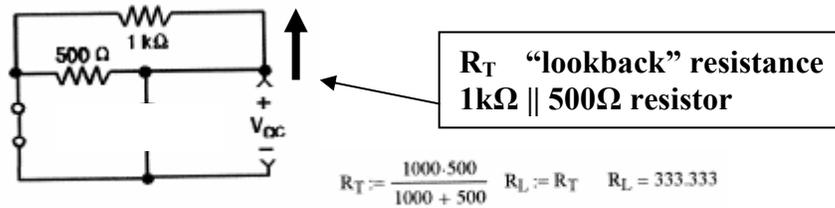


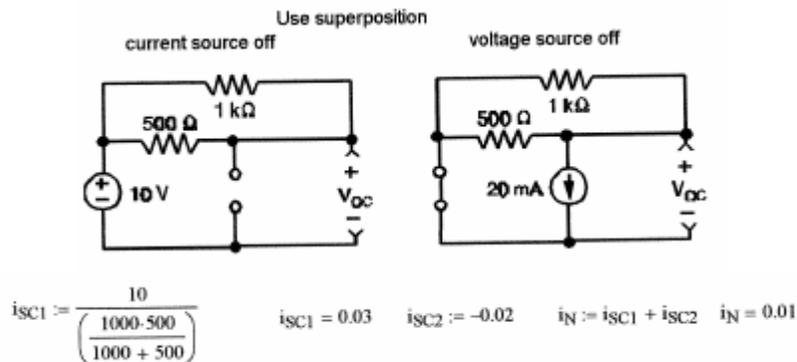
## Homework Solutions 6

(3-52) Find the maximum power available to the load resistance in the Figure P3-52. What is the value of  $R_L$  will extract maximum power?

*Step (1) Find the Thevenin (“lookback”) resistance, open the current source and short the voltage source, then find the resistance by looking back into the circuit from the load.*



*Step (2) Using superposition to find the two different  $I_{sc}$  (short circuit) currents. Therefore, open the current source and use the voltage source to find the first short circuit current. Next short the voltage source and use the current source to find the second short circuit current.*

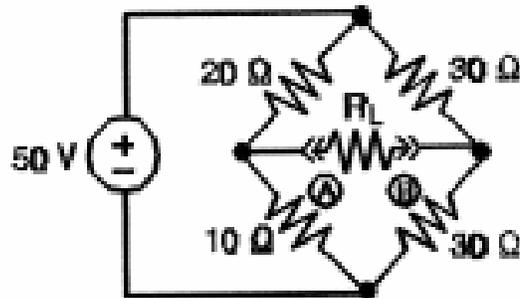


**Simply add  $i_{sc1}$  to  $i_{sc2}$  to find the total  $i_{sc} \rightarrow i_N$**

Using the equation  $P_{max} = (0.25) \cdot i_N^2 \cdot R_T = (0.25) \cdot (0.01)^2 \cdot 333.33 = 8.333 \text{mW}$   
 Therefore,  $P_{max} = \underline{\underline{8.333 \text{mW}}}$ .

(3-53) Find the maximum power available to the load resistance in Figure P3-53. What is the value of  $R_L$  will extract the maximum power?

*First find the “lookback” resistance in the wheatstone bridge, open the load and short the voltage source. Now find the resistance in the path from terminal A to terminal B.*



Finding the equivalent “lookback” resistance or Thevenin resistance is quite hard to visualize but if you rearrange the circuit drawing enough you can clearly see that  $10\Omega \parallel 20\Omega$  which is in series with the  $30\Omega \parallel 30\Omega$ . Therefore,

$$R_T := \frac{10 \cdot 20}{10 + 20} + \frac{30 \cdot 30}{30 + 30}$$

**$R_T = 21.67\Omega$**

Next, consider finding the Thevenin voltage  $V_T$  which is the voltage across terminal A and terminal B:

$$V_T = V_A - V_B$$

Find the voltage at A and B using voltage division;

$$v_{AB} := \frac{10}{10 + 20} \cdot 50 - \frac{30}{30 + 30} \cdot 50 \quad v_{AB} = -8.333$$

Therefore,  **$V_T = V_{AB} = -8.3333$**

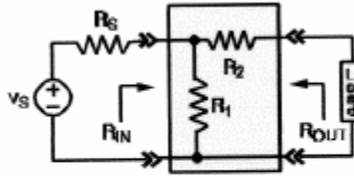
Now, solve for  $i_N = V_T / R_T = -0.3846A$

And,

**$P_{max} = (0.25) \cdot (-0.3846A)^2 \cdot 21.67\Omega = \underline{0.801W}$**

(3-64) In Figure P3-61 the load is a 500Ω resistor and the  $R_S = 75\Omega$ . Design an interface circuit so that the input resistance of the two port is  $75\Omega \pm 10\%$  and the output resistance seen by the load is  $500\Omega \pm 10\%$ .

3-64  $R_S := 75$   $R_L := 500$



First guess let:  $R_1 := 75$   $R_2 := 500$

$$R_{IN} := \frac{R_1 \cdot (R_2 + R_L)}{R_1 + R_2 + R_L} \quad R_{IN} = 69.767$$

$$R_{OUT} := R_2 + \frac{R_1 \cdot R_S}{R_1 + R_S} \quad R_{OUT} = 537.5$$

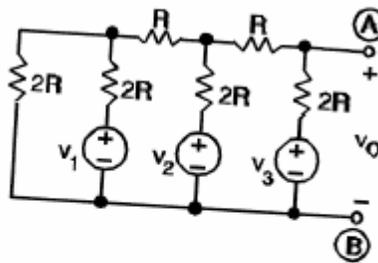
Both answers are with  $\pm 10\%$

$$\text{Given } \frac{R_1 \cdot (R_2 + 500)}{R_1 + R_2 + 500} = 75 \quad R_2 + \frac{R_1 \cdot 75}{R_1 + 75} = 500 \quad \text{Find}(R_1, R_2) = \begin{pmatrix} 81.349 \\ 460.977 \end{pmatrix} \quad \leftarrow \text{exact solutions}$$

The best way to solve these design problems is to try each Interface Circuit equivalent shown in Figure 3-52 on pg. 118 of the text. Since this is a design problem you can guess some values and use logic into which is the best interface circuit to use for specifications required.

(3-71) Comparison of Analysis Methods for (a), (b), (c); problem statement located in the text

The maximum power available is less than 1 mW. Hence no interface circuit is required.  
3-71 (a) Writing node-voltage equations:



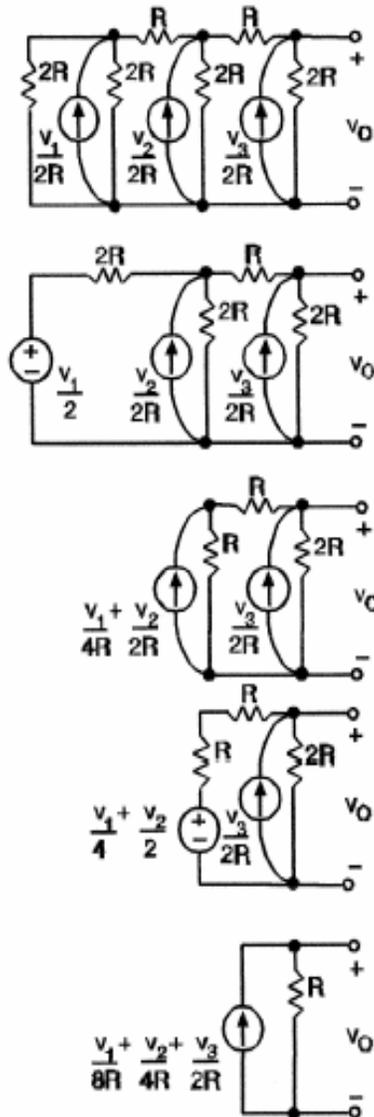
$$\begin{pmatrix} \frac{2}{R} & \frac{1}{R} & 0 \\ \frac{1}{R} & \frac{5}{2R} & \frac{1}{R} \\ 0 & \frac{1}{R} & \frac{3}{2R} \end{pmatrix} \begin{pmatrix} v_A \\ v_B \\ v_C \end{pmatrix} = \begin{pmatrix} \frac{v_1}{2R} \\ \frac{v_2}{2R} \\ \frac{v_3}{2R} \end{pmatrix}$$

Solving for the node-voltage vector

$$\begin{pmatrix} v_A \\ v_B \\ v_C \end{pmatrix} = \begin{pmatrix} \frac{2}{R} & \frac{1}{R} & 0 \\ \frac{1}{R} & \frac{5}{2R} & \frac{1}{R} \\ 0 & \frac{1}{R} & \frac{3}{2R} \end{pmatrix}^{-1} \begin{pmatrix} \frac{v_1}{2R} \\ \frac{v_2}{2R} \\ \frac{v_3}{2R} \end{pmatrix} = \begin{pmatrix} \frac{11}{16}R & \frac{3}{8}R & \frac{1}{4}R \\ \frac{3}{8}R & \frac{3}{4}R & \frac{1}{2}R \\ \frac{1}{4}R & \frac{1}{2}R & R \end{pmatrix} \begin{pmatrix} \frac{v_1}{2R} \\ \frac{v_2}{2R} \\ \frac{v_3}{2R} \end{pmatrix} = \begin{pmatrix} \frac{11}{32}v_1 + \frac{3}{16}v_2 + \frac{1}{8}v_3 \\ \frac{3}{16}v_1 + \frac{3}{8}v_2 + \frac{1}{4}v_3 \\ \frac{1}{8}v_1 + \frac{1}{4}v_2 + \frac{1}{2}v_3 \end{pmatrix} \quad \leftarrow \text{output}$$

$$\text{Hence } v_O = v_C = \frac{1}{8}v_1 + \frac{1}{4}v_2 + \frac{1}{2}v_3$$

3-71 (b) Using circuit reduction methods



Step 1: Convert the voltage sources in series with  $2R$  to equivalent current sources in parallel

Step 2: Replace left-most  $2R||2R$  by a single resistor  $R$  and then convert the left-most current source to an equivalent voltage source  $v_1/2$  in series with  $R + R = 2R$ .

Step 3: Convert the left-most voltage source to an equivalent current source in parallel with  $2R$  and then combine the two left-most current sources that are connected in parallel to an equivalent current source  $\frac{v_1}{4 \cdot R} + \frac{v_2}{2 \cdot R}$  connected in parallel with  $2R||2R = R$

Step 4: Convert the left-most current source to an equivalent voltage source  $\frac{v_1}{4} + \frac{v_2}{2}$  in parallel with  $R$ .

Step 5: Convert the left most voltage source in series with  $2R$  to an equivalent current source  $\frac{v_1}{8 \cdot R} + \frac{v_2}{4 \cdot R}$  in parallel with  $2R$  and then combine with the right most current source to produce an equivalent current source  $\frac{v_1}{8 \cdot R} + \frac{v_2}{4 \cdot R} + \frac{v_3}{2 \cdot R}$  in parallel with  $R$ .

$$\text{Hence } v_O = \left( \frac{v_1}{8 \cdot R} + \frac{v_2}{4 \cdot R} + \frac{v_3}{2 \cdot R} \right) \cdot R = \frac{1}{8} \cdot v_1 + \frac{1}{4} \cdot v_2 + \frac{1}{2} \cdot v_3$$

(c) Either method is acceptable. Method (a) is analytical and abstract. Method (b) is more intuitive since it works directly with the circuit model.

(4-4) The circuit in Figure P4-4 is an ideal voltage amplifier with the negative feedback provided via the resistor  $R_F$ .

- (a) Find the output voltage  $V_2$  and the current gain  $i_2 / i_1$  when  $V_s = 10\text{mV}$  and  $R_F = 10\text{k}\Omega$ .  
 (b) Find the input resistance  $R_{IN} = v_1 / i_1$ .

4-4  $R_F := 10 \cdot 10^3$   $v_s := 0.01$  (a) Writing a KCL equation at Node A yields:

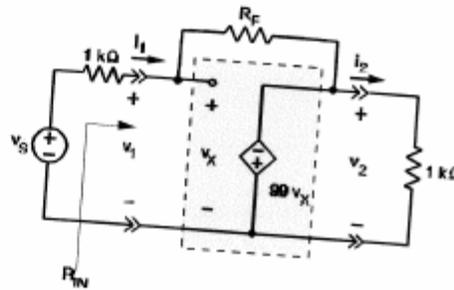
$$\frac{v_x - v_s}{1000} + \frac{v_x - (-99v_x)}{R_F} = 0$$

solving for  $v_x$  yields  $v_x := \frac{R_F \cdot v_s}{R_F + 100000}$

$$v_2 := -99 \cdot v_x \quad v_2 = -9 \times 10^{-2} \quad i_2 := \frac{v_2}{1000}$$

$$i_1 := \frac{v_s - v_x}{1000} \quad K_I := \frac{i_2}{i_1} \quad K_I = -9.9$$

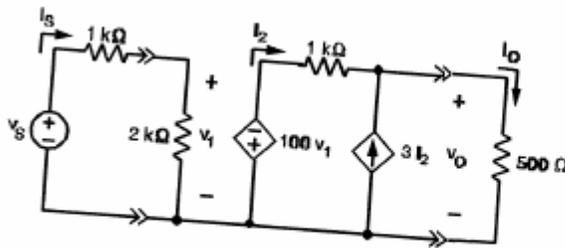
(b)  $R_{IN} := \frac{v_x}{i_1} \quad R_{IN} = 100$



Therefore,  $\mathbf{K = -9.9}$  for part (a); and  $\mathbf{R_{IN} = 100}$  for part (b)

(4-6) Find the voltage gain  $v_O / v_S$  and the current gain  $i_O / i_S$  in Figure P4-6.

4-6 By voltage division  $v_1 = \frac{2000}{1000 + 2000} \cdot v_S = \frac{2 \cdot v_S}{3}$  (a) Writing a KCL equation at Node A yields:



$$i_2 + 3i_2 - i_O = 0 \quad i_O = 4 \cdot i_2$$

$$i_2 = \frac{(-100 \cdot v_1) - v_O}{1000} = \frac{-v_S}{15} - \frac{v_O}{1000}$$

$$i_2 = \frac{i_O}{4} = \frac{v_O}{4 \cdot 500} = \frac{v_O}{2000} \quad \text{hence,}$$

$$\frac{-v_S}{15} - \frac{v_O}{1000} = \frac{v_O}{2200} \quad \text{Solve for } v_O :$$

$$v_O = \frac{-400}{9} \cdot v_S \quad K_V := \frac{-400}{9}$$

(b)  $i_S = \frac{v_S}{3000} \quad i_O = \frac{v_O}{500} = \frac{1}{500} \left( \frac{-400}{9} \cdot v_S \right) \quad K_I := \frac{-400 \cdot 3000}{500 \cdot 9}$

$$K_V = -44.444 \quad K_I = -266.667$$

Therefore,  $\mathbf{K_V = -44.44}$  for part (a); and  $\mathbf{K_I = -266.667}$  for part (b)