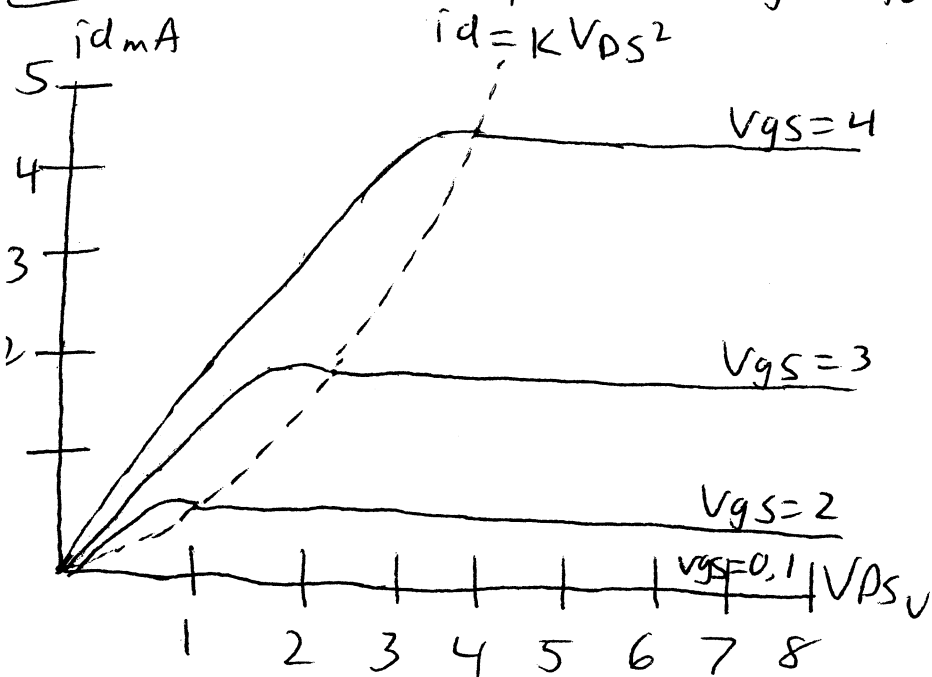


EECS 245 HMWK 6 Solution

5.5 In saturation, $i_d = K(V_{gs} - V_{TO})^2$ $K = \frac{50 \times 10^{-6}}{2} \left(\frac{w}{L}\right) = 5 \times 10^{-4}$



V_{gs}	$i_{d,sat}$
2	0.5 mA
3	2 mA
4	4.5 mA

Now, for each V_{gs} , we start at the saturation current and $i_d = K V_{DS}^2$ intersection. To the right,

a straight line; to the left, a ray to 0. For $V_{gs} < 2$, $i_d = 0$. See next page for PSPICE results. See Dr. Meratz NMOS notes for how to generate this graph.

5.13

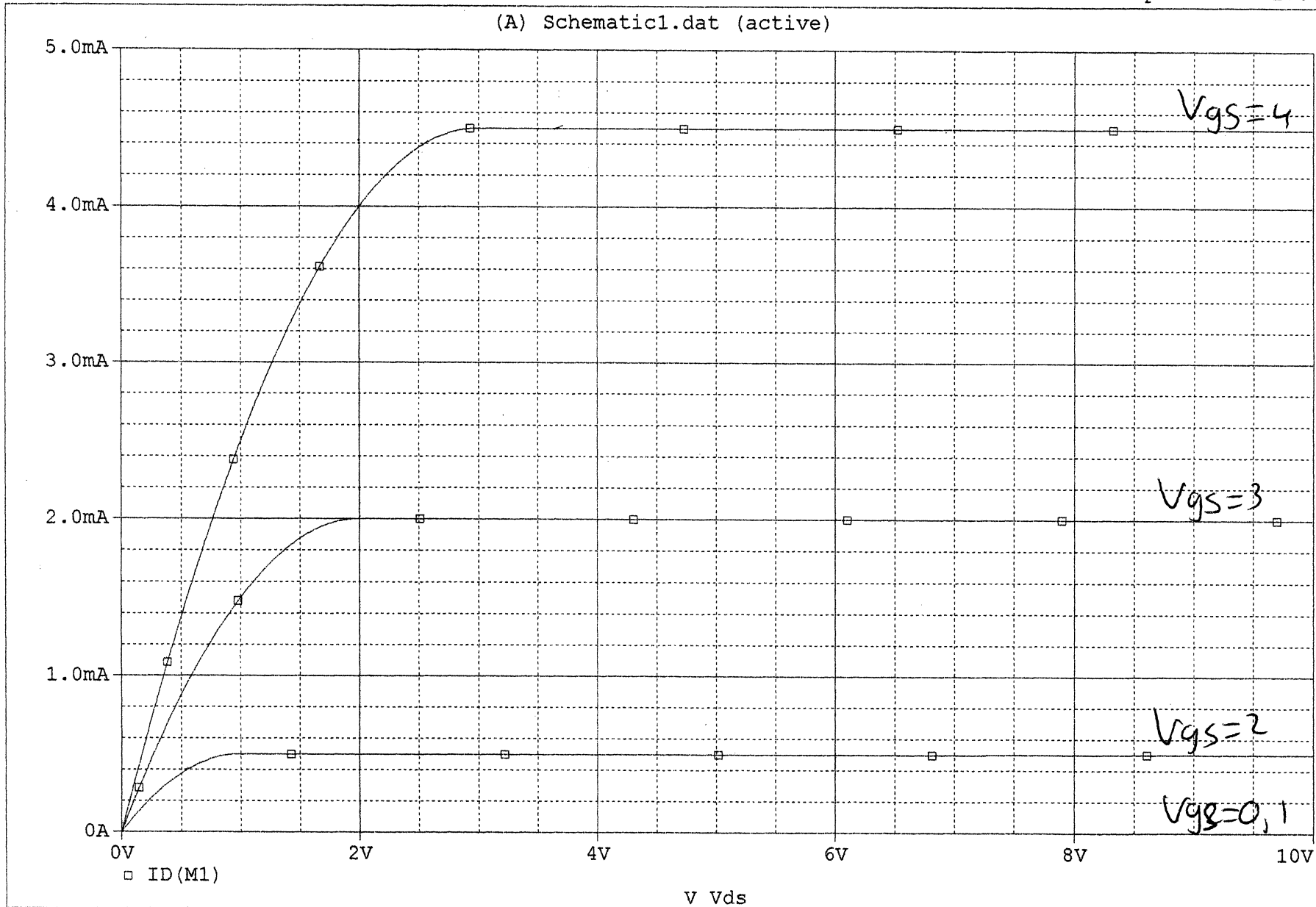
In the triode region, $i_d = K [2(V_{gs} - V_{TO})V_{DS} - V_{DS}^2]$

If $V_{DS} \ll V_{gs} - V_{TO}$, this reduces to $i_d \approx 2K(V_{gs} - V_{TO})V_{DS}$

$$r_d = \frac{V_{DS}}{i_D} \therefore r_d = \frac{1}{2K(V_{gs} - V_{TO})}$$

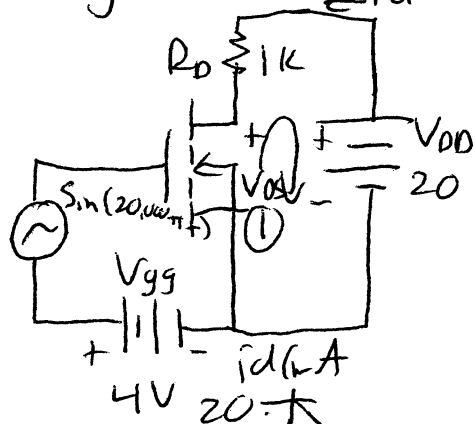
If $V_{gs} < V_{TO}$ (cutoff), r_d is infinite because $i_d = 0$

$V_{gs} (V)$	$r_d (k\Omega)$
0.5	∞
1.0	∞
1.5	4
2.0	2

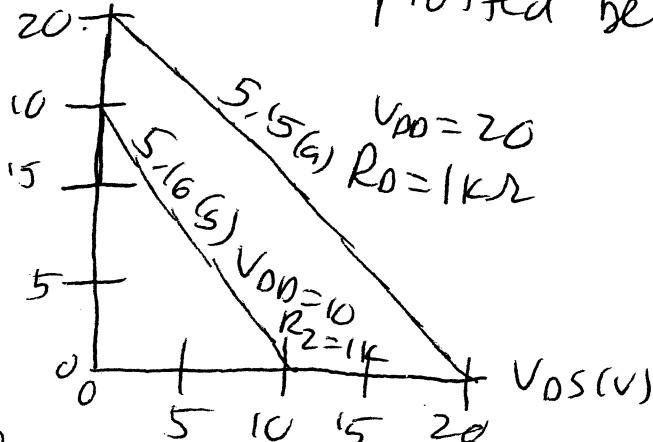


5.15 (a)

Figure 5.13: i_D



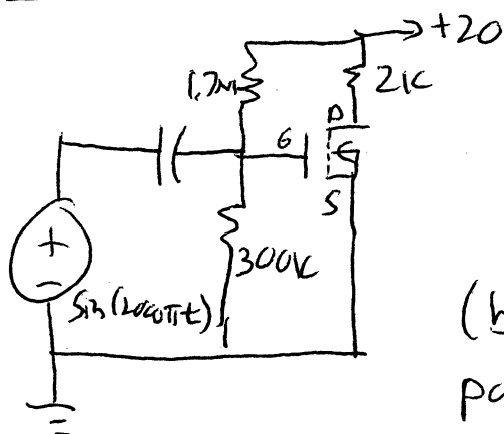
Writing a loop equation around (1) yields $-V_{PS} - i_D R_D + V_{DD} = 0$ or $V_{DD} = i_D R_D + V_{PS}$. This is our load line equation. Graph is plotted below for $V_{DD} = 20$, $R_D = 1k\Omega$



5.16 (b)

Again, $V_{DD} = i_D R_D + V_{PS}$. Graph above for $V_{DD} = 10$, $R_D = 1k\Omega$

5.18



$$(a) V_{GS}(t) = \sin(20000\pi t) + V_{GSQ}$$

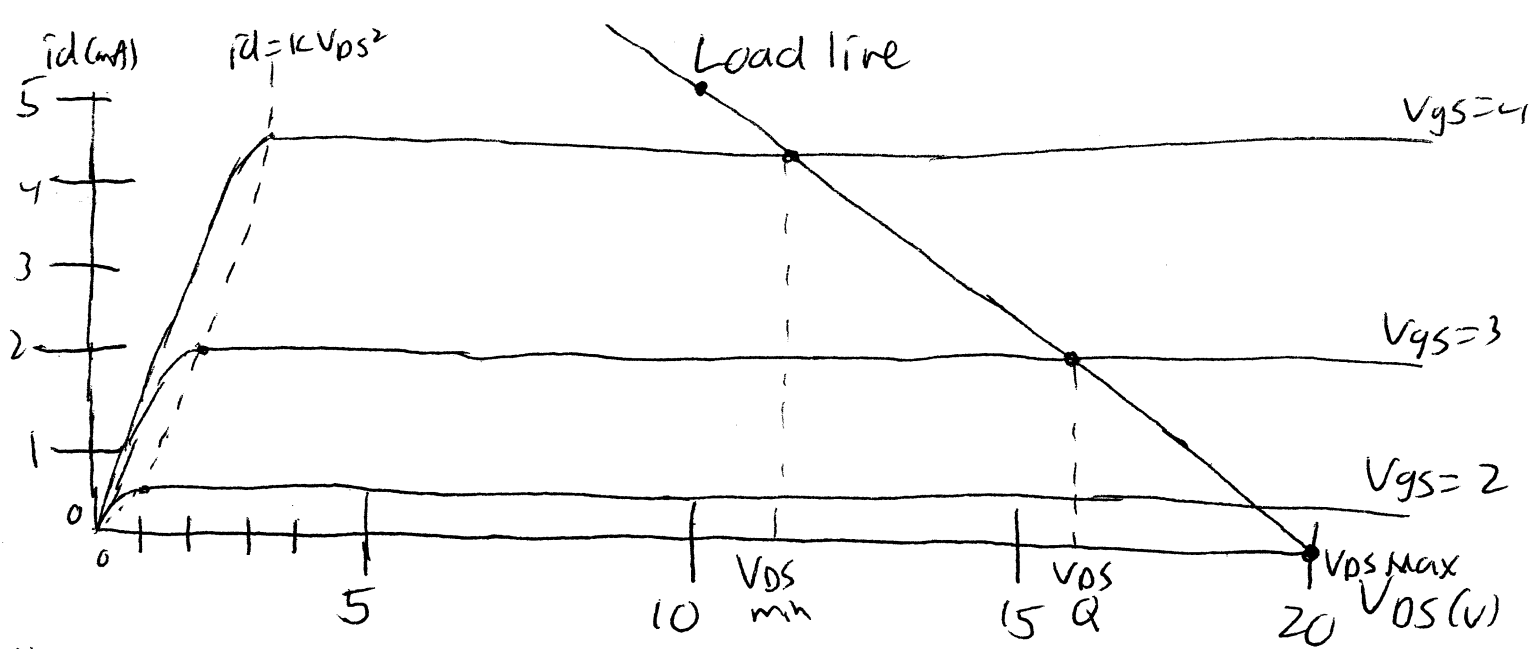
$$V_{GSQ} = 20 \left(\frac{300k}{1.7M + 300k} \right) = 3V \therefore$$

$$V_{GS}(t) = \sin(20000\pi t) + 3$$

(b) $i_{Dsat} = 0.5 \times 10^{-3} (V_{GS} - 1)^2$ see next page for graph, see problem 5.5 for how to draw it. Actually, it's the same as 5.5!

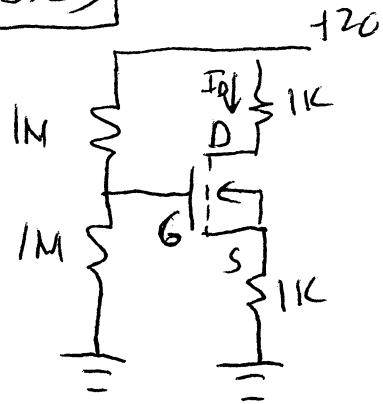
(c) Load line = $V_{DD} = i_D R_D + V_{PS}$; $20 = i_D (2k) + V_{GS}$

plotted on next page



(d) As can be seen from the above graph, $V_{DS\min} \approx 11V$ $V_{DS\max} = 20V$
 $V_{DSQ} \approx 16V$

5.23



(a) $V_g = 20 \left(\frac{1M}{1M+1M} \right) = 10V$

$V_s = I_s (1k) \quad I_D = I_s \therefore V_s = I_D (1k\Omega) \therefore$

① $V_{gs} = 10 - I_D (1k\Omega)$

we also know that in saturation,

$I_D = K (V_{gs} - V_{TO})^2$ Substituting into ①,

$V_{gs} = 10 - (1k)(1 \times 10^{-3})(V_{gs} - 4)^2 \rightarrow V_{gs}^2 - 7V_{gs} + 6 = 0$

Solving yields $V_{gs} = 1, 6$ If $V_{gs} = 1$, transistor is 1 $\therefore V_{gsQ} = 6$

From ①, $I_{DQ} = 4mA$ $V_{DSQ} = 10 - (2k\Omega)(I_{DQ})$ $V_{DSQ} = 12$

Check: is $V_{DS} \geq V_{gs} - V_{TO}$? $12 \geq 6 - 4 \rightarrow$ correct!

As with BJTs, assume saturation, then check your assumption

$V_{DS} \geq V_{gs} - V_{TO}$ for saturation.

(b) Same equations, different numbers

$$V_{GS} = 10 - (1K)(2 \times 10^{-3})(V_{GS} - 2)^2 \rightarrow V_{GS}^2 - 3.5V_{GS} - 1 = 0$$

$$V_{GSQ} = 3.765, -0.265 \rightarrow V_{GSQ} = 3.765V$$

$$I_{DQ} = \frac{3.765 - 10}{-1K} = 6.235mA \quad V_{DSQ} = 20 - (2K)(6.235mA)$$

$$V_{DSQ} = 7.53V$$

$$7.53 \geq 3.765 - 2 \rightarrow \text{correct}$$

5.26

$$V_S = 0 \therefore V_{GS} = V_G$$

$$V_G = 10 \left(\frac{50K}{50K + 150K} \right) = 2.5V = V_{GS}$$

$$\text{Assume saturation: } I_{DQ} = K(V_{GSQ} - V_{TO})^2$$

$$I_{DQ} = (.25 \times 10^{-3})(2.5 - 1)^2 = .5625mA$$

$$V_{DSQ} = V_{DD} - R_D I_{DQ} = 10 - (10K)(.5625mA)$$

$$V_{DSQ} = 4.375V$$

