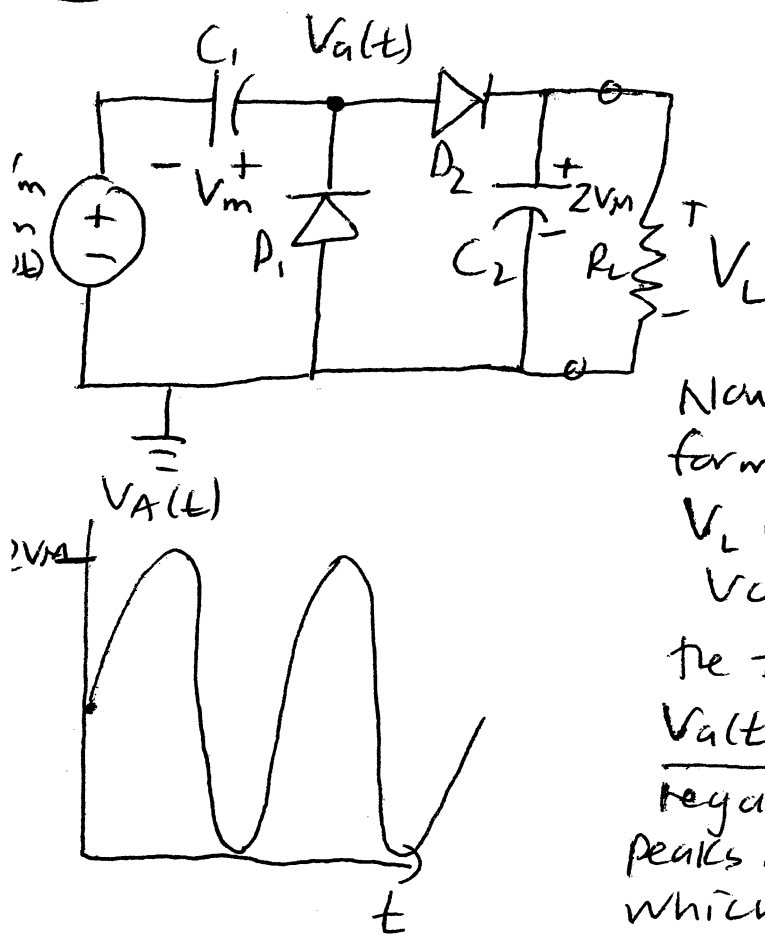


EECS 245 HMWK 3 SOLUTION

3.32, 3.33
2.14, 2.22
2.23

3.32



First, notice that D_1 & C_1 form a "clamp" circuit; i.e. when $V_m \sin(\omega t) < 0$, D_1 conducts charging C_1 . Thus, negative peaks are clamped to $0V$.

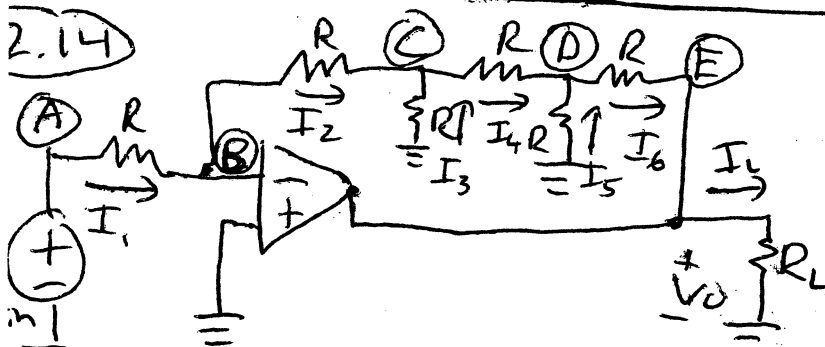
Now, notice that D_2 & C_2 & R_L form a half-wave rectifier; thus, V_L (V_{C_2}) will charge to the peak voltage seen at $V_A(t)$. Combining the two, $V_A(t)$ will be:

$V_A(t) = V_m + V_m \sin(\omega t)$ to clamp negative peaks at $0V$. Positive peaks of $V_A(t)$ will thus be at $2V_m$, which is what V_L will be.

$$V_O = V_L = V_{C_2} = 2V_m$$

Peak inverse $D_2 = 2V_m$ Peak inverse $D_1 = 2V_m$

2.14



Refer to labeled diagram.

$V_B = 0$ since $V_p = V_n$ for op-amp

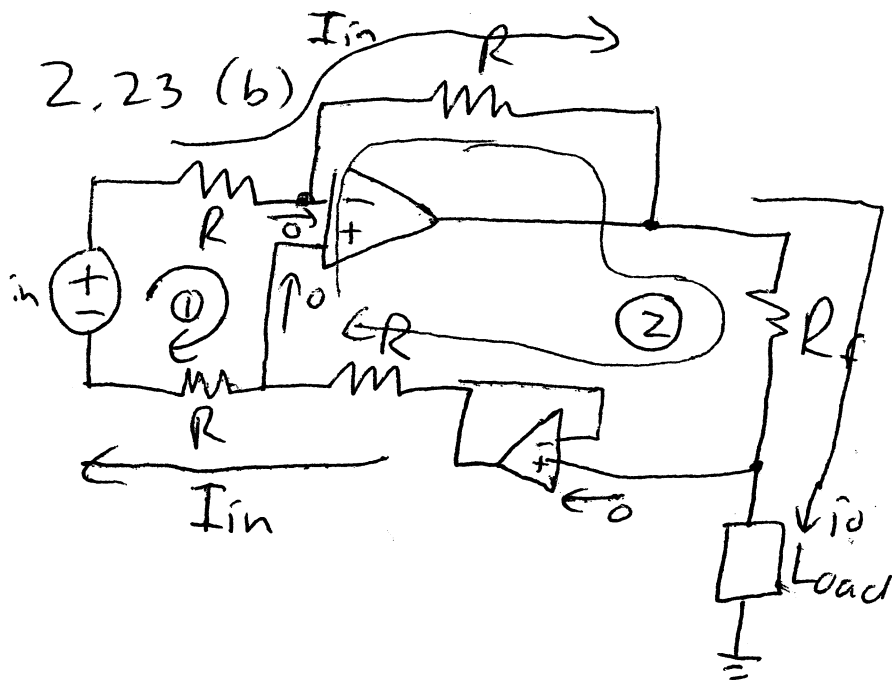
$$I_1 = \frac{A-B}{R} = \frac{V_{in}}{R} = I_1$$

$$I_1 = I_2 \text{ since } I_n = 0$$

$$I_2 = \frac{B-C}{R} = \frac{V_{in}}{R} \therefore C = -V_{in} \quad I_3 = \frac{0-C}{R} \therefore I_3 = \frac{V_{in}}{R}$$

$$I_4 = I_3 + I_2 = \frac{2V_{in}}{R} \quad I_4 = \frac{C-D}{R} = \frac{2V_{in}}{R} \quad D = -3V_{in}$$

2.23 (b)



First, because $i_n = i_p = 0$, $i_{in} + i_{out}$ must flow as shown on the diagram. Once we know this, we can apply KVL around 2 loops to get the relationship.

Loop 1: $V_{in} = I_{in}R + 0 + I_{in}R$ $V_{in} = 2I_{in}R$

Loop 2: $R I_{in} + R_f I_o + R I_{in} = 0$ $2I_{in}R = -R_f I_o$

Solving, $\boxed{i_o = -V_{in}/R_f}$

Since i_o is independent of load
Output impedance = ∞

$$D = -3V_{in} \quad I_5 = \frac{0-D}{R} \therefore I_5 = \frac{3V_{in}}{R}$$

2.14 cont

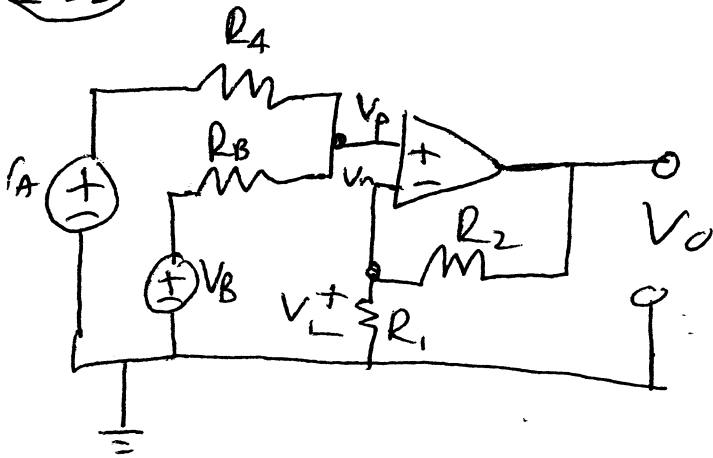
$$I_6 = I_5 + I_4 \therefore I_6 = \frac{5V_{in}}{R} \quad I_6 = \frac{D-E}{R}$$

$$E = -8V_{in}$$

$$E = V_0 \therefore V_0 = -8V_{in}$$

$$\boxed{V_0/V_{in} = -8}$$

2.22



$V_n = V_p = V_i$. Now, i_p must be 0 since this is the input of an OP-AMP $\therefore$

$$\frac{V_A - V_i}{R_A} + \frac{V_i - V_B}{R_B} = 0 \text{ solving,}$$

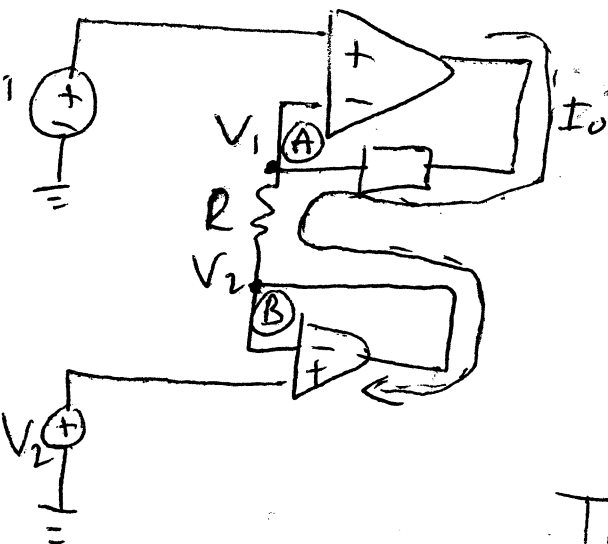
$$V_i = \frac{V_A R_B + V_B R_A}{R_A + R_B}$$

Now, rest of the circuit is a standard non-inverting amplifier:

$$V_0 = \frac{R_1 + R_2}{R_1} V_i \therefore \boxed{V_0 = \left(\frac{R_1 + R_2}{R_1} \right) \left(\frac{V_A R_B + V_B R_A}{R_A + R_B} \right)}$$

2.23

(a)



$$V_p = V_n \therefore V_A = V_1 \text{ \& } V_B = V_2$$

Since $i_{in} = 0$ for both OP-Amps, i_0 must travel as shown.

$$i_0 = \frac{V_A - V_B}{R} \therefore \boxed{i_0 = \frac{V_1 - V_2}{R}}$$

i_0 is independent of load $\therefore$

$$\boxed{\text{Output impedance} = \infty}$$