left[\frac{1}{2} J_0^2(3.832) 2\pi a d + R_s \left[\frac{H_0^2 \gamma^2}{k_c^2} \frac{3.832}{a} \pi a^2 J_0^2(3.832) \right] \right]$$

$$Q = \frac{W_L}{U} = \frac{\cancel{\frac{d\pi H_0^2}{2\omega^2 \epsilon_0}} (3.832)^2 J_0^2(3.832)}{\frac{R_s}{2} \cancel{J_0^2(3.832)} 2\pi a d + \frac{R_s H_0^2 \gamma^2}{k_c^2} \left(\frac{3.832}{a} \right) a^2 \cancel{J_0^2(3.832)}}$$

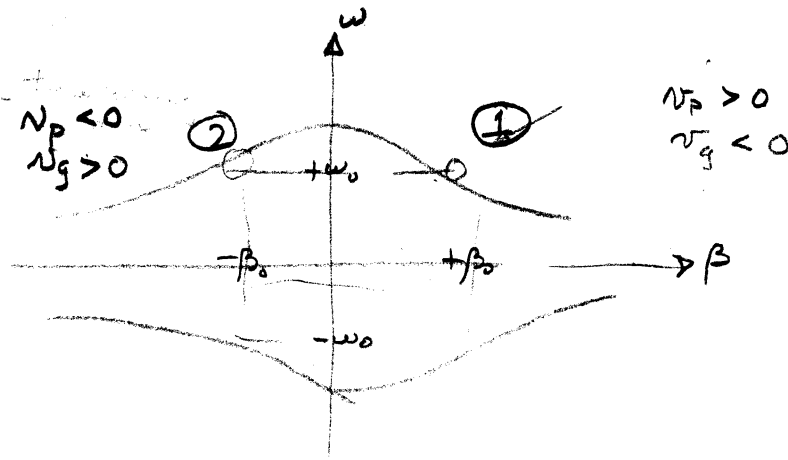
$$= \frac{\frac{d H_0^2}{2\omega^2 \epsilon_0} (3.832)^2}{\frac{R_s}{2} a d + \frac{R_s H_0^2 \gamma^2}{k_c^2} (3.832) a}$$

$$\frac{d H_0^2}{2\omega^2 \epsilon_0} (3.832)^2$$

I don't like the "3.832" in the expression why not?

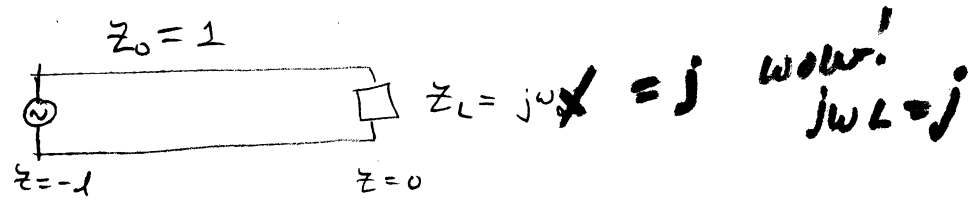


$C j(\omega t - \beta z)$



7/10

obviously $N_g > 0$ for real waves
 Therefore if a signal of frequency ω_0 appeared at the load the point on the $\omega-\beta$ diagram being considered is point ②.



$$P(z=0) = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{j\omega_0 - 1}{j\omega_0 + 1} \quad \tau = \frac{2Z_L}{Z_L + Z_0} = \frac{j2\omega_0}{j\omega_0 + 1}$$

let the voltage measured across the load be denoted by V_L

then $\frac{V_L}{V_+} = \tau = \frac{j2\omega_0}{j\omega_0 + 1}$

$$V_+ = \frac{j\omega_0 + 1}{j2\omega_0}$$

$$\frac{V_-}{V_+} = \rho = \frac{j\omega_0 - 1}{j\omega_0 + 1}$$

$$V_- = \frac{j\omega_0 - 1}{j\omega_0 + 1} V_+$$

$$V_- = \frac{j\omega_0 - 1}{j\omega_0 + 1} \cdot \frac{j\omega_0 + 1}{j2\omega_0} V_L = \frac{j\omega_0 - 1}{j2\omega_0} V_L$$

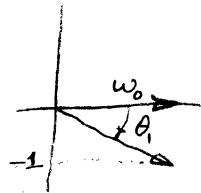
$$\therefore V_- = \frac{j\omega_0 - 1}{j2\omega_0}$$

$$I_+ = \frac{V_+}{Z_0} \quad ; \quad I_- = -\frac{V_-}{Z_0}$$

$$I_+ = \frac{j\omega_0 + 1}{j2\omega_0} \quad I_- = \frac{1 - j\omega_0}{j2\omega_0}$$

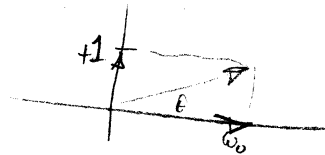
$$V_+ = \frac{j\omega_0 + 1}{j2\omega_0} \quad V_- = \frac{j\omega_0 - 1}{j2\omega_0}$$

$$V_+ = \frac{j\omega_0 + 1}{j2\omega_0} = \frac{\omega_0 - j}{2\omega_0} = \frac{1}{2\omega_0} \sqrt{\omega_0^2 + 1} e^{j\theta_1} \quad ; \quad \theta_1 = -\tan^{-1} \frac{1}{\omega_0}$$



$$I_+ = \frac{1}{2\omega_0} \sqrt{\omega_0^2 + 1} e^{j\theta_1}$$

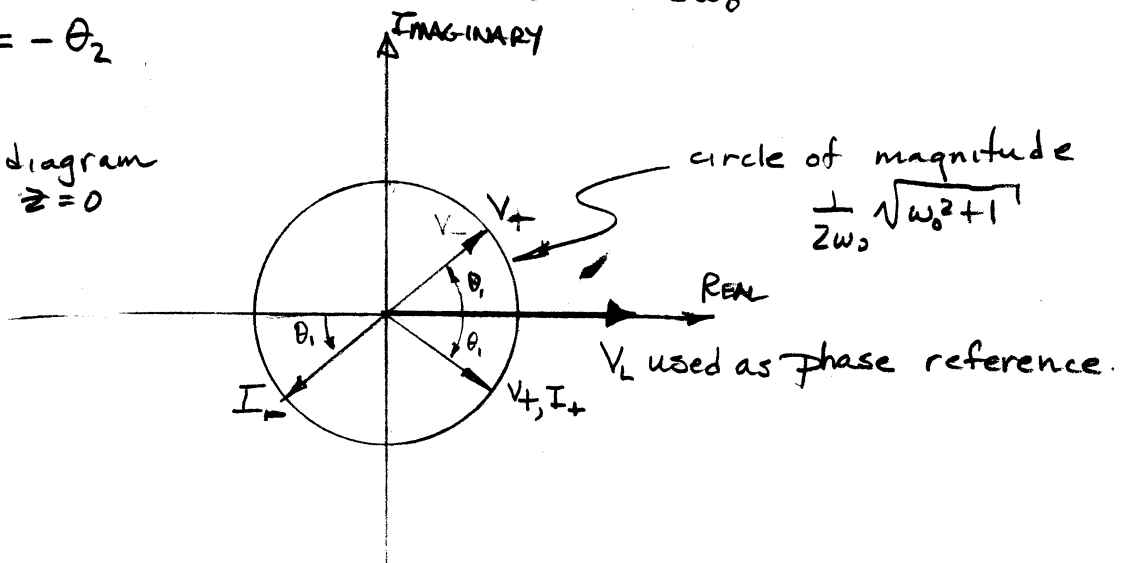
$$V_- = \frac{j\omega_0 - 1}{j2\omega_0} = \frac{\omega_0 + j}{2\omega_0} = \frac{1}{2\omega_0} \sqrt{\omega_0^2 + 1} e^{j\theta_2} \quad ; \quad \theta_2 = \tan^{-1} \frac{1}{\omega_0}$$



$$I_- = \frac{1 - j\omega_0}{j2\omega_0} = -\frac{\omega_0 + j}{2\omega_0} = -\frac{1}{2\omega_0} \sqrt{\omega_0^2 + 1} e^{j\theta_2}$$

Note: $\theta_1 = -\theta_2$

Phasor diagram
at $z=0$



(c) at the source

$$\hat{V}_+(z) = \hat{V}_+ e^{-j\beta z} \quad ; \quad \hat{V}_-(z) = \hat{V}_- e^{+j\beta z}$$

if $z = -\frac{\lambda}{4}$ and $\beta < 0 \Rightarrow \beta = -\frac{2\pi}{\lambda} \quad \lambda > 0$

$$\beta z = -\beta \frac{\lambda}{4} = + \frac{2\pi}{\lambda} \cdot \frac{\lambda}{4} = \frac{\pi}{2}$$

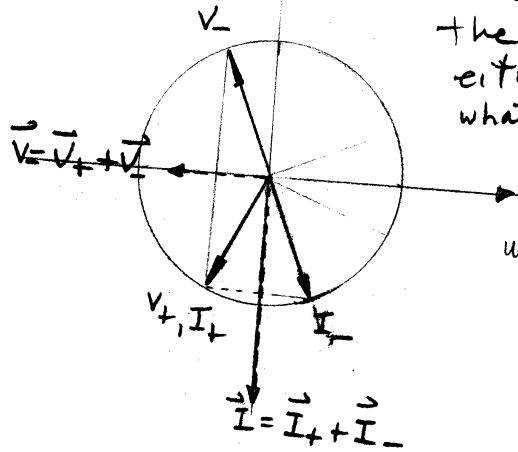
$$\therefore \hat{V}_+(-l) = \hat{V}_+ e^{-j\frac{\pi}{2}}$$

$$\hat{V}_-(-l) = \hat{V}_+ e^{+j\frac{\pi}{2}}$$

$$\hat{I}_+(-l) = \hat{V}_+ e^{-j\frac{\pi}{2}}$$

$$\hat{I}_-(-l) = -\hat{V}_+ e^{+j\frac{\pi}{2}}$$

I cannot say what the source sees in terms of reflected and incident waves because I do not know enough about the source, i.e. I need to know either its internal impedance or what voltage it is putting out (phase & magnitude)



"the source sees"
 does not mean to include its own impedance
 i.e. e.

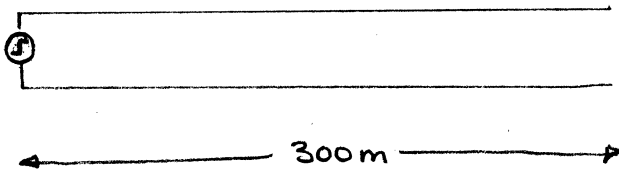
(d)

by inspection I leads V by 90° and the line appears to be a capacitive load to the voltage source.

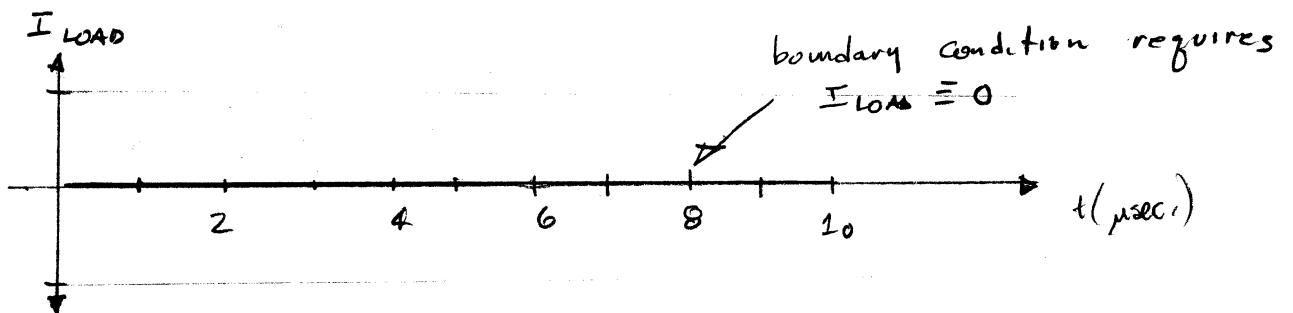
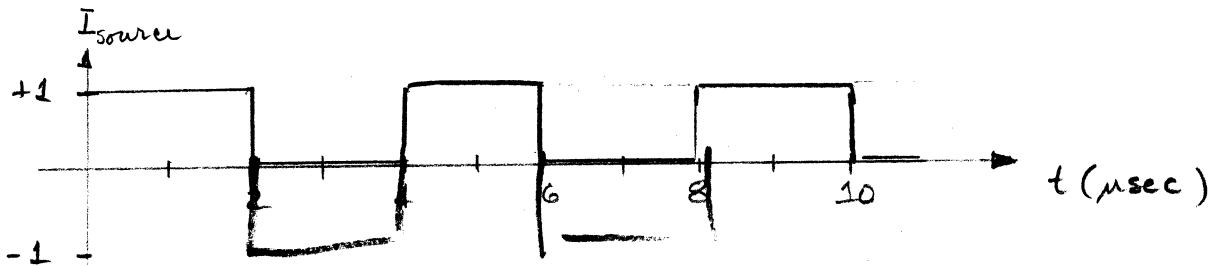
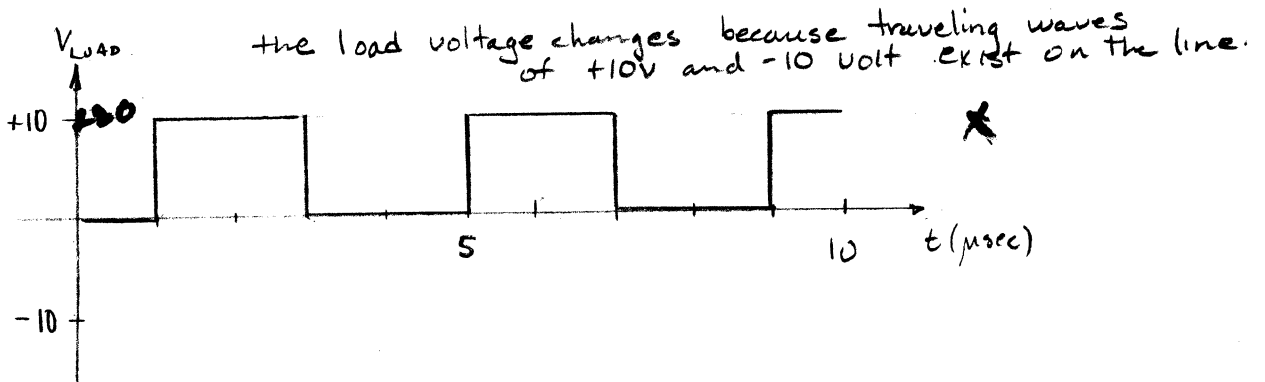
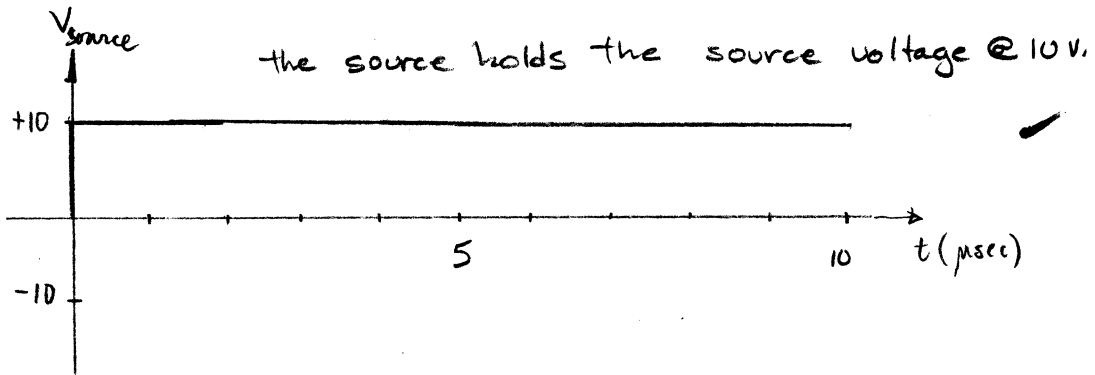
2.

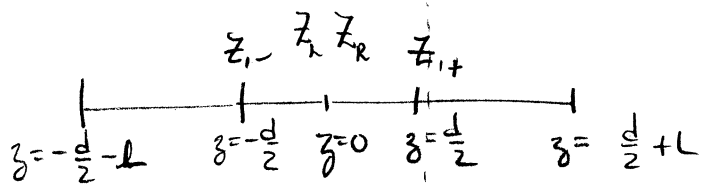
ideal
Z=0

$$Z_0 = 10 \Omega$$



$$t = \frac{3 \times 10^2 \text{ m}}{3 \times 10^8 \text{ m/sec}} = 10^{-6} \text{ sec} = 1 \mu\text{sec.}$$





$$Z_{i+} = Z_0 \left[\frac{j Z_0 \sin kL}{Z_0 \cos kL} \right] \quad \text{because } Z_L = 0$$

$$Z_{i+} = Z_0 [j \tan kL] \quad \checkmark$$

$$Z_{i-} = Z_0 \left[\frac{j Z_0 \sin(-kL)}{Z_0 \cos(-kL)} \right] \quad \text{because } Z_L = 0$$

$$= Z_0 [-j \tan kL]$$

$$Z_R = Z_1 \left[\frac{Z_{i+} \cos \frac{kd}{2} + j Z_1 \sin \frac{kd}{2}}{Z_1 \cos \frac{kd}{2} + j Z_{i+} \sin \frac{kd}{2}} \right] \quad \checkmark$$

$$Z_L = Z_1 \left[\frac{Z_{i-} \cos \frac{kd}{2} - j Z_1 \sin \frac{kd}{2}}{Z_1 \cos \frac{kd}{2} - j Z_{i-} \sin \frac{kd}{2}} \right]$$

for resonance $Z_R = Z_L \quad \checkmark$

$$\frac{Z_{i+} \cos \frac{kd}{2} + j Z_1 \sin \frac{kd}{2}}{Z_1 \cos \frac{kd}{2} + j Z_{i+} \sin \frac{kd}{2}} = \frac{Z_{i-} \cos \frac{kd}{2} - j Z_1 \sin \frac{kd}{2}}{Z_1 \cos \frac{kd}{2} - j Z_{i-} \sin \frac{kd}{2}}$$

$$\begin{aligned}
 & z_1 z_{1+} \cos^2 \frac{kd}{2} - j z_{1+} z_{1-} \cos \frac{kd}{2} \sin \frac{kd}{2} + j z_1 z_1 \sin \frac{kd}{2} \cos \frac{kd}{2} + z_1 z_{1-} \sin^2 \frac{kd}{2} \\
 &= z_1 z_{1-} \cos^2 \frac{kd}{2} - j z_1 z_1 \sin \frac{kd}{2} \cos \frac{kd}{2} + j z_{1-} z_{1+} \cos \frac{kd}{2} \sin \frac{kd}{2} + z_1 z_{1+} \sin^2 \frac{kd}{2}
 \end{aligned}$$

∴ for equality

$$z_1 z_{1+} \cos^2 \frac{kd}{2} + z_1 z_{1-} \sin^2 \frac{kd}{2} = z_1 z_{1-} \cos^2 \frac{kd}{2} + z_1 z_{1+} \sin^2 \frac{kd}{2}$$

$$z_{1+} \cos^2 \frac{kd}{2} + z_{1-} \sin^2 \frac{kd}{2} = z_{1-} \cos^2 \frac{kd}{2} + z_{1+} \sin^2 \frac{kd}{2}$$

$$\cancel{-z_{1+} z_{1-} \cos \frac{kd}{2} \sin \frac{kd}{2}} + \cancel{z_1 z_1 \sin \frac{kd}{2} \cos \frac{kd}{2}} = \cancel{-z_1 z_1 \sin \frac{kd}{2} \cos \frac{kd}{2}} + \cancel{z_{1-} z_{1+} \cos \frac{kd}{2} \sin \frac{kd}{2}}$$

$$-z_{1+} z_{1-} + z_1^2 = -z_1^2 + z_{1-} z_{1+}$$

$$(-z_{1+} z_{1-} + z_1^2) = -(z_1^2 - z_{1-} z_{1+})$$

$$\therefore z_1^2 = z_{1+} z_{1-}$$

$$\cancel{z_0} [\cancel{+j \tan kL}] \cos^2 \frac{kd}{2} + \cancel{z_0} [\cancel{-j \tan kL}] \sin^2 \frac{kd}{2} = \cancel{z_0} [\cancel{-j \tan kL}] \cos^2 \frac{kd}{2} + \cancel{z_0} [\cancel{+j \tan kL}] \sin^2 \frac{kd}{2}$$

$$\cos^2 \frac{kd}{2} + \sin^2 \frac{kd}{2} = -\cos^2 \frac{kd}{2} + \sin^2 \frac{kd}{2}$$

$$\therefore \cos^2 \frac{kd}{2} - \sin^2 \frac{kd}{2} = 0$$

$$\frac{kd}{2} = \frac{\pi}{4}$$

$$k = \frac{\pi}{2d}$$

k is measured in the dielectric region of the wave structure

i.e. $k = \omega \sqrt{\mu_0 \epsilon_0}$

$$Z_1 = \sqrt{\frac{\mu_0}{\epsilon_1}}$$

$$\omega \sqrt{\mu_0 \epsilon_0} = \frac{\pi}{2d}$$

$$\omega = \frac{\pi}{2d \sqrt{\mu_0 \epsilon_0}}$$

$$Z_0 = \sqrt{\frac{\mu_0}{\epsilon_0}}$$

$k' \triangleq$ propagation constant in the free space region

$$\sqrt{\frac{\mu_0}{\epsilon_1}} \sqrt{\frac{\mu_0}{\epsilon_1}} = \sqrt{\frac{\mu_0}{\epsilon_0}} (j \tan k'L) \sqrt{\frac{\mu_0}{\epsilon_0}} (-j \tan k'L)$$

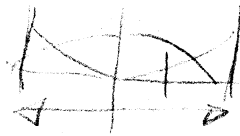
$$\frac{\epsilon_0 \epsilon_1}{\mu_0} \frac{\mu_0}{\epsilon_1} = \frac{\mu_0}{\epsilon_0} \tan^2 k'L \frac{\epsilon_0 \epsilon_1}{\mu_0}$$

$$\frac{\epsilon_0}{\epsilon_1} = \tan^2 k'L$$

$$\sqrt{\frac{\epsilon_0}{\epsilon_1}} = \tan k'L$$

$$k'L = \tan^{-1} \sqrt{\frac{\epsilon_0}{\epsilon_1}}$$

$$k' = \frac{\tan^{-1} \sqrt{\frac{\epsilon_0}{\epsilon_1}}}{L}$$



for resonance:

The propagation constants β & β' must be equal at the interface

$$\Rightarrow k = k'$$

$$\omega \sqrt{\mu_0 \epsilon_0'} = \frac{\tan^{-1} \sqrt{\frac{\epsilon_0}{\epsilon_1}}}{L}$$

$$\omega_{\text{resonant}} = \frac{\tan^{-1} \sqrt{\frac{\epsilon_0}{\epsilon_1}}}{L \sqrt{\mu_0 \epsilon_0}}$$

I was trying to do this using an impedance concept

I used as a reference

"Electromagnetic Theory For Engineering Applications"
by W.L. Weeks

which said that if one breaks open a cavity at a point, measures the impedance looking to the right, and then measures the impedance looking to the left, call these values Z_R & Z_L ,

If $Z_R = Z_L$ the circuit is resonant.

But using this technique I only obtained one resonant frequency. \Rightarrow something is wrong.