

Chapter 10, Solution 1.

$$\omega = 1$$

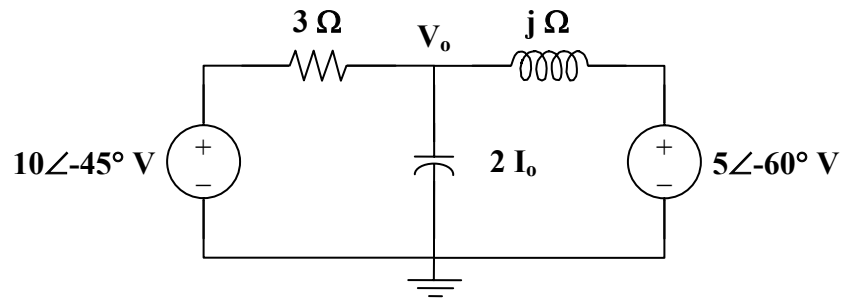
$$10 \cos(t - 45^\circ) \longrightarrow 10 \angle -45^\circ$$

$$5 \sin(t + 30^\circ) \longrightarrow 5 \angle -60^\circ$$

$$1 \text{ H} \longrightarrow j\omega L = j$$

$$1 \text{ F} \longrightarrow \frac{1}{j\omega C} = -j$$

The circuit becomes as shown below.



Applying nodal analysis,

$$\frac{(10 \angle -45^\circ) - V_o}{3} + \frac{(5 \angle -60^\circ) - V_o}{j} = \frac{V_o}{-j}$$

$$j10 \angle -45^\circ + 15 \angle -60^\circ = jV_o$$

$$V_o = 10 \angle -45^\circ + 15 \angle -150^\circ = 15.73 \angle 247.9^\circ$$

Therefore, $v_o(t) = \underline{\underline{15.73 \cos(t + 247.9^\circ) \text{ V}}}$

Chapter 10, Solution 2.

$$\omega = 10$$

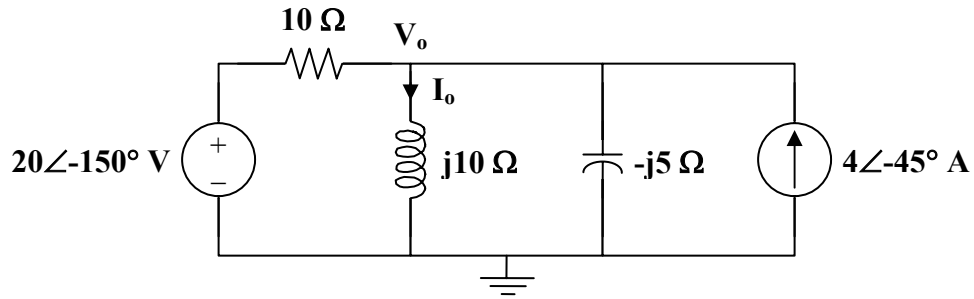
$$4 \cos(10t - \pi/4) \longrightarrow 4 \angle -45^\circ$$

$$20 \sin(10t + \pi/3) \longrightarrow 20 \angle -150^\circ$$

$$1 \text{ H} \longrightarrow j\omega L = j10$$

$$0.02 \text{ F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j0.2} = -j5$$

The circuit becomes that shown below.



Applying nodal analysis,

$$\frac{(20\angle -150^\circ) - V_o}{10} + 4\angle -45^\circ = \frac{V_o}{j10} + \frac{V_o}{-j5}$$

$$20\angle -150^\circ + 4\angle -45^\circ = 0.1(1 + j)V_o$$

$$I_o = \frac{V_o}{j10} = \frac{2\angle -150^\circ + 4\angle -45^\circ}{j(1 + j)} = 2.816\angle 150.98^\circ$$

Therefore, $i_o(t) = \underline{\underline{2.816 \cos(10t + 150.98^\circ) \text{ A}}}$

Chapter 10, Solution 3.

$$\omega = 4$$

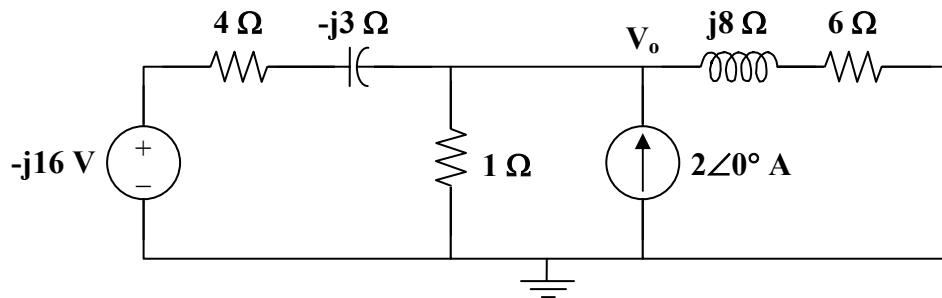
$$2\cos(4t) \longrightarrow 2\angle 0^\circ$$

$$16\sin(4t) \longrightarrow 16\angle -90^\circ = -j16$$

$$2 \text{ H} \longrightarrow j\omega L = j8$$

$$1/12 \text{ F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(4)(1/12)} = -j3$$

The circuit is shown below.



Applying nodal analysis,

$$\frac{-j16 - V_o}{4 - j3} + 2 = \frac{V_o}{1} + \frac{V_o}{6 + j8}$$

$$\frac{-j16}{4 - j3} + 2 = \left(1 + \frac{1}{4 - j3} + \frac{1}{6 + j8}\right) V_o$$

$$V_o = \frac{3.92 - j2.56}{1.22 + j0.04} = \frac{4.682 \angle -33.15^\circ}{1.2207 \angle 1.88^\circ} = 3.835 \angle -35.02^\circ$$

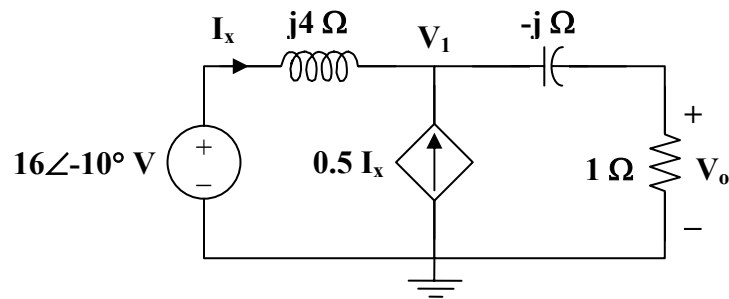
Therefore, $v_o(t) = \underline{\underline{3.835 \cos(4t - 35.02^\circ) \text{ V}}}$

Chapter 10, Solution 4.

$$16 \sin(4t - 10^\circ) \longrightarrow 16 \angle -10^\circ, \quad \omega = 4$$

$$1 \text{ H} \longrightarrow j\omega L = j4$$

$$0.25 \text{ F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(4)(1/4)} = -j$$



$$\frac{(16 \angle -10^\circ) - V_1}{j4} + \frac{1}{2} I_x = \frac{V_1}{1 - j}$$

But

$$I_x = \frac{(16 \angle -10^\circ) - V_1}{j4}$$

So,
$$\frac{3((16 \angle -10^\circ) - V_1)}{j8} = \frac{V_1}{1 - j}$$

$$V_1 = \frac{48\angle -10^\circ}{-1 + j4}$$

Using voltage division,

$$V_o = \frac{1}{1-j} V_1 = \frac{48\angle -10^\circ}{(1-j)(-1+j4)} = 8.232\angle -69.04^\circ$$

Therefore, $v_o(t) = \underline{8.232 \sin(4t - 69.04^\circ) \text{ V}}$

Chapter 10, Solution 5.

Let the voltage across the capacitor and the inductor be V_x and we get:

$$\frac{V_x - 0.5I_x - 10\angle 30^\circ}{4} + \frac{V_x}{-j2} + \frac{V_x}{j3} = 0$$

$$(3 + j6 - j4)V_x - 1.5I_x = 30\angle 30^\circ \text{ but } I_x = \frac{V_x}{-j2} = j0.5V_x$$

Combining these equations we get:

$$(3 + j2 - j0.75)V_x = 30\angle 30^\circ \text{ or } V_x = \frac{30\angle 30^\circ}{3 + j1.25}$$

$$I_x = j0.5 \frac{30\angle 30^\circ}{3 + j1.25} = \underline{4.615\angle 97.38^\circ \text{ A}}$$

Chapter 10, Solution 6.

Let V_o be the voltage across the current source. Using nodal analysis we get:

$$\frac{V_o - 4V_x}{20} - 3 + \frac{V_o}{20 + j10} = 0 \text{ where } V_x = \frac{20}{20 + j10} V_o$$

Combining these we get:

$$\frac{V_o}{20} - \frac{4V_o}{20 + j10} - 3 + \frac{V_o}{20 + j10} = 0 \rightarrow (1 + j0.5 - 3)V_o = 60 + j30$$

$$V_o = \frac{60 + j30}{-2 + j0.5} \text{ or } V_x = \frac{20(3)}{-2 + j0.5} = \underline{29.11\angle -166^\circ \text{ V.}}$$

Chapter 10, Solution 7.

At the main node,

$$\frac{120\angle -15^\circ - V}{40 + j20} = 6\angle 30^\circ + \frac{V}{-j30} + \frac{V}{50} \longrightarrow \frac{115.91 - j31.058}{40 + j20} - 5.196 - j3 =$$

$$V \left(\frac{1}{40 + j20} + \frac{j}{30} + \frac{1}{50} \right)$$

$$V = \frac{-3.1885 - j4.7805}{0.04 + j0.0233} = \underline{124.08\angle -154^\circ \text{ V}}$$

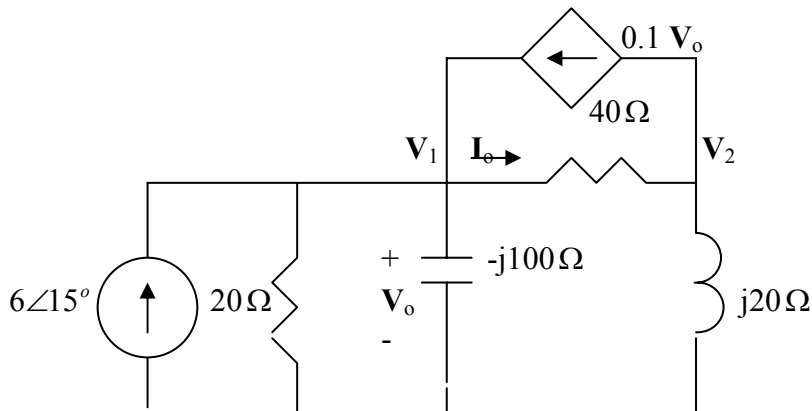
Chapter 10, Solution 8.

$$\omega = 200,$$

$$100\text{mH} \longrightarrow j\omega L = j200 \times 0.1 = j20$$

$$50\mu\text{F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j200 \times 50 \times 10^{-6}} = -j100$$

The frequency-domain version of the circuit is shown below.



At node 1,

$$6\angle 15^\circ + 0.1V_1 = \frac{V_1}{20} + \frac{V_1}{-j100} + \frac{V_1 - V_2}{40}$$

$$\text{or} \quad 5.7955 + j1.5529 = (-0.025 + j0.01)V_1 - 0.025V_2 \quad (1)$$

At node 2,

$$\frac{V_1 - V_2}{40} = 0.1V_1 + \frac{V_2}{j20} \longrightarrow 0 = 3V_1 + (1 - j2)V_2 \quad (2)$$

From (1) and (2),

$$\begin{bmatrix} (-0.025 + j0.01) & -0.025 \\ 3 & (1 - j2) \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} (5.7955 + j1.5529) \\ 0 \end{bmatrix} \quad \text{or} \quad \mathbf{AV} = \mathbf{B}$$

Using MATLAB,

$$\mathbf{V} = \text{inv}(\mathbf{A}) * \mathbf{B}$$

leads to $V_1 = -70.63 - j127.23$, $V_2 = -110.3 + j161.09$

$$I_o = \frac{V_1 - V_2}{40} = 7.276 \angle -82.17^\circ$$

Thus,

$$\underline{i_o(t) = 7.276 \cos(200t - 82.17^\circ) \text{ A}}$$

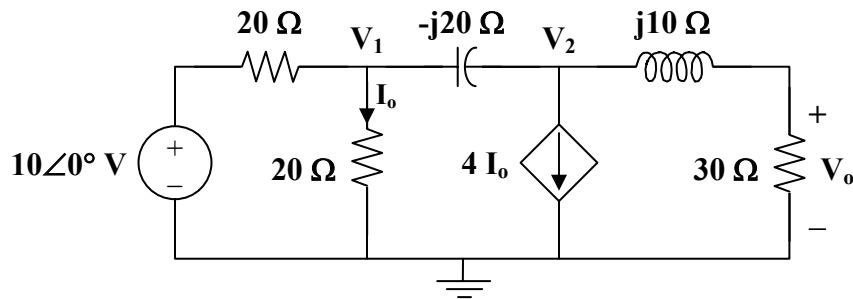
Chapter 10, Solution 9.

$$10 \cos(10^3 t) \longrightarrow 10 \angle 0^\circ, \quad \omega = 10^3$$

$$10 \text{ mH} \longrightarrow j\omega L = j10$$

$$50 \mu\text{F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(10^3)(50 \times 10^{-6})} = -j20$$

Consider the circuit shown below.



At node 1,

$$\frac{10 - V_1}{20} = \frac{V_1}{20} + \frac{V_1 - V_2}{-j20}$$

$$10 = (2 + j)V_1 - jV_2 \quad (1)$$

At node 2,

$$\frac{V_1 - V_2}{-j20} = (4) \frac{V_1}{20} + \frac{V_2}{30 + j10}, \text{ where } I_o = \frac{V_1}{20} \text{ has been substituted.}$$

$$(-4 + j)V_1 = (0.6 + j0.8)V_2$$

$$V_1 = \frac{0.6 + j0.8}{-4 + j} V_2 \quad (2)$$

Substituting (2) into (1)

$$10 = \frac{(2 + j)(0.6 + j0.8)}{-4 + j} V_2 - jV_2$$

or
$$V_2 = \frac{170}{0.6 - j26.2}$$

$$V_o = \frac{30}{30 + j10} V_2 = \frac{3}{3 + j} \cdot \frac{170}{0.6 - j26.2} = 6.154 \angle 70.26^\circ$$

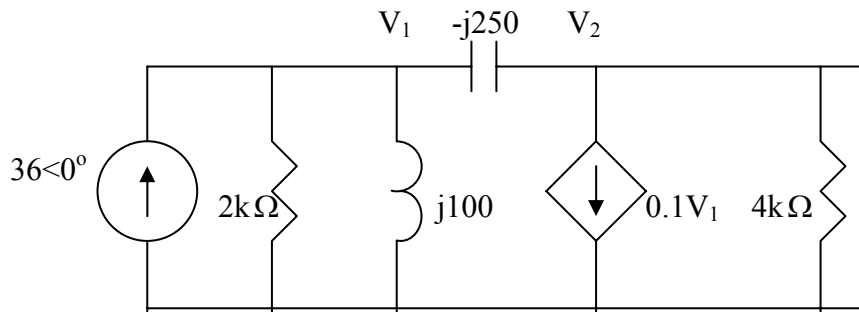
Therefore,
$$v_o(t) = \underline{\underline{6.154 \cos(10^3 t + 70.26^\circ) \text{ V}}}$$

Chapter 10, Solution 10.

$$50 \text{ mH} \longrightarrow j\omega L = j2000 \times 50 \times 10^{-3} = j100, \quad \omega = 2000$$

$$2 \mu\text{F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j2000 \times 2 \times 10^{-6}} = -j250$$

Consider the frequency-domain equivalent circuit below.



At node 1,

$$36 = \frac{V_1}{2000} + \frac{V_1}{j100} + \frac{V_1 - V_2}{-j250} \longrightarrow 36 = (0.0005 - j0.006)V_1 - j0.004V_2 \quad (1)$$

At node 2,

$$\frac{V_1 - V_2}{-j250} = 0.1V_1 + \frac{V_2}{4000} \longrightarrow 0 = (0.1 - j0.004)V_1 + (0.00025 + j0.004)V_2 \quad (2)$$

Solving (1) and (2) gives

$$V_o = V_2 = -535.6 + j893.5 = 8951.1 \angle 93.43^\circ$$

$$v_o(t) = \underline{\underline{8.951 \sin(2000t + 93.43^\circ) \text{ kV}}}$$

Chapter 10, Solution 11.

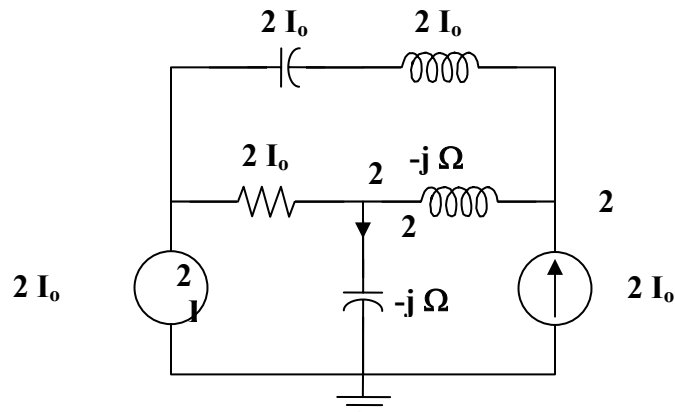
$$\cos(2t) \longrightarrow 1 \angle 0^\circ, \quad \omega = 2$$

$$8 \sin(2t + 30^\circ) \longrightarrow 8 \angle -60^\circ$$

$$1 \text{ H} \longrightarrow j\omega L = j2 \qquad 1/2 \text{ F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(2)(1/2)} = -j$$

$$2 \text{ H} \longrightarrow j\omega L = j4 \qquad 1/4 \text{ F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(2)(1/4)} = -j2$$

Consider the circuit below.



At node 1,

$$\frac{(8\angle -60^\circ) - V_1}{2} = \frac{V_1}{-j} + \frac{V_1 - V_2}{j2}$$

$$8\angle -60^\circ = (1 + j)V_1 + jV_2 \quad (1)$$

At node 2,

$$1 + \frac{V_1 - V_2}{j2} + \frac{(8\angle -60^\circ) - V_2}{j4 - j2} = 0$$

$$V_2 = 4\angle -60^\circ + j + 0.5V_1 \quad (2)$$

Substituting (2) into (1),

$$1 + 8\angle -60^\circ - 4\angle 30^\circ = (1 + jl.5)V_1$$

$$V_1 = \frac{1 + 8\angle -60^\circ - 4\angle 30^\circ}{1 + jl.5}$$

$$I_o = \frac{V_1}{-j} = \frac{1 + 8\angle -60^\circ - 4\angle 30^\circ}{1.5 - j} = 5.024\angle -46.55^\circ$$

Therefore, $i_o(t) = \underline{5.024 \cos(2t - 46.55^\circ)}$

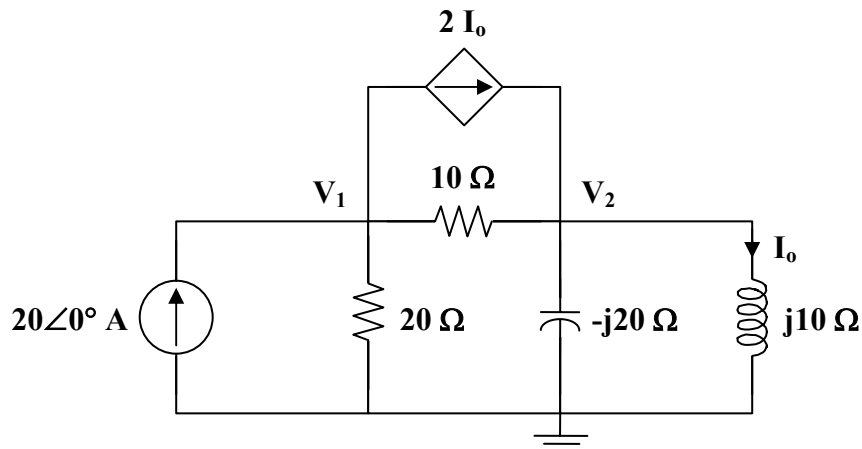
Chapter 10, Solution 12.

$$20 \sin(1000t) \longrightarrow 20\angle 0^\circ, \quad \omega = 1000$$

$$10 \text{ mH} \longrightarrow j\omega L = j10$$

$$50 \mu\text{F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(10^3)(50 \times 10^{-6})} = -j20$$

The frequency-domain equivalent circuit is shown below.



At node 1,

$$20 = 2\mathbf{I}_o + \frac{\mathbf{V}_1}{20} + \frac{\mathbf{V}_1 - \mathbf{V}_2}{10},$$

where

$$\mathbf{I}_o = \frac{\mathbf{V}_2}{j10}$$

$$20 = \frac{2\mathbf{V}_2}{j10} + \frac{\mathbf{V}_1}{20} + \frac{\mathbf{V}_1 - \mathbf{V}_2}{10}$$

$$400 = 3\mathbf{V}_1 - (2 + j4)\mathbf{V}_2 \quad (1)$$

At node 2,

$$\frac{2\mathbf{V}_2}{j10} + \frac{\mathbf{V}_1 - \mathbf{V}_2}{10} = \frac{\mathbf{V}_2}{-j20} + \frac{\mathbf{V}_2}{j10}$$

$$j2\mathbf{V}_1 = (-3 + j2)\mathbf{V}_2$$

or

$$\mathbf{V}_1 = (1 + j1.5)\mathbf{V}_2 \quad (2)$$

Substituting (2) into (1),

$$400 = (3 + j4.5)\mathbf{V}_2 - (2 + j4)\mathbf{V}_2 = (1 + j0.5)\mathbf{V}_2$$

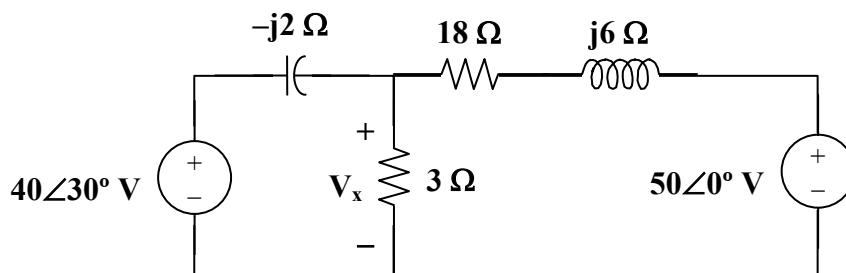
$$\mathbf{V}_2 = \frac{400}{1 + j0.5}$$

$$\mathbf{I}_o = \frac{\mathbf{V}_2}{j10} = \frac{40}{j(1 + j0.5)} = 35.74 \angle -116.6^\circ$$

Therefore, $i_o(t) = \underline{\underline{35.74 \sin(1000t - 116.6^\circ) \text{ A}}}$

Chapter 10, Solution 13.

Nodal analysis is the best approach to use on this problem. We can make our work easier by doing a source transformation on the right hand side of the circuit.



$$\frac{V_x - 40\angle 30^\circ}{-j2} + \frac{V_x}{3} + \frac{V_x - 50}{18 + j6} = 0$$

which leads to $V_x = \underline{29.36\angle 62.88^\circ \text{ A}}$.

Chapter 10, Solution 14.

At node 1,

$$\frac{0 - V_1}{-j2} + \frac{0 - V_1}{10} + \frac{V_2 - V_1}{j4} = 20\angle 30^\circ$$

$$-(1 + j2.5)V_1 - j2.5V_2 = 173.2 + j100 \quad (1)$$

At node 2,

$$\frac{V_2}{j2} + \frac{V_2}{-j5} + \frac{V_2 - V_1}{j4} = 20\angle 30^\circ$$

$$-j5.5V_2 + j2.5V_1 = 173.2 + j100 \quad (2)$$

Equations (1) and (2) can be cast into matrix form as

$$\begin{bmatrix} 1 + j2.5 & j2.5 \\ j2.5 & -j5.5 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} -200\angle 30^\circ \\ 200\angle 30^\circ \end{bmatrix}$$

$$\Delta = \begin{vmatrix} 1 + j2.5 & j2.5 \\ j2.5 & -j5.5 \end{vmatrix} = 20 - j5.5 = 20.74\angle -15.38^\circ$$

$$\Delta_1 = \begin{vmatrix} -200\angle 30^\circ & j2.5 \\ 200\angle 30^\circ & -j5.5 \end{vmatrix} = j3(200\angle 30^\circ) = 600\angle 120^\circ$$

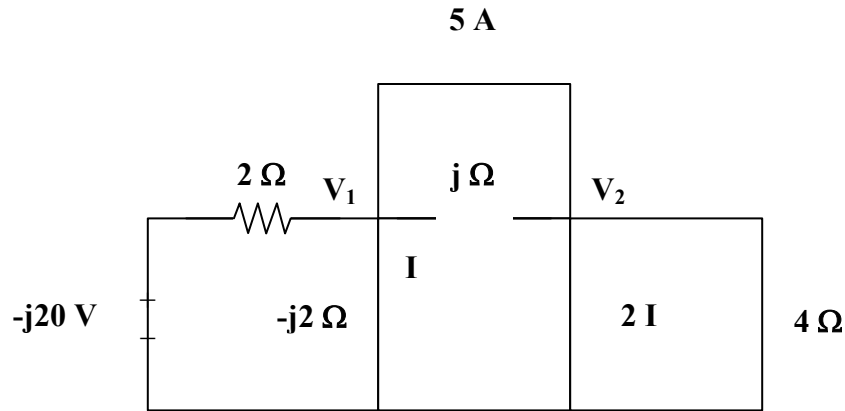
$$\Delta_2 = \begin{vmatrix} 1 + j2.5 & -200\angle 30^\circ \\ j2.5 & 200\angle 30^\circ \end{vmatrix} = (200\angle 30^\circ)(1 + j5) = 1020\angle 108.7^\circ$$

$$V_1 = \frac{\Delta_1}{\Delta} = 28.93\angle 135.38^\circ$$

$$V_2 = \frac{\Delta_2}{\Delta} = 49.18\angle 124.08^\circ$$

Chapter 10, Solution 15.

We apply nodal analysis to the circuit shown below.



At node 1,

$$\frac{-j20 - V_1}{2} = 5 + \frac{V_1}{-j2} + \frac{V_1 - V_2}{j}$$

$$-5 - j10 = (0.5 - j0.5)V_1 + jV_2 \quad (1)$$

At node 2,

$$5 + 2I + \frac{V_1 - V_2}{j} = \frac{V_2}{4},$$

$$\text{where } I = \frac{V_1}{-j2}$$

$$V_2 = \frac{5}{0.25 - j} V_1 \quad (2)$$

Substituting (2) into (1),

$$-5 - j10 - \frac{j5}{0.25 - j} = 0.5(1 - j)V_1$$

$$(1 - j)V_1 = -10 - j20 - \frac{j40}{1 - j4}$$

$$(\sqrt{2} \angle -45^\circ)V_1 = -10 - j20 + \frac{160}{17} - \frac{j40}{17}$$

$$V_1 = 15.81 \angle 313.5^\circ$$

$$\mathbf{I} = \frac{\mathbf{V}_1}{-j2} = (0.5\angle 90^\circ)(15.81\angle 313.5^\circ)$$

$$\mathbf{I} = \underline{\underline{7.906\angle 43.49^\circ \text{ A}}}$$

Chapter 10, Solution 16.

At node 1,

$$j2 = \frac{\mathbf{V}_1}{20} + \frac{\mathbf{V}_1 - \mathbf{V}_2}{10} + \frac{\mathbf{V}_1 - \mathbf{V}_2}{-j5}$$

$$j40 = (3 + j4)\mathbf{V}_1 - (2 + j4)\mathbf{V}_2$$

At node 2,

$$\frac{\mathbf{V}_1 - \mathbf{V}_2}{10} + \frac{\mathbf{V}_1 - \mathbf{V}_2}{-j5} + 1 + j = \frac{\mathbf{V}_2}{j10}$$

$$10(1 + j) = -(1 + j2)\mathbf{V}_1 + (1 + j)\mathbf{V}_2$$

Thus,

$$\begin{bmatrix} j40 \\ 10(1 + j) \end{bmatrix} = \begin{bmatrix} 3 + j4 & -2(1 + j2) \\ -(1 + j2) & 1 + j \end{bmatrix} \begin{bmatrix} \mathbf{V}_1 \\ \mathbf{V}_2 \end{bmatrix}$$

$$\Delta = \begin{vmatrix} 3 + j4 & -2(1 + j2) \\ -(1 + j2) & 1 + j \end{vmatrix} = 5 - j = 5.099\angle -11.31^\circ$$

$$\Delta_1 = \begin{vmatrix} j40 & -2(1 + j2) \\ 10(1 + j) & 1 + j \end{vmatrix} = -60 + j100 = 116.62\angle 120.96^\circ$$

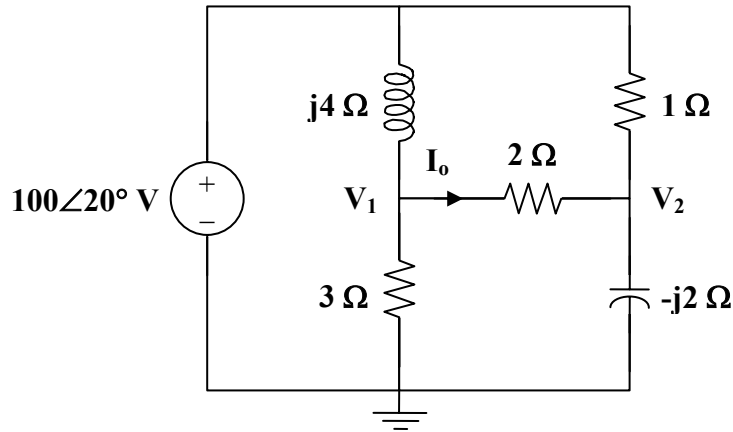
$$\Delta_2 = \begin{vmatrix} 3 + j4 & j40 \\ -(1 + j2) & 10(1 + j) \end{vmatrix} = -90 + j110 = 142.13\angle 129.29^\circ$$

$$\mathbf{V}_1 = \frac{\Delta_1}{\Delta} = \underline{\underline{22.87\angle 132.27^\circ \text{ V}}}$$

$$\mathbf{V}_2 = \frac{\Delta_2}{\Delta} = \underline{\underline{27.87\angle 140.6^\circ \text{ V}}}$$

Chapter 10, Solution 17.

Consider the circuit below.



At node 1,

$$\frac{100\angle 20^\circ - V_1}{j4} = \frac{V_1}{3} + \frac{V_1 - V_2}{2}$$

$$100\angle 20^\circ = \frac{V_1}{3}(3 + j10) - j2 V_2 \quad (1)$$

At node 2,

$$\frac{100\angle 20^\circ - V_2}{1} + \frac{V_1 - V_2}{2} = \frac{V_2}{-j2}$$

$$100\angle 20^\circ = -0.5 V_1 + (1.5 + j0.5) V_2 \quad (2)$$

From (1) and (2),

$$\begin{bmatrix} 100\angle 20^\circ \\ 100\angle 20^\circ \end{bmatrix} = \begin{bmatrix} -0.5 & 0.5(3 + j) \\ 1 + j10/3 & -j2 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

$$\Delta = \begin{vmatrix} -0.5 & 1.5 + j0.5 \\ 1 + j10/3 & -j2 \end{vmatrix} = 0.1667 - j4.5$$

$$\Delta_1 = \begin{vmatrix} 100\angle 20^\circ & 1.5 + j0.5 \\ 100\angle 20^\circ & -j2 \end{vmatrix} = -55.45 - j286.2$$

$$\Delta_2 = \begin{vmatrix} -0.5 & 100\angle 20^\circ \\ 1 + j10/3 & 100\angle 20^\circ \end{vmatrix} = -26.95 - j364.5$$

$$\mathbf{V}_1 = \frac{\Delta_1}{\Delta} = 64.74 \angle -13.08^\circ$$

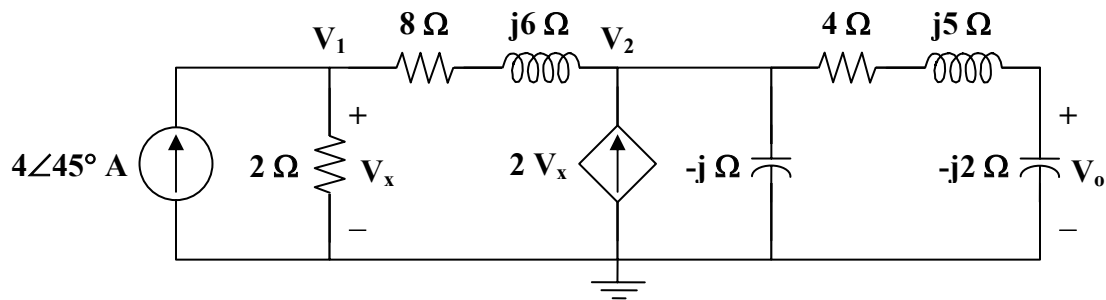
$$\mathbf{V}_2 = \frac{\Delta_2}{\Delta} = 81.17 \angle -6.35^\circ$$

$$\mathbf{I}_o = \frac{\mathbf{V}_1 - \mathbf{V}_2}{2} = \frac{\Delta_1 - \Delta_2}{2\Delta} = \frac{-28.5 + j78.31}{0.3333 - j9}$$

$$\mathbf{I}_o = 9.25 \angle -162.12^\circ$$

Chapter 10, Solution 18.

Consider the circuit shown below.



At node 1,

$$4\angle 45^\circ = \frac{\mathbf{V}_1}{2} + \frac{\mathbf{V}_1 - \mathbf{V}_2}{8 + j6}$$

$$200\angle 45^\circ = (29 - j3)\mathbf{V}_1 - (4 - j3)\mathbf{V}_2 \quad (1)$$

At node 2,

$$\frac{\mathbf{V}_1 - \mathbf{V}_2}{8 + j6} + 2\mathbf{V}_x = \frac{\mathbf{V}_2}{-j} + \frac{\mathbf{V}_2}{4 + j5 - j2}, \quad \text{where } \mathbf{V}_x = \mathbf{V}_1$$

$$(104 - j3)\mathbf{V}_1 = (12 + j41)\mathbf{V}_2$$

$$\mathbf{V}_1 = \frac{12 + j41}{104 - j3}\mathbf{V}_2 \quad (2)$$

Substituting (2) into (1),

$$200\angle 45^\circ = (29 - j3)\frac{(12 + j41)}{104 - j3}\mathbf{V}_2 - (4 - j3)\mathbf{V}_2$$

$$200\angle 45^\circ = (14.21\angle 89.17^\circ) \mathbf{V}_2$$

$$\mathbf{V}_2 = \frac{200\angle 45^\circ}{14.21\angle 89.17^\circ}$$

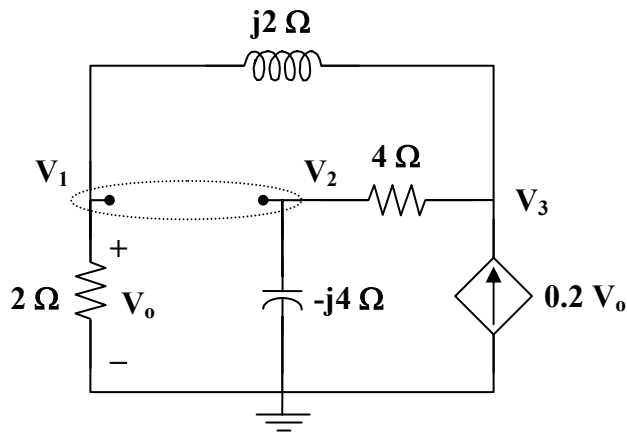
$$\mathbf{V}_o = \frac{-j2}{4+j5-j2} \mathbf{V}_2 = \frac{-j2}{4+j3} \mathbf{V}_2 = \frac{-6-j8}{25} \mathbf{V}_2$$

$$\mathbf{V}_o = \frac{10\angle 233.13^\circ}{25} \cdot \frac{200\angle 45^\circ}{14.21\angle 89.17^\circ}$$

$$\mathbf{V}_o = \underline{\underline{5.63\angle 189^\circ \text{ V}}}$$

Chapter 10, Solution 19.

We have a supernode as shown in the circuit below.



Notice that $\mathbf{V}_o = \mathbf{V}_1$.

At the supernode,

$$\frac{\mathbf{V}_3 - \mathbf{V}_2}{4} = \frac{\mathbf{V}_2}{-j4} + \frac{\mathbf{V}_1}{2} + \frac{\mathbf{V}_1 - \mathbf{V}_3}{j2}$$

$$0 = (2 - j2) \mathbf{V}_1 + (1 + j) \mathbf{V}_2 + (-1 + j2) \mathbf{V}_3 \quad (1)$$

At node 3,

$$0.2 \mathbf{V}_1 + \frac{\mathbf{V}_1 - \mathbf{V}_3}{j2} = \frac{\mathbf{V}_3 - \mathbf{V}_2}{4}$$

$$(0.8 - j2) \mathbf{V}_1 + \mathbf{V}_2 + (-1 + j2) \mathbf{V}_3 = 0 \quad (2)$$

Subtracting (2) from (1),

$$0 = 1.2\mathbf{V}_1 + j\mathbf{V}_2 \quad (3)$$

But at the supernode,

$$\mathbf{V}_1 = 12\angle 0^\circ + \mathbf{V}_2$$

or

$$\mathbf{V}_2 = \mathbf{V}_1 - 12 \quad (4)$$

Substituting (4) into (3),

$$0 = 1.2\mathbf{V}_1 + j(\mathbf{V}_1 - 12)$$

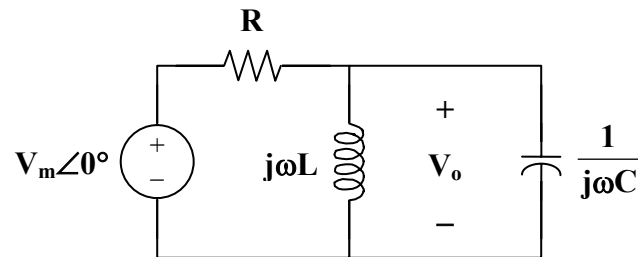
$$\mathbf{V}_1 = \frac{j12}{1.2 + j} = \mathbf{V}_o$$

$$\mathbf{V}_o = \frac{12\angle 90^\circ}{1.562\angle 39.81^\circ}$$

$$\mathbf{V}_o = \underline{\underline{7.682\angle 50.19^\circ \text{ V}}}$$

Chapter 10, Solution 20.

The circuit is converted to its frequency-domain equivalent circuit as shown below.



$$\text{Let } \mathbf{Z} = j\omega L \parallel \frac{1}{j\omega C} = \frac{\frac{L}{C}}{j\omega L + \frac{1}{j\omega C}} = \frac{j\omega L}{1 - \omega^2 LC}$$

$$\mathbf{V}_o = \frac{\mathbf{Z}}{R + \mathbf{Z}} \mathbf{V}_m = \frac{\frac{j\omega L}{1 - \omega^2 LC}}{R + \frac{j\omega L}{1 - \omega^2 LC}} \mathbf{V}_m = \frac{j\omega L}{R(1 - \omega^2 LC) + j\omega L} \mathbf{V}_m$$

$$\mathbf{V}_o = \frac{\omega L \mathbf{V}_m}{\sqrt{R^2 (1 - \omega^2 LC)^2 + \omega^2 L^2}} \angle \left(90^\circ - \tan^{-1} \frac{\omega L}{R(1 - \omega^2 LC)} \right)$$

If $V_o = A\angle\phi$, then

$$A = \frac{\omega L V_m}{\sqrt{R^2 (1 - \omega^2 LC)^2 + \omega^2 L^2}}$$

and $\phi = \underline{90^\circ - \tan^{-1} \frac{\omega L}{R(1 - \omega^2 LC)}}$

Chapter 10, Solution 21.

$$(a) \quad \frac{V_o}{V_i} = \frac{\frac{1}{j\omega C}}{R + j\omega L + \frac{1}{j\omega C}} = \frac{1}{1 - \omega^2 LC + j\omega RC}$$

At $\omega = 0$, $\frac{V_o}{V_i} = \frac{1}{1} = \underline{1}$

As $\omega \rightarrow \infty$, $\frac{V_o}{V_i} = \underline{0}$

At $\omega = \frac{1}{\sqrt{LC}}$, $\frac{V_o}{V_i} = \frac{1}{jRC \cdot \frac{1}{\sqrt{LC}}} = \underline{\frac{-j}{R} \sqrt{\frac{L}{C}}}$

$$(b) \quad \frac{V_o}{V_i} = \frac{j\omega L}{R + j\omega L + \frac{1}{j\omega C}} = \frac{-\omega^2 LC}{1 - \omega^2 LC + j\omega RC}$$

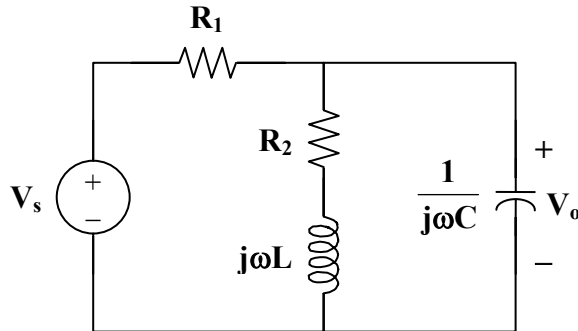
At $\omega = 0$, $\frac{V_o}{V_i} = \underline{0}$

As $\omega \rightarrow \infty$, $\frac{V_o}{V_i} = \frac{1}{1} = \underline{1}$

At $\omega = \frac{1}{\sqrt{LC}}$, $\frac{V_o}{V_i} = \frac{-1}{jRC \cdot \frac{1}{\sqrt{LC}}} = \underline{\frac{j}{R} \sqrt{\frac{L}{C}}}$

Chapter 10, Solution 22.

Consider the circuit in the frequency domain as shown below.



$$\text{Let } \mathbf{Z} = (R_2 + j\omega L) \parallel \frac{1}{j\omega C}$$

$$\mathbf{Z} = \frac{\frac{1}{j\omega C} (R_2 + j\omega L)}{R_2 + j\omega L + \frac{1}{j\omega C}} = \frac{R_2 + j\omega L}{1 + j\omega R_2 - \omega^2 LC}$$

$$\frac{\mathbf{V}_o}{\mathbf{V}_s} = \frac{\mathbf{Z}}{\mathbf{Z} + R_1} = \frac{\frac{R_2 + j\omega L}{1 - \omega^2 LC + j\omega R_2 C}}{R_1 + \frac{R_2 + j\omega L}{1 - \omega^2 LC + j\omega R_2 C}}$$

$$\frac{\mathbf{V}_o}{\mathbf{V}_s} = \frac{\mathbf{R}_2 + j\omega L}{\mathbf{R}_1 + \mathbf{R}_2 - \omega^2 LCR_1 + j\omega(L + R_1 R_2 C)}$$

Chapter 10, Solution 23.

$$\frac{V - V_s}{R} + \frac{V}{j\omega L + \frac{1}{j\omega C}} + j\omega CV = 0$$

$$V + \frac{j\omega RCV}{-\omega^2 LC + 1} + j\omega RCV = V_s$$

$$\left(\frac{1 - \omega^2 LC + j\omega RC + j\omega RC - j\omega^3 RLC^2}{1 - \omega^2 LC} \right) V = V_s$$

$$V = \frac{(1 - \omega^2 LC)V_s}{1 - \omega^2 LC + j\omega RC(2 - \omega^2 LC)}$$

Chapter 10, Solution 24.

For mesh 1,

$$V_s = \left(\frac{1}{j\omega C_1} + \frac{1}{j\omega C_2} \right) I_1 - \frac{1}{j\omega C_2} I_2 \quad (1)$$

For mesh 2,

$$0 = \frac{-1}{j\omega C_2} I_1 + \left(R + j\omega L + \frac{1}{j\omega C_2} \right) I_2 \quad (2)$$

Putting (1) and (2) into matrix form,

$$\begin{bmatrix} V_s \\ 0 \end{bmatrix} = \begin{bmatrix} \frac{1}{j\omega C_1} + \frac{1}{j\omega C_2} & \frac{-1}{j\omega C_2} \\ \frac{-1}{j\omega C_2} & R + j\omega L + \frac{1}{j\omega C_2} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$

$$\Delta = \left(\frac{1}{j\omega C_1} + \frac{1}{j\omega C_2} \right) \left(R + j\omega L + \frac{1}{j\omega C_2} \right) + \frac{1}{\omega^2 C_1 C_2}$$

$$\Delta_1 = V_s \left(R + j\omega L + \frac{1}{j\omega C_2} \right) \quad \text{and} \quad \Delta_2 = \frac{V_s}{j\omega C_2}$$

$$I_1 = \frac{\Delta_1}{\Delta} = \frac{V_s \left(R + j\omega L + \frac{1}{j\omega C_2} \right)}{\left(\frac{1}{j\omega C_1} + \frac{1}{j\omega C_2} \right) \left(R + j\omega L + \frac{1}{j\omega C_2} \right) + \frac{1}{\omega^2 C_1 C_2}}$$

$$I_2 = \frac{\Delta_2}{\Delta} = \frac{\frac{V_s}{j\omega C_2}}{\left(\frac{1}{j\omega C_1} + \frac{1}{j\omega C_2} \right) \left(R + j\omega L + \frac{1}{j\omega C_2} \right) + \frac{1}{\omega^2 C_1 C_2}}$$

Chapter 10, Solution 25.

$$\omega = 2$$

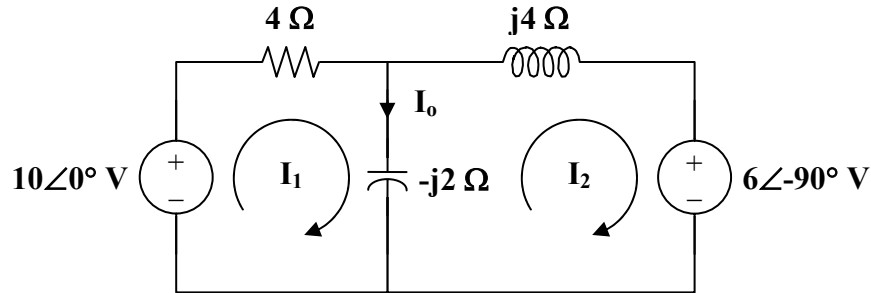
$$10 \cos(2t) \longrightarrow 10 \angle 0^\circ$$

$$6 \sin(2t) \longrightarrow 6 \angle -90^\circ = -j6$$

$$2 \text{ H} \longrightarrow j\omega L = j4$$

$$0.25 \text{ F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(2)(1/4)} = -j2$$

The circuit is shown below.



For loop 1,

$$-10 + (4 - j2)\mathbf{I}_1 + j2\mathbf{I}_2 = 0$$

$$5 = (2 - j)\mathbf{I}_1 + j\mathbf{I}_2 \quad (1)$$

For loop 2,

$$j2\mathbf{I}_1 + (j4 - j2)\mathbf{I}_2 + (-j6) = 0$$

$$\mathbf{I}_1 + \mathbf{I}_2 = 3 \quad (2)$$

In matrix form (1) and (2) become

$$\begin{bmatrix} 2-j & j \\ 1 & 1 \end{bmatrix} \begin{bmatrix} \mathbf{I}_1 \\ \mathbf{I}_2 \end{bmatrix} = \begin{bmatrix} 5 \\ 3 \end{bmatrix}$$

$$\Delta = 2(1 - j), \quad \Delta_1 = 5 - j3, \quad \Delta_2 = 1 - j3$$

$$\mathbf{I}_o = \mathbf{I}_1 - \mathbf{I}_2 = \frac{\Delta_1 - \Delta_2}{\Delta} = \frac{4}{2(1 - j)} = 1 + j = 1.414 \angle 45^\circ$$

Therefore, $i_o(t) = \underline{\underline{1.414 \cos(2t + 45^\circ) \text{ A}}}$

Chapter 10, Solution 26.

We apply mesh analysis to the circuit shown below.

For mesh 1,

$$-10 + 40\mathbf{I}_1 - 20\mathbf{I}_2 = 0$$

$$1 = 4\mathbf{I}_1 - 2\mathbf{I}_2 \quad (1)$$

For the supermesh,

$$(20 - j20)\mathbf{I}_2 - 20\mathbf{I}_1 + (30 + j10)\mathbf{I}_3 = 0$$

$$-2\mathbf{I}_1 + (2 - j2)\mathbf{I}_2 + (3 + j)\mathbf{I}_3 = 0 \quad (2)$$

At node A,

$$\mathbf{I}_o = \mathbf{I}_1 - \mathbf{I}_2 \quad (3)$$

At node B,

$$\mathbf{I}_2 = \mathbf{I}_3 + 4\mathbf{I}_o \quad (4)$$

Substituting (3) into (4)

$$\begin{aligned} \mathbf{I}_2 &= \mathbf{I}_3 + 4\mathbf{I}_1 - 4\mathbf{I}_2 \\ \mathbf{I}_3 &= 5\mathbf{I}_2 - 4\mathbf{I}_1 \end{aligned} \quad (5)$$

Substituting (5) into (2) gives

$$0 = -(14 + j4)\mathbf{I}_1 + (17 + j3)\mathbf{I}_2 \quad (6)$$

From (1) and (6),

$$\begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 4 & -2 \\ -(14 + j4) & 17 + j3 \end{bmatrix} \begin{bmatrix} \mathbf{I}_1 \\ \mathbf{I}_2 \end{bmatrix}$$

$$\Delta = 40 + j4$$

$$\Delta_1 = \begin{vmatrix} 1 & -2 \\ 0 & 17 + j3 \end{vmatrix} = 17 + j3, \quad \Delta_2 = \begin{vmatrix} 4 & 1 \\ -(14 + j4) & 0 \end{vmatrix} = 14 + j4$$

$$\mathbf{I}_3 = 5\mathbf{I}_2 - 4\mathbf{I}_1 = \frac{5\Delta_2 - 4\Delta_1}{\Delta} = \frac{2 + j8}{40 + j4}$$

$$\mathbf{V}_o = 30\mathbf{I}_3 = \frac{15(1 + j4)}{10 + j} = 6.154 \angle 70.25^\circ$$

Therefore, $v_o(t) = \underline{\underline{6.154 \cos(10^3 t + 70.25^\circ) \text{ V}}}$

Chapter 10, Solution 27.

For mesh 1,

$$\begin{aligned} -40 \angle 30^\circ + (j10 - j20)\mathbf{I}_1 + j20\mathbf{I}_2 &= 0 \\ 4 \angle 30^\circ &= -j\mathbf{I}_1 + j2\mathbf{I}_2 \end{aligned} \quad (1)$$

For mesh 2,

$$\begin{aligned} 50 \angle 0^\circ + (40 - j20)\mathbf{I}_2 + j20\mathbf{I}_1 &= 0 \\ 5 &= -j2\mathbf{I}_1 - (4 - j2)\mathbf{I}_2 \end{aligned} \quad (2)$$

From (1) and (2),

$$\begin{bmatrix} 4 \angle 30^\circ \\ 5 \end{bmatrix} = \begin{bmatrix} -j & j2 \\ -j2 & -(4 - j2) \end{bmatrix} \begin{bmatrix} \mathbf{I}_1 \\ \mathbf{I}_2 \end{bmatrix}$$

$$\Delta = -2 + 4j = 4.472 \angle 116.56^\circ$$

$$\Delta_1 = -(4\angle 30^\circ)(4 - j2) - j10 = 21.01\angle 211.8^\circ$$

$$\Delta_2 = -j5 + 8\angle 120^\circ = 4.44\angle 154.27^\circ$$

$$\mathbf{I}_1 = \frac{\Delta_1}{\Delta} = \underline{\underline{4.698\angle 95.24^\circ \text{ A}}}$$

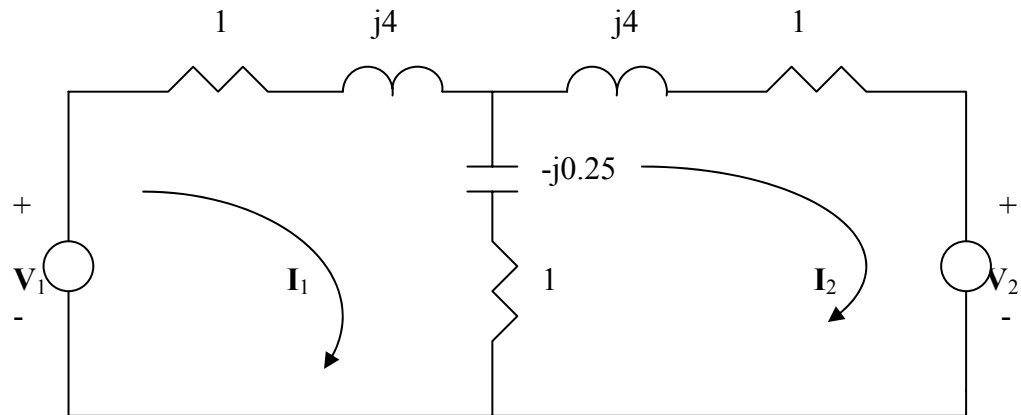
$$\mathbf{I}_2 = \frac{\Delta_2}{\Delta} = \underline{\underline{0.9928\angle 37.71^\circ \text{ A}}}$$

Chapter 10, Solution 28.

$$1\text{H} \longrightarrow j\omega L = j4, \quad 1\text{F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j1 \times 4} = -j0.25$$

The frequency-domain version of the circuit is shown below, where

$$\mathbf{V}_1 = 10\angle 0^\circ, \quad \mathbf{V}_2 = 20\angle -30^\circ.$$



$$\mathbf{V}_1 = 10\angle 0^\circ, \quad \mathbf{V}_2 = 20\angle -30^\circ$$

Applying mesh analysis,

$$10 = (2 + j3.75)\mathbf{I}_1 - (1 - j0.25)\mathbf{I}_2 \quad (1)$$

$$-20\angle -30^\circ = -(1 - j0.025)\mathbf{I}_1 + (2 + j3.75)\mathbf{I}_2 \quad (2)$$

From (1) and (2), we obtain

$$\begin{pmatrix} 10 \\ -17.32 + j10 \end{pmatrix} = \begin{pmatrix} 2 + j3.75 & -1 + j0.25 \\ -1 + j0.25 & 2 + j3.75 \end{pmatrix} \begin{pmatrix} I_1 \\ I_2 \end{pmatrix}$$

Solving this leads to

$$I_1 = 1.3602 - j0.9769 = 1.6747 \angle -35.69^\circ, \quad I_2 = -4.1438 + j2.111 = 4.6505 \angle 153^\circ$$

Hence,

$$\underline{i_1 = 1.675 \cos(4t - 35.69^\circ) \text{ A}, \quad i_2 = 4.651 \cos(4t + 153^\circ) \text{ A}}$$

Chapter 10, Solution 29.

For mesh 1,

$$\begin{aligned} (5 + j5)I_1 - (2 + j)I_2 - 30 \angle 20^\circ &= 0 \\ 30 \angle 20^\circ &= (5 + j5)I_1 - (2 + j)I_2 \end{aligned} \quad (1)$$

For mesh 2,

$$\begin{aligned} (5 + j3 - j6)I_2 - (2 + j)I_1 &= 0 \\ 0 &= -(2 + j)I_1 + (5 - j3)I_2 \end{aligned} \quad (2)$$

From (1) and (2),

$$\begin{bmatrix} 30 \angle 20^\circ \\ 0 \end{bmatrix} = \begin{bmatrix} 5 + j5 & -(2 + j) \\ -(2 + j) & 5 - j3 \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$

$$\Delta = 37 + j6 = 37.48 \angle 9.21^\circ$$

$$\Delta_1 = (30 \angle 20^\circ)(5.831 \angle -30.96^\circ) = 175 \angle -10.96^\circ$$

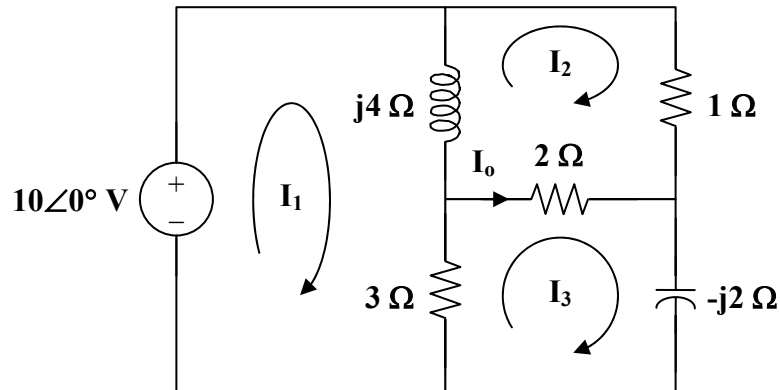
$$\Delta_2 = (30 \angle 20^\circ)(2.356 \angle 26.56^\circ) = 67.08 \angle 46.56^\circ$$

$$I_1 = \frac{\Delta_1}{\Delta} = \underline{\underline{4.67 \angle -20.17^\circ \text{ A}}}$$

$$I_2 = \frac{\Delta_2}{\Delta} = \underline{\underline{1.79 \angle 37.35^\circ \text{ A}}}$$

Chapter 10, Solution 30.

Consider the circuit shown below.



For mesh 1,

$$100\angle 20^\circ = (3 + j4)\mathbf{I}_1 - j4\mathbf{I}_2 - 3\mathbf{I}_3 \quad (1)$$

For mesh 2,

$$0 = -j4\mathbf{I}_1 + (3 + j4)\mathbf{I}_2 - j2\mathbf{I}_3 \quad (2)$$

For mesh 3,

$$0 = -3\mathbf{I}_1 - 2\mathbf{I}_2 + (5 - j2)\mathbf{I}_3 \quad (3)$$

Put (1), (2), and (3) into matrix form.

$$\begin{bmatrix} 3 + j4 & -j4 & -3 \\ -j4 & 3 + j4 & -j2 \\ -3 & -2 & 5 - j2 \end{bmatrix} \begin{bmatrix} \mathbf{I}_1 \\ \mathbf{I}_2 \\ \mathbf{I}_3 \end{bmatrix} = \begin{bmatrix} 100\angle 20^\circ \\ 0 \\ 0 \end{bmatrix}$$

$$\Delta = \begin{vmatrix} 3 + j4 & -j4 & -3 \\ -j4 & 3 + j4 & -j2 \\ -3 & -2 & 5 - j2 \end{vmatrix} = 106 + j30$$

$$\Delta_2 = \begin{vmatrix} 3 + j4 & 100\angle 20^\circ & -3 \\ -j4 & 0 & -j2 \\ -3 & 0 & 5 - j2 \end{vmatrix} = (100\angle 20^\circ)(8 + j26)$$

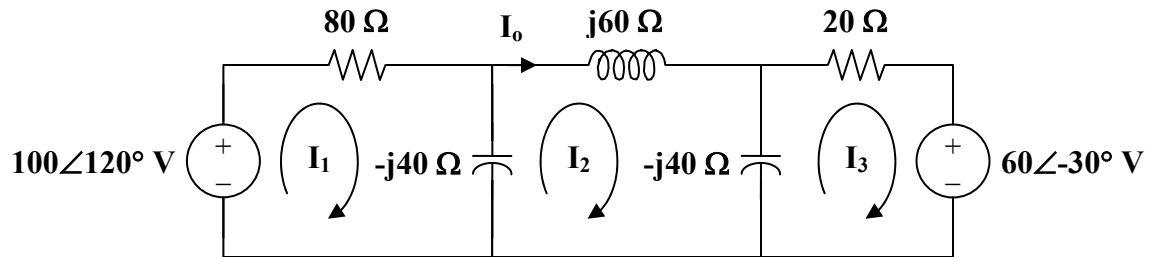
$$\Delta_3 = \begin{vmatrix} 3 + j4 & -j4 & 100\angle 20^\circ \\ -j4 & 3 + j4 & 0 \\ -3 & -2 & 0 \end{vmatrix} = (100\angle 20^\circ)(9 + j20)$$

$$\mathbf{I}_o = \mathbf{I}_3 - \mathbf{I}_2 = \frac{\Delta_3 - \Delta_2}{\Delta} = \frac{(100\angle 20^\circ)(1 - j6)}{106 + j30}$$

$$\mathbf{I}_o = \underline{\underline{5.521\angle -76.34^\circ \text{ A}}}$$

Chapter 10, Solution 31.

Consider the network shown below.



For loop 1,

$$\begin{aligned} -100\angle 120^\circ + (80 - j40)\mathbf{I}_1 + j40\mathbf{I}_2 &= 0 \\ 10\angle 20^\circ &= 4(2 - j)\mathbf{I}_1 + j4\mathbf{I}_2 \end{aligned} \quad (1)$$

For loop 2,

$$\begin{aligned} j40\mathbf{I}_1 + (j60 - j80)\mathbf{I}_2 + j40\mathbf{I}_3 &= 0 \\ 0 &= 2\mathbf{I}_1 - \mathbf{I}_2 + 2\mathbf{I}_3 \end{aligned} \quad (2)$$

For loop 3,

$$\begin{aligned} 60\angle -30^\circ + (20 - j40)\mathbf{I}_3 + j40\mathbf{I}_2 &= 0 \\ -6\angle -30^\circ &= j4\mathbf{I}_2 + 2(1 - j2)\mathbf{I}_3 \end{aligned} \quad (3)$$

From (2),

$$2\mathbf{I}_3 = \mathbf{I}_2 - 2\mathbf{I}_1$$

Substituting this equation into (3),

$$-6\angle -30^\circ = -2(1 - j2)\mathbf{I}_1 + (1 + j2)\mathbf{I}_2 \quad (4)$$

From (1) and (4),

$$\begin{bmatrix} 10\angle 120^\circ \\ -6\angle -30^\circ \end{bmatrix} = \begin{bmatrix} 4(2 - j) & j4 \\ -2(1 - j2) & 1 + j2 \end{bmatrix} \begin{bmatrix} \mathbf{I}_1 \\ \mathbf{I}_2 \end{bmatrix}$$

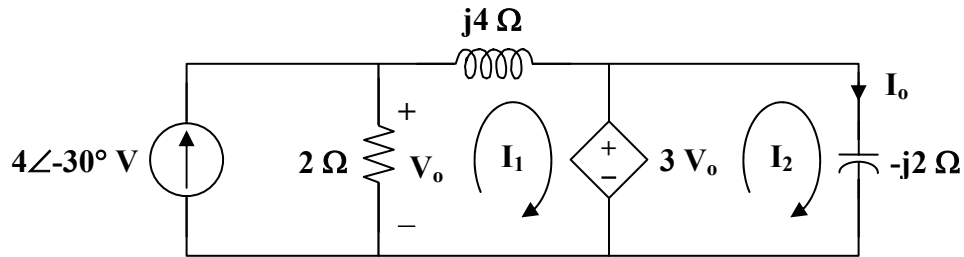
$$\Delta = \begin{vmatrix} 8 - j4 & -j4 \\ -2 + j4 & 1 + j2 \end{vmatrix} = 32 + j20 = 37.74\angle 32^\circ$$

$$\Delta_2 = \begin{vmatrix} 8 - j4 & 10\angle 120^\circ \\ -2 + j4 & -6\angle -30^\circ \end{vmatrix} = -4.928 + j82.11 = 82.25\angle 93.44^\circ$$

$$\mathbf{I}_o = \mathbf{I}_2 = \frac{\Delta_2}{\Delta} = \underline{\underline{2.179\angle 61.44^\circ \text{ A}}}$$

Chapter 10, Solution 32.

Consider the circuit below.



For mesh 1,

$$(2 + j4)I_1 - 2(4\angle -30^\circ) + 3V_o = 0$$

where

$$V_o = 2(4\angle -30^\circ - I_1)$$

Hence,

$$(2 + j4)I_1 - 8\angle -30^\circ + 6(4\angle -30^\circ - I_1) = 0$$

$$4\angle -30^\circ = (1 - j)I_1$$

or

$$I_1 = 2\sqrt{2}\angle 15^\circ$$

$$I_o = \frac{3V_o}{-j2} = \frac{3}{-j2}(2)(4\angle -30^\circ - I_1)$$

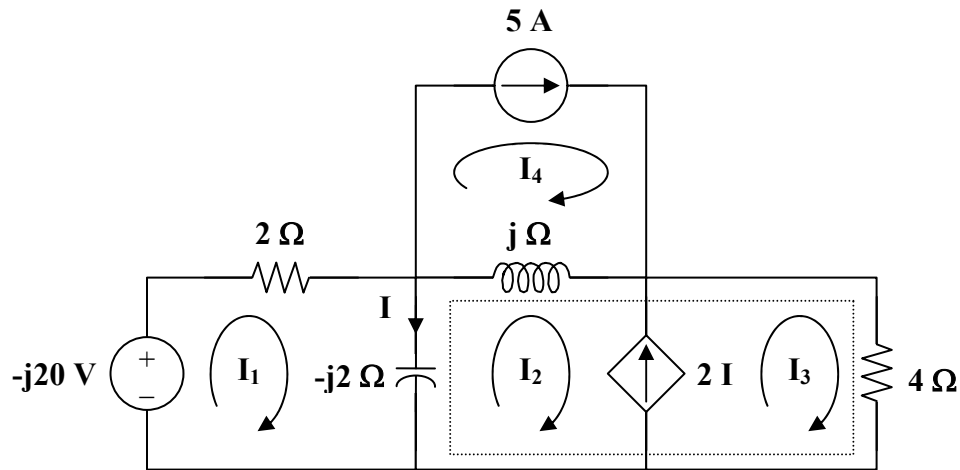
$$I_o = j3(4\angle -30^\circ - 2\sqrt{2}\angle 15^\circ)$$

$$I_o = \underline{\underline{8.485\angle 15^\circ \text{ A}}}$$

$$V_o = \frac{-j2I_o}{3} = \underline{\underline{5.657\angle -75^\circ \text{ V}}}$$

Chapter 10, Solution 33.

Consider the circuit shown below.



For mesh 1,

$$\begin{aligned} j20 + (2 - j2)\mathbf{I}_1 + j2\mathbf{I}_2 &= 0 \\ (1 - j)\mathbf{I}_1 + j\mathbf{I}_2 &= -j10 \end{aligned} \quad (1)$$

For the supermesh,

$$(j - j2)\mathbf{I}_2 + j2\mathbf{I}_1 + 4\mathbf{I}_3 - j\mathbf{I}_4 = 0 \quad (2)$$

Also,

$$\begin{aligned} \mathbf{I}_3 - \mathbf{I}_2 &= 2\mathbf{I} = 2(\mathbf{I}_1 - \mathbf{I}_2) \\ \mathbf{I}_3 &= 2\mathbf{I}_1 - \mathbf{I}_2 \end{aligned} \quad (3)$$

For mesh 4,

$$\mathbf{I}_4 = 5 \quad (4)$$

Substituting (3) and (4) into (2),

$$(8 + j2)\mathbf{I}_1 - (-4 + j)\mathbf{I}_2 = j5 \quad (5)$$

Putting (1) and (5) in matrix form,

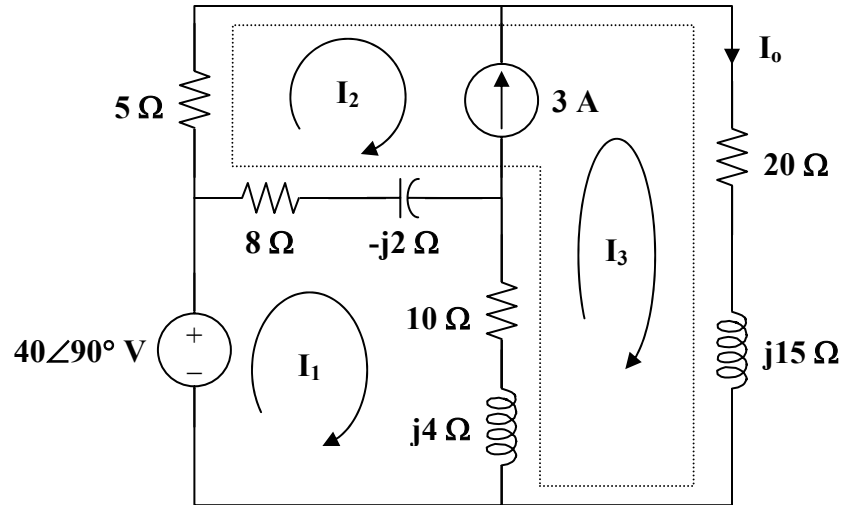
$$\begin{bmatrix} 1 - j & j \\ 8 + j2 & 4 - j \end{bmatrix} \begin{bmatrix} \mathbf{I}_1 \\ \mathbf{I}_2 \end{bmatrix} = \begin{bmatrix} -j10 \\ j5 \end{bmatrix}$$

$$\Delta = -3 - j5, \quad \Delta_1 = -5 + j40, \quad \Delta_2 = -15 + j85$$

$$\mathbf{I} = \mathbf{I}_1 - \mathbf{I}_2 = \frac{\Delta_1 - \Delta_2}{\Delta} = \frac{10 - j45}{-3 - j5} = \underline{\underline{7.906 \angle 43.49^\circ \text{ A}}}$$

Chapter 10, Solution 34.

The circuit is shown below.



For mesh 1,

$$-j40 + (18 + j2)\mathbf{I}_1 - (8 - j2)\mathbf{I}_2 - (10 + j4)\mathbf{I}_3 = 0 \quad (1)$$

For the supermesh,

$$(13 - j2)\mathbf{I}_2 + (30 + j19)\mathbf{I}_3 - (18 + j2)\mathbf{I}_1 = 0 \quad (2)$$

Also,

$$\mathbf{I}_2 = \mathbf{I}_3 - 3 \quad (3)$$

Adding (1) and (2) and incorporating (3),

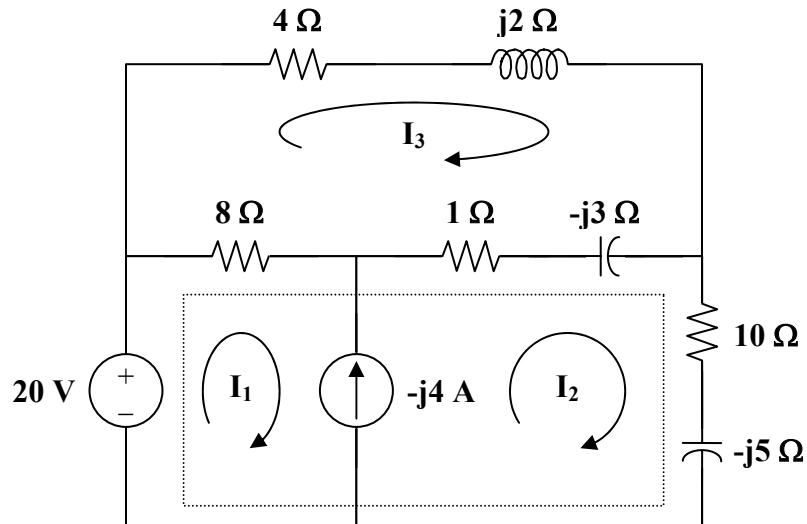
$$-j40 + 5(\mathbf{I}_3 - 3) + (20 + j15)\mathbf{I}_3 = 0$$

$$\mathbf{I}_3 = \frac{3 + j8}{5 + j3} = 1.465 \angle 38.48^\circ$$

$$\mathbf{I}_0 = \mathbf{I}_3 = \underline{\underline{1.465 \angle 38.48^\circ \text{ A}}}$$

Chapter 10, Solution 35.

Consider the circuit shown below.



For the supermesh,

$$-20 + 8\mathbf{I}_1 + (11 - j8)\mathbf{I}_2 - (9 - j3)\mathbf{I}_3 = 0 \quad (1)$$

Also,

$$\mathbf{I}_1 = \mathbf{I}_2 + j4 \quad (2)$$

For mesh 3,

$$(13 - j)\mathbf{I}_3 - 8\mathbf{I}_1 - (1 - j3)\mathbf{I}_2 = 0 \quad (3)$$

Substituting (2) into (1),

$$(19 - j8)\mathbf{I}_2 - (9 - j3)\mathbf{I}_3 = 20 - j32 \quad (4)$$

Substituting (2) into (3),

$$-(9 - j3)\mathbf{I}_2 + (13 - j)\mathbf{I}_3 = j32 \quad (5)$$

From (4) and (5),

$$\begin{bmatrix} 19 - j8 & -(9 - j3) \\ -(9 - j3) & 13 - j \end{bmatrix} \begin{bmatrix} \mathbf{I}_2 \\ \mathbf{I}_3 \end{bmatrix} = \begin{bmatrix} 20 - j32 \\ j32 \end{bmatrix}$$

$$\Delta = 167 - j69,$$

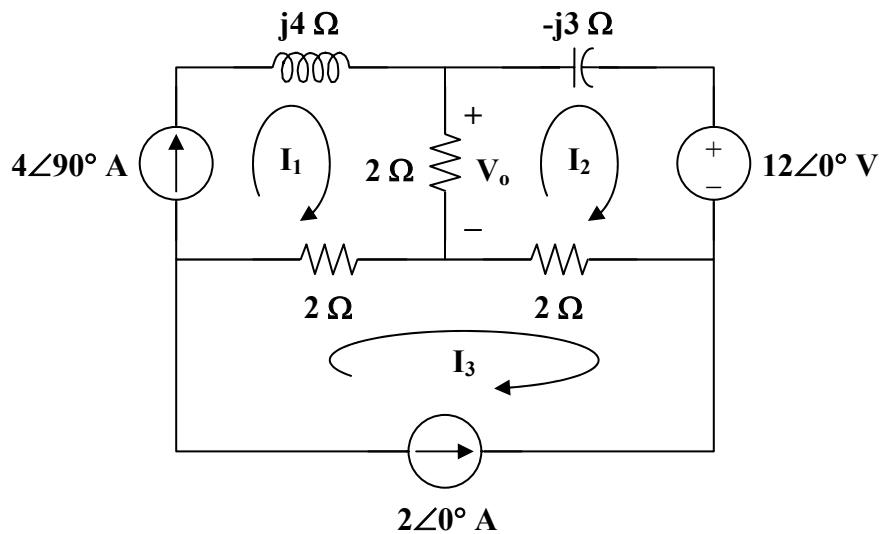
$$\Delta_2 = 324 - j148$$

$$\mathbf{I}_2 = \frac{\Delta_2}{\Delta} = \frac{324 - j148}{167 - j69} = \frac{356.2 \angle -24.55^\circ}{180.69 \angle -22.45^\circ}$$

$$\mathbf{I}_2 = \underline{\underline{1.971 \angle -2.1^\circ \text{ A}}}$$

Chapter 10, Solution 36.

Consider the circuit below.



Clearly,

$$\mathbf{I_1 = 4\angle 90^\circ = j4} \quad \text{and} \quad \mathbf{I_3 = -2}$$

For mesh 2,

$$(4 - j3)\mathbf{I_2} - 2\mathbf{I_1} - 2\mathbf{I_3} + 12 = 0$$

$$(4 - j3)\mathbf{I_2} - j8 + 4 + 12 = 0$$

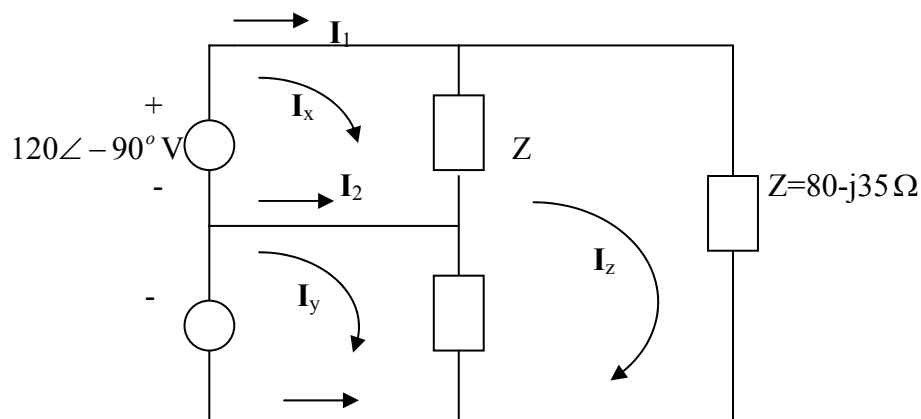
$$\mathbf{I_2 = \frac{-16 + j8}{4 - j3} = -3.52 - j0.64}$$

Thus,

$$\mathbf{V_o = 2(I_1 - I_2) = (2)(3.52 + j4.64) = 7.04 + j9.28}$$

$$\mathbf{V_o = \underline{11.648\angle 52.82^\circ} \text{ V}}$$

Chapter 10, Solution 37.



$$120\angle -30^\circ \text{ V} \quad \quad \quad \text{Z}$$

+ $\quad \quad \quad \mathbf{I}_3$

For mesh x,

$$ZI_x - ZI_z = -j120 \quad (1)$$

For mesh y,

$$ZI_y - ZI_z = -120\angle 30^\circ = -103.92 + j60 \quad (2)$$

For mesh z,

$$-ZI_x - ZI_y + 3ZI_z = 0 \quad (3)$$

Putting (1) to (3) together leads to the following matrix equation:

$$\begin{pmatrix} (80 - j35) & 0 & (-80 + j35) \\ 0 & (80 - j35) & (-80 + j35) \\ (-80 + j35) & (-80 + j35) & (240 - j105) \end{pmatrix} \begin{pmatrix} I_x \\ I_y \\ I_z \end{pmatrix} = \begin{pmatrix} -j120 \\ -103.92 + j60 \\ 0 \end{pmatrix} \longrightarrow \mathbf{AI} = \mathbf{B}$$

Using MATLAB, we obtain

$$\mathbf{I} = \text{inv}(\mathbf{A}) * \mathbf{B} = \begin{pmatrix} -1.9165 + j1.4115 \\ -2.1806 - j0.954 \\ -1.3657 + j0.1525 \end{pmatrix}$$

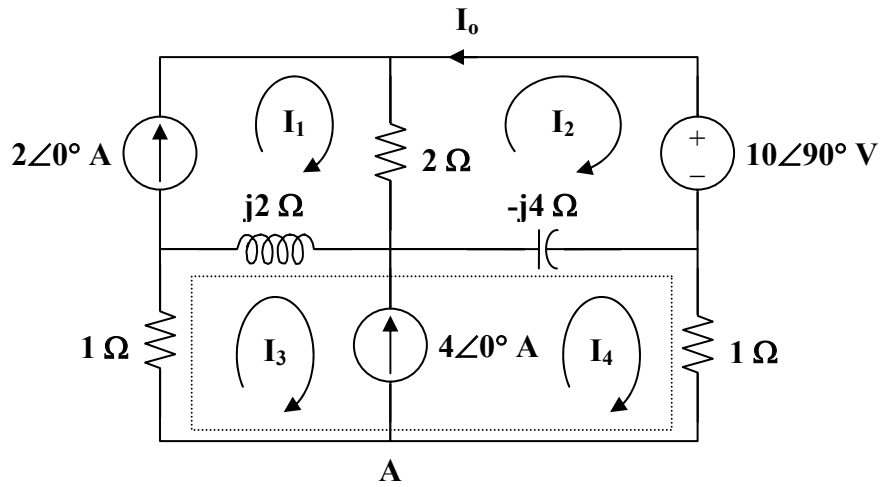
$$I_1 = I_x = -1.9165 + j1.4115 = \underline{2.3802\angle 143.6^\circ} \text{ A}$$

$$I_2 = I_y - I_x = -0.2641 - j2.3655 = \underline{2.3802\angle -96.37^\circ} \text{ A}$$

$$I_3 = -I_y = 2.1806 + j0.954 = \underline{2.3802\angle 23.63^\circ} \text{ A}$$

Chapter 10, Solution 38.

Consider the circuit below.



Clearly,

$$\mathbf{I}_1 = 2 \quad (1)$$

For mesh 2,

$$(2 - j4)\mathbf{I}_2 - 2\mathbf{I}_1 + j4\mathbf{I}_4 + 10\angle 90^\circ = 0 \quad (2)$$

Substitute (1) into (2) to get

$$(1 - j2)\mathbf{I}_2 + j2\mathbf{I}_4 = 2 - j5$$

For the supermesh,

$$(1 + j2)\mathbf{I}_3 - j2\mathbf{I}_1 + (1 - j4)\mathbf{I}_4 + j4\mathbf{I}_2 = 0$$

$$j4\mathbf{I}_2 + (1 + j2)\mathbf{I}_3 + (1 - j4)\mathbf{I}_4 = j4 \quad (3)$$

At node A,

$$\mathbf{I}_3 = \mathbf{I}_4 - 4 \quad (4)$$

Substituting (4) into (3) gives

$$j2\mathbf{I}_2 + (1 - j)\mathbf{I}_4 = 2(1 + j3) \quad (5)$$

From (2) and (5),

$$\begin{bmatrix} 1 - j2 & j2 \\ j2 & 1 - j \end{bmatrix} \begin{bmatrix} \mathbf{I}_2 \\ \mathbf{I}_4 \end{bmatrix} = \begin{bmatrix} 2 - j5 \\ 2 + j6 \end{bmatrix}$$

$$\Delta = 3 - j3, \quad \Delta_1 = 9 - j11$$

$$\mathbf{I}_o = -\mathbf{I}_2 = \frac{-\Delta_1}{\Delta} = \frac{-(9 - j11)}{3 - j3} = \frac{1}{3}(-10 + j)$$

$$\mathbf{I}_o = \underline{\underline{3.35\angle 174.3^\circ \text{ A}}}$$

Chapter 10, Solution 39.

For mesh 1,

$$(28 - j15)I_1 - 8I_2 + j15I_3 = 12\angle 64^\circ \quad (1)$$

For mesh 2,

$$-8I_1 + (8 - j9)I_2 - j16I_3 = 0 \quad (2)$$

For mesh 3,

$$j15I_1 - j16I_2 + (10 + j)I_3 = 0 \quad (3)$$

In matrix form, (1) to (3) can be cast as

$$\begin{pmatrix} (28 - j15) & -8 & j15 \\ -8 & (8 - j9) & -j16 \\ j15 & -j16 & (10 + j) \end{pmatrix} \begin{pmatrix} I_1 \\ I_2 \\ I_3 \end{pmatrix} = \begin{pmatrix} 12\angle 64^\circ \\ 0 \\ 0 \end{pmatrix} \quad \text{or} \quad \mathbf{AI} = \mathbf{B}$$

Using MATLAB,

$$\mathbf{I} = \text{inv}(\mathbf{A}) * \mathbf{B}$$

$$I_1 = -0.128 + j0.3593 = \underline{0.3814\angle 109.6^\circ \text{ A}}$$

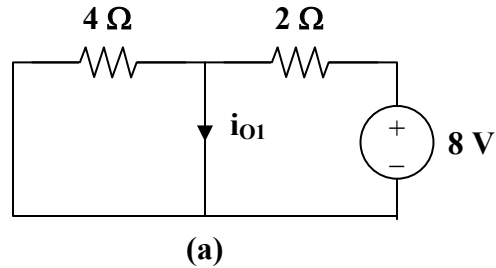
$$I_2 = -0.1946 + j0.2841 = \underline{0.3443\angle 124.4^\circ \text{ A}}$$

$$I_3 = 0.0718 - j0.1265 = \underline{0.1455\angle -60.42^\circ \text{ A}}$$

$$I_x = I_1 - I_2 = 0.0666 + j0.0752 = \underline{0.1005 \angle 48.5^\circ \text{ A}}$$

Chapter 10, Solution 40.

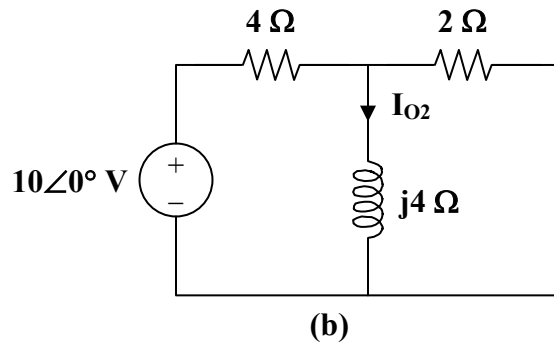
Let $i_o = i_{o1} + i_{o2}$, where i_{o1} is due to the dc source and i_{o2} is due to the ac source. For i_{o1} , consider the circuit in Fig. (a).



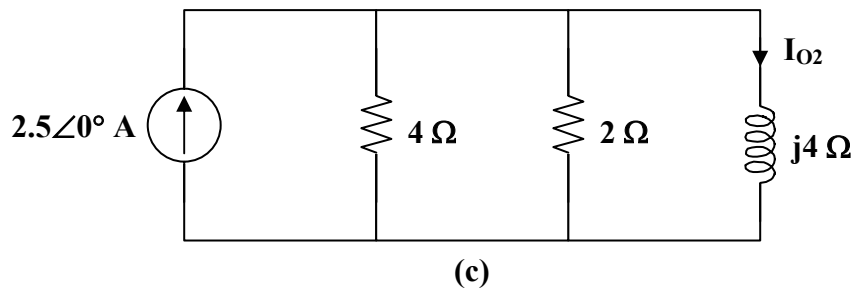
Clearly,

$$i_{o1} = 8/2 = 4 \text{ A}$$

For i_{o2} , consider the circuit in Fig. (b).



If we transform the voltage source, we have the circuit in Fig. (c), where $4 \parallel 2 = 4/3 \Omega$.



By the current division principle,

$$I_{o2} = \frac{4/3}{4/3 + j4} (2.5 \angle 0^\circ)$$

$$I_{o2} = 0.25 - j0.75 = 0.79 \angle -71.56^\circ$$

Thus, $i_{O2} = 0.79 \cos(4t - 71.56^\circ) \text{ A}$

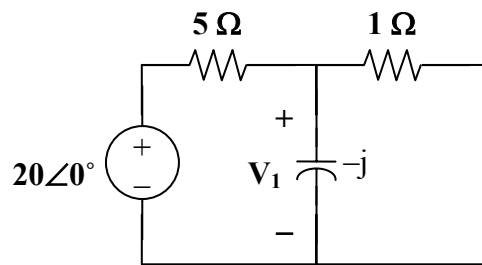
Therefore,

$$i_O = i_{O1} + i_{O2} = 4 + 0.79 \cos(4t - 71.56^\circ) \text{ A}$$

Chapter 10, Solution 41.

Let $v_x = v_1 + v_2$.

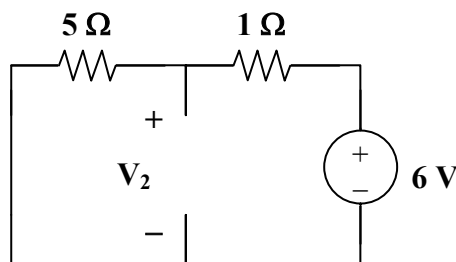
For v_1 we let the DC source equal zero.



$$\frac{V_1 - 20}{5} + \frac{V_1}{-j} + \frac{V_1}{1} = 0 \text{ which simplifies to } (1j - 5 + 5j)V_1 = 100j$$

$$V_1 = 2.56 \angle -39.8^\circ \text{ or } v_1 = 2.56 \sin(500t - 39.8^\circ) \text{ V}$$

Setting the AC signal to zero produces:



The 1-ohm resistor in series with the 5-ohm resistor creating a simple voltage divider yielding:

$$v_2 = (5/6)6 = 5 \text{ V.}$$

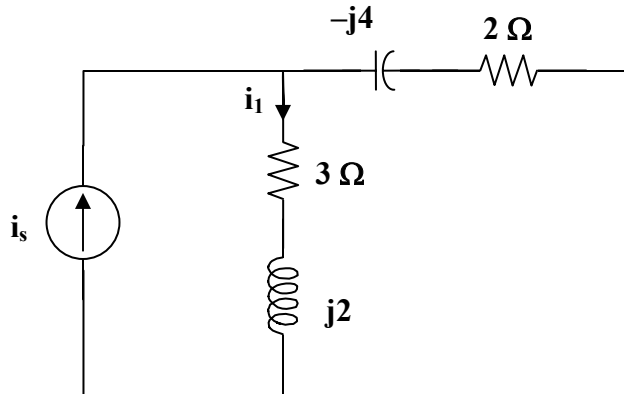
$$v_x = \underline{\underline{2.56 \sin(500t - 39.8^\circ) + 5 \text{ V.}}}$$

Chapter 10, Solution 42.

Let $i_x = i_1 + i_2$, where i_1 and i_2 which are generated by i_s and v_s respectively. For i_1 we let $i_s = 6\sin 2t$ A becomes $I_s = 6\angle 0^\circ$, where $\omega = 2$.

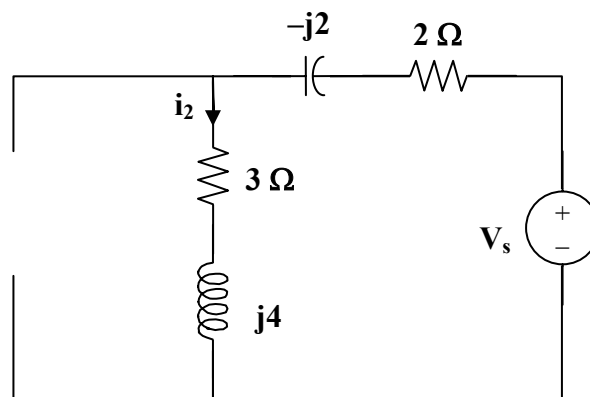
$$I_1 = \frac{2 - j4}{3 + j2 + 2 - j4} 6 = 12 \frac{1 - j2}{5 - j2} = 3.724 - j3.31 = 4.983\angle -41.63^\circ$$

$$i_1 = 4.983\sin(2t - 41.63^\circ) \text{ A}$$



For i_2 , we transform $v_s = 12\cos(4t - 30^\circ)$ into the frequency domain and get $V_s = 12\angle -30^\circ$.

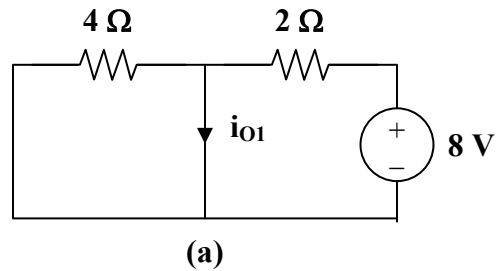
$$\text{Thus, } I_2 = \frac{12\angle -30^\circ}{2 - j2 + 3 + j4} = 5.385\angle 8.2^\circ \text{ or } i_2 = 5.385\cos(4t + 8.2^\circ) \text{ A}$$



$$i_x = \underline{[5.385\cos(4t + 8.2^\circ) + 4.983\sin(2t - 41.63^\circ)] \text{ A.}}$$

Chapter 10, Solution 43.

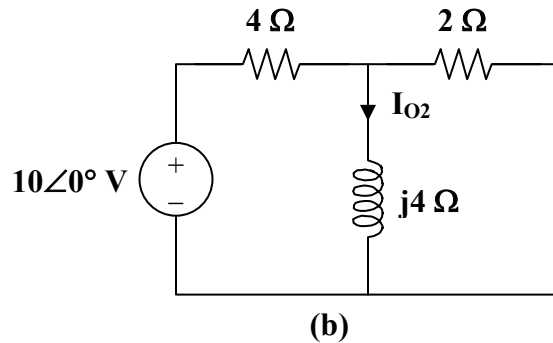
Let $i_o = i_{o1} + i_{o2}$, where i_{o1} is due to the dc source and i_{o2} is due to the ac source. For i_{o1} , consider the circuit in Fig. (a).



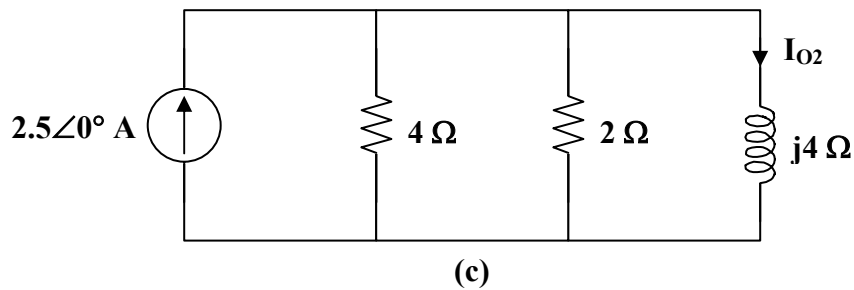
Clearly,

$$i_{o1} = 8/2 = 4 \text{ A}$$

For i_{o2} , consider the circuit in Fig. (b).



If we transform the voltage source, we have the circuit in Fig. (c), where $4 \parallel 2 = 4/3 \Omega$.



By the current division principle,

$$I_{o2} = \frac{4/3}{4/3 + j4} (2.5 \angle 0^\circ)$$

$$I_{o2} = 0.25 - j0.75 = 0.79 \angle -71.56^\circ$$

Thus,

$$i_{o2} = 0.79 \cos(4t - 71.56^\circ) \text{ A}$$

Therefore,

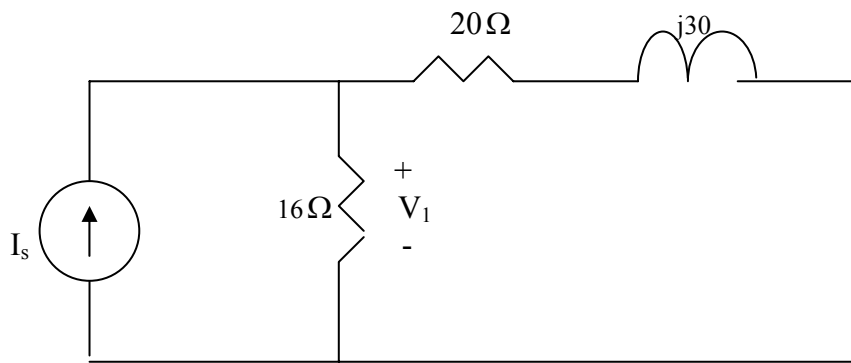
$$i_o = i_{o1} + i_{o2} = \underline{\underline{4 + 0.79 \cos(89)(4t - 71.56^\circ) \text{ A}}}$$

Chapter 10, Solution 44.

Let $v_x = v_1 + v_2$, where v_1 and v_2 are due to the current source and voltage source respectively.

For v_1 , $\omega = 6$, $5 \text{ H} \longrightarrow j\omega L = j30$

The frequency-domain circuit is shown below.

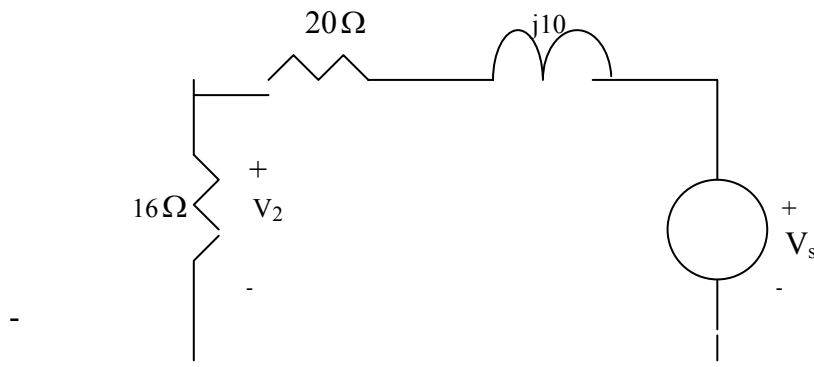


$$\text{Let } Z = 16 \parallel (20 + j30) = \frac{16(20 + j30)}{36 + j30} = 11.8 + j3.497 = 12.31 \angle 16.5^\circ$$

$$V_1 = I_s Z = (12 \angle 10^\circ)(12.31 \angle 16.5^\circ) = 147.7 \angle 26.5^\circ \longrightarrow v_1 = 147.7 \cos(6t + 26.5^\circ) \text{ V}$$

For v_2 , $\omega = 2$, $5 \text{ H} \longrightarrow j\omega L = j10$

The frequency-domain circuit is shown below.



Using voltage division,

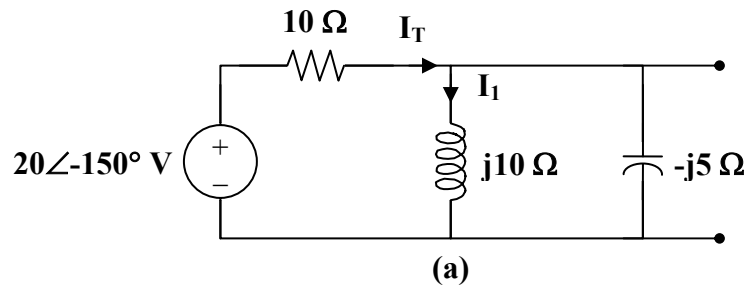
$$V_2 = \frac{16}{16 + 20 + j10} V_s = \frac{16(50\angle 0^\circ)}{36 + j10} = 21.41\angle -15.52^\circ \longrightarrow v_2 = 21.41\sin(2t - 15.52^\circ) \text{ V}$$

Thus,

$$v_x = \underline{147.7 \cos(6t + 26.5^\circ) + 21.41 \sin(2t - 15.52^\circ) \text{ V}}$$

Chapter 10, Solution 45.

Let $\mathbf{I}_o = \mathbf{I}_1 + \mathbf{I}_2$, where $\mathbf{I}_1$ is due to the voltage source and $\mathbf{I}_2$ is due to the current source. For $\mathbf{I}_1$, consider the circuit in Fig. (a).



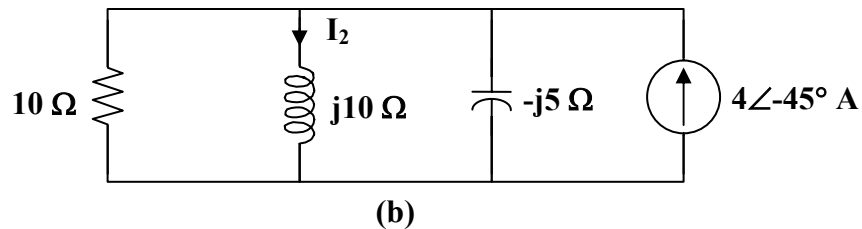
$$j10 \parallel -j5 = -j10$$

$$\mathbf{I}_T = \frac{20\angle -150^\circ}{10 - j10} = \frac{2\angle -150^\circ}{1 - j}$$

Using current division,

$$\mathbf{I}_1 = \frac{-j5}{j10 - j5} \mathbf{I}_T = \frac{-j5}{j5} \cdot \frac{2\angle -150^\circ}{1 - j} = -(1 + j)\angle -150^\circ$$

For $\mathbf{I}_2$, consider the circuit in Fig. (b).



$$10 \parallel -j5 = \frac{-j10}{2 - j}$$

Using current division,

$$\mathbf{I}_2 = \frac{-j10/(2-j)}{-j10/(2-j) + j10} (4\angle -45^\circ) = -2(1+j)\angle -45^\circ$$

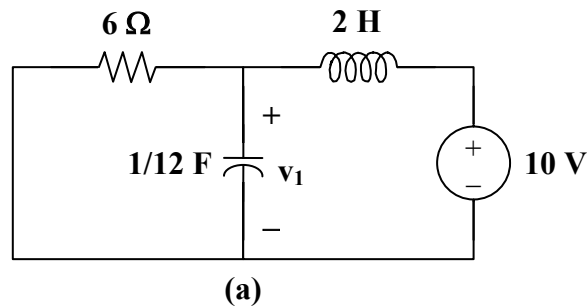
$$\mathbf{I}_o = \mathbf{I}_1 + \mathbf{I}_2 = -\sqrt{2}\angle -105^\circ - 2\sqrt{2}\angle 0^\circ$$

$$\mathbf{I}_o = -2.462 + j1.366 = 2.816\angle 150.98^\circ$$

Therefore, $i_o = \underline{\mathbf{2.816 \cos(10t + 150.98^\circ) A}}$

Chapter 10, Solution 46.

Let $v_o = v_1 + v_2 + v_3$, where v_1 , v_2 , and v_3 are respectively due to the 10-V dc source, the ac current source, and the ac voltage source. For v_1 consider the circuit in Fig. (a).



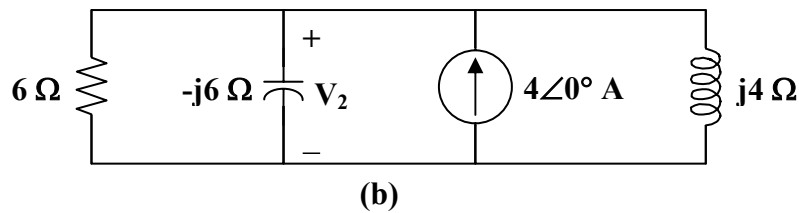
The capacitor is open to dc, while the inductor is a short circuit. Hence,
 $v_1 = 10 \text{ V}$

For v_2 , consider the circuit in Fig. (b).

$$\omega = 2$$

$$2 \text{ H} \longrightarrow j\omega L = j4$$

$$\frac{1}{12} \text{ F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(2)(1/12)} = -j6$$



Applying nodal analysis,

$$4 = \frac{\mathbf{V}_2}{6} + \frac{\mathbf{V}_2}{-j6} + \frac{\mathbf{V}_2}{j4} = \left(\frac{1}{6} + \frac{j}{6} - \frac{j}{4} \right) \mathbf{V}_2$$

$$\mathbf{V}_2 = \frac{24}{1 - j0.5} = 21.45\angle 26.56^\circ$$

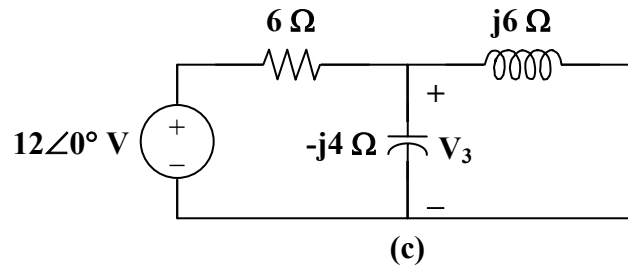
Hence, $v_2 = 21.45 \sin(2t + 26.56^\circ) \text{ V}$

For v_3 , consider the circuit in Fig. (c).

$$\omega = 3$$

$$2 \text{ H} \longrightarrow j\omega L = j6$$

$$\frac{1}{12} \text{ F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(3)(1/12)} = -j4$$



At the non-reference node,

$$\frac{12 - V_3}{6} = \frac{V_3}{-j4} + \frac{V_3}{j6}$$

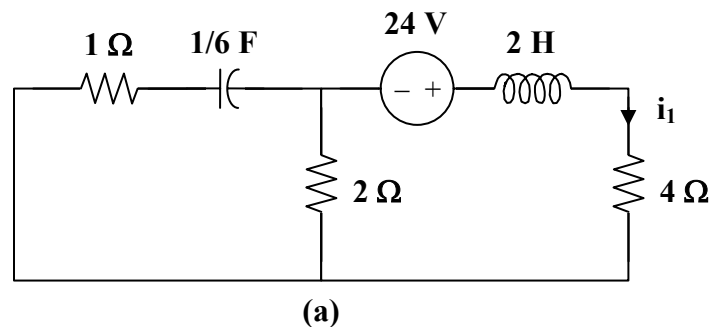
$$V_3 = \frac{12}{1 + j0.5} = 10.73 \angle -26.56^\circ$$

Hence, $v_3 = 10.73 \cos(3t - 26.56^\circ) \text{ V}$

Therefore, $v_o = \underline{10 + 21.45 \sin(2t + 26.56^\circ) + 10.73 \cos(3t - 26.56^\circ) \text{ V}}$

Chapter 10, Solution 47.

Let $i_o = i_1 + i_2 + i_3$, where i_1 , i_2 , and i_3 are respectively due to the 24-V dc source, the ac voltage source, and the ac current source. For i_1 , consider the circuit in Fig. (a).



Since the capacitor is an open circuit to dc,

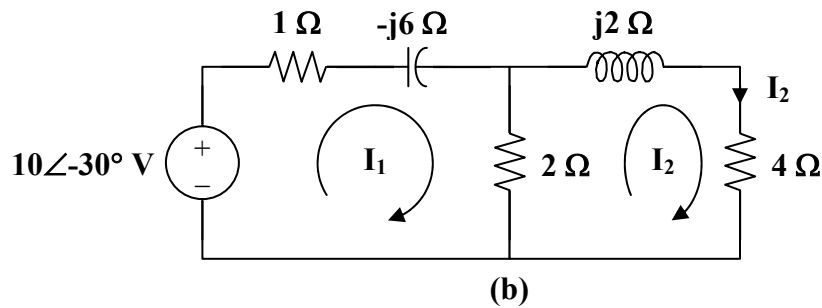
$$i_1 = \frac{24}{4+2} = 4 \text{ A}$$

For i_2 , consider the circuit in Fig. (b).

$$\omega = 1$$

$$2 \text{ H} \longrightarrow j\omega L = j2$$

$$\frac{1}{6} \text{ F} \longrightarrow \frac{1}{j\omega C} = -j6$$



For mesh 1,

$$-10\angle -30^\circ + (3 - j6)\mathbf{I}_1 - 2\mathbf{I}_2 = 0$$

$$10\angle -30^\circ = 3(1 - 2j)\mathbf{I}_1 - 2\mathbf{I}_2$$

(1)

For mesh 2,

$$0 = -2\mathbf{I}_1 + (6 + j2)\mathbf{I}_2$$

$$\mathbf{I}_1 = (3 + j)\mathbf{I}_2$$

(2)

Substituting (2) into (1)

$$10\angle -30^\circ = 13 - j15\mathbf{I}_2$$

$$\mathbf{I}_2 = 0.504\angle 19.1^\circ$$

Hence,

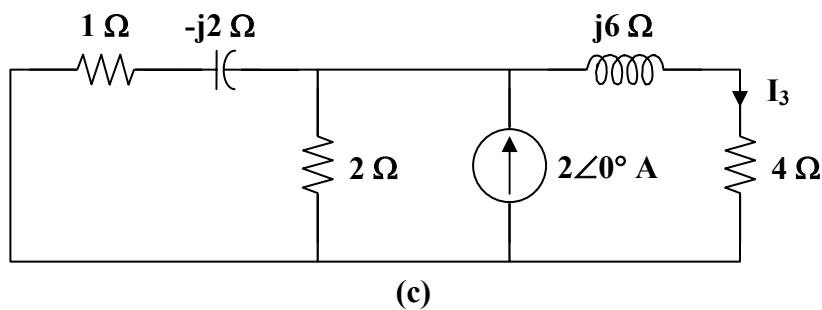
$$i_2 = 0.504\sin(t + 19.1^\circ) \text{ A}$$

For i_3 , consider the circuit in Fig. (c).

$$\omega = 3$$

$$2 \text{ H} \longrightarrow j\omega L = j6$$

$$\frac{1}{6} \text{ F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(3)(1/6)} = -j2$$



$$2 \parallel (1 - j2) = \frac{2(1 - j2)}{3 - j2}$$

Using current division,

$$\mathbf{I}_3 = \frac{\frac{2(1 - j2)}{3 - j2} \cdot (2 \angle 0^\circ)}{4 + j6 + \frac{2(1 - j2)}{3 - j2}} = \frac{2(1 - j2)}{13 + j3}$$

$$\mathbf{I}_3 = 0.3352 \angle -76.43^\circ$$

Hence $i_3 = 0.3352 \cos(3t - 76.43^\circ) \text{ A}$

Therefore, $i_o = \underline{\underline{4 + 0.504 \sin(t + 19.1^\circ) + 0.3352 \cos(3t - 76.43^\circ) \text{ A}}}$

Chapter 10, Solution 48.

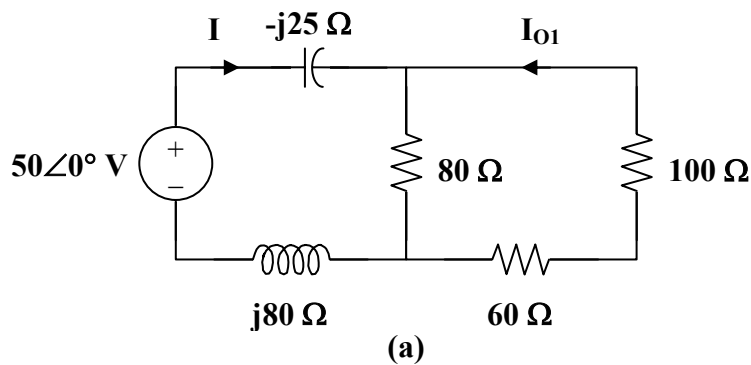
Let $i_o = i_{o1} + i_{o2} + i_{o3}$, where i_{o1} is due to the ac voltage source, i_{o2} is due to the dc voltage source, and i_{o3} is due to the ac current source. For i_{o1} , consider the circuit in Fig. (a).

$$\omega = 2000$$

$$50 \cos(2000t) \longrightarrow 50 \angle 0^\circ$$

$$40 \text{ mH} \longrightarrow j\omega L = j(2000)(40 \times 10^{-3}) = j80$$

$$20 \text{ } \mu\text{F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(2000)(20 \times 10^{-6})} = -j25$$



$$80 \parallel (60 + 100) = 160/3$$

$$\mathbf{I} = \frac{50}{160/3 + j80 - j25} = \frac{30}{32 + j33}$$

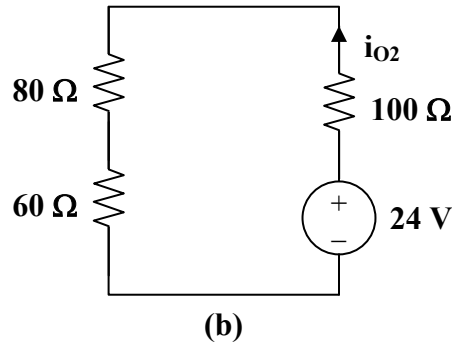
Using current division,

$$\mathbf{I}_{o1} = \frac{-80\mathbf{I}}{80+160} = \frac{-1}{3}\mathbf{I} = \frac{10\angle 180^\circ}{46\angle 45.9^\circ}$$

$$\mathbf{I}_{o1} = 0.217\angle 134.1^\circ$$

Hence, $i_{o1} = 0.217 \cos(2000t + 134.1^\circ) \text{ A}$

For i_{o2} , consider the circuit in Fig. (b).



$$i_{o2} = \frac{24}{80+60+100} = 0.1 \text{ A}$$

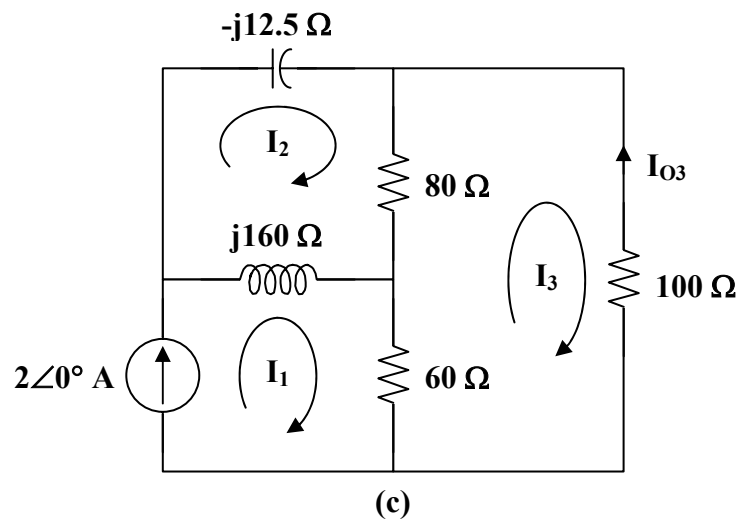
For i_{o3} , consider the circuit in Fig. (c).

$$\omega = 4000$$

$$2 \cos(4000t) \longrightarrow 2\angle 0^\circ$$

$$40 \text{ mH} \longrightarrow j\omega L = j(4000)(40 \times 10^{-3}) = j160$$

$$20 \text{ } \mu\text{F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(4000)(20 \times 10^{-6})} = -j12.5$$



For mesh 1,

$$\mathbf{I}_1 = 2$$

For mesh 2,

(1)

$$(80 + j160 - j12.5)\mathbf{I}_2 - j160\mathbf{I}_1 - 80\mathbf{I}_3 = 0$$

Simplifying and substituting (1) into this equation yields

$$(8 + j14.75)\mathbf{I}_2 - 8\mathbf{I}_3 = j32 \quad (2)$$

For mesh 3,

$$240\mathbf{I}_3 - 60\mathbf{I}_1 - 80\mathbf{I}_2 = 0$$

Simplifying and substituting (1) into this equation yields

$$\mathbf{I}_2 = 3\mathbf{I}_3 - 1.5 \quad (3)$$

Substituting (3) into (2) yields

$$(16 + j44.25)\mathbf{I}_3 = 12 + j54.125$$

$$\mathbf{I}_3 = \frac{12 + j54.125}{16 + j44.25} = 1.1782 \angle 7.38^\circ$$

$$\mathbf{I}_{O3} = -\mathbf{I}_3 = -1.1782 \angle 7.38^\circ$$

Hence,

$$i_{O3} = -1.1782 \sin(4000t + 7.38^\circ) \text{ A}$$

Therefore, $i_o = \underline{\mathbf{0.1 + 0.217 \cos(2000t + 134.1^\circ) - 1.1782 \sin(4000t + 7.38^\circ) \text{ A}}}$

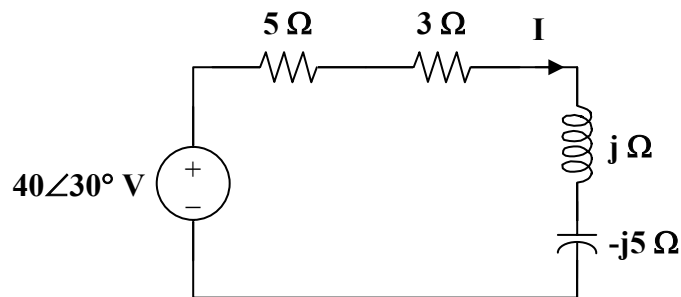
Chapter 10, Solution 49.

$$8 \sin(200t + 30^\circ) \longrightarrow 8 \angle 30^\circ, \quad \omega = 200$$

$$5 \text{ mH} \longrightarrow j\omega L = j(200)(5 \times 10^{-3}) = j$$

$$1 \text{ mF} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(200)(1 \times 10^{-3})} = -j5$$

After transforming the current source, the circuit becomes that shown in the figure below.



$$\mathbf{I} = \frac{40 \angle 30^\circ}{5 + 3 + j - j5} = \frac{40 \angle 30^\circ}{8 - j4} = 4.472 \angle 56.56^\circ$$

$$i = \underline{\mathbf{4.472 \sin(200t + 56.56^\circ) \text{ A}}}$$

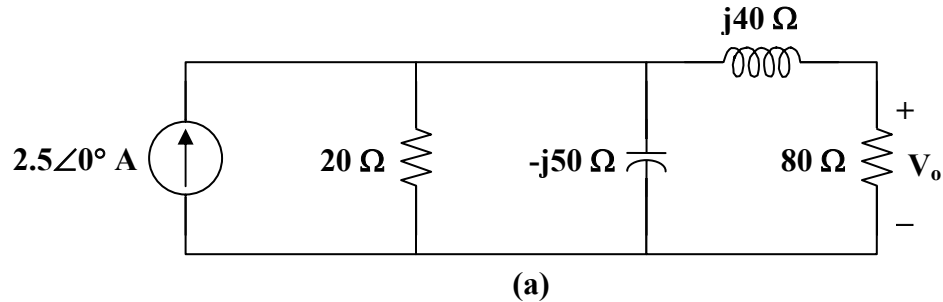
Chapter 10, Solution 50.

$$50 \cos(10^5 t) \longrightarrow 50 \angle 0^\circ, \quad \omega = 10^5$$

$$0.4 \text{ mH} \longrightarrow j\omega L = j(10^5)(0.4 \times 10^{-3}) = j40$$

$$0.2 \text{ } \mu\text{F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(10^5)(0.2 \times 10^{-6})} = -j50$$

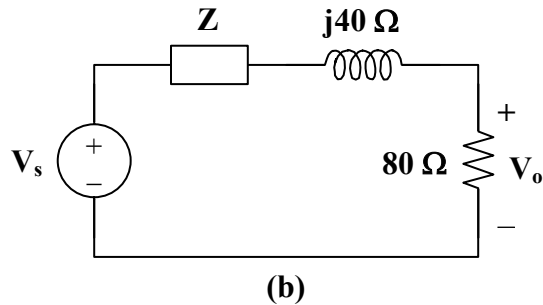
After transforming the voltage source, we get the circuit in Fig. (a).



$$\text{Let } \mathbf{Z} = 20 \parallel -j50 = \frac{-j100}{2 - j5}$$

$$\text{and } \mathbf{V}_s = (2.5 \angle 0^\circ) \mathbf{Z} = \frac{-j250}{2 - j5}$$

With these, the current source is transformed to obtain the circuit in Fig.(b).



By voltage division,

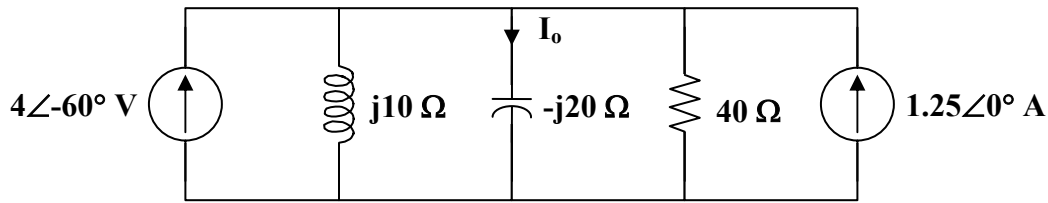
$$\mathbf{V}_o = \frac{80}{\mathbf{Z} + 80 + j40} \mathbf{V}_s = \frac{80}{\frac{-j100}{2 - j5} + 80 + j40} \cdot \frac{-j250}{2 - j5}$$

$$\mathbf{V}_o = \frac{8(-j250)}{36 - j42} = 36.15 \angle -40.6^\circ$$

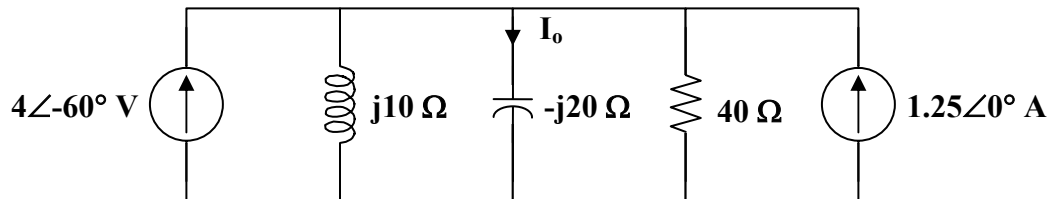
$$\text{Therefore, } v_o = \underline{\underline{36.15 \cos(10^5 t - 40.6^\circ) \text{ V}}}$$

Chapter 10, Solution 51.

The original circuit with mesh currents and a node voltage labeled is shown below.



The following circuit is obtained by transforming the voltage sources.



Use nodal analysis to find V_x .

$$4\angle -60^\circ + 1.25\angle 0^\circ = \left(\frac{1}{j10} + \frac{1}{-j20} + \frac{1}{40} \right) V_x$$

$$3.25 - j3.464 = (0.025 - j0.05) V_x$$

$$V_x = \frac{3.25 - j3.464}{0.025 - j0.05} = 81.42 + j24.29 = 84.97\angle 16.61^\circ$$

Thus, from the original circuit,

$$I_1 = \frac{40\angle 30^\circ - V_x}{j10} = \frac{(34.64 + j20) - (81.42 + j24.29)}{j10}$$

$$I_1 = \frac{-46.78 - j4.29}{j10} = -0.429 + j4.678 = \underline{\underline{4.698\angle 95.24^\circ \text{ A}}}$$

$$I_2 = \frac{V_x - 50\angle 0^\circ}{40} = \frac{31.42 + j24.29}{40}$$

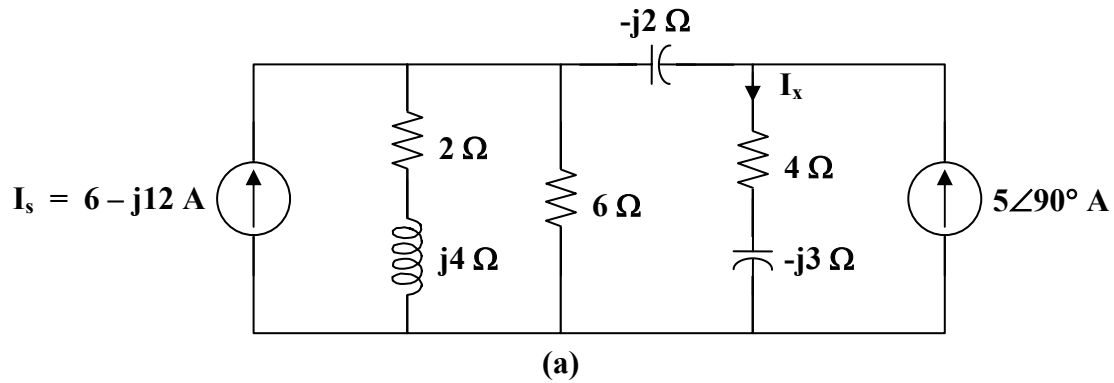
$$I_2 = 0.7855 + j0.6072 = 0.9928\angle 37.7^\circ = \underline{\underline{0.9928\angle 37.7^\circ \text{ A}}}$$

Chapter 10, Solution 52.

We transform the voltage source to a current source.

$$I_s = \frac{60\angle 0^\circ}{2 + j4} = 6 - j12$$

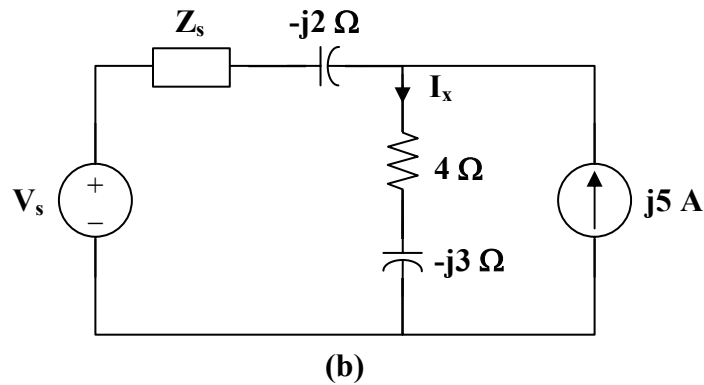
The new circuit is shown in Fig. (a).



Let
$$\mathbf{Z}_s = 6 \parallel (2 + j4) = \frac{6(2 + j4)}{8 + j4} = 2.4 + j1.8$$

$$\mathbf{V}_s = \mathbf{I}_s \mathbf{Z}_s = (6 - j12)(2.4 + j1.8) = 36 - j18 = 18(2 - j)$$

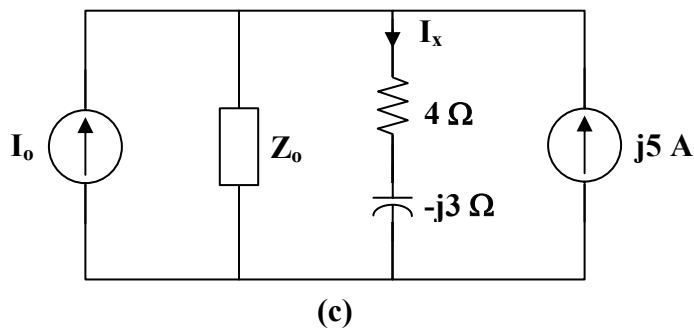
With these, we transform the current source on the left hand side of the circuit to a voltage source. We obtain the circuit in Fig. (b).



Let
$$\mathbf{Z}_o = \mathbf{Z}_s - j2 = 2.4 - j0.2 = 0.2(12 - j)$$

$$\mathbf{I}_o = \frac{\mathbf{V}_s}{\mathbf{Z}_o} = \frac{18(2 - j)}{0.2(12 - j)} = 15.517 - j6.207$$

With these, we transform the voltage source in Fig. (b) to a current source. We obtain the circuit in Fig. (c).



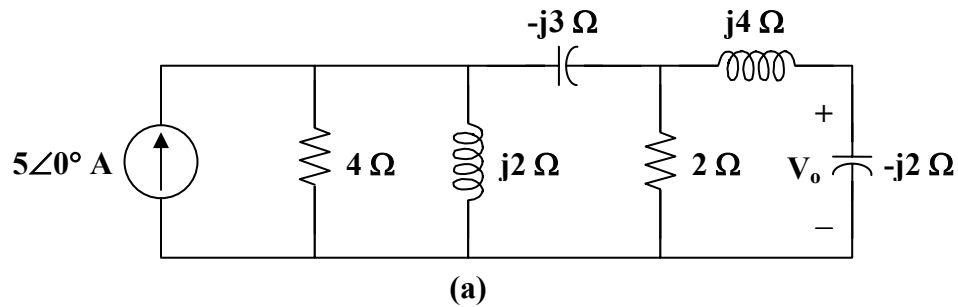
Using current division,

$$\mathbf{I}_x = \frac{\mathbf{Z}_o}{\mathbf{Z}_o + 4 - j3} (\mathbf{I}_o + j5) = \frac{2.4 - j0.2}{6.4 - j3.2} (15.517 - j1.207)$$

$$\mathbf{I}_x = 5 + j1.5625 = \underline{\underline{5.238 \angle 17.35^\circ \text{ A}}}$$

Chapter 10, Solution 53.

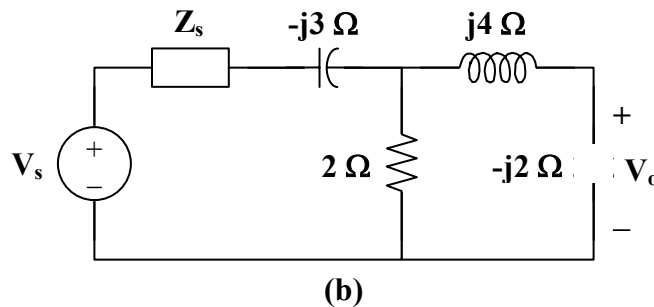
We transform the voltage source to a current source to obtain the circuit in Fig. (a).



Let $\mathbf{Z}_s = 4 \parallel j2 = \frac{j8}{4 + j2} = 0.8 + j1.6$

$$\mathbf{V}_s = (5 \angle 0^\circ) \mathbf{Z}_s = (5)(0.8 + j1.6) = 4 + j8$$

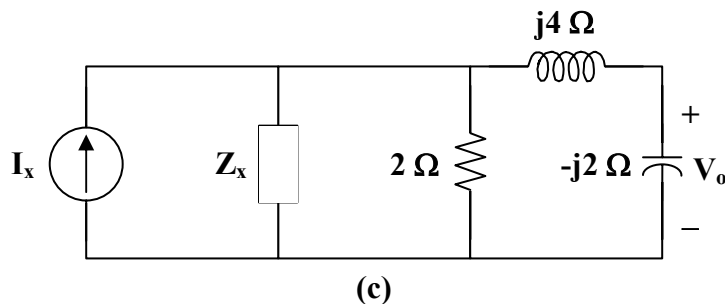
With these, the current source is transformed so that the circuit becomes that shown in Fig. (b).



Let $\mathbf{Z}_x = \mathbf{Z}_s - j3 = 0.8 - j1.4$

$$\mathbf{I}_x = \frac{\mathbf{V}_s}{\mathbf{Z}_s} = \frac{4 + j8}{0.8 - j1.4} = -3.0769 + j4.6154$$

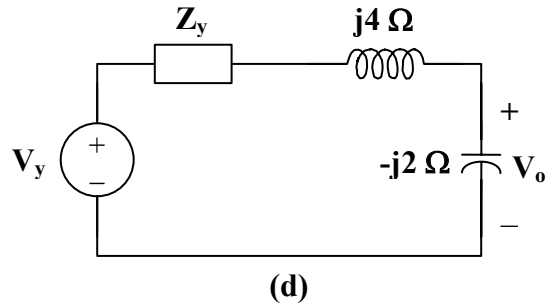
With these, we transform the voltage source in Fig. (b) to obtain the circuit in Fig. (c).



Let $\mathbf{Z}_y = 2 \parallel \mathbf{Z}_x = \frac{1.6 - j2.8}{2.8 - j1.4} = 0.8571 - j0.5714$

$$\mathbf{V}_y = \mathbf{I}_x \mathbf{Z}_y = (-3.0769 + j4.6154) \cdot (0.8571 - j0.5714) = j5.7143$$

With these, we transform the current source to obtain the circuit in Fig. (d).



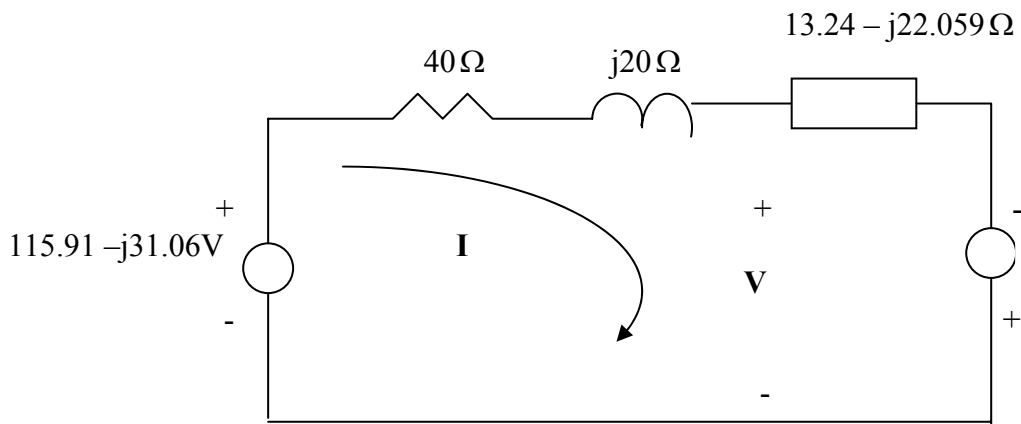
Using current division,

$$\mathbf{V}_o = \frac{-j2}{\mathbf{Z}_y + j4 - j2} \mathbf{V}_y = \frac{-j2(j5.7143)}{0.8571 - j0.5714 + j4 - j2} = \underline{\underline{(3.529 - j5.883) \text{ V}}}$$

Chapter 10, Solution 54.

$$50 \parallel (-j30) = \frac{50(-j30)}{50 - j30} = 13.24 - j22.059$$

We convert the current source to voltage source and obtain the circuit below.



Applying KVL gives

$$-115.91 + j31.058 + (53.24 - j2.059)I - 134.95 + j74.912 = 0$$

$$\text{or } I = \frac{-250.86 + j105.97}{53.24 - j2.059} = -4.7817 + j1.8055$$

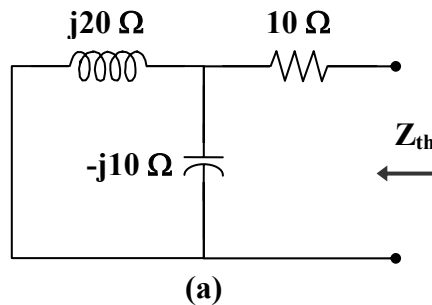
$$\text{But } -V + (40 + j20)I + V = 0 \longrightarrow V = V_s - (40 + j20)I$$

$$V = 115.91 - j31.05 - (40 + j20)(-4.7817 + j1.8055) = \underline{124.06 \angle -154^\circ \text{ V}}$$

which agrees with the result in Prob. 10.7.

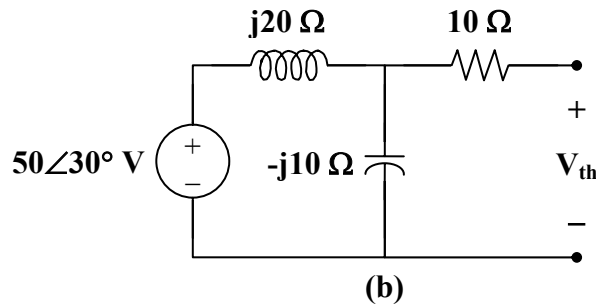
Chapter 10, Solution 55.

(a) To find $\mathbf{Z}_{th}$, consider the circuit in Fig. (a).



$$\begin{aligned} \mathbf{Z}_N = \mathbf{Z}_{th} &= 10 + j20 \parallel (-j10) = 10 + \frac{(j20)(-j10)}{j20 - j10} \\ &= 10 - j20 = \underline{22.36 \angle -63.43^\circ \Omega} \end{aligned}$$

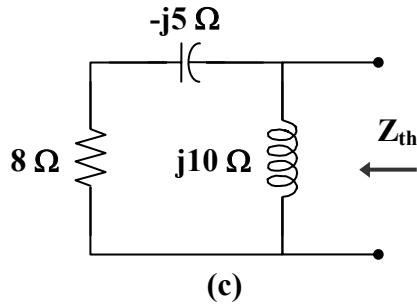
To find $\mathbf{V}_{th}$, consider the circuit in Fig. (b).



$$\mathbf{V}_{th} = \frac{-j10}{j20 - j10} (50 \angle 30^\circ) = \underline{-50 \angle 30^\circ \text{ V}}$$

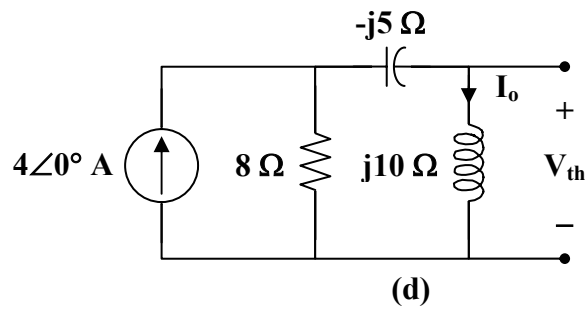
$$\mathbf{I}_N = \frac{\mathbf{V}_{th}}{\mathbf{Z}_{th}} = \frac{-50 \angle 30^\circ}{22.36 \angle -63.43^\circ} = \underline{2.236 \angle 273.4^\circ \text{ A}}$$

(b) To find $\mathbf{Z}_{th}$, consider the circuit in Fig. (c).



$$\mathbf{Z}_N = \mathbf{Z}_{th} = j10 \parallel (8 - j5) = \frac{(j10)(8 - j5)}{j10 + 8 - j5} = \underline{\underline{10 \angle 26^\circ \Omega}}$$

To obtain $\mathbf{V}_{th}$, consider the circuit in Fig. (d).



By current division,

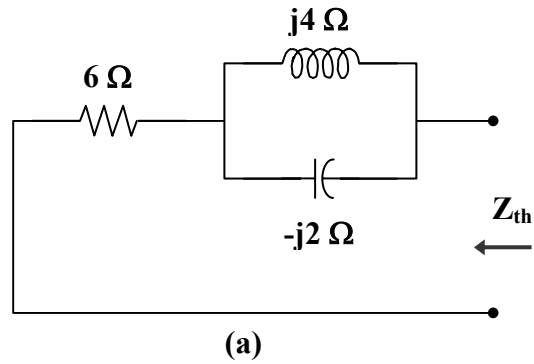
$$\mathbf{I}_o = \frac{8}{8 + j10 - j5} (4 \angle 0^\circ) = \frac{32}{8 + j5}$$

$$\mathbf{V}_{th} = j10 \mathbf{I}_o = \frac{j320}{8 + j5} = \underline{\underline{33.92 \angle 58^\circ \text{ V}}}$$

$$\mathbf{I}_N = \frac{\mathbf{V}_{th}}{\mathbf{Z}_{th}} = \frac{33.92 \angle 58^\circ}{10 \angle 26^\circ} = \underline{\underline{3.392 \angle 32^\circ \text{ A}}}$$

Chapter 10, Solution 56.

- (a) To find $\mathbf{Z}_{th}$, consider the circuit in Fig. (a).



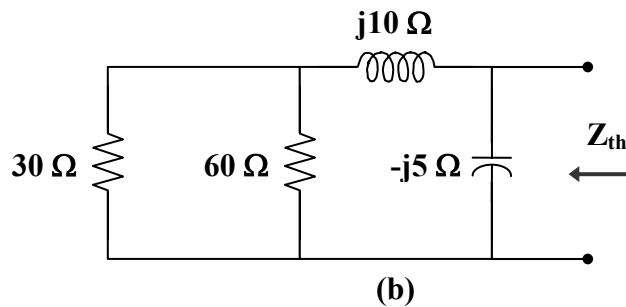
$$\begin{aligned}\mathbf{Z}_N = \mathbf{Z}_{th} &= 6 + j4 \parallel (-j2) = 6 + \frac{(j4)(-j2)}{j4 - j2} = 6 - j4 \\ &= \underline{\underline{7.211 \angle -33.69^\circ \Omega}}\end{aligned}$$

By placing short circuit at terminals a-b, we obtain,

$$\mathbf{I}_N = \underline{\underline{2 \angle 0^\circ \text{ A}}}$$

$$\mathbf{V}_{th} = \mathbf{Z}_{th} \mathbf{I}_{th} = (7.211 \angle -33.69^\circ)(2 \angle 0^\circ) = \underline{\underline{14.422 \angle -33.69^\circ \text{ V}}}$$

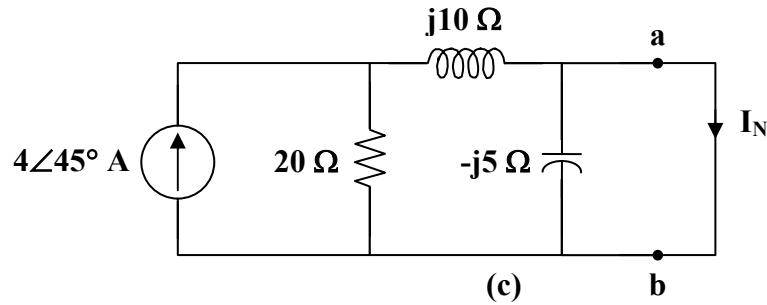
- (b) To find $\mathbf{Z}_{th}$, consider the circuit in Fig. (b).



$$30 \parallel 60 = 20$$

$$\begin{aligned}\mathbf{Z}_N = \mathbf{Z}_{th} &= -j5 \parallel (20 + j10) = \frac{(-j5)(20 + j10)}{20 + j5} \\ &= \underline{\underline{5.423 \angle -77.47^\circ \Omega}}\end{aligned}$$

To find V_{th} and I_N , we transform the voltage source and combine the $30\ \Omega$ and $60\ \Omega$ resistors. The result is shown in Fig. (c).



$$I_N = \frac{20}{20 + j10} (4\angle 45^\circ) = \frac{2}{5} (2 - j)(4\angle 45^\circ)$$

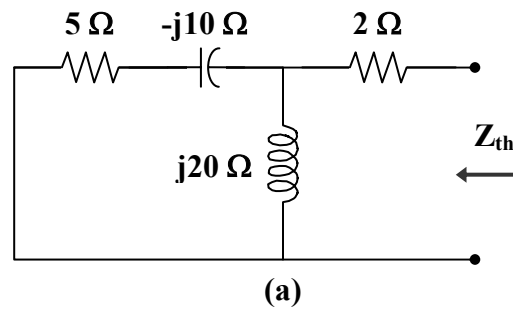
$$= \underline{3.578\angle 18.43^\circ \text{ A}}$$

$$V_{th} = Z_{th} I_N = (5.423\angle -77.47^\circ)(3.578\angle 18.43^\circ)$$

$$= \underline{19.4\angle -59^\circ \text{ V}}$$

Chapter 10, Solution 57.

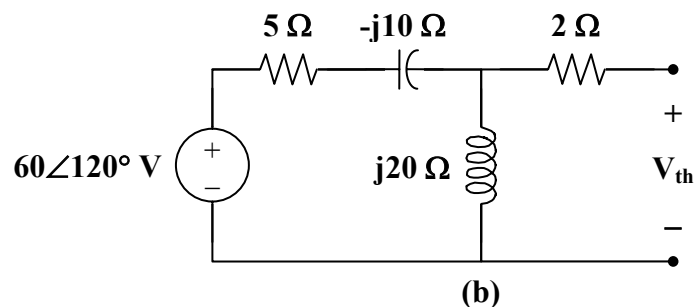
To find Z_{th} , consider the circuit in Fig. (a).



$$Z_N = Z_{th} = 2 + j20 \parallel (5 - j10) = 2 + \frac{(j20)(5 - j10)}{5 + j10}$$

$$= 18 - j12 = \underline{21.633\angle -33.7^\circ \Omega}$$

To find V_{th} , consider the circuit in Fig. (b).

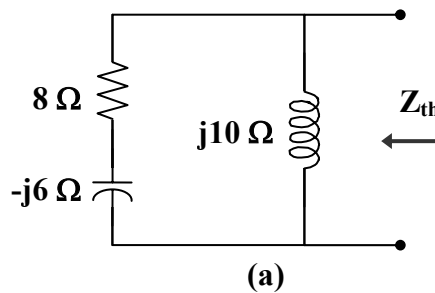


$$\begin{aligned} V_{th} &= \frac{j20}{5 - j10 + j20} (60 \angle 120^\circ) = \frac{j4}{1 + j2} (60 \angle 120^\circ) \\ &= \underline{\underline{107.3 \angle 146.56^\circ \text{ V}}} \end{aligned}$$

$$I_N = \frac{V_{th}}{Z_{th}} = \frac{107.3 \angle 146.56^\circ}{21.633 \angle -33.7^\circ} = \underline{\underline{4.961 \angle -179.7^\circ \text{ A}}}$$

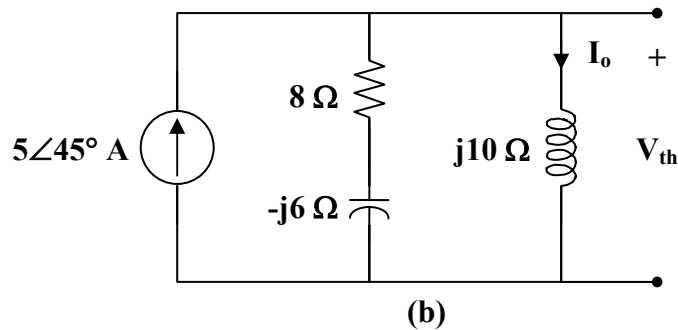
Chapter 10, Solution 58.

Consider the circuit in Fig. (a) to find Z_{th} .



$$\begin{aligned} Z_{th} &= j10 \parallel (8 - j6) = \frac{(j10)(8 - j6)}{8 + j4} = 5(2 + j) \\ &= \underline{\underline{11.18 \angle 26.56^\circ \Omega}} \end{aligned}$$

Consider the circuit in Fig. (b) to find V_{th} .

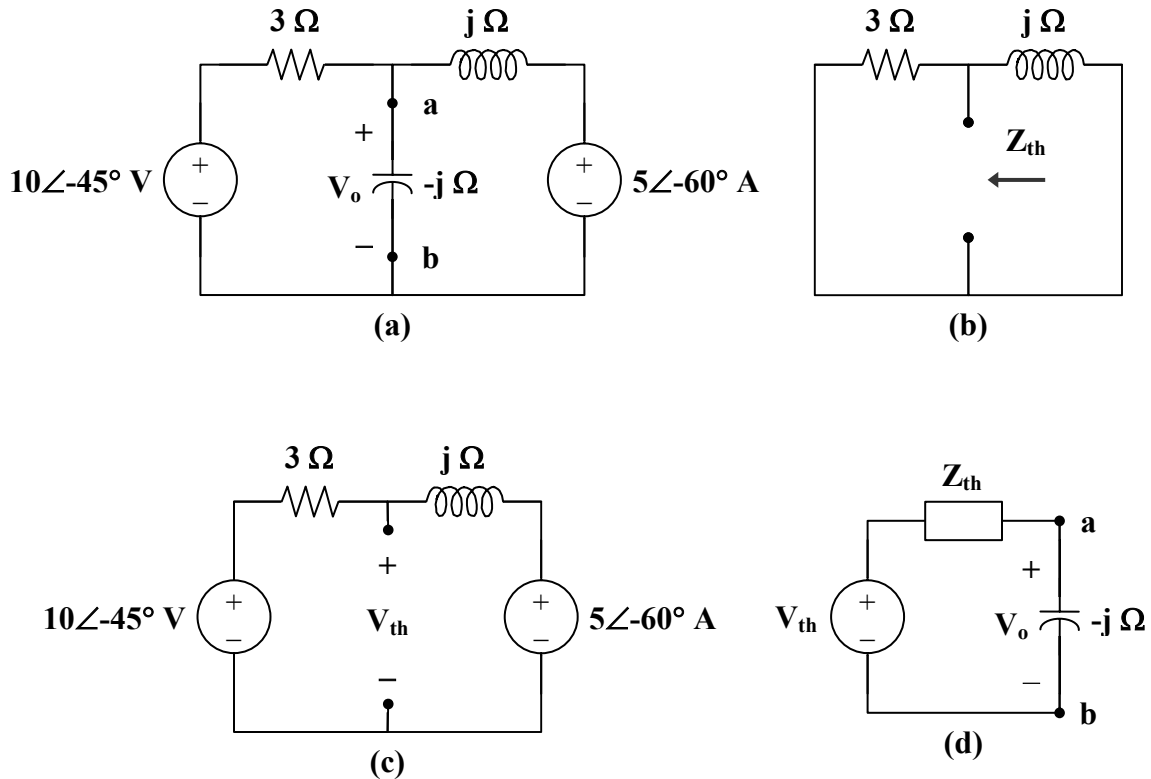


$$I_o = \frac{8 - j6}{8 - j6 + j10} (5 \angle 45^\circ) = \frac{4 - j3}{4 + j2} (5 \angle 45^\circ)$$

$$V_{th} = j10 I_o = \frac{(j10)(4 - j3)(5 \angle 45^\circ)}{(2)(2 + j)} = \underline{\underline{55.9 \angle 71.56^\circ \text{ V}}}$$

Chapter 10, Solution 59.

The frequency-domain equivalent circuit is shown in Fig. (a). Our goal is to find V_{th} and Z_{th} across the terminals of the capacitor as shown in Figs. (b) and (c).



From Fig. (b),

$$Z_{th} = 3 \parallel j = \frac{j3}{3+j} = \frac{3}{10}(1+j3)$$

From Fig. (c),

$$\frac{10\angle-45^\circ - V_{th}}{3} + \frac{5\angle-60^\circ - V_{th}}{j} = 0$$

$$V_{th} = \frac{10\angle-45^\circ - 15\angle30^\circ}{1-j3}$$

From Fig. (d),

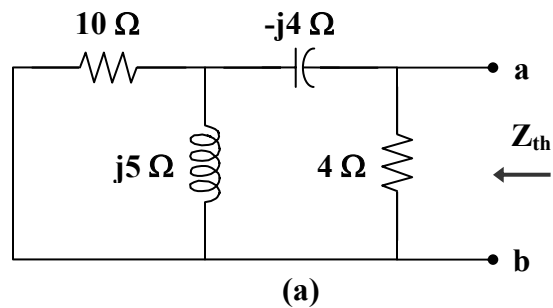
$$\mathbf{V}_o = \frac{-j}{\mathbf{Z}_{th} - j} \mathbf{V}_{th} = 10 \angle -45^\circ - 15 \angle 30^\circ$$

$$\mathbf{V}_o = 15.73 \angle 247.9^\circ \text{ V}$$

Therefore, $v_o = \underline{\mathbf{15.73 \cos(t + 247.9^\circ) \text{ V}}}$

Chapter 10, Solution 60.

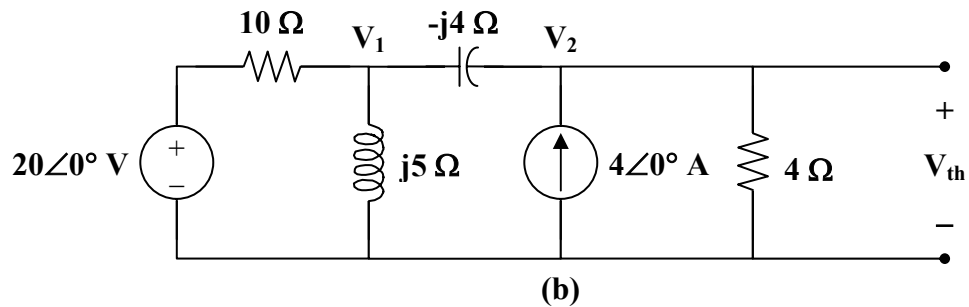
(a) To find $\mathbf{Z}_{th}$, consider the circuit in Fig. (a).



$$\mathbf{Z}_{th} = 4 \parallel (-j4 + 10 \parallel j5) = 4 \parallel (-j4 + 2 + j4)$$

$$\mathbf{Z}_{th} = 4 \parallel 2 = \underline{\mathbf{1.333 \Omega}}$$

To find $\mathbf{V}_{th}$, consider the circuit in Fig. (b).



At node 1,

$$\begin{aligned} \frac{20 - \mathbf{V}_1}{10} &= \frac{\mathbf{V}_1}{j5} + \frac{\mathbf{V}_1 - \mathbf{V}_2}{-j4} \\ (1 + j0.5)\mathbf{V}_1 - j2.5\mathbf{V}_2 &= 20 \end{aligned}$$

(1)

At node 2,

$$4 + \frac{V_1 - V_2}{-j4} = \frac{V_2}{4}$$

$$V_1 = (1 - j)V_2 + j16$$

$$(2)$$

Substituting (2) into (1) leads to

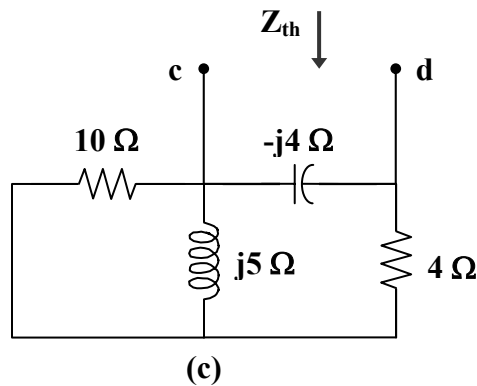
$$28 - j16 = (1.5 - j3)V_2$$

$$V_2 = \frac{28 - j16}{1.5 - j3} = 8 + j5.333$$

Therefore,

$$V_{th} = V_2 = \underline{\underline{9.615 \angle 33.69^\circ \text{ V}}}$$

(b) To find Z_{th} , consider the circuit in Fig. (c).



$$Z_{th} = -j4 \parallel (4 + 10 \parallel j5) = -j4 \parallel \left(4 + \frac{j10}{2 + j}\right)$$

$$Z_{th} = -j4 \parallel (6 + j4) = \frac{-j4}{6} (6 + j4) = \underline{\underline{2.667 - j4 \Omega}}$$

To find V_{th} , we will make use of the result in part (a).

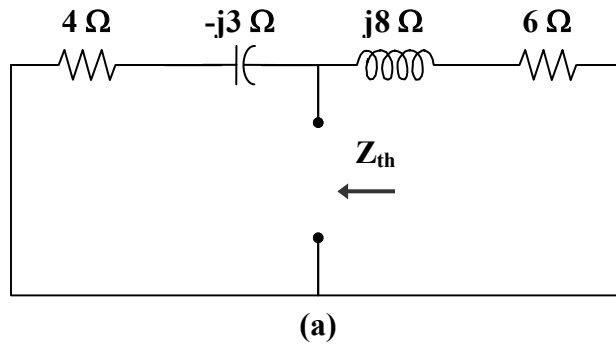
$$V_2 = 8 + j5.333 = (8/3)(3 + j2)$$

$$V_1 = (1 - j)V_2 + j16 = j16 + (8/3)(5 - j)$$

$$V_{th} = V_1 - V_2 = 16/3 + j8 = \underline{\underline{9.614 \angle 56.31^\circ \text{ V}}}$$

Chapter 10, Solution 61.

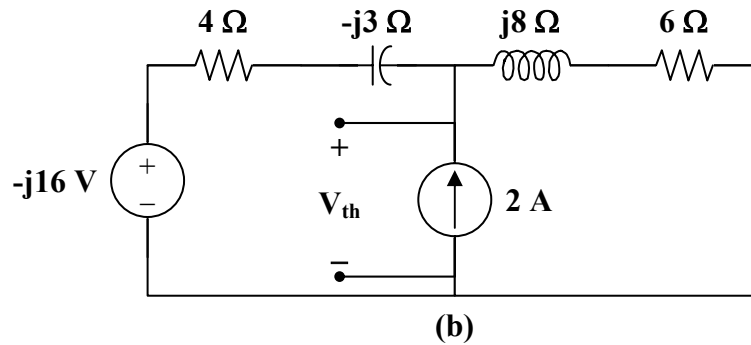
First, we need to find V_{th} and Z_{th} across the $1\ \Omega$ resistor.



From Fig. (a),

$$Z_{th} = (4 - j3) \parallel (6 + j8) = \frac{(4 - j3)(6 + j8)}{10 + j5} = 4.4 - j0.8$$

$$Z_{th} = \underline{4.472 \angle -10.3^\circ \Omega}$$



From Fig. (b),

$$\frac{-j16 - V_{th}}{4 - j3} + 2 = \frac{V_{th}}{6 + j8}$$

$$V_{th} = \frac{3.92 - j2.56}{0.22 + j0.4} = 20.93 \angle -43.45^\circ$$

$$V_o = \frac{V_{th}}{1 + Z_{th}} = \frac{20.93 \angle -43.45^\circ}{5.46 \angle -8.43^\circ}$$

$$V_o = 3.835 \angle -35.02^\circ$$

Therefore, $v_o = \underline{3.835 \cos(4t - 35.02^\circ) V}$

Chapter 10, Solution 62.

First, we transform the circuit to the frequency domain.

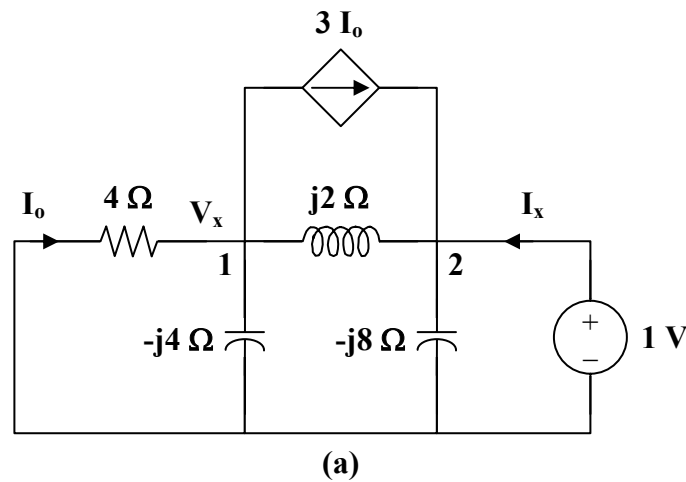
$$12 \cos(t) \longrightarrow 12 \angle 0^\circ, \quad \omega = 1$$

$$2 \text{ H} \longrightarrow j\omega L = j2$$

$$\frac{1}{4} \text{ F} \longrightarrow \frac{1}{j\omega C} = -j4$$

$$\frac{1}{8} \text{ F} \longrightarrow \frac{1}{j\omega C} = -j8$$

To find $\mathbf{Z}_{\text{th}}$, consider the circuit in Fig. (a).



At node 1,

$$\frac{\mathbf{V}_x}{4} + \frac{\mathbf{V}_x}{-j4} + 3\mathbf{I}_o = \frac{1 - \mathbf{V}_x}{j2}, \quad \text{where } \mathbf{I}_o = \frac{-\mathbf{V}_x}{4}$$

Thus,
$$\frac{\mathbf{V}_x}{-j4} - \frac{2\mathbf{V}_x}{4} = \frac{1 - \mathbf{V}_x}{j2}$$

$$\mathbf{V}_x = 0.4 + j0.8$$

At node 2,

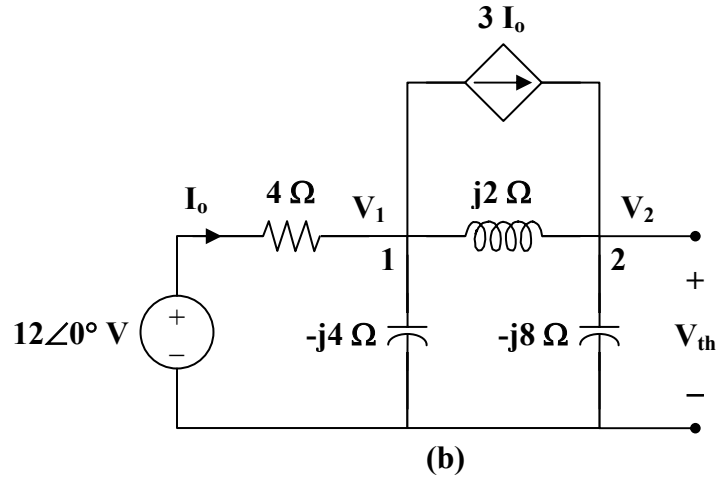
$$\mathbf{I}_x + 3\mathbf{I}_o = \frac{1}{-j8} + \frac{1 - \mathbf{V}_x}{j2}$$

$$\mathbf{I}_x = (0.75 + j0.5)\mathbf{V}_x - j\frac{3}{8}$$

$$\mathbf{I}_x = -0.1 + j0.425$$

$$\mathbf{Z}_{\text{th}} = \frac{1}{\mathbf{I}_x} = -0.5246 - j2.229 = 2.29 \angle -103.24^\circ \Omega$$

To find V_{th} , consider the circuit in Fig. (b).



At node 1,

$$\frac{12 - V_1}{4} = 3I_o + \frac{V_1}{-j4} + \frac{V_1 - V_2}{j2}, \quad \text{where } I_o = \frac{12 - V_1}{4}$$

$$24 = (2 + j)V_1 - j2V_2 \quad (1)$$

At node 2,

$$\frac{V_1 - V_2}{j2} + 3I_o = \frac{V_2}{-j8}$$

$$72 = (6 + j4)V_1 - j3V_2 \quad (2)$$

From (1) and (2),

$$\begin{bmatrix} 24 \\ 72 \end{bmatrix} = \begin{bmatrix} 2 + j & -j2 \\ 6 + j4 & -j3 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

$$\Delta = -5 + j6,$$

$$\Delta_2 = -j24$$

$$V_{th} = V_2 = \frac{\Delta_2}{\Delta} = 3.073 \angle -219.8^\circ$$

Thus,

$$V_o = \frac{2}{2 + Z_{th}} V_{th} = \frac{(2)(3.073 \angle -219.8^\circ)}{1.4754 - j2.229}$$

$$V_o = \frac{6.146 \angle -219.8^\circ}{2.673 \angle -56.5^\circ} = 2.3 \angle -163.3^\circ$$

Therefore, $v_o = \underline{\underline{2.3 \cos(t - 163.3^\circ) \text{ V}}}$

Chapter 10, Solution 63.

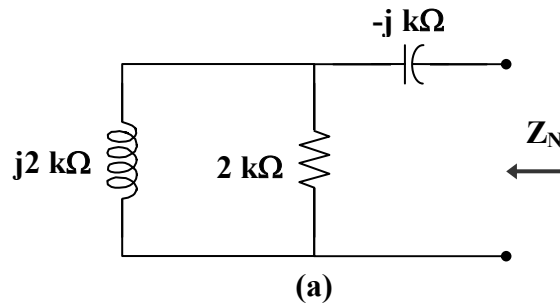
Transform the circuit to the frequency domain.

$$4 \cos(200t + 30^\circ) \longrightarrow 4 \angle 30^\circ, \quad \omega = 200$$

$$10 \text{ H} \longrightarrow j\omega L = j(200)(10) = j2 \text{ k}\Omega$$

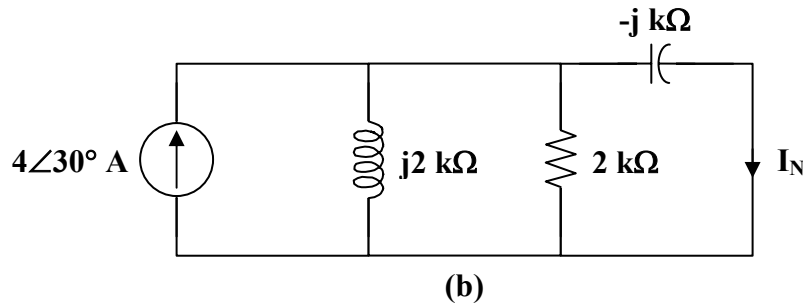
$$5 \text{ }\mu\text{F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(200)(5 \times 10^{-6})} = -j \text{ k}\Omega$$

Z_N is found using the circuit in Fig. (a).



$$Z_N = -j + 2 \parallel j2 = -j + 1 + j = 1 \text{ k}\Omega$$

We find I_N using the circuit in Fig. (b).



$$j2 \parallel 2 = 1 + j$$

By the current division principle,

$$I_N = \frac{1 + j}{1 + j - j} (4 \angle 30^\circ) = 5.657 \angle 75^\circ$$

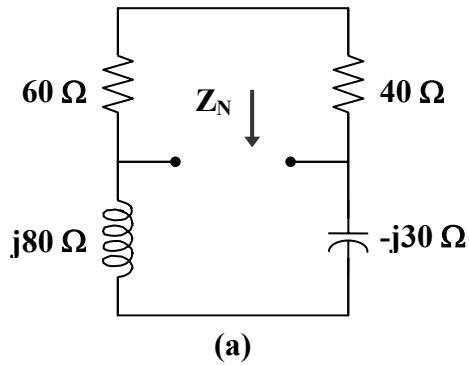
Therefore,

$$i_N = \underline{\underline{5.657 \cos(200t + 75^\circ) \text{ A}}}$$

$$Z_N = \underline{\underline{1 \text{ k}\Omega}}$$

Chapter 10, Solution 64.

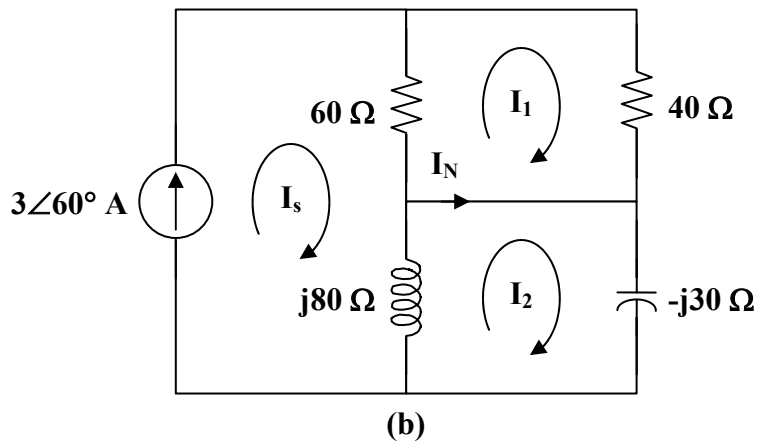
$\mathbf{Z}_N$ is obtained from the circuit in Fig. (a).



$$\mathbf{Z}_N = (60 + 40) \parallel (j80 - j30) = 100 \parallel j50 = \frac{(100)(j50)}{100 + j50}$$

$$\mathbf{Z}_N = 20 + j40 = \underline{\underline{44.72\angle 63.43^\circ \Omega}}$$

To find $\mathbf{I}_N$, consider the circuit in Fig. (b).



$$\mathbf{I}_s = 3\angle 60^\circ$$

For mesh 1,

$$100\mathbf{I}_1 - 60\mathbf{I}_s = 0$$

$$\mathbf{I}_1 = 1.8\angle 60^\circ$$

For mesh 2,

$$(j80 - j30)\mathbf{I}_2 - j80\mathbf{I}_s = 0$$

$$\mathbf{I}_2 = 4.8\angle 60^\circ$$

$$\mathbf{I}_N = \mathbf{I}_1 - \mathbf{I}_2 = \underline{\underline{3\angle 60^\circ \text{ A}}}$$

Chapter 10, Solution 65.

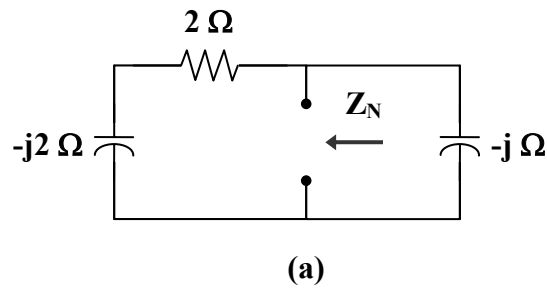
$$5 \cos(2t) \longrightarrow 5 \angle 0^\circ, \quad \omega = 2$$

$$4 \text{ H} \longrightarrow j\omega L = j(2)(4) = j8$$

$$\frac{1}{4} \text{ F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(2)(1/4)} = -j2$$

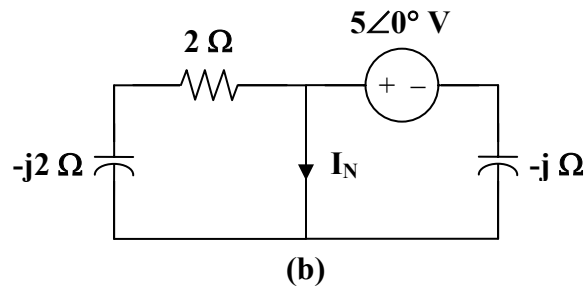
$$\frac{1}{2} \text{ F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(2)(1/2)} = -j$$

To find $\mathbf{Z}_N$, consider the circuit in Fig. (a).



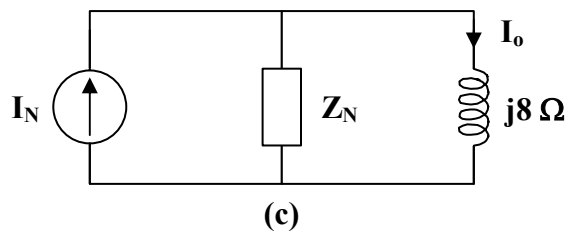
$$\mathbf{Z}_N = -j \parallel (2 - j2) = \frac{-j(2 - j2)}{2 - j3} = \frac{1}{13}(2 - j10)$$

To find $\mathbf{I}_N$, consider the circuit in Fig. (b).



$$\mathbf{I}_N = \frac{5 \angle 0^\circ}{-j} = j5$$

The Norton equivalent of the circuit is shown in Fig. (c).



Using current division,

$$\mathbf{I}_o = \frac{\mathbf{Z}_N}{\mathbf{Z}_N + j8} \mathbf{I}_N = \frac{(1/13)(2 - j10)(j5)}{(1/13)(2 - j10) + j8} = \frac{50 + j10}{2 + j94}$$

$$\mathbf{I}_o = 0.1176 - j0.5294 = 0.542 \angle -77.47^\circ$$

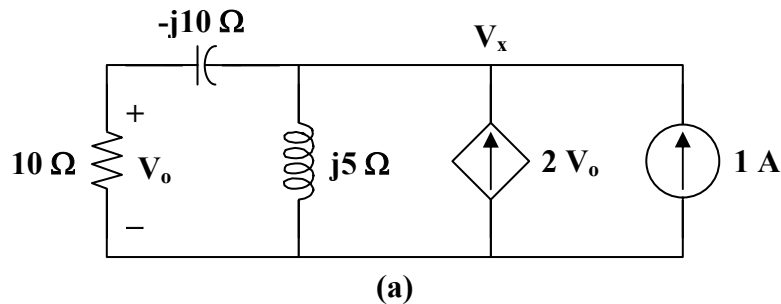
Therefore, $i_o = \underline{\mathbf{0.542 \cos(2t - 77.47^\circ) A}}$

Chapter 10, Solution 66.

$$\omega = 10$$

$$0.5 \text{ H} \longrightarrow j\omega L = j(10)(0.5) = j5$$

$$10 \text{ mF} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(10)(10 \times 10^{-3})} = -j10$$



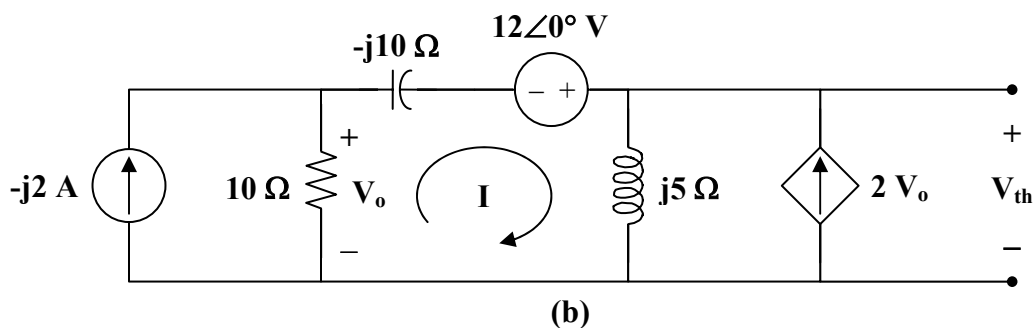
To find $\mathbf{Z}_{th}$, consider the circuit in Fig. (a).

$$1 + 2\mathbf{V}_o = \frac{\mathbf{V}_x}{j5} + \frac{\mathbf{V}_x}{10 - j10}, \quad \text{where } \mathbf{V}_o = \frac{10\mathbf{V}_x}{10 - j10}$$

$$1 + \frac{19\mathbf{V}_x}{10 - j10} = \frac{\mathbf{V}_x}{j5} \longrightarrow \mathbf{V}_x = \frac{-10 + j10}{21 + j2}$$

$$\mathbf{Z}_N = \mathbf{Z}_{th} = \frac{\mathbf{V}_x}{1} = \frac{14.142 \angle 135^\circ}{21.095 \angle 5.44^\circ} = \underline{\mathbf{0.67 \angle 129.56^\circ \Omega}}$$

To find $\mathbf{V}_{th}$ and $\mathbf{I}_N$, consider the circuit in Fig. (b).



$$(10 - j10 + j5)\mathbf{I} - (10)(-j2) + j5(2\mathbf{V}_o) - 12 = 0$$

where $\mathbf{V}_o = (10)(-j2 - \mathbf{I})$

Thus,

$$(10 - j105)\mathbf{I} = -188 - j20$$

$$\mathbf{I} = \frac{188 + j20}{-10 + j105}$$

$$\mathbf{V}_{th} = j5(\mathbf{I} + 2\mathbf{V}_o) = j5(21\mathbf{I} + j40) = j105\mathbf{I} - 200$$

$$\mathbf{V}_{th} = \frac{j105(188 + j20)}{-10 + j105} - 200 = -11.802 + j2.076$$

$$\mathbf{V}_{th} = \underline{\underline{11.97\angle 170^\circ \text{ V}}}$$

$$\mathbf{I}_N = \frac{\mathbf{V}_{th}}{\mathbf{Z}_{th}} = \frac{11.97\angle 170^\circ}{0.67\angle 129.56^\circ} = \underline{\underline{17.86\angle 40.44^\circ \text{ A}}}$$

Chapter 10, Solution 67.

$$Z_N = Z_{Th} = 10 \parallel (13 - j5) + 12 \parallel (8 + j6) = \frac{10(13 - j5)}{23 - j5} + \frac{12(8 + j6)}{20 + j6} = \underline{\underline{11.243 + j1.079\Omega}}$$

$$\mathbf{V}_a = \frac{10}{23 - j5}(60\angle 45^\circ) = 13.78 + j21.44, \quad \mathbf{V}_b = \frac{(8 + j6)}{20 + j6}(60\angle 45^\circ) = 25.93 + j454.37\Omega$$

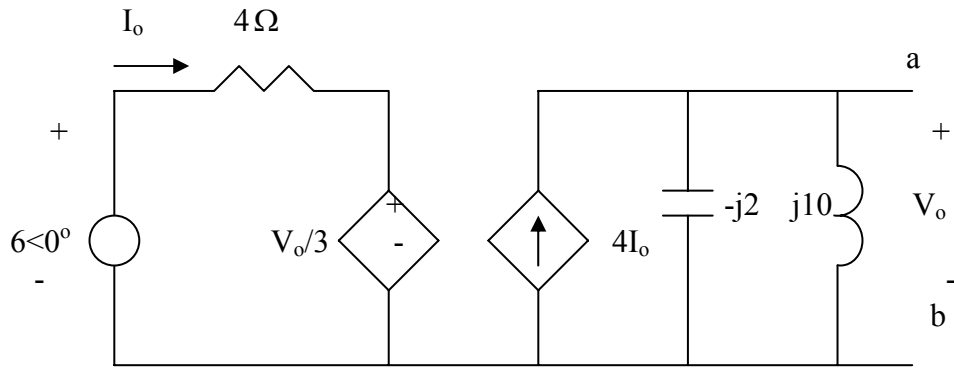
$$\mathbf{V}_{Th} = \mathbf{V}_a - \mathbf{V}_b = \underline{\underline{433.1\angle -1.599^\circ \text{ V}}}, \quad \mathbf{I}_N = \frac{\mathbf{V}_{Th}}{\mathbf{Z}_{Th}} = \underline{\underline{38.34\angle -97.09^\circ \text{ A}}}$$

Chapter 10, Solution 68.

$$1H \longrightarrow j\omega L = j10 \times 1 = j10$$

$$\frac{1}{20}F \longrightarrow \frac{1}{j\omega C} = \frac{1}{j10 \times \frac{1}{20}} = -j2$$

We obtain $\mathbf{V}_{Th}$ using the circuit below.



$$j10 // (-j2) = \frac{j10(-j2)}{j10 - j2} = -j2.5$$

$$V_o = 4I_o \times (-j2.5) = -j10I_o \quad (1)$$

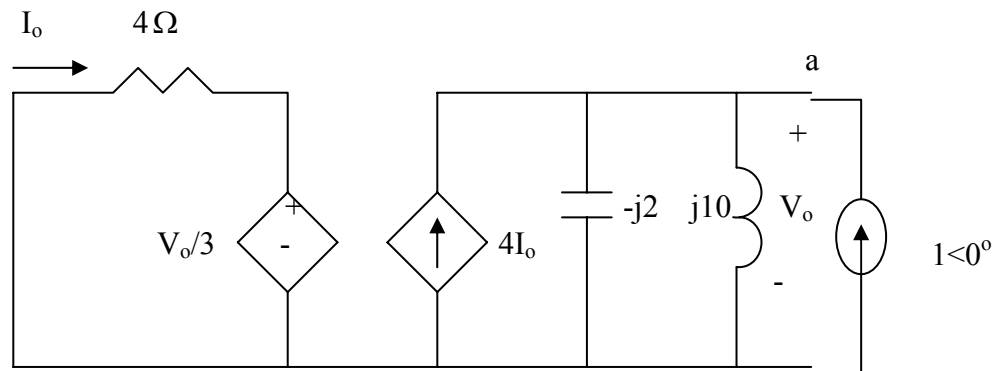
$$-6 + 4I_o + \frac{1}{3}V_o = 0 \quad (2)$$

Combining (1) and (2) gives

$$I_o = \frac{6}{4 - j10/3}, \quad V_{Th} = V_o = -j10I_o = \frac{-j60}{4 - j10/3} = 11.52 \angle -50.19^\circ$$

$$\underline{v_{Th} = 11.52 \sin(10t - 50.19^\circ)}$$

To find R_{Th} , we insert a 1-A source at terminals a-b, as shown below.



$$4I_o + \frac{1}{3}V_o = 0 \quad \longrightarrow \quad I_o = -\frac{V_o}{12}$$

$$1 + 4I_o = \frac{V_o}{-j2} + \frac{V_o}{j10}$$

Combining the two equations leads to

$$V_o = \frac{1}{0.333 + j0.4} = 1.2293 - j1.4766$$

$$Z_{Th} = \frac{V_o}{1} = \underline{1.2293 - j1.477\Omega}$$

Chapter 10, Solution 69.

This is an inverting op amp so that

$$\frac{V_o}{V_s} = \frac{-Z_f}{Z_i} = \frac{-R}{1/j\omega C} = \underline{-j\omega RC}$$

When $V_s = V_m$ and $\omega = 1/RC$,

$$V_o = -j \cdot \frac{1}{RC} \cdot RC \cdot V_m = -jV_m = V_m \angle -90^\circ$$

Therefore,

$$v_o(t) = V_m \sin(\omega t - 90^\circ) = \underline{-V_m \cos(\omega t)}$$

Chapter 10, Solution 70.

This may also be regarded as an inverting amplifier.

$$2 \cos(4 \times 10^4 t) \longrightarrow 2 \angle 0^\circ, \quad \omega = 4 \times 10^4$$

$$10 \text{ nF} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(4 \times 10^4)(10 \times 10^{-9})} = -j2.5 \text{ k}\Omega$$

$$\frac{V_o}{V_s} = \frac{-Z_f}{Z_i}$$

$$\text{where } Z_i = 50 \text{ k}\Omega \text{ and } Z_f = 100\text{k} \parallel (-j2.5\text{k}) = \frac{-j100}{40 - j} \text{ k}\Omega.$$

$$\text{Thus, } \frac{V_o}{V_s} = \frac{-j2}{40 - j}$$

If $V_s = 2 \angle 0^\circ$,

$$V_o = \frac{-j4}{40 - j} = \frac{4 \angle -90^\circ}{40.01 \angle -1.43^\circ} = 0.1 \angle -88.57^\circ$$

Therefore,

$$v_o(t) = \underline{0.1 \cos(4 \times 10^4 t - 88.57^\circ) \text{ V}}$$

Chapter 10, Solution 71.

$$8 \cos(2t + 30^\circ) \longrightarrow 8 \angle 30^\circ$$

$$0.5 \mu\text{F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j2 \times 0.5 \times 10^{-6}} = -j1 \text{ k}\Omega$$

At the inverting terminal,

$$\frac{V_o - 8 \angle 30^\circ}{-j1 \text{ k}} + \frac{V_o - 8 \angle 30^\circ}{10 \text{ k}} = \frac{8 \angle 30^\circ}{2 \text{ k}} \longrightarrow V_o(0.1 + j) = 8 \angle 30^\circ(0.6 + j)$$

$$V_o = \frac{(6.9282 + j4)(0.6 + j)}{0.1 + j} = 9.283 \angle 4.747^\circ$$

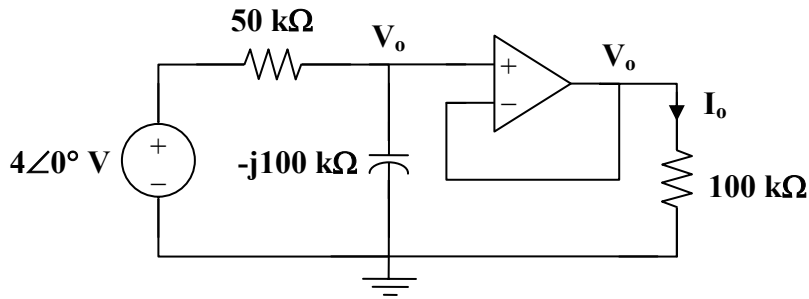
$$v_o(t) = \underline{\underline{9.283 \cos(2t + 4.75^\circ) \text{ V}}}$$

Chapter 10, Solution 72.

$$4 \cos(10^4 t) \longrightarrow 4 \angle 0^\circ, \quad \omega = 10^4$$

$$1 \text{ nF} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(10^4)(10^{-9})} = -j100 \text{ k}\Omega$$

Consider the circuit as shown below.



At the noninverting node,

$$\frac{4 - V_o}{50} = \frac{V_o}{-j100} \longrightarrow V_o = \frac{4}{1 + j0.5}$$

$$I_o = \frac{V_o}{100 \text{ k}} = \frac{4}{(100)(1 + j0.5)} \text{ mA} = 35.78 \angle -26.56^\circ \mu\text{A}$$

Therefore,

$$i_o(t) = \underline{\underline{35.78 \cos(10^4 t - 26.56^\circ) \mu\text{A}}}$$

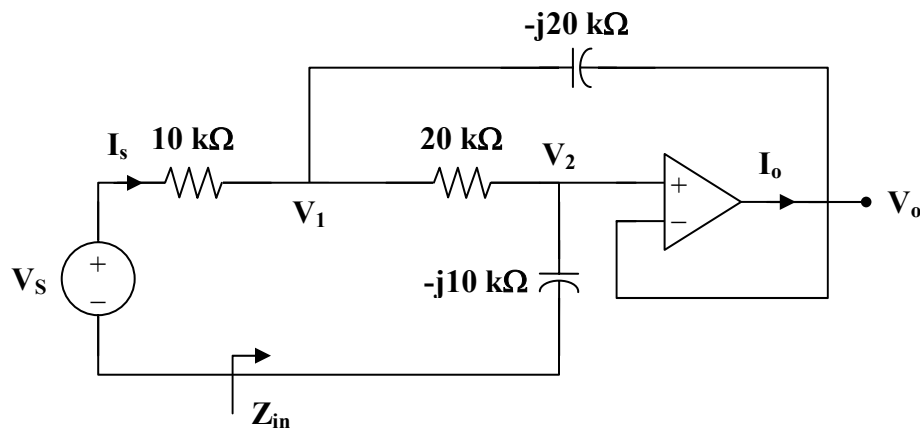
Chapter 10, Solution 73.

As a voltage follower, $V_2 = V_o$

$$C_1 = 10 \text{ nF} \longrightarrow \frac{1}{j\omega C_1} = \frac{1}{j(5 \times 10^3)(10 \times 10^{-9})} = -j20 \text{ k}\Omega$$

$$C_2 = 20 \text{ nF} \longrightarrow \frac{1}{j\omega C_2} = \frac{1}{j(5 \times 10^3)(20 \times 10^{-9})} = -j10 \text{ k}\Omega$$

Consider the circuit in the frequency domain as shown below.



At node 1,

$$\begin{aligned} \frac{V_s - V_1}{10} &= \frac{V_1 - V_o}{-j20} + \frac{V_1 - V_o}{20} \\ 2V_s &= (3 + j)V_1 - (1 + j)V_o \end{aligned} \quad (1)$$

At node 2,

$$\begin{aligned} \frac{V_1 - V_o}{20} &= \frac{V_o - 0}{-j10} \\ V_1 &= (1 + j2)V_o \end{aligned} \quad (2)$$

Substituting (2) into (1) gives

$$2V_s = j6V_o \quad \text{or} \quad V_o = -j\frac{1}{3}V_s$$

$$V_1 = (1 + j2)V_o = \left(\frac{2}{3} - j\frac{1}{3}\right)V_s$$

$$I_s = \frac{V_s - V_1}{10k} = \frac{(1/3)(1 - j)}{10k}V_s$$

$$\frac{\mathbf{I}_s}{\mathbf{V}_s} = \frac{1-j}{30k}$$

$$\mathbf{Z}_{in} = \frac{\mathbf{V}_s}{\mathbf{I}_s} = \frac{30k}{1-j} = 15(1+j)k$$

$$\mathbf{Z}_{in} = \underline{\underline{21.21\angle 45^\circ \text{ k}\Omega}}$$

Chapter 10, Solution 74.

$$\mathbf{Z}_i = \mathbf{R}_1 + \frac{1}{j\omega C_1},$$

$$\mathbf{Z}_f = \mathbf{R}_2 + \frac{1}{j\omega C_2}$$

$$\mathbf{A}_v = \frac{\mathbf{V}_o}{\mathbf{V}_s} = \frac{-\mathbf{Z}_f}{\mathbf{Z}_i} = \frac{\mathbf{R}_2 + \frac{1}{j\omega C_2}}{\mathbf{R}_1 + \frac{1}{j\omega C_1}} = \left(\frac{\mathbf{C}_1}{\mathbf{C}_2} \right) \left(\frac{1 + j\omega \mathbf{R}_2 \mathbf{C}_2}{1 + j\omega \mathbf{R}_1 \mathbf{C}_1} \right)$$

$$\text{At } \omega = 0, \quad \mathbf{A}_v = \underline{\underline{\frac{\mathbf{C}_1}{\mathbf{C}_2}}}$$

$$\text{As } \omega \rightarrow \infty, \quad \mathbf{A}_v = \underline{\underline{\frac{\mathbf{R}_2}{\mathbf{R}_1}}}$$

$$\text{At } \omega = \frac{1}{\mathbf{R}_1 \mathbf{C}_1}, \quad \mathbf{A}_v = \underline{\underline{\left(\frac{\mathbf{C}_1}{\mathbf{C}_2} \right) \left(\frac{1 + j\mathbf{R}_2 \mathbf{C}_2 / \mathbf{R}_1 \mathbf{C}_1}{1 + j} \right)}}$$

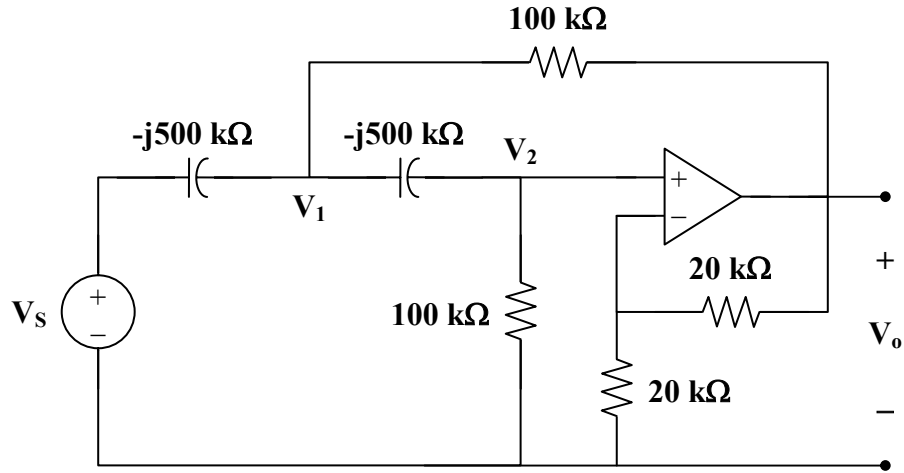
$$\text{At } \omega = \frac{1}{\mathbf{R}_2 \mathbf{C}_2}, \quad \mathbf{A}_v = \underline{\underline{\left(\frac{\mathbf{C}_1}{\mathbf{C}_2} \right) \left(\frac{1 + j}{1 + j\mathbf{R}_1 \mathbf{C}_1 / \mathbf{R}_2 \mathbf{C}_2} \right)}}$$

Chapter 10, Solution 75.

$$\omega = 2 \times 10^3$$

$$\mathbf{C}_1 = \mathbf{C}_2 = 1 \text{ nF} \longrightarrow \frac{1}{j\omega \mathbf{C}_1} = \frac{1}{j(2 \times 10^3)(1 \times 10^{-9})} = -j500 \text{ k}\Omega$$

Consider the circuit shown below.



At node 1,

$$\frac{V_s - V_1}{-j500} = \frac{V_o - V_1}{100} + \frac{V_1 - V_2}{-j500}$$

$$V_s = (2 + j5)V_1 - j5V_o - V_2 \quad (1)$$

At node 2,

$$\frac{V_1 - V_2}{-j500} = \frac{V_2}{100}$$

$$V_1 = (1 - j5)V_2 \quad (2)$$

But

$$V_2 = \frac{R_3}{R_3 + R_4} V_o = \frac{V_o}{2} \quad (3)$$

From (2) and (3),

$$V_1 = \frac{1}{2} \cdot (1 - j5) V_o \quad (4)$$

Substituting (3) and (4) into (1),

$$V_s = \frac{1}{2} \cdot (2 + j5)(1 - j5) V_o - j5 V_o - \frac{1}{2} V_o$$

$$V_s = \frac{1}{2} \cdot (26 - j25) V_o$$

$$\frac{V_o}{V_s} = \frac{2}{26 - j25} = \underline{\underline{0.0554 \angle 43.88^\circ}}$$

Let the voltage between the $-j\text{k}\Omega$ capacitor and the $10\text{k}\Omega$ resistor be V_1 .

$$\frac{2\angle 30^\circ - V_1}{-j4\text{k}} = \frac{V_1 - V_o}{10\text{k}} + \frac{V_1 - V_o}{20\text{k}} \longrightarrow \quad (1)$$

$$2\angle 30^\circ = (1 - j0.6)V_1 + j0.6V_o$$

Also,

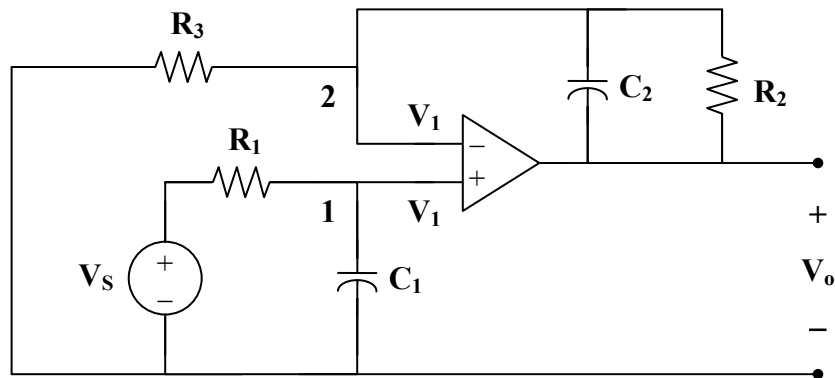
$$\frac{V_1 - V_o}{10\text{k}} = \frac{V_o}{-j2\text{k}} \longrightarrow V_1 = (1 + j5)V_o \quad (2)$$

Solving (2) into (1) yields

$$V_o = 0.047 - j0.3088 = \underline{0.3123\angle -81.34^\circ \text{ V}}$$

Chapter 10, Solution 77.

Consider the circuit below.



At node 1,

$$\frac{V_s - V_1}{R_1} = j\omega C V_1$$

$$V_s = (1 + j\omega R_1 C_1) V_1 \quad (1)$$

At node 2,

$$\frac{0 - V_1}{R_3} = \frac{V_1 - V_o}{R_2} + j\omega C_2 (V_1 - V_o)$$

$$V_1 = (V_o - V_1) \left(\frac{R_3}{R_2} + j\omega C_2 R_3 \right)$$

$$\mathbf{V}_o = \left(1 + \frac{1}{(\mathbf{R}_3/\mathbf{R}_2) + j\omega C_2 \mathbf{R}_3} \right) \mathbf{V}_1 \quad (2)$$

From (1) and (2),

$$\mathbf{V}_o = \frac{\mathbf{V}_s}{1 + j\omega \mathbf{R}_1 \mathbf{C}_1} \left(1 + \frac{\mathbf{R}_2}{\mathbf{R}_3 + j\omega C_2 \mathbf{R}_2 \mathbf{R}_3} \right)$$

$$\frac{\mathbf{V}_o}{\mathbf{V}_s} = \frac{\mathbf{R}_2 + \mathbf{R}_3 + j\omega C_2 \mathbf{R}_2 \mathbf{R}_3}{(1 + j\omega \mathbf{R}_1 \mathbf{C}_1)(\mathbf{R}_3 + j\omega C_2 \mathbf{R}_2 \mathbf{R}_3)}$$

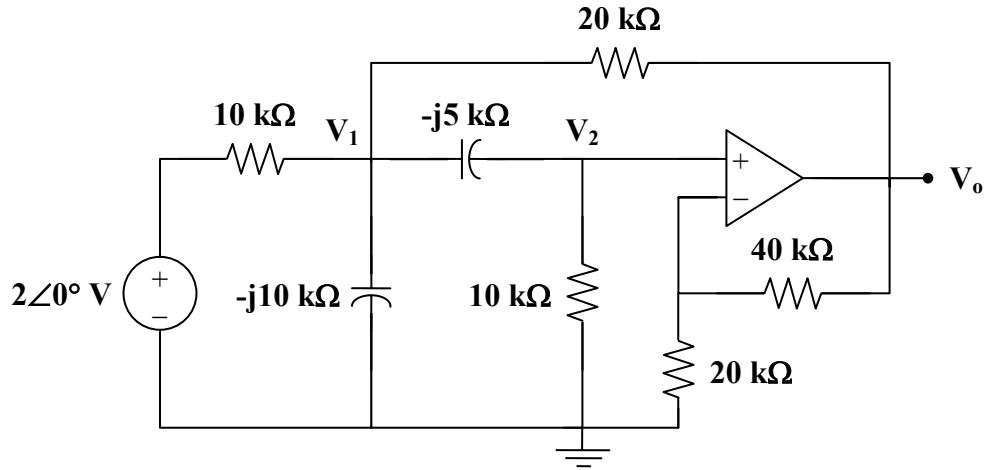
Chapter 10, Solution 78.

$$2 \sin(400t) \longrightarrow 2 \angle 0^\circ, \quad \omega = 400$$

$$0.5 \mu\text{F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(400)(0.5 \times 10^{-6})} = -j5 \text{ k}\Omega$$

$$0.25 \mu\text{F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(400)(0.25 \times 10^{-6})} = -j10 \text{ k}\Omega$$

Consider the circuit as shown below.



At node 1,

$$\begin{aligned} \frac{2 - \mathbf{V}_1}{10} &= \frac{\mathbf{V}_1}{-j10} + \frac{\mathbf{V}_1 - \mathbf{V}_2}{-j5} + \frac{\mathbf{V}_1 - \mathbf{V}_o}{20} \\ 4 &= (3 + j6)\mathbf{V}_1 - j4\mathbf{V}_2 - \mathbf{V}_o \end{aligned} \quad (1)$$

At node 2,

$$\begin{aligned} \frac{\mathbf{V}_1 - \mathbf{V}_2}{-j5} &= \frac{\mathbf{V}_2}{10} \\ \mathbf{V}_1 &= (1 - j0.5)\mathbf{V}_2 \end{aligned} \quad (2)$$

But

$$\mathbf{V}_2 = \frac{20}{20 + 40} \mathbf{V}_o = \frac{1}{3} \mathbf{V}_o \quad (3)$$

From (2) and (3),

$$\mathbf{V}_1 = \frac{1}{3} \cdot (1 - j0.5) \mathbf{V}_o \quad (4)$$

Substituting (3) and (4) into (1) gives

$$4 = (3 + j6) \cdot \frac{1}{3} \cdot (1 - j0.5) \mathbf{V}_o - j\frac{4}{3} \mathbf{V}_o - \mathbf{V}_o = \left(1 - j\frac{1}{6}\right) \mathbf{V}_o$$

$$\mathbf{V}_o = \frac{24}{6 - j} = 3.945 \angle 9.46^\circ$$

Therefore,

$$v_o(t) = \underline{\underline{3.945 \sin(400t + 9.46^\circ) \text{ V}}}$$

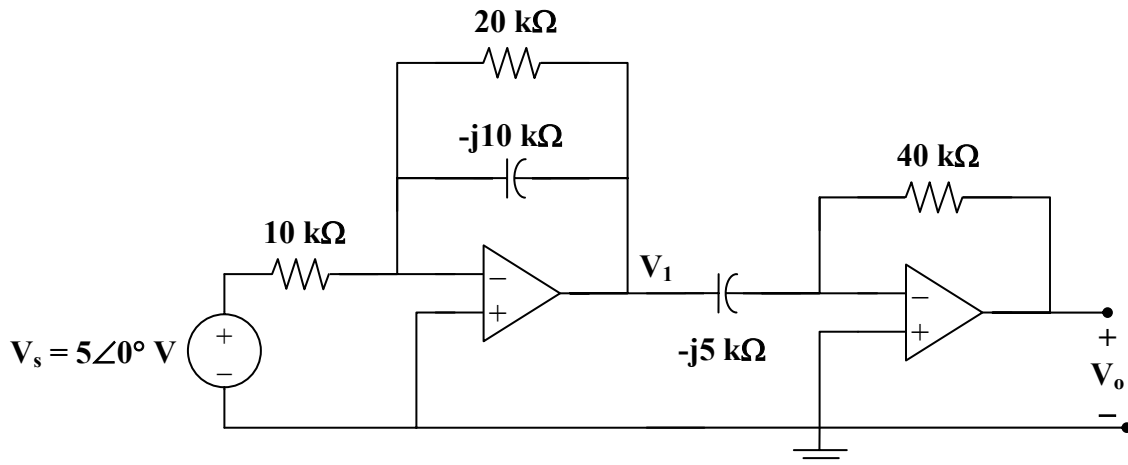
Chapter 10, Solution 79.

$$5 \cos(1000t) \longrightarrow 5 \angle 0^\circ, \quad \omega = 1000$$

$$0.1 \mu\text{F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(1000)(0.1 \times 10^{-6})} = -j10 \text{ k}\Omega$$

$$0.2 \mu\text{F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(1000)(0.2 \times 10^{-6})} = -j5 \text{ k}\Omega$$

Consider the circuit shown below.



Since each stage is an inverter, we apply $\mathbf{V}_o = \frac{-\mathbf{Z}_f}{\mathbf{Z}_i} \mathbf{V}_i$ to each stage.

$$\mathbf{V}_o = \frac{-40}{-j15} \mathbf{V}_1 \quad (1)$$

and

$$\mathbf{V}_1 = \frac{-20 \parallel (-j10)}{10} \mathbf{V}_s \quad (2)$$

From (1) and (2),

$$\mathbf{V}_o = \left(\frac{-j8}{10} \right) \left(\frac{-(20)(-j10)}{20 - j10} \right) 5 \angle 0^\circ$$

$$\mathbf{V}_o = 16(2 + j) = 35.78 \angle 26.56^\circ$$

Therefore, $v_o(t) = \underline{\underline{35.78 \cos(1000t + 26.56^\circ) \text{ V}}}$

Chapter 10, Solution 80.

$$4 \cos(1000t - 60^\circ) \longrightarrow 4 \angle -60^\circ, \quad \omega = 1000$$

$$0.1 \mu\text{F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(1000)(0.1 \times 10^{-6})} = -j10 \text{ k}\Omega$$

$$0.2 \mu\text{F} \longrightarrow \frac{1}{j\omega C} = \frac{1}{j(1000)(0.2 \times 10^{-6})} = -j5 \text{ k}\Omega$$

The two stages are inverters so that

$$\mathbf{V}_o = \left(\frac{20}{-j10} \cdot (4 \angle -60^\circ) + \frac{20}{50} \mathbf{V}_o \right) \left(\frac{-j5}{10} \right)$$

$$= \frac{-j}{2} \cdot (j2) \cdot (4 \angle -60^\circ) + \frac{-j}{2} \cdot \frac{2}{5} \mathbf{V}_o$$

$$(1 + j/5) \mathbf{V}_o = 4 \angle -60^\circ$$

$$\mathbf{V}_o = \frac{4 \angle -60^\circ}{1 + j/5} = 3.922 \angle -71.31^\circ$$

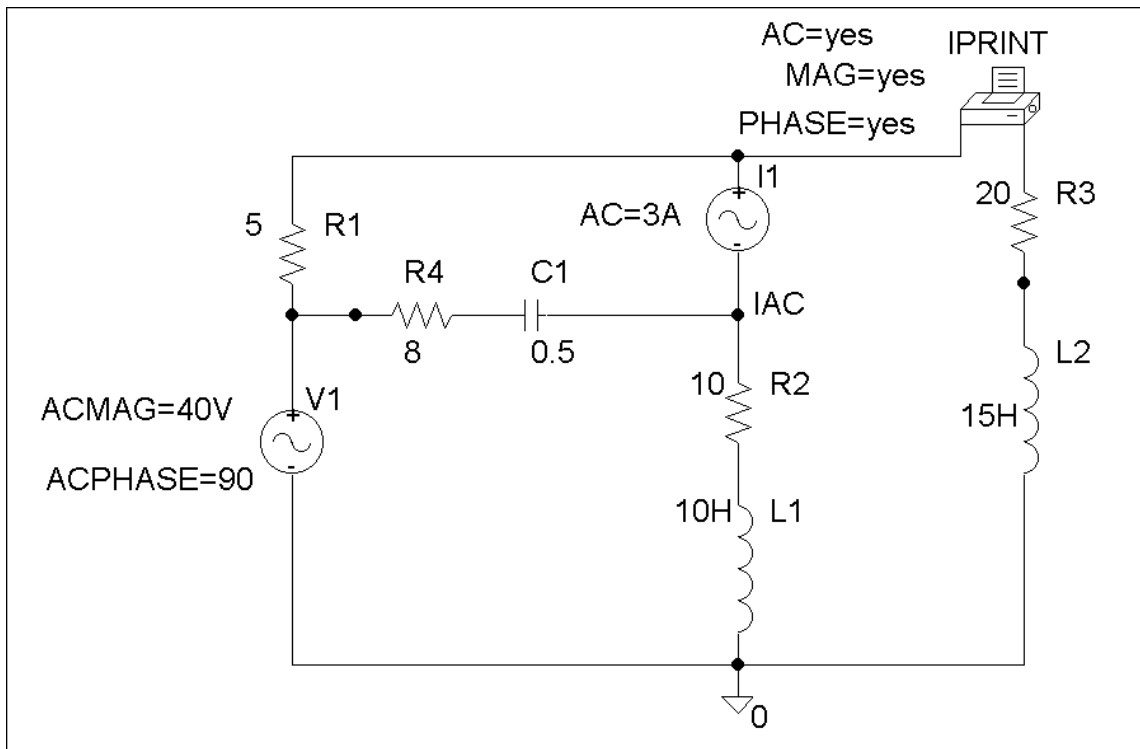
Therefore, $v_o(t) = \underline{\underline{3.922 \cos(1000t - 71.31^\circ) \text{ V}}}$

Chapter 10, Solution 81.

The schematic is shown below. The pseudocomponent IPRINT is inserted to print the value of I_o in the output. We click Analysis/Setup/AC Sweep and set Total Pts. = 1, Start Freq = 0.1592, and End Freq = 0.1592. Since we assume that $\omega = 1$. The output file includes:

FREQ	IM(V_PRINT1)	IP(V_PRINT1)
1.592 E-01	1.465 E+00	7.959 E+01

Thus, $I_o = \underline{1.465 \angle 79.59^\circ \text{ A}}$



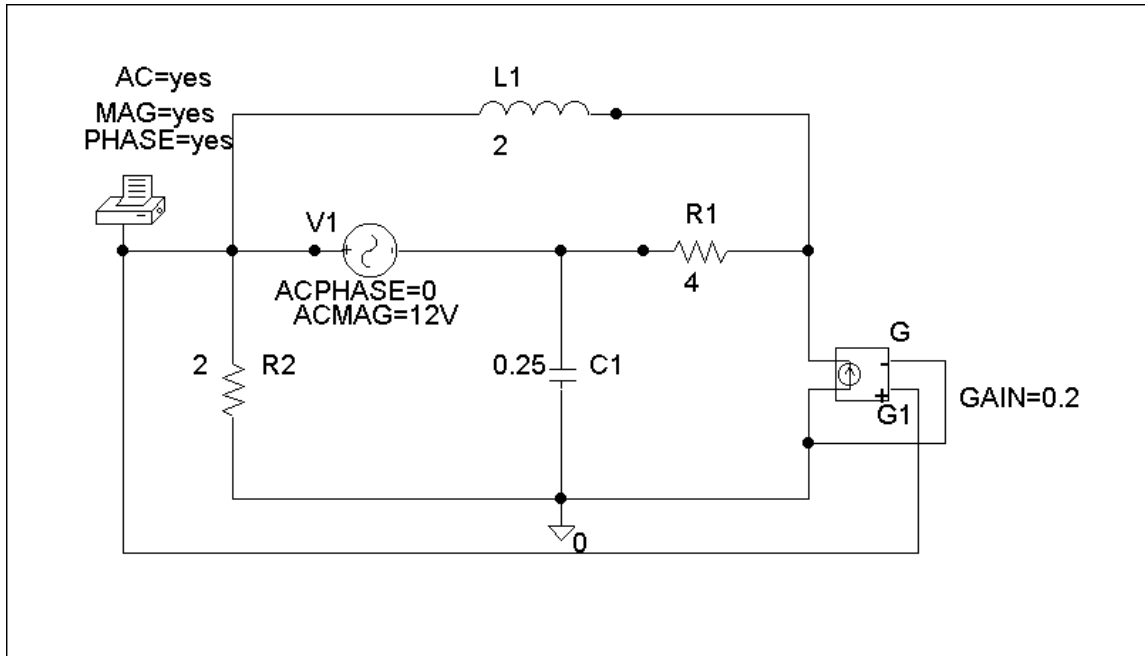
Chapter 10, Solution 82.

The schematic is shown below. We insert PRINT to print V_o in the output file. For AC Sweep, we set Total Pts = 1, Start Freq = 0.1592, and End Freq = 0.1592. After simulation, we print out the output file which includes:

FREQ	VM(\$N_0001)	VP(\$N_0001)
1.592 E-01	7.684 E+00	5.019 E+01

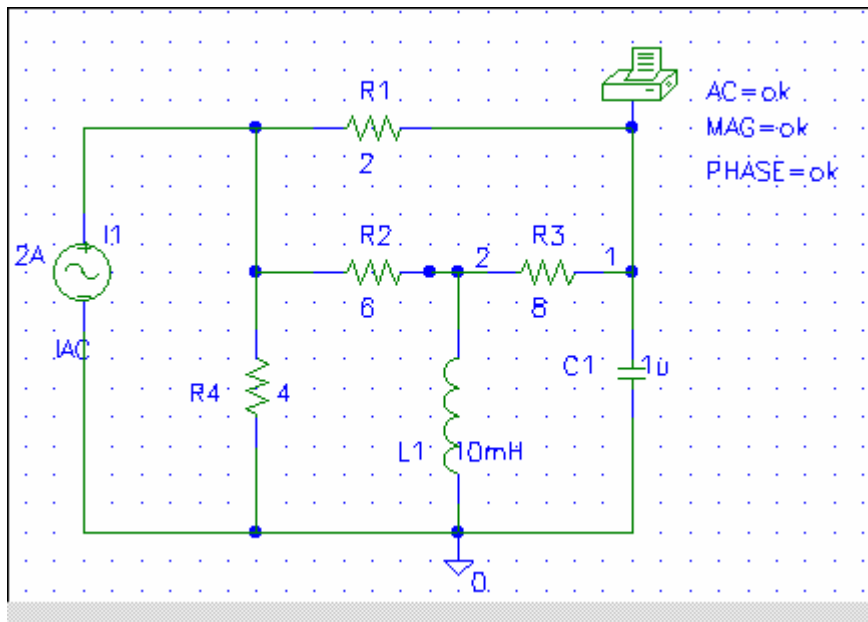
which means that

$$V_o = \underline{7.684 \angle 50.19^\circ \text{ V}}$$



Chapter 10, Solution 83.

The schematic is shown below. The frequency is $f = \omega / 2\pi = \frac{1000}{2\pi} = 159.15$



When the circuit is saved and simulated, we obtain from the output file

FREQ	VM(1)	VP(1)
1.592E+02	6.611E+00	-1.592E+02

Thus,

$$v_o = \underline{6.611 \cos(1000t - 159.2^\circ) \text{ V}}$$

Chapter 10, Solution 84.

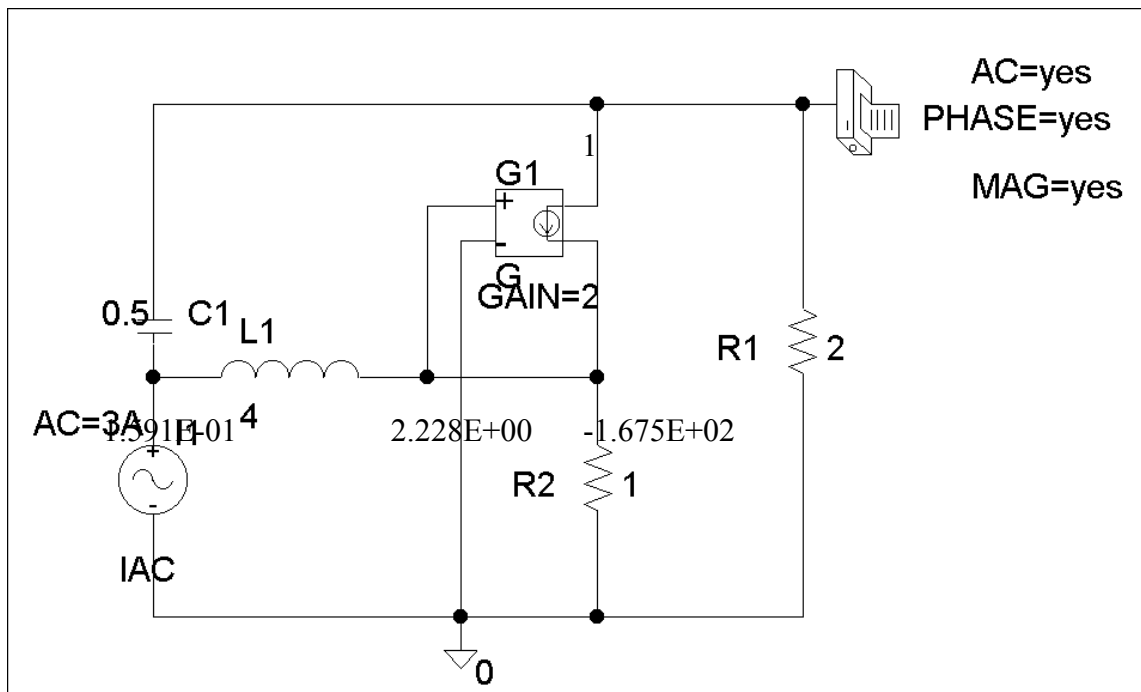
The schematic is shown below. We set PRINT to print V_o in the output file. In AC Sweep box, we set Total Pts = 1, Start Freq = 0.1592, and End Freq = 0.1592. After simulation, we obtain the output file which includes:

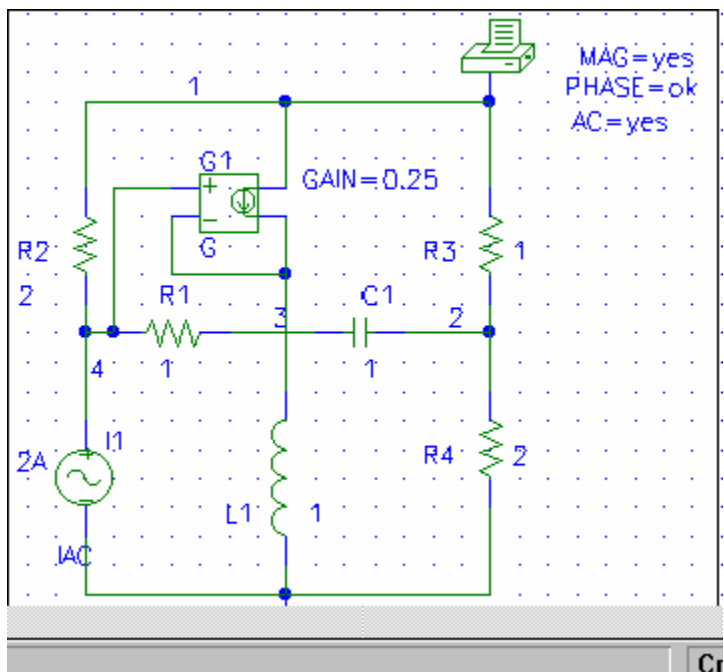
	FREQ	VM(\$N_0003)	
VP(\$N_0003)	1.592 E-01	1.664 E+00	-1.646
E+02			

Namely,

$$V_o = \underline{1.664 \angle -146.4^\circ \text{ V}}$$

Chapter 10, Solution 85.





Chapter 10, Solution 86.

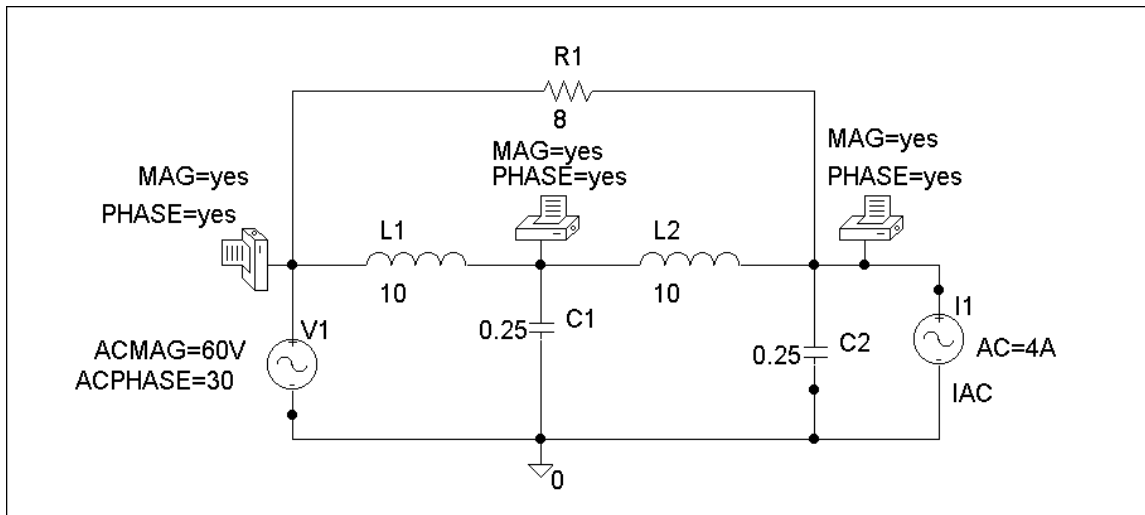
We insert three pseudocomponent PRINTs at nodes 1, 2, and 3 to print V_1 , V_2 , and V_3 , into the output file. Assume that $w = 1$, we set Total Pts = 1, Start Freq = 0.1592, and End Freq = 0.1592. After saving and simulating the circuit, we obtain the output file which includes:

	FREQ	VM(\$N_0002)	
VP(\$N_0002)	1.592 E-01	6.000 E+01	3.000
E+01			
	FREQ	VM(\$N_0003)	
VP(\$N_0003)	1.592 E-01	2.367 E+02	-8.483
E+01			

		FREQ	VM(\$N_0001)
VP(\$N_0001)		1.592 E-01	1.082 E+02
E+02			1.254

Therefore,

$$V_1 = \underline{60\angle 30^\circ \text{ V}} \quad V_2 = \underline{236.7\angle -84.83^\circ \text{ V}} \quad V_3 = \underline{108.2\angle 125.4^\circ \text{ V}}$$



Chapter 10, Solution 87.

The schematic is shown below. We insert three PRINTs at nodes 1, 2, and 3. We set Total Pts = 1, Start Freq = 0.1592, End Freq = 0.1592 in the AC Sweep box. After simulation, the output file includes:

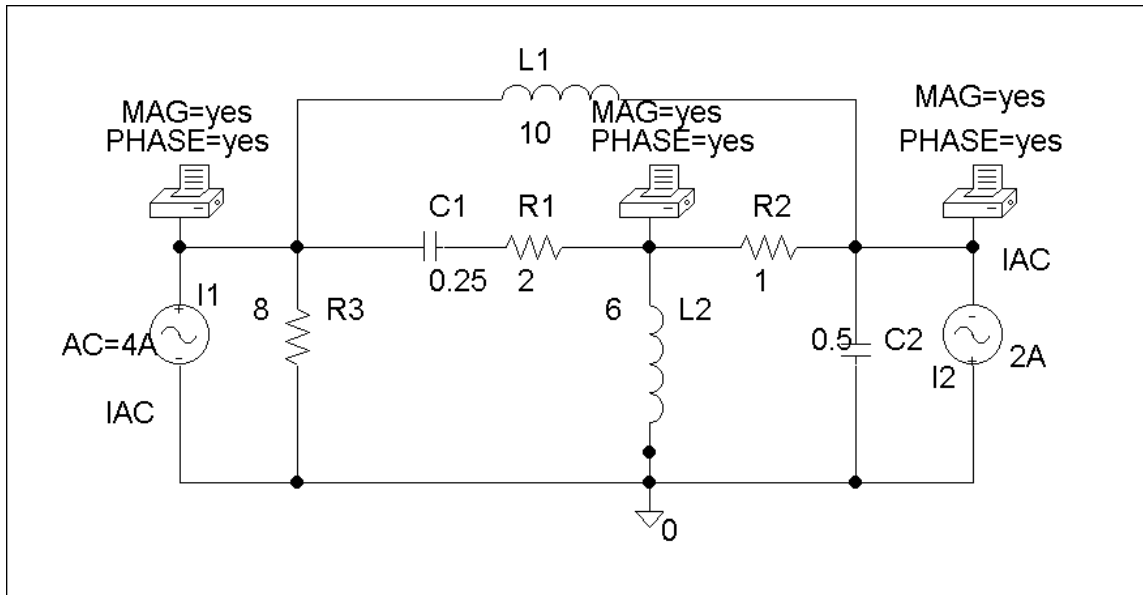
		FREQ	VM(\$N_0004)
VP(\$N_0004)		1.592 E-01	1.591 E+01
E+02			1.696

		FREQ	VM(\$N_0001)
VP(\$N_0001)		1.592 E-01	5.172 E+00
E+02			-1.386

VP(\$N_0003)	FREQ	VM(\$N_0003)	
	1.592 E-01	2.270 E+00	-1.524
E+02			

Therefore,

$$V_1 = \underline{15.91\angle 169.6^\circ \text{ V}} \quad V_2 = \underline{5.172\angle -138.6^\circ \text{ V}} \quad V_3 = \underline{2.27\angle -152.4^\circ \text{ V}}$$



Chapter 10, Solution 88.

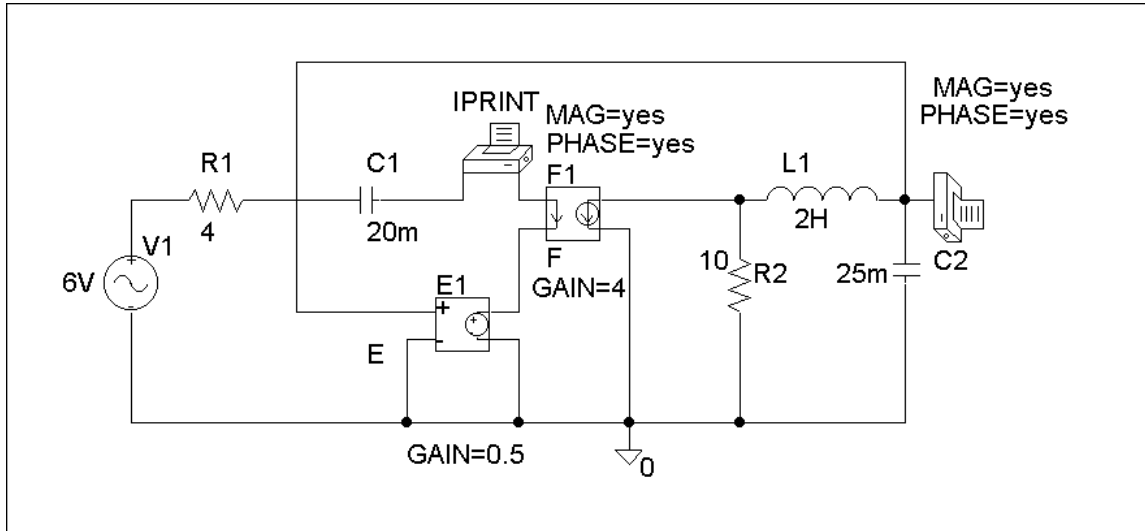
The schematic is shown below. We insert IPRINT and PRINT to print I_o and V_o in the output file. Since $\omega = 4$, $f = \omega/2\pi = 0.6366$, we set Total Pts = 1, Start Freq = 0.6366, and End Freq = 0.6366 in the AC Sweep box. After simulation, the output file includes:

VP(\$N_0002)	FREQ	VM(\$N_0002)	
	6.366 E-01	3.496 E+01	1.261
E+01			

(V_PRINT2)	FREQ	IM(V_PRINT2)	IP
	6.366 E-01	8.912 E-01	
-8.870 E+01			

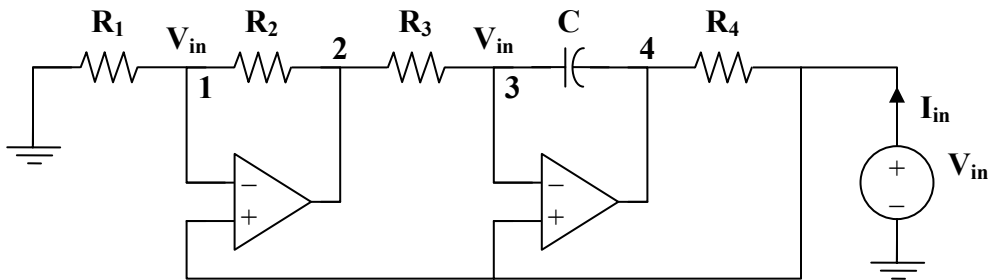
Therefore, $V_o = 34.96\angle 12.6^\circ \text{ V}$, $I_o = 0.8912\angle -88.7^\circ \text{ A}$

$$v_o = \underline{34.96 \cos(4t + 12.6^\circ) \text{ V}}, \quad i_o = \underline{0.8912 \cos(4t - 88.7^\circ) \text{ A}}$$



Chapter 10, Solution 89.

Consider the circuit below.



At node 1,

$$\frac{0 - V_{in}}{R_1} = \frac{V_{in} - V_2}{R_2}$$

$$-V_{in} + V_2 = \frac{R_2}{R_1} V_{in} \quad (1)$$

At node 3,

$$\frac{V_2 - V_{in}}{R_3} = \frac{V_{in} - V_4}{1/j\omega C}$$

$$-V_{in} + V_4 = \frac{V_{in} - V_2}{j\omega CR_3} \quad (2)$$

From (1) and (2),

$$-V_{in} + V_4 = \frac{-R_2}{j\omega CR_3 R_1} V_{in}$$

Thus,

$$I_{in} = \frac{V_{in} - V_4}{R_4} = \frac{R_2}{j\omega CR_3 R_1 R_4} V_{in}$$

$$Z_{in} = \frac{V_{in}}{I_{in}} = \frac{j\omega CR_1 R_3 R_4}{R_2} = j\omega L_{eq}$$

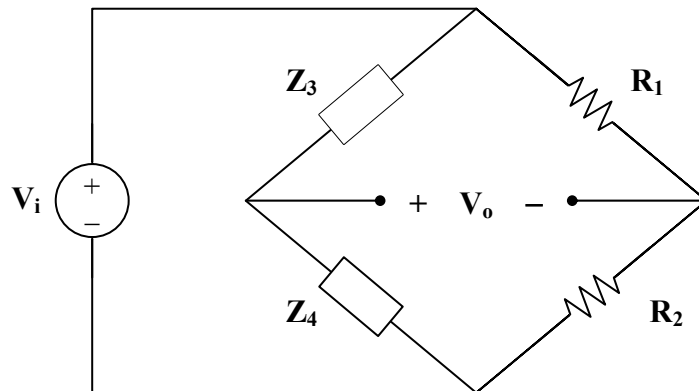
$$\text{where } L_{eq} = \frac{R_1 R_3 R_4 C}{R_2}$$

Chapter 10, Solution 90.

$$\text{Let } Z_4 = R \parallel \frac{1}{j\omega C} = \frac{R}{1 + j\omega RC}$$

$$Z_3 = R + \frac{1}{j\omega C} = \frac{1 + j\omega RC}{j\omega C}$$

Consider the circuit shown below.



$$\mathbf{V}_o = \frac{\mathbf{Z}_4}{\mathbf{Z}_3 + \mathbf{Z}_4} \mathbf{V}_i - \frac{\mathbf{R}_2}{\mathbf{R}_1 + \mathbf{R}_2} \mathbf{V}_i$$

$$\frac{\mathbf{V}_o}{\mathbf{V}_i} = \frac{\frac{\mathbf{R}}{1 + j\omega\mathbf{C}}}{\frac{\mathbf{R}}{1 + j\omega\mathbf{C}} + \frac{1 + j\omega\mathbf{R}\mathbf{C}}{j\omega\mathbf{C}}} - \frac{\mathbf{R}_2}{\mathbf{R}_1 + \mathbf{R}_2}$$

$$= \frac{j\omega\mathbf{R}\mathbf{C}}{j\omega\mathbf{R}\mathbf{C} + (1 + j\omega\mathbf{R}\mathbf{C})^2} - \frac{\mathbf{R}_2}{\mathbf{R}_1 + \mathbf{R}_2}$$

$$\frac{\mathbf{V}_o}{\mathbf{V}_i} = \frac{j\omega\mathbf{R}\mathbf{C}}{1 - \omega^2\mathbf{R}^2\mathbf{C}^2 + j\omega\mathbf{R}\mathbf{C}} - \frac{\mathbf{R}_2}{\mathbf{R}_1 + \mathbf{R}_2}$$

For $\mathbf{V}_o$ and $\mathbf{V}_i$ to be in phase, $\frac{\mathbf{V}_o}{\mathbf{V}_i}$ must be purely real. This happens when

$$1 - \omega^2\mathbf{R}^2\mathbf{C}^2 = 0$$

$$\omega = \frac{1}{\mathbf{R}\mathbf{C}} = 2\pi f$$

or $f = \frac{1}{2\pi\mathbf{R}\mathbf{C}}$

At this frequency,

$$\mathbf{A}_v = \frac{\mathbf{V}_o}{\mathbf{V}_i} = \frac{1}{3} - \frac{\mathbf{R}_2}{\mathbf{R}_1 + \mathbf{R}_2}$$

Chapter 10, Solution 91.

(a) Let $\mathbf{V}_2$ = voltage at the noninverting terminal of the op amp

$\mathbf{V}_o$ = output voltage of the op amp

$$\mathbf{Z}_p = 10 \text{ k}\Omega = \mathbf{R}_o$$

$$\mathbf{Z}_s = \mathbf{R} + j\omega\mathbf{L} + \frac{1}{j\omega\mathbf{C}}$$

As in Section 10.9,

$$\frac{V_2}{V_o} = \frac{Z_p}{Z_s + Z_p} = \frac{R_o}{R + R_o + j\omega L - \frac{j}{\omega C}}$$

$$\frac{V_2}{V_o} = \frac{\omega C R_o}{\omega C (R + R_o) + j(\omega^2 LC - 1)}$$

For this to be purely real,

$$\omega_o^2 LC - 1 = 0 \longrightarrow \omega_o = \frac{1}{\sqrt{LC}}$$

$$f_o = \frac{1}{2\pi\sqrt{LC}} = \frac{1}{2\pi\sqrt{(0.4 \times 10^{-3})(2 \times 10^{-9})}}$$

$$f_o = \underline{\underline{180 \text{ kHz}}}$$

(b) At oscillation,

$$\frac{V_2}{V_o} = \frac{\omega_o C R_o}{\omega_o C (R + R_o)} = \frac{R_o}{R + R_o}$$

This must be compensated for by

$$A_v = \frac{V_o}{V_2} = 1 + \frac{80}{20} = 5$$

$$\frac{R_o}{R + R_o} = \frac{1}{5} \longrightarrow R = 4R_o = \underline{\underline{40 \text{ k}\Omega}}$$

Chapter 10, Solution 92.

Let V_2 = voltage at the noninverting terminal of the op amp

V_o = output voltage of the op amp

$$Z_s = R_o$$

$$Z_p = j\omega L \parallel \frac{1}{j\omega C} \parallel R = \frac{1}{\frac{1}{R} + j\omega C + \frac{1}{j\omega L}} = \frac{\omega RL}{\omega L + jR(\omega^2 LC - 1)}$$

As in Section 10.9,

$$\frac{V_2}{V_o} = \frac{Z_p}{Z_s + Z_p} = \frac{\frac{\omega RL}{\omega L + jR(\omega^2 LC - 1)}}{R_o + \frac{\omega RL}{\omega L + jR(\omega^2 LC - 1)}}$$

$$\frac{V_2}{V_o} = \frac{\omega RL}{\omega RL + \omega R_o L + jR_o R (\omega^2 LC - 1)}$$

For this to be purely real,

$$\omega_o^2 LC = 1 \longrightarrow f_o = \frac{1}{2\pi\sqrt{LC}}$$

(a) At $\omega = \omega_o$,

$$\frac{V_2}{V_o} = \frac{\omega_o RL}{\omega_o RL + \omega_o R_o L} = \frac{R}{R + R_o}$$

This must be compensated for by

$$A_v = \frac{V_o}{V_2} = 1 + \frac{R_f}{R_o} = 1 + \frac{1000k}{100k} = 11$$

Hence,

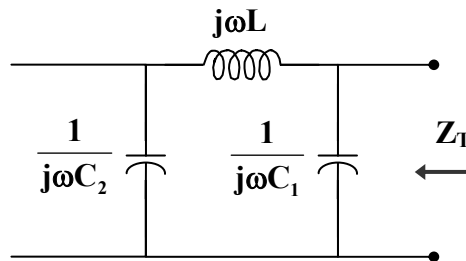
$$\frac{R}{R + R_o} = \frac{1}{11} \longrightarrow R_o = 10R = \underline{\underline{100 \text{ k}\Omega}}$$

$$(b) \quad f_o = \frac{1}{2\pi\sqrt{(10 \times 10^{-6})(2 \times 10^{-9})}}$$

$$f_o = \underline{\underline{1.125 \text{ MHz}}}$$

Chapter 10, Solution 93.

As shown below, the impedance of the feedback is



$$Z_T = \frac{1}{j\omega C_1} \parallel \left(j\omega L + \frac{1}{j\omega C_2} \right)$$

$$\mathbf{Z}_T = \frac{\frac{-j}{\omega C_1} \left(j\omega L + \frac{-j}{\omega C_2} \right)}{\frac{-j}{\omega C_1} + j\omega L + \frac{-j}{\omega C_2}} = \frac{\frac{1}{\omega} - \omega L C_2}{j(C_1 + C_2 - \omega^2 L C_1 C_2)}$$

In order for $\mathbf{Z}_T$ to be real, the imaginary term must be zero; i.e.

$$C_1 + C_2 - \omega_0^2 L C_1 C_2 = 0$$

$$\omega_0^2 = \frac{C_1 + C_2}{L C_1 C_2} = \frac{1}{L C_T}$$

$$\underline{\underline{f_o = \frac{1}{2\pi\sqrt{L C_T}}}}$$

Chapter 10, Solution 94.

If we select $C_1 = C_2 = 20 \text{ nF}$

$$C_T = \frac{C_1 C_2}{C_1 + C_2} = \frac{C_1}{2} = 10 \text{ nF}$$

Since $f_o = \frac{1}{2\pi\sqrt{L C_T}}$,

$$L = \frac{1}{(2\pi f)^2 C_T} = \frac{1}{(4\pi^2)(2500 \times 10^6)(10 \times 10^{-9})} = 10.13 \text{ mH}$$

$$X_c = \frac{1}{\omega C_2} = \frac{1}{(2\pi)(50 \times 10^3)(20 \times 10^{-9})} = 159 \Omega$$

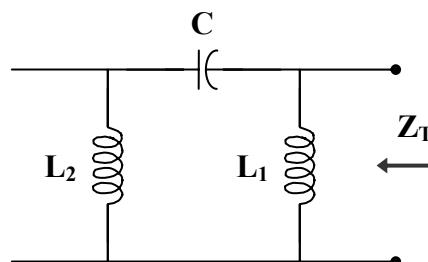
We may select $R_i = 20 \text{ k}\Omega$ and $R_f \geq R_i$, say $R_f = 20 \text{ k}\Omega$.

Thus,

$$C_1 = C_2 = \underline{\underline{20 \text{ nF}}}, \quad L = \underline{\underline{10.13 \text{ mH}}} \quad R_f = R_i = \underline{\underline{20 \text{ k}\Omega}}$$

Chapter 10, Solution 95.

First, we find the feedback impedance.



$$\mathbf{Z}_T = j\omega L_1 \parallel \left(j\omega L_2 + \frac{1}{j\omega C} \right)$$

$$\mathbf{Z}_T = \frac{j\omega L_1 \left(j\omega L_2 - \frac{j}{\omega C} \right)}{j\omega L_1 + j\omega L_2 - \frac{j}{\omega C}} = \frac{\omega^2 L_1 C (1 - \omega L_2)}{j(\omega^2 C (L_1 + L_2) - 1)}$$

In order for $\mathbf{Z}_T$ to be real, the imaginary term must be zero; i.e.

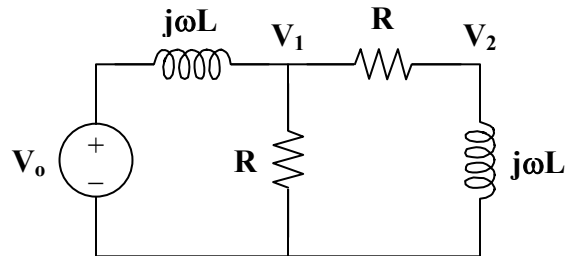
$$\omega_o^2 C (L_1 + L_2) - 1 = 0$$

$$\omega_o = 2\pi f_o = \frac{1}{C(L_1 + L_2)}$$

$$\underline{f_o = \frac{1}{2\pi\sqrt{C(L_1 + L_2)}}}$$

Chapter 10, Solution 96.

- (a) Consider the feedback portion of the circuit, as shown below.



$$\mathbf{V}_2 = \frac{j\omega L}{R + j\omega L} \mathbf{V}_1 \longrightarrow \mathbf{V}_1 = \frac{R + j\omega L}{j\omega L} \mathbf{V}_2 \quad (1)$$

Applying KCL at node 1,

$$\frac{\mathbf{V}_o - \mathbf{V}_1}{j\omega L} = \frac{\mathbf{V}_1}{R} + \frac{\mathbf{V}_1}{R + j\omega L}$$

$$\mathbf{V}_o - \mathbf{V}_1 = j\omega L \mathbf{V}_1 \left(\frac{1}{R} + \frac{1}{R + j\omega L} \right)$$

$$\mathbf{V}_o = \mathbf{V}_1 \left(1 + \frac{j2\omega RL - \omega^2 L^2}{R(R + j\omega L)} \right)$$

(2)

From (1) and (2),

$$\mathbf{V}_o = \left(\frac{R + j\omega L}{j\omega L} \right) \left(1 + \frac{j2\omega RL - \omega^2 L^2}{R(R + j\omega L)} \right) \mathbf{V}_2$$

$$\frac{\mathbf{V}_o}{\mathbf{V}_2} = \frac{R^2 + j\omega RL + j2\omega RL - \omega^2 L^2}{j\omega RL}$$

$$\frac{\mathbf{V}_2}{\mathbf{V}_o} = \frac{1}{3 + \frac{R^2 - \omega^2 L^2}{j\omega RL}}$$

$$\frac{\mathbf{V}_2}{\mathbf{V}_o} = \frac{\mathbf{1}}{\mathbf{3 + j(\omega L/R - R/\omega L)}}$$

(b) Since the ratio $\frac{\mathbf{V}_2}{\mathbf{V}_o}$ must be real,

$$\frac{\omega_o L}{R} - \frac{R}{\omega_o L} = 0$$

$$\omega_o L = \frac{R^2}{\omega_o L}$$

$$\omega_o = 2\pi f_o = \frac{R}{L}$$

$$\underline{\mathbf{f}_o = \frac{\mathbf{R}}{2\pi \mathbf{L}}}$$

(c) When $\omega = \omega_o$

$$\frac{\mathbf{V}_2}{\mathbf{V}_o} = \frac{1}{3}$$

This must be compensated for by $\mathbf{A}_v = 3$. But

$$\mathbf{A}_v = 1 + \frac{\mathbf{R}_2}{\mathbf{R}_1} = 3$$

$$\underline{\mathbf{R}_2 = 2 \mathbf{R}_1}$$