

COMPLEX POYNTING'S THEOREM

①

Maxwell's equations in Complex Form for a linear medium (isotropic)

$$\textcircled{1} \quad \nabla \times \underline{\hat{E}} = -j\omega \mu \underline{\hat{H}}$$

$$\textcircled{2} \quad \nabla \times \underline{\hat{H}} = \underline{\hat{J}} + j\omega \epsilon \underline{\hat{E}}$$

$$\textcircled{3} \quad \nabla \cdot \mu \underline{\hat{H}} = 0$$

$$\textcircled{4} \quad \nabla \cdot \epsilon \underline{\hat{E}} = \hat{\rho}$$

Let us mathematically manipulate ① and ② by taking ① and dotting it into $\underline{\hat{H}}^*$ conjugate $\equiv \underline{\hat{H}}^*$ and taking ② conjugated and ^{dot} multiply it by $\underline{\hat{E}}^*$ then subtracting one resulting equation from the other so that we have

$$\underline{\hat{E}} \cdot \nabla \times \underline{\hat{H}}^* - \underline{\hat{H}}^* \cdot \nabla \times \underline{\hat{E}} = \underline{\hat{E}} \cdot \underline{\hat{J}}^* + j\omega (\mu \underline{\hat{H}} \cdot \underline{\hat{H}}^* - \epsilon \underline{\hat{E}} \cdot \underline{\hat{E}}^*)$$

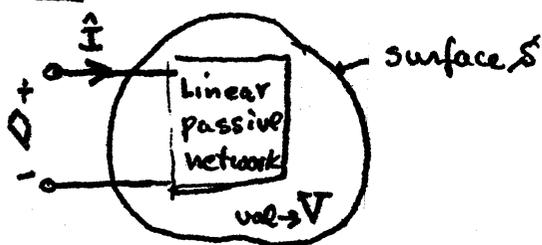
$$\text{or} \quad -\nabla \cdot (\underline{\hat{E}} \times \underline{\hat{H}}^* / 2) = \frac{\underline{\hat{E}} \cdot \underline{\hat{J}}^*}{2} + 2j\omega \left[\frac{1}{4} \mu |\hat{H}|^2 - \frac{1}{4} \epsilon |\hat{E}|^2 \right]$$

now $\frac{1}{4} \mu |\hat{H}|^2 = \langle u_m \rangle$, the time average magnetic energy ^{density} stored

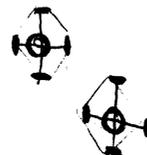
and $\frac{1}{4} \epsilon |\hat{E}|^2 = \langle u_e \rangle$ " " " electric energy density

we define $\underline{\hat{P}} = \frac{1}{2} (\underline{\hat{E}} \times \underline{\hat{H}}^*)$ as the complex Poynting vector

Example



within some surface we have a linear passive network (which can be a lumped element representation of a distributed system at the frequency ω)



We can define the impedance of this network at some position in space by determining the complex voltage \hat{V} and current \hat{I} at this position

$$Z = \frac{\hat{V}}{\hat{I}} = \frac{\hat{V} \hat{I}^*}{|\hat{I}|^2}$$

but $\frac{1}{2} \hat{V} \hat{I}^* = - \oint_S \vec{P} \cdot d\vec{s}$ since it is the complex power flowing into the volume! hence

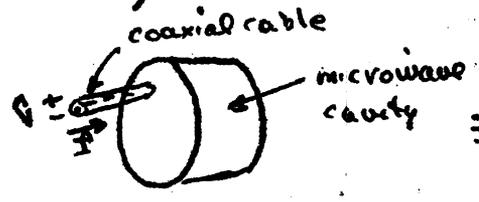
$$Z = \frac{2}{|\hat{I}|^2} \left[\frac{1}{2} \oint_{vol} \vec{J} \cdot \vec{E} dV + 2j\omega \int_{vol} (\langle U_m \rangle - \langle U_e \rangle) dV \right]$$

$$= \frac{2}{|\hat{I}|^2} \left[\langle P_d \rangle + 2j\omega (\langle U_m \rangle - \langle U_e \rangle) \right]$$

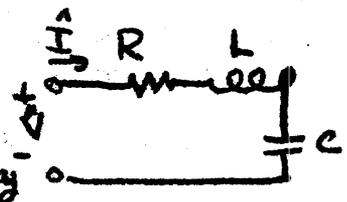
resistance, $R = \text{Re } Z = \frac{2 \langle P_d \rangle}{|\hat{I}|^2}$

time ave stored mag. energy time average elect. energy stored

reactance, $X = \text{Im } Z = \frac{4\omega}{|\hat{I}|^2} (\langle U_m \rangle - \langle U_e \rangle)$



equivalent to at some frequency near resonance.



$$\langle U_m \rangle = \frac{1}{4} L |\hat{I}|^2$$

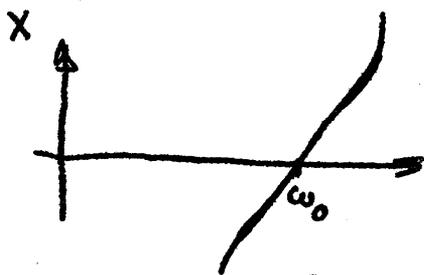
$$\langle U_e \rangle = \frac{1}{4} \frac{|\hat{I}|^2}{\omega^2 C}$$

$$\langle P_d \rangle = \frac{1}{2} R |\hat{I}|^2$$

$$Z = R + jX = \frac{2}{|\hat{I}|^2} \left[\frac{|\hat{I}|^2 R}{2} + 2 \left[\frac{\omega L |\hat{I}|^2}{4} - \frac{|\hat{I}|^2}{4\omega C} \right] \right]$$

resonance occurs for $X = 0$
or $\omega_0^2 = \frac{1}{LC}$

③



Let us expand the reactance near resonance in a Taylor series

$$X \approx X(\omega_0) + (\omega - \omega_0) \left. \frac{\partial X}{\partial \omega} \right|_{\omega = \omega_0}$$

but $\frac{\partial X}{\partial \omega} = \frac{4}{|I|^2} \left[\frac{L|I|^2}{4} + \frac{|I|^2}{4\omega^2 C} \right] = \frac{4}{|I|^2} [\langle U_m \rangle + \langle U_e \rangle]$

by direct substitution.

this is a general result in spite of our specific use of a series RLC net.

hence near resonance

$$Z = \frac{2}{|I|^2} \left[\langle P_d \rangle + 2j(\omega - \omega_0) (\langle U_m \rangle + \langle U_e \rangle) \right] \quad (\text{note } \langle U_m \rangle = \langle U_e \rangle \text{ at resonance})$$

the Q is found by setting $X = R$ at some $\omega - \omega_0$ and

is given by $Q = \frac{2\langle U_e \rangle_{\omega = \omega_0}}{\langle P_d \rangle}$ resonant frequency
bandwidth

now let us perturb the system in the volume by introducing a small modification of its dielectric constant

say which gives a $\Delta \langle U_e \rangle_{\omega = \omega_0} \ll \langle U_e \rangle_{\omega = \omega_0}$ then the

change in reactance is

$$\Delta X = \left. \frac{\partial X}{\partial \omega} \right|_{\omega_0} (\omega - \omega_0) + \left. \frac{\partial X}{\partial U_e} \right|_{\omega = \omega_0} \langle \Delta U_e \rangle = \frac{4}{|I|^2} (\langle U_m \rangle + \langle U_e \rangle) (\omega - \omega_0) - \frac{4\omega_0}{|I|^2} \langle \Delta U_e \rangle$$

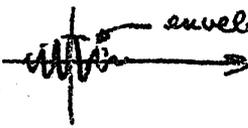
So the frequency shifts $\omega - \omega_0 = \Delta \omega$ to return to resonance ($\Delta X = 0$) by an amount $\frac{\Delta \omega}{\omega_0} = \frac{\langle \Delta U_e \rangle}{2\langle U_e \rangle}$ (we have used $\langle U_m \rangle = \langle U_e \rangle$)

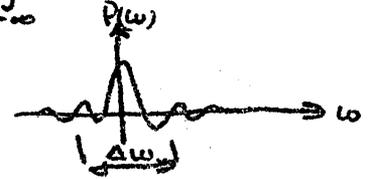
GROUP VELOCITY (See SEC 1.2F)

We consider propagation of a pulse modulated r.f. carrier $f(t)$

pulse = $P(t)$ 

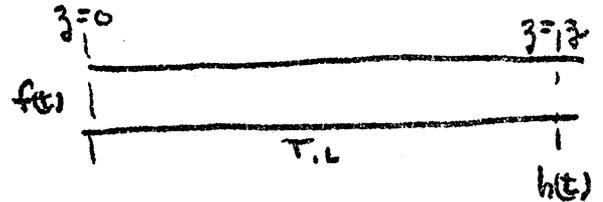
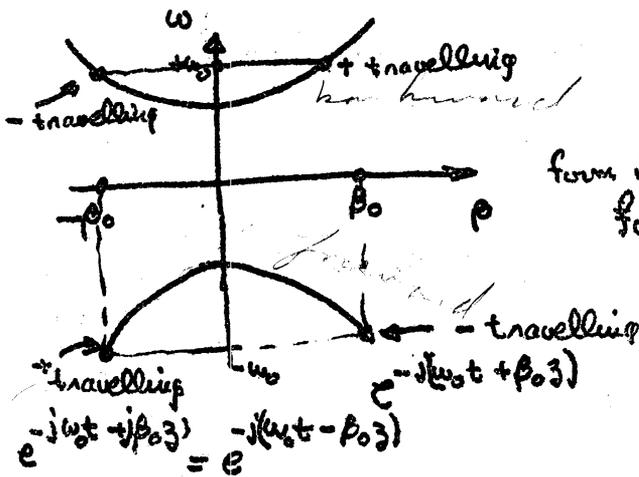
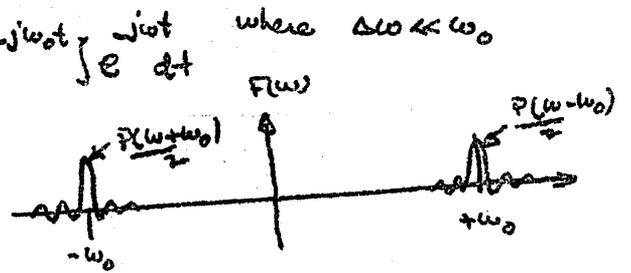
$$P(\omega) = \int_{-\infty}^{\infty} P(t) e^{-j\omega t} dt$$

$f(t) = P(t) \cos \omega_0 t$ 



$$F(\omega) = \int_{-\infty}^{\infty} f(t) e^{-j\omega t} dt = \frac{1}{2} \int_{-\infty}^{\infty} P(t) [e^{j\omega_0 t} + e^{-j\omega_0 t}] e^{-j\omega t} dt$$

$$= \frac{1}{2} [P(\omega + \omega_0) + P(\omega - \omega_0)]$$



$$h(t) = \frac{1}{2\pi} \int_0^{\infty} e^{j(\omega t - \beta z)} F(\omega) d\omega + \frac{1}{2\pi} \int_{-\infty}^0 e^{j(\omega t + \beta z)} F(\omega) d\omega$$

$$= 2 \operatorname{Re} \frac{1}{2\pi} \int_0^{\infty} F(\omega) e^{j(\omega t - \beta z)} d\omega = 2 \operatorname{Re} \frac{1}{2\pi} \int_0^{\infty} P\left(\frac{\omega - \omega_0}{2}\right) e^{j(\omega t - \beta z)} d\omega$$

but $\beta \approx \beta_0 + \left. \frac{\partial \beta}{\partial \omega} \right|_{\omega = \omega_0} (\omega - \omega_0)$ so $h(t) = 2 \operatorname{Re} e^{j(\omega_0 t - \beta_0 z)} \frac{1}{2\pi} \int_0^{\infty} P\left(\frac{\omega - \omega_0}{2}\right) e^{j(\omega - \omega_0) \left(t - \frac{\partial \beta}{\partial \omega} z\right)} d\omega$

$$\approx h(t) = \cos(\omega_0 t - \beta_0 z) P\left(t - \frac{\partial \beta}{\partial \omega} z\right)$$

so the envelope propagates with the velocity, $v_{g \text{ group}}$ (called the group velocity) which is $v_g = \left. \frac{\partial \omega}{\partial \beta} \right|_{\omega = \omega_0}$.

The carrier propagates with the velocity $v_{\text{phase}} = \omega_0 / \beta_0$.

BACKWARD WAVES

the Group velocity is $\frac{d\omega}{d\beta}$ which we saw is the velocity of the propagation of the envelope of a pulsed mod signal.

Let's consider a simple periodic transmission line whose structure is



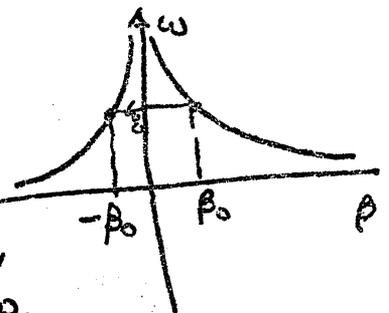
$$Z = \frac{1}{j\omega C}$$

$$Y = \frac{1}{j\omega L}$$

the propagation constant

$$\gamma = \sqrt{ZY} = \pm \frac{1}{\omega\sqrt{LC}} = j\beta \quad \text{so the}$$

dispersion diagram is



$$-\beta^2 = \gamma^2 = \frac{1}{j\omega C} \cdot \frac{1}{j\omega L} = -\frac{1}{\omega^2 LC}$$

$$\beta^2 = \frac{1}{\omega^2 LC} \quad \beta = \frac{1}{\omega\sqrt{LC}}$$

$$\beta = \frac{1}{\omega\sqrt{LC}}, \quad \beta_0 = \frac{1}{\omega_0\sqrt{LC}}$$

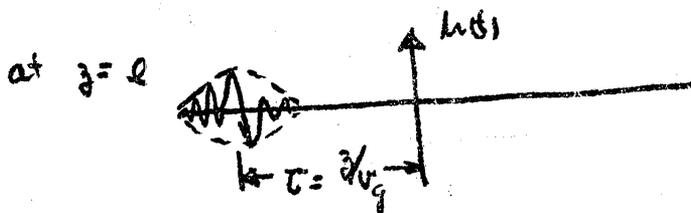
$$\left. \frac{\partial \beta}{\partial \omega} \right|_{\omega_0} = -\frac{1}{\omega_0^2 \sqrt{LC}} = -\beta_0 / \omega_0$$

hence β_0 and $\left. \frac{\partial \beta}{\partial \omega} \right|_{\omega_0}$ have opposite signs!

for a wave travelling in the $+z$ -direction could we use $P(t + \beta_0 z / \omega_0) \cos(\omega_0 t - \beta_0 z)$?

what does this form imply?

envelope arrives before the carrier.



actually for a backward wave the direction is the same sign as appears in the equation!

that is the wave has arrived before it has been transmitted! - (called ESP)

actually the $+z$ travelling wave is $P(t - \beta_0 / \omega_0 z) \cos(\omega_0(t + \beta_0 z))$

These are called BACKWARD WAVES