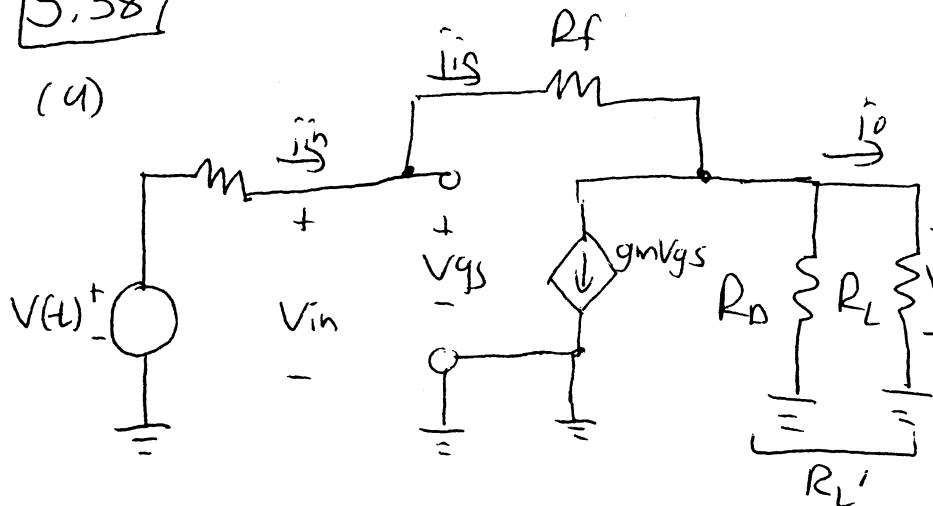


EECS 245 HWK #7 Soln

5.38

(a)



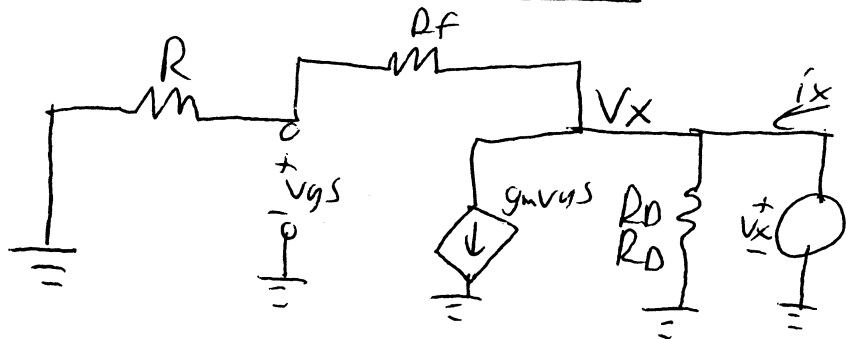
Remember, for small-signal model, C's + DC voltage sources are shorted, but the small signal, $V(t)$ is not shorted!

(b) From above, $V_o = R_L' i_o$ $i_o = i_{in} - g_m V_{gs}$. $V_o = R_L' (i_{in} - g_m V_{gs})$

$i_{in} = \frac{V_{in} - V_o}{R_f}$. Combining these two yields $\boxed{\frac{V_o}{V_{in}} = \frac{R_L' - g_m R_L' R_f}{R_L' + R_f} = A_v}$

$R_{in} = \frac{V_{in}}{i_{in}}$. $i_{in} = \frac{(V_{in} - V_o)}{R_f} \Rightarrow \frac{i_{in}}{V_{in}} = \left(\frac{1 - \frac{V_o}{V_{in}}}{R_f} \right) \Rightarrow \frac{V_{in}}{i_{in}} = \frac{R_f}{1 - \frac{V_o}{V_{in}}}$

$$\frac{V_o}{V_{in}} = A_v \therefore \boxed{R_{in} = \frac{R_f}{1 - A_v}}$$



To measure output impedance, use the following circuit. $V(t)$ is shorted, but the dependent source cannot be ignored.

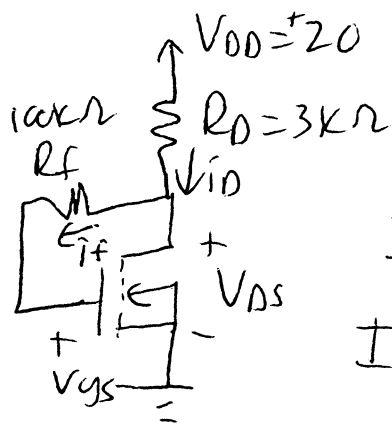
Note that $R_D \parallel (R + R_f) = R_D'$ (R_D is in parallel with $(R + R_f)$)

$V_{gs} = V_x \left(\frac{R}{R + R_f} \right)$ (V_{gs} will divide along $R + R_f$) $i_x = \frac{V_x}{R_D'} + g_m V_{gs}$

Combining, $\frac{V_x}{i_x} = \boxed{R_o = \frac{1}{\frac{1}{R_D'} + \frac{g_m R}{R_f + R}}} = \frac{R_D' (R_f + R)}{R_f + R(1 + g_m R_D')}$

(c) The dc circuit is:

$i_f = 0$ since input impedance of MOSFET for DC $= \infty$ $\therefore$



$$V_{GSQ} = V_{DSQ} \quad \text{Assuming saturation} \rightarrow$$

$$I_{DSQ} = K(V_{GSQ} - V_{TO})^2 = K(V_{DSQ} - V_{TO})^2$$

$$I_{DQ} = \frac{(V_{DD} - V_{DSQ})}{R_D}$$

Combining $\Rightarrow$

$$3V_{DSQ}^2 - 24V_{DSQ} + 55 = 0$$

Solving, $V_{DSQ} = 7.08, 2.54$

Since $V_{DS} = V_{GS}$, & $V_{TO} = 5V$, V_{DS} must $= 7.08$ for transistor to be on.

$$V_{DSQ} = 7.08 \quad I_{DQ} = \frac{(20 - 7.08)}{3K} = 4.31mA$$

Check: $7.08 > 7.08 - 5 \checkmark$
Saturation assumption correct

$$g_m = \left. \frac{\partial i_D}{\partial V_{GS}} \right|_{Q\text{-point}} \quad I_{DQ} = K(V_{GSQ} - V_{TO})^2 \Rightarrow \frac{\partial I_{DQ}}{\partial V_{GSQ}} = 2K(V_{GSQ} - V_{TO})$$

$$g_m = 4.16 \times 10^{-3} S$$

(d) $R_L' = R_D \parallel R_L = 2.31K\Omega$ plugging into expressions in (d) yields:

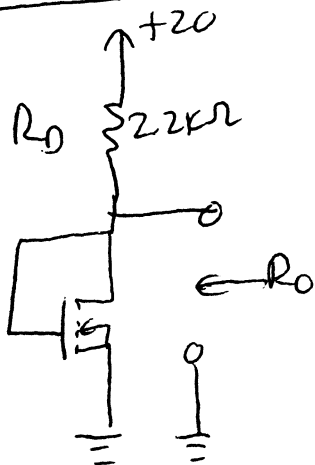
$$A_v = -9.37 \quad R_{in} = 9.64K\Omega \quad R_o = 414\Omega$$

$$(e) v_o(t) = v(t) \left(\frac{R_{in}}{R_{in} + R_o} \right) A_v \quad v_o(t) = (-164) \sin(2000\pi t)$$

(f) This is a inverting amplifier (A_v is negative). The input impedance is very low in comparison with most FET amplifiers

This is generally not a good thing, as seen in part (e); the output is smaller than the input because $R_{in} \ll R_o$.

5.34



$$V_{GSQ} = V_{DSQ} \therefore I_{DQ} = K(V_{DSQ} - V_{TO})^2$$

$$I_{DQ} = \frac{(V_{DD} - V_{DSQ})}{R_D}$$

Combining, $1.1V_{DSQ}^2 - 5.6V_{DSQ} - 10.1 = 0$

$$V_{DSQ} = 6.5, -1.41 \therefore V_{DSQ} = 6.5, I_{DQ} = 6.135 \text{ mA}$$

$$g_m = \frac{dI_D}{dV_{GS}} = 2K(V_{GS} - V_{TO}) = 3.5 \text{ mS}$$

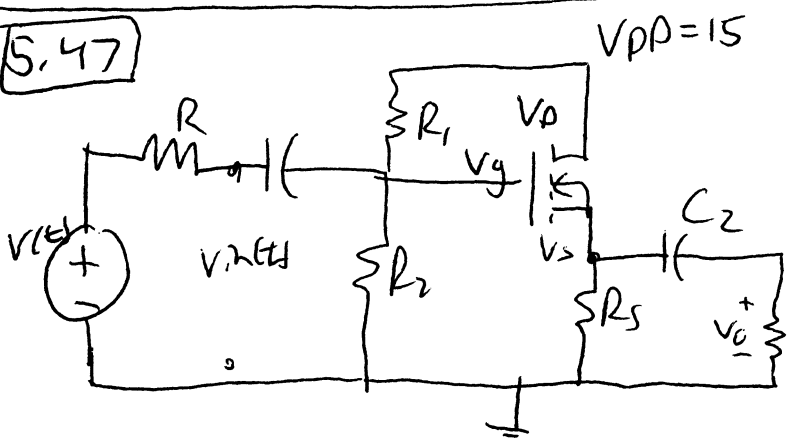


(V_X & i_X are used to calculate R_O and are NOT part of the normal Small-Signal model)

$$i_X = \frac{V_X}{R_D} + g_m V_{GS} \quad V_{GS} = V_X \therefore R_O = \frac{V_X}{i_X} = \frac{V_X}{\frac{V_X}{R_D} + g_m V_X} =$$

$$\frac{1}{\frac{1}{R_D} + g_m} \quad R_O = 253 \Omega$$

5.47



First, $K = \left(\frac{W}{L}\right) \left(\frac{\mu_p}{2}\right) = \left(\frac{160}{10}\right) \left(\frac{50 \times 10^{-6}}{2}\right)$

$$K = 400 \frac{\mu A}{V^2}$$

$$I_{DQ} = K(V_{GSQ} - V_{TO})^2 \Rightarrow$$

$$V_{GSQ} = V_{TO} + \sqrt{\frac{I_{DQ}}{K}} \quad V_{GSQ} = 3.236$$

$$V_G = 15 \left(\frac{2M}{1M + 2M}\right) = 10V$$

$$V_G - V_S = V_{GS} \quad V_S = I_{DQ} R_S$$

$$V_{GS} = V_G - I_{DQ} R_S \quad R_S = \frac{V_{GS} - V_G}{-I_{DQ}} \quad R_S = 3.382 \text{ k}\Omega$$

From eqn. 5.26, $g_m = 2K(V_{GSQ} - V_{TO})$

$$g_m = 1.79 \text{ mS}$$

Looking at pg 321 in the text, $R_L' = \frac{1}{\frac{1}{r_d} + \frac{1}{R_S} + \frac{1}{R_L}}$ $r_d = \infty$:

$$\underline{R_L' = 1.257 \text{ k}\Omega}$$

$$A_v = \frac{g_m R_L'}{1 + g_m R_L'} \quad \boxed{A_v = 0.6923}$$

$$R_{in} = R_1 // R_2$$

$$\boxed{R_{in} = 666.7 \text{ k}\Omega}$$

$$R_o = \frac{1}{g_m + \frac{1}{R_S} + \frac{1}{r_d}}$$

$$\boxed{R_o = 479.5 \Omega}$$