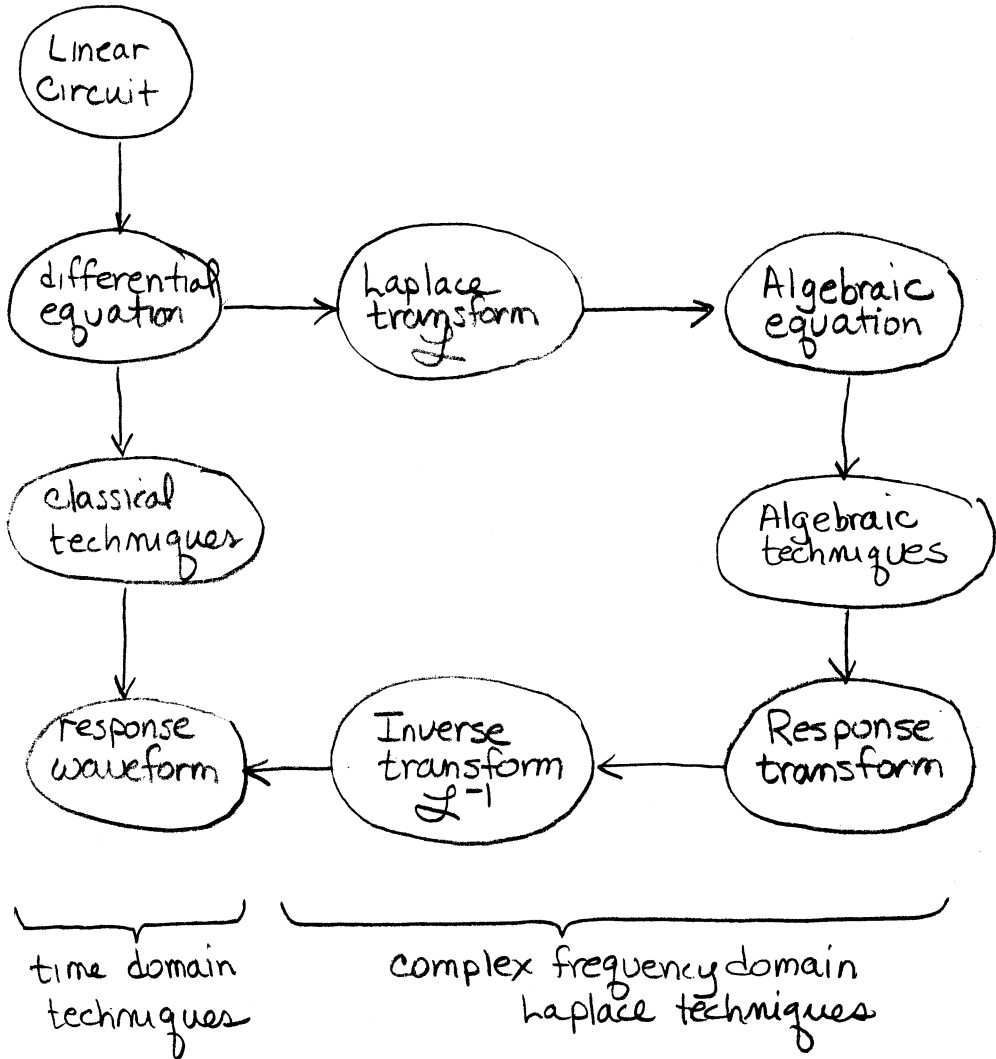


Laplace Transforms

(Read Chapter 9)

1



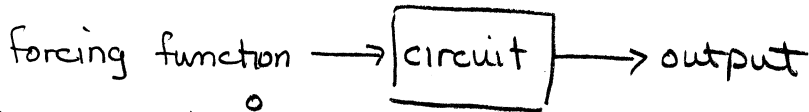
Basic Laplace transformation properties

Properties	Time Domain	Frequency Domain
Independent variable	t	s
Signal representation	$f(t)$	$F(s)$
Uniqueness	$\mathcal{L}^{-1}\{F(s)\} = f(t)u(t)$	$\mathcal{L}\{f(t)\} = F(s)$
Linearity	$A_1 f_1(t) + A_2 f_2(t)$	$A_1 F_1(s) + A_2 F_2(s)$
Integration	$\int_0^t f(\tau) d\tau$	$\frac{F(s)}{s}$
Differentiation	$\frac{df(t)}{dt}$	$sF(s) - f(0^-)$
	$\frac{d^2f(t)}{dt^2}$	$s^2F(s) - sf(0^-) - f'(0^-)$
	$\frac{d^3f(t)}{dt^3}$	$s^3F(s) - s^2f(0^-) - sf'(0^-) - f''(0^-)$
s-Domain translation	$e^{-\alpha t} f(t)$	$F(s + \alpha)$
t-Domain translation	$f(t-a)u(t-a)$	$e^{-as} F(s)$

Basic Laplace transform pairs

signal	waveform $f(t)$	transform $F(s)$
Impulse	$\delta(t)$	1
Step function	$u(t)$	$\frac{1}{s}$
Ramp	$t u(t)$	$\frac{1}{s^2}$
Exponential	$e^{-at} u(t)$	$\frac{1}{s+a}$
Damped Ramp	$t e^{-at} u(t)$	$\frac{1}{(s+a)^2}$
Sine	$\sin \beta t u(t)$	$\frac{\beta}{s^2 + \beta^2}$
Cosine	$\cos \beta t u(t)$	$\frac{s}{s^2 + \beta^2}$
Damped sine	$e^{-at} \sin \beta t u(t)$	$\frac{\beta}{(s+\alpha)^2 + \beta^2}$
Damped cosine	$e^{-at} \cos \beta t u(t)$	$\frac{s+\alpha}{(s+\alpha)^2 + \beta^2}$

circuit analysis



- DC $V_0 e^0$
- transient $V_0 e^{kt}$
- sinusoids $V_0 e^{j\theta} e^{j\omega t}$

In general the response will be $V_0 e^{j\theta} \underbrace{e^{(\sigma + j\omega)t}}_{\text{complex number}}$

DC	$s = 0$
transient (exponential)	$s = \sigma$
sinusoid	$s = j\omega$
exponential sinusoid	$s = \sigma + j\omega$

$$v(t) = \frac{1}{2\pi j} \int_{\sigma - j\infty}^{\sigma + j\infty} e^{st} v(s) ds = \mathcal{L}^{-1}[v(s)]$$

bilateral Laplace transform

$$v(s) = \int_{-\infty}^{\infty} e^{-st} v(t) u(t) dt = \int_0^{\infty} e^{-st} v(t) dt = \mathcal{L}[v(t)]$$

one-sided Laplace transform

$$v(t) \longleftrightarrow v(s)$$

Some sample transforms:

$$\mathcal{L}[u(t)] = \int_0^{\infty} e^{-st} u(t) dt = \int_0^{\infty} e^{-st} dt = -\frac{1}{s} e^{-st} \Big|_0^{\infty} = \frac{1}{s}$$

unit step

$$\mathcal{L}[\delta(t-t_0)] = \int_0^{\infty} e^{-st} \delta(t-t_0) dt = e^{-st_0}$$

delayed impulse
(time shifted)

$$\therefore \delta(t-t_0) \iff e^{-st_0}$$

$$\delta(t) \iff 1$$

$$\mathcal{L}[e^{-\alpha t} u(t)] = \int_0^{\infty} e^{-\alpha t} e^{-st} dt = -\frac{1}{s+\alpha} e^{-(s+\alpha)t} \Big|_0^{\infty} = \frac{1}{s+\alpha}$$

exponential

$$e^{-\alpha t} u(t) \iff \frac{1}{s+\alpha}$$

What about initial conditions

Suppose $v(t) \iff V(s)$

$$\text{then } \mathcal{L}\left\{\frac{dv}{dt}\right\} = \int_0^{\infty} e^{-st} \left(\frac{dv}{dt}\right) dt = \int_0^{\infty} e^{-st} dv$$

integrate by parts

$$= e^{-st} v \Big|_{0^-}^{\infty} - \int_{0^-}^{\infty} (-s e^{-st}) v(t) dt$$

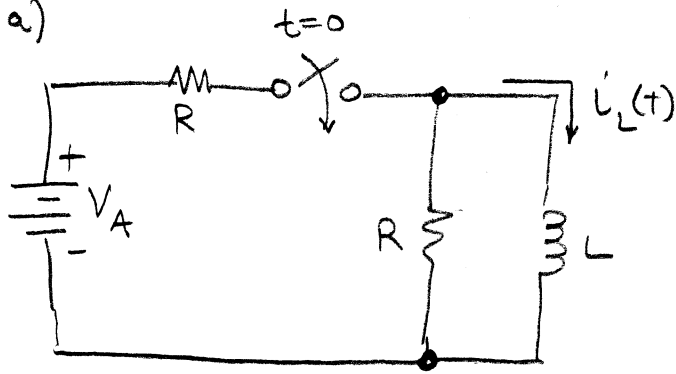
this is the derivative of e^{-st}

$$= 0 - v(0^-) + s \int_{0^-}^{\infty} e^{-st} v(t) dt$$

$$= sV(s) - v(0^-)$$

$V(s)$

9-33 (a)

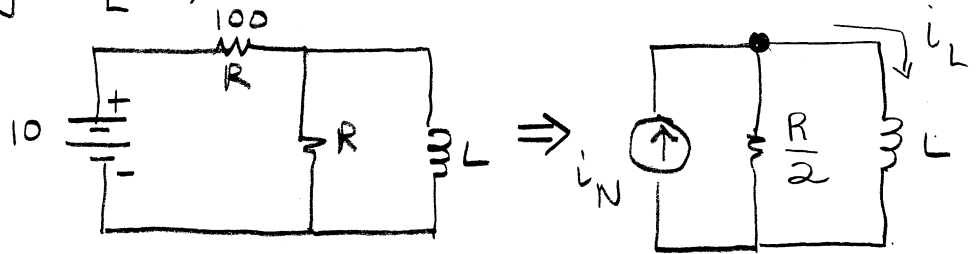


$R = 100 \Omega$
 $L = 100 \text{ mH}$
 $V_A = 10 \text{ V}$

(a) Find the D.E. and the initial condition for $i_L(t)$

initially $i_L(0^-) = 0$

$t > 0$



where $i_N = \frac{10}{100} = 0.1 \text{ A}$.

do KCL at node $\sum i = 0$

$$+i_N - \frac{v_L}{R/2} - i_L = 0$$

$$i_N - L \frac{di_L}{dt} - i_L = 0$$

$$i_N - \frac{2L}{R} \frac{di_L}{dt} - i_L = 0$$

$$\frac{2(100 \times 10^{-3})}{100} \frac{di_L}{dt} + i_L = +i_N = 0.1 \text{ u(t)}$$

$$\underbrace{2 \times 10^{-3} \frac{di_L}{dt}}_{\text{homogeneous}} + \underbrace{i_L}_{\text{forced}} = 0.1 \text{ u(t)}$$

(b) Solve for $i_L(t)$ using Laplace transforms.

Laplace transforming $2 \times 10^{-3} [sI_L(s) - \cancel{i_L(0^-)}] + I_L(s) = \frac{0.1}{s}$

$$I_L(s) [0.002s + 1] = \frac{0.1}{s}$$

$$I_L(s) = \frac{0.1}{s(0.002s + 1)} \cdot \frac{500}{500} = \frac{50}{s(s + 500)}$$

$$= \frac{a}{s} + \frac{b}{s + 500} = \frac{50}{s(s + 500)}$$

$$\therefore bs + as + a500 = 50$$

$$bs + as = 0$$

$$a500 = 50$$

$$\Rightarrow a = \frac{50}{500} = \frac{1}{10}$$

$$b = -a \Rightarrow b = -\frac{1}{10}$$

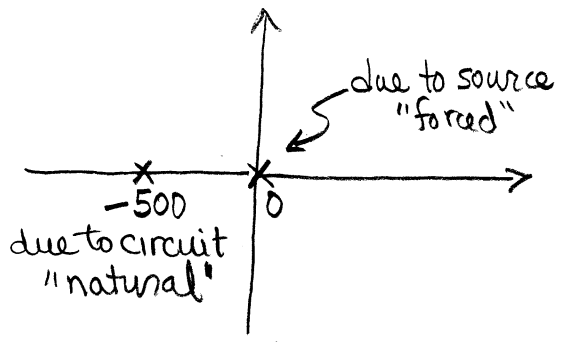
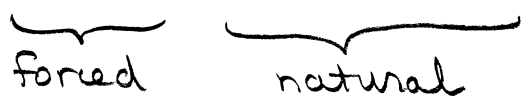
$$I_L(s) = \frac{0.1}{s} - \frac{0.1}{s + 500}$$

Now look up in Laplace transform table.

$$\frac{1}{s + \alpha} \leftrightarrow e^{-\alpha t} u(t) ; \frac{1}{s} \leftrightarrow u(t)$$

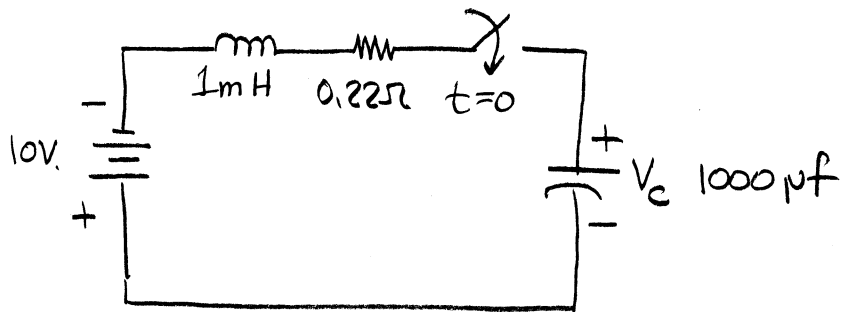
$$\therefore i_L(t) = 0.1 u(t) - 0.1 e^{-500t} u(t)$$

(c) Identify the forced and natural response terms.

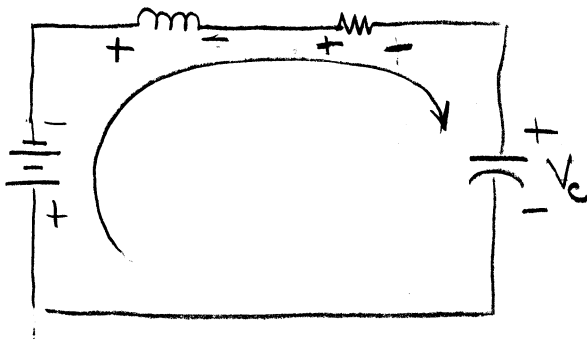


pole-zero diagram

Detailed example



For switch closed

solve for $i(t)$

using KVL $+10 + L \frac{di}{dt} + iR + V_c = 0$.

where $V_c(t) = \frac{1}{C} \int_0^t i(x) dx$

How do we get Laplace transform of $V_c(t)$?

$$\mathcal{L} \left[\int_0^t i(x) dx \right] = \int_0^{\infty} e^{-st} \left[\int_0^t i(x) dx \right] dt$$

Integrate by parts: $\int_0^{\infty} u dw = uw \Big|_0^{\infty} - \int_0^{\infty} w du$

identify $u = \int_0^t i(x) dx$ $dw = e^{-st} dt$

then $du = i(t) dt$ and $w = \frac{e^{-st}}{-s} = -\frac{1}{s} e^{-st}$

$$\begin{aligned} \text{Then } \mathcal{L} \left[\int_0^t i(x) dx \right] &= \int_0^{\infty} \int_0^t i(x) dx \left[-\frac{1}{s} e^{-st} \right]_0^{\infty} + \int_0^{\infty} \frac{e^{-st}}{s} i(t) dt \\ &= 0 + \frac{1}{s} I(s) \end{aligned}$$

$$\text{Then } 10 + L \frac{di}{dt} + iR + \frac{1}{C} \int_0^t i(x) dx = 0$$

$$\text{becomes } 10 + L [sI(s) - i(0^-)] + I(s)R + \frac{1}{C} \left[\frac{1}{s} I(s) \right] = 0$$

Before the switch closed $i(0^-) = 0$ since there was no current through the capacitor.

$$10 + sL I(s) + R I(s) + \frac{1}{sC} I(s) = 0$$

Solving this algebraically

$$I(s) = \frac{-10}{\frac{1}{sC} + R + sL} = \frac{-10sC}{1 + sRC + s^2LC}$$

Putting in the numbers

$$\begin{aligned} I(s) &= \frac{-10s (1000 \times 10^{-6})}{1 + s(0.2)(1000 \times 10^{-6}) + s^2(1 \times 10^{-3})(1000 \times 10^{-6})} \\ &= \frac{-10s}{10^3 + 0.2s + 10^{-3}s^2} = \frac{-10,000s}{10^6 + 200s + s^2} \\ &= \frac{-10,000s}{s^2 + 200s + 10^6} \end{aligned}$$

We want to express denominator as product of terms.
Use quadratic formula

$$s = \frac{-200 \pm \sqrt{(200)^2 - 4(1)(10^6)}}{2} = -100 \pm j995$$

$$I(s) = \frac{-10,000s}{(s+100+j995)(s+100-j995)}$$

Now use partial fraction expansion to separate terms

$$= \frac{a}{s+100-j995} + \frac{b}{s+100+j995}$$

Cross-multiply and solve for a and b

$$a(s+100+j995) + b(s+100-j995) = -10,000s$$

separating terms

$$as + bs = -10,000s$$

$$a + b = -10,000 \tag{1}$$

$$a(100+j995) + b(100-j995) = 0$$

$$a = -b \frac{(100-j995)}{(100+j995)}$$

substituting this result back into (1) we get

$$-b \frac{(100-j995)}{(100+j995)} + b = -10,000$$

Solving for b

$$b = \frac{-10,000}{1 - \frac{(100-j995)}{(100+j995)}} = \frac{-10,000}{\frac{(100+j995) - (100-j995)}{100+j995}}$$

$$= \frac{-10,000(100+j995)}{j1990}$$

$$= -5000 + j503$$

10a

$$\begin{aligned} a &= -10,000 - b \\ &= -10,000 - (-5000 + j503) \end{aligned}$$

$$a = -5000 - j503$$

$$I(s) = \frac{-5000 - j503}{s + 100 - j995} + \frac{-5000 + j503}{s + 100 + j995}$$

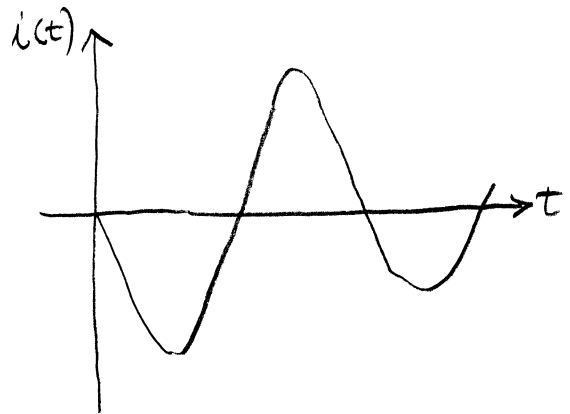
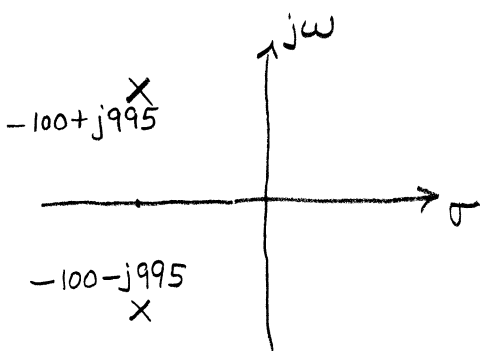
$$i(t) = \mathcal{L}^{-1}[I(s)] = \left[(-5000 - j503)e^{-(100 - j995)t} + (-5000 + j503)e^{-(100 + j995)t} \right] u(t)$$

$$= e^{-100t} \left[(-5000 - j503)e^{+j995t} + (-5000 + j503)e^{-j995t} \right] u(t)$$

$$= e^{-100t} \left[-5000(e^{j995t} + e^{-j995t}) - j503(e^{j995t} - e^{-j995t}) \right] u(t)$$

$$= e^{-100t} \left[-5000(2\cos 995t) - j503(2j\sin 995t) \right] u(t)$$

$$= e^{-100t} \left[-10000 \cos 995t + 1006 \sin 995t \right] u(t)$$



Network functions

Definition of network function

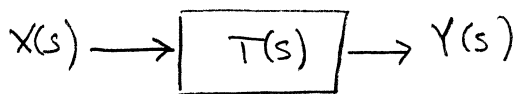
For linear circuits the output of a circuit $y(t)$ is proportional to the input $x(t)$

In the s -domain this proportionality factor is a rational function called a network function,

$$Y(s) = T(s) X(s)$$

More formally

$$\text{Network function} \triangleq \frac{\text{Zero-state Response Transform (Output)}}{\text{Input Signal Transform (Input)}}$$



In general,

$$Y(s) = \underbrace{\sum_{j=1}^N \frac{k_j}{s-p_j}}_{\text{natural poles}} + \underbrace{\sum_{l=1}^M \frac{k_l}{s-p_l}}_{\text{forced poles}}$$

and

$$y(t) = \underbrace{\sum_{j=1}^N k_j e^{p_j t}}_{\text{natural response}} + \underbrace{\sum_{l=1}^M k_l e^{p_l t}}_{\text{forced response}}$$

in a stable circuit all natural poles are in LHP and all exponential terms in natural response decay to zero.

the poles of $X(s)$ cause the forced response. The elements that do NOT decay to zero are called the steady-state response.

$$F(s) = K \frac{(s-z_1)(s-z_2)\dots(s-z_m)}{(s-p_1)(s-p_2)\dots(s-p_n)}$$

12

The Cover-Up Algorithm (P. 448)

For the case of proper rational functions ($n > m$) and no repeated poles we can find the inverse transform.

$$\text{Consider } F(s) = \frac{k_1}{s-p_1} + \frac{k_2}{s-p_2} + \dots + \frac{k_n}{s-p_n}$$

a partial fraction expansion of $F(s)$

The k 's are called residues.

Inverse Laplace transform this to get

$$f(t) = [k_1 e^{p_1 t} + k_2 e^{p_2 t} + \dots + k_n e^{p_n t}] u(t)$$

If we know the residues the transform is easy to determine.

Example:

$$F(s) = 2 \frac{s+3}{s(s+1)(s+2)}$$

Do a partial fraction expansion

$$F(s) = \frac{k_1}{s} + \frac{k_2}{s+1} + \frac{k_3}{s+2}$$

$$(s+1)F(s) = \cancel{(s+1)} 2 \frac{(s+3)}{s \cancel{(s+1)} (s+2)} = (s+1) \frac{k_1}{s} + (s+1) \frac{k_2}{s+1} + (s+1) \frac{k_3}{s+2}$$

If we evaluate this at $s = -1$ a lot of terms vanish to give k_2

$$(s+1)F(s) \Big|_{s=-1} = \frac{2(-1+3)}{(-1)(-1+2)} = \cancel{(-1+1)} \frac{k_1}{s} + k_2 + \cancel{(-1+1)} \frac{k_3}{s+2}$$

$$\text{or } (s+1)F(s) \Big|_{s=-1} = -4 = k_2$$

Continuing

$$k_1 = sF(s) \Big|_{s=0} = \frac{2(s+3)}{(s+1)(s+2)} \Big|_{s=0} = \frac{2(3)}{(1)(2)} = 3$$

$$k_3 = (s+2)F(s) \Big|_{s=-2} = \frac{2(s+3)}{s(s+1)} \Big|_{s=-2} = \frac{2(-2+3)}{(-2)(-2+1)} = 1$$

$$\therefore f(t) = \frac{3}{s} + \frac{-4}{s+1} + \frac{1}{s+2}$$

There are two other techniques we need to know.

I. What if $F(s)$ is an improper fraction, $m \geq n$?

We need to divide the denominator into the numerator to put $F(s)$ into the form of a proper fraction.

See Problem 9-26a.

II. What if $F(s)$ has a multiple pole?

Factor out one of the multiple poles and do partial fraction expansion of what is left.

See Example 9.14.

Problem 9.26 (a)

Find the inverse transform of $F(s) = \frac{(s+50)^2}{(s+10)(s+100)}$

This is an improper fraction. Multiply out to get

$$F(s) = \frac{s^2 + 100s + 2500}{s^2 + 110s + 1000}$$

Divide to get a proper fraction remainder:

$$\begin{array}{r} \overline{) s^2 + 100s + 2500} \\ \underline{s^2 + 110s + 1000} \\ -10s + 1500 \end{array}$$

Rewrite F(s) as

$$F(s) = 1 + \frac{-10s + 1500}{(s+10)(s+100)}$$

$F'(s)$

$$= 1 + \frac{k_1}{s+10} + \frac{k_2}{s+100}$$

Using the cover-up algorithm

$$k_1 = (s+10) F'(s) \Big|_{s=-10} = \frac{-10(-10) + 1500}{(-10 + 100)} = \frac{100 + 1500}{90} = \frac{160}{9}$$

$$k_2 = (s+100) F'(s) \Big|_{s=-100} = \frac{-10(-100) + 1500}{(-100 + 10)} = \frac{2500}{-90} = -\frac{250}{9}$$

Then $F(s) = 1 + \frac{\frac{160}{9}}{s+10} - \frac{\frac{250}{9}}{s+100}$

$$f(t) = \delta(t) + \frac{160}{9} e^{-10t} u(t) - \frac{250}{9} e^{-100t} u(t)$$

Example 9-14

Inverse transform $F(s) = \frac{s}{(s+1)(s+2)^2}$

This has a multiple root, Factor out one multiple root and do a partial fraction expansion.

$$F(s) = \frac{1}{s+2} \left[\underbrace{\frac{s}{(s+1)(s+2)}}_{F(s)} \right] = \frac{1}{s+2} \left[\frac{k_1}{s+1} + \frac{k_2}{s+2} \right]$$

$$k_1 = (s+1)F'(s) \Big|_{s=-1} = \frac{-1}{-1+2} = -1$$

$$k_2 = (s+2)F'(s) \Big|_{s=-2} = \frac{-2}{-2+1} = 2$$

$$\therefore F(s) = \frac{1}{s+2} \left[\frac{-1}{s+1} + \frac{2}{s+2} \right] = \frac{-1}{(s+1)(s+2)} + \frac{2}{(s+2)^2}$$

expand this as $F''(s)$

$$F(s) = \frac{k_3}{s+1} + \frac{k_4}{s+2} + \frac{2}{(s+2)^2}$$

$$k_3 = (s+1)F''(s) \Big|_{s=-1} = \frac{-1}{-1+2} = -1$$

$$k_4 = (s+2)F''(s) \Big|_{s=-2} = \frac{-1}{-2+1} = 1$$

$$F(s) = \frac{-1}{s+1} + \frac{1}{s+2} + \frac{2}{(s+2)^2}$$

$$f(t) = \left[-e^{-t} + e^{-2t} + 2te^{-2t} \right] u(t)$$

Superposition in the s-domain

For a linear circuit $y = k_1 x_1 + k_2 x_2 + k_3 x_3 + \dots$
where y is the output and the x_i are inputs

We can do this in the s-domain

but the k 's become rational functions in s .

Two types of s-domain inputs:

(1) voltage & current sources representing the external driving inputs for $t \geq 0$

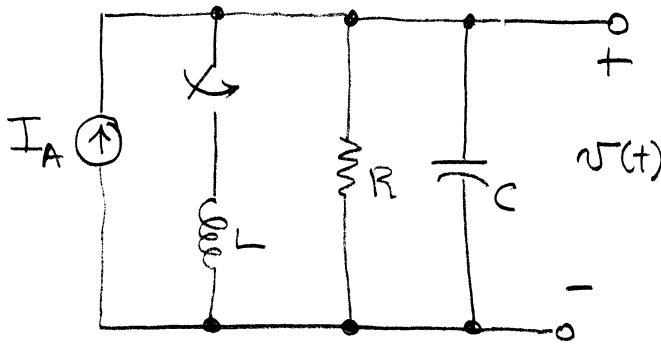
(2) initial condition voltage & current sources representing energy stored at $t = 0$.

$$\text{Then } V(s) = \underbrace{V_{zs}(s)} + \underbrace{V_{zi}(s)}$$

zero-state zero-input

caused by external inputs with initial conditions turned off

caused by initial conditions with external inputs turned off.



(a) Transform into the s-domain

find initial conditions

$i_L(0^-) = 0$ amps since switch is open

capacitor charges to $V_C = I_A R$ since no current through C.

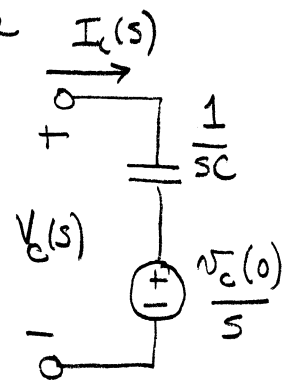
Better to use current source to represent $v_C(0^-)$

See Ch. 10, p. 485-6 Impedance and admittance

$$v_C(t) = \frac{1}{C} \int_0^t i_C(\sigma) d\sigma + v_C(0)$$

$$V_C(s) = \frac{1}{sC} I_C(s) + \frac{v_C(0)}{s}$$

initial condition

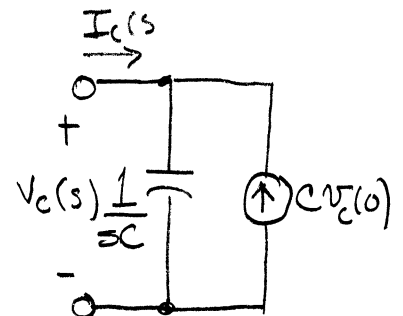


However, this can also be written as

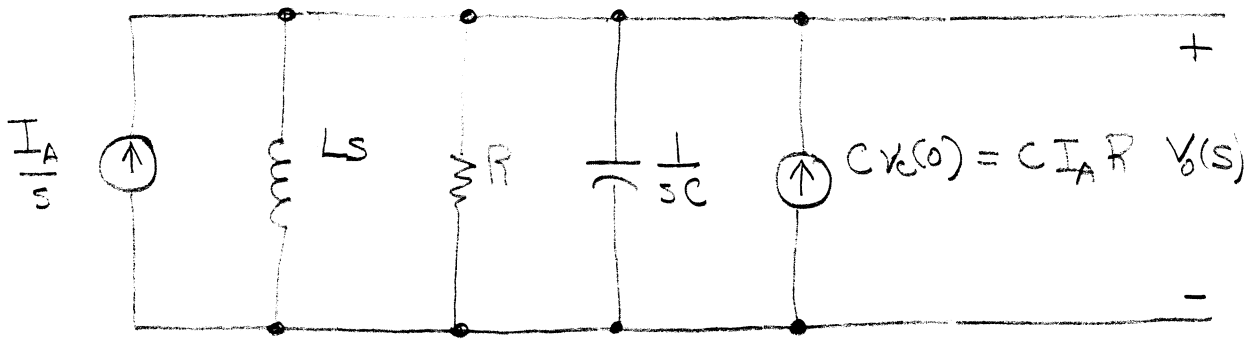
$$sC [V_C(s) = \frac{1}{sC} I_C(s) + \frac{v_C(0)}{s}]$$

$$sC V_C(s) = I_C(s) + C v_C(0)$$

$$I_C(s) = sC V_C(s) - C v_C(0)$$

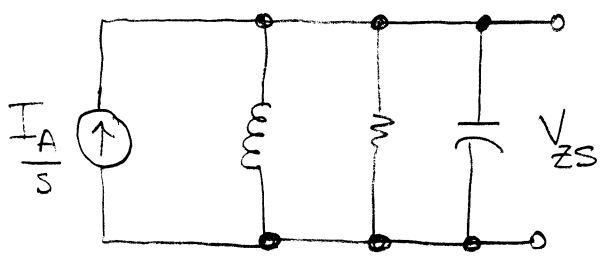


Transformed circuit

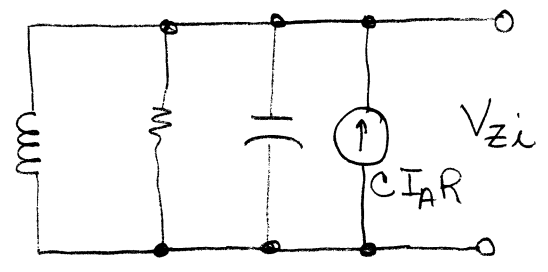


put switch here

(b) Find the zero-state and zero-input components of $v(s)$



zero-state
(replaced initial condition
by open)



zero-input
(replaced external input
by open)

combine R, L, C.

$$Z_{EQ} = \frac{1}{Y_{EQ}} = \frac{1}{\frac{1}{sL} + \frac{1}{R} + sC} = \frac{sLR}{R + sL + RLCs^2}$$

$$V_{ZS} = Z_{EQ}(s) \frac{I_A}{s} = \frac{RLs}{RLCs^2 + Ls + R} \cdot \frac{I_A}{s} = \frac{I_A k}{s^2 + \frac{s}{RC} + \frac{1}{LC}}$$

$$V_{ZI} = Z_{EQ}(s) [C I_A] = \frac{RLs}{RLCs^2 + Ls + R} R C I_A = \frac{R I_A s}{s^2 + \frac{s}{RC} + \frac{1}{LC}}$$

(c) Find $v(t)$ if

$$I_A = 1 \text{ mA}, L = 2 \text{ H}, R = 1.5 \text{ k}\Omega, C = \frac{1}{6} \mu\text{F}$$

$$V_{zs}(s) = \frac{10^{-3} / \frac{1}{6} \times 10^{-6}}{s^2 + \frac{s}{(1500)(\frac{1}{6} \times 10^{-6})} + \frac{1}{(2)(\frac{1}{6} \times 10^{-6})}} = \frac{6000}{s^2 + 4000s + 3000000}$$

$$= \frac{6000}{(s+1000)(s+3000)} = \frac{k_1}{s+1000} + \frac{k_2}{s+3000}$$

$$k_1 = (s+1000) V_{zs}(s) \Big|_{s=-1000} = \frac{6000}{(-1000+3000)} = 3$$

$$k_2 = (s+3000) V_{zs}(s) \Big|_{s=-3000} = \frac{6000}{(-3000+1000)} = -3$$

$$V_{zs}(s) = \frac{3}{s+1000} - \frac{3}{s+3000}$$

$$V_{zi}(s) = \frac{(1500)(10^{-3})s}{s^2 + \frac{s}{(1500)(\frac{1}{6} \times 10^{-6})} + \frac{1}{2(\frac{1}{6} \times 10^{-6})}} = \frac{1.5s}{(s+1000)(s+3000)}$$

$$= \frac{k_3}{s+1000} + \frac{k_4}{s+3000}$$

$$k_3 = (s+1000) V_{zi}(s) \Big|_{s=-1000} = \frac{1.5(-1000)}{(-1000+3000)} = -0.75$$

$$k_4 = (s+3000) V_{zi}(s) \Big|_{s=-3000} = \frac{1.5(-3000)}{(-3000+1000)} = +2.25$$

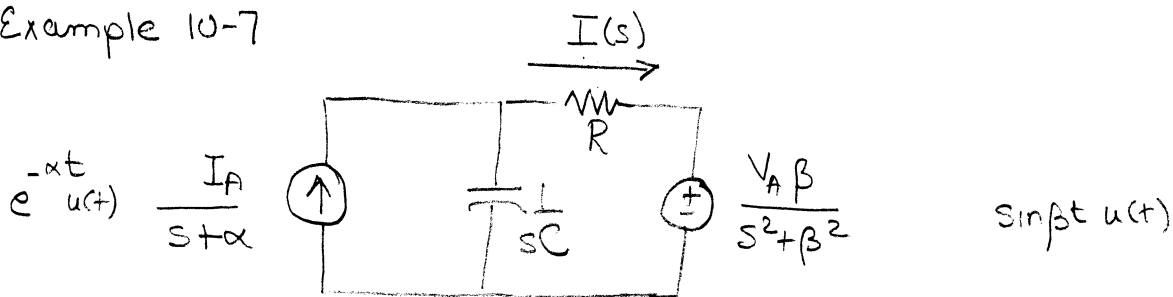
$$V_{zi}(s) = \frac{-0.75}{s+1000} + \frac{2.25}{s+3000}$$

$$v_{zs}(t) = [3e^{-1000t} - 3e^{-3000t}] u(t)$$

$$v_{zi}(t) = [-0.75e^{-1000t} + 2.25e^{-3000t}] u(t).$$

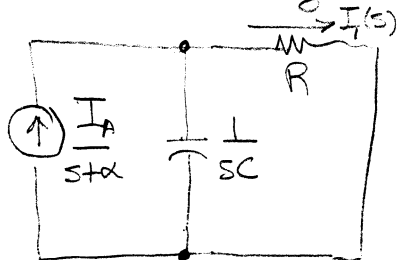
No steady state. Acts like a short in time domain. No forced response since forced pole canceled by zero.

Example 10-7

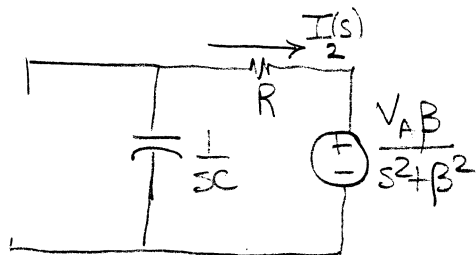


Find the zero state component of $I(s)$.

Easiest to find by superposition.



$$I_1(s) = \frac{\frac{1}{sC}}{\frac{1}{sC} + R} \cdot \frac{I_A}{(s+\alpha)} = \frac{I_A}{(1+sRC)(s+\alpha)}$$



$$I_2(s) = - \frac{\frac{V_{AB}}{s^2 + \beta^2}}{R + \frac{1}{sC}} = - \frac{V_{AB} s C}{(1+sRC)(s^2 + \beta^2)}$$

$$I(s) = I_1(s) + I_2(s) = \frac{I_A}{(1+sRC)(s+\alpha)} - \frac{V_{AB} s C}{(1+sRC)(s^2 + \beta^2)}$$

natural pole comes from circuit

$$s = -\frac{1}{RC}$$

forced poles come from sources

$$s = -\alpha, s = \pm j\beta$$

$$k_1 e^{-t/RC} + k_2 e^{-\alpha t} + k_3 \cos \beta t + k_4 \sin \beta t$$

transient due to natural pole

forced transient due to forced pole

forced component due to forced poles $\pm j\beta$

11-5 Steady State Frequency Response

Consider general sinusoidal input

$$x(t) = X_A \cos(\omega t + \phi) = X_A (\cos \omega t \cos \phi - \sin \omega t \sin \phi)$$

Transform this to get

$$X(s) = X_A \cos \phi \frac{s}{s^2 + \omega^2} - X_A \sin \phi \frac{\omega}{s^2 + \omega^2}$$

$$X(s) = X_A \frac{s \cos \phi - \omega \sin \phi}{s^2 + \omega^2}$$

Consider the output of a system described by $T(s)$

$$Y(s) = X_A \left[\frac{s \cos \phi - \omega \sin \phi}{s^2 + \omega^2} \right] T(s) = X_A \frac{s \cos \phi - \omega \sin \phi}{(s - j\omega)(s + j\omega)} T(s)$$

Expanding by partial fractions

$$Y(s) = \underbrace{\frac{k}{s - j\omega} + \frac{k^*}{s + j\omega}}_{\text{forced poles}} + \underbrace{\frac{k_1}{s - p_1} + \frac{k_2}{s - p_2} + \dots + \frac{k_N}{s - p_N}}_{\text{natural poles of transfer function}}$$

Inverse transforming

$$y(t) = \underbrace{k e^{j\omega t} + k^* e^{-j\omega t}}_{\substack{\text{forced response} \\ \text{is a sinusoidal} \\ \text{steady-state}}} + \underbrace{k_1 e^{p_1 t} + k_2 e^{p_2 t} + \dots + k_N e^{p_N t}}_{\substack{\text{natural response} \\ \text{decays to zero!}}}$$

To find k use cover-up algorithm

$$k = (s - j\omega) X_A \frac{s \cos \phi - \omega \sin \phi}{(s - j\omega)(s + j\omega)} T(s) \Big|_{s = j\omega}$$

$$k = X_A \frac{j\omega \cos \phi - \omega \sin \phi}{2j\omega} T(j\omega) = X_A \frac{\cos \phi + j \sin \phi}{2} T(j\omega)$$

$$k = \frac{1}{2} X_A e^{j\phi} T(j\omega) = \frac{1}{2} X_A e^{j\phi} |T(j\omega)| e^{j\theta}$$

$$k = \frac{1}{2} X_A |T(j\omega)| e^{j(\phi + \theta)}$$

$$y(t) = \frac{1}{2} X_A |T(j\omega)| e^{j(\theta+\phi)} e^{j\omega t} + \frac{1}{2} X_A |T(j\omega)| e^{-j(\theta+\phi)} e^{-j\omega t}$$

$$y(t) = \underset{\substack{\uparrow \\ \text{input amplitude}}}{X_A} |T(j\omega)| \cos(\omega t + \theta + \phi)$$

- (1) Output frequency = Input frequency = ω
- (2) Output amplitude = Input Amplitude * $|T(j\omega)|$
- (3) Output phase = Input phase + $\angle T(j\omega)$

Exercise 11-8

The transfer function of a linear circuit is

$$T(s) = \frac{5(s+100)}{(s+500)}$$

Find the steady state output for (a) $x(t) = 3 \cos 100t$

$$\begin{aligned} |T(j100)| &= \left| \frac{5(j100+100)}{(j100+500)} \right| = \left| \frac{5(100+j100)}{500+j100} \right| \\ &= \left| 1.1538 + j0.7692 \right| = \left| 1.3868 e^{j33.7^\circ} \right| = 1.387 \end{aligned}$$

$$\angle T(j100) = 33.7^\circ$$

$$y_{ss}(t) = (1.387)(3) \cos(100t + 33.7^\circ)$$

$$y_{ss}(t) = 4.16 \cos(100t + 33.7^\circ)$$

You will often see the terms step response and impulse response.

The step response is the zero-state response when the driving function (input) is a unit step applied at $t=0$.

The impulse response is the zero state response when the driving function (input) is a unit impulse applied at $t=0$.

11-49 Step response of a linear circuit is

$$g(t) = 10e^{-1000t} \sin(1000t)$$

$$G(s) = \frac{10000}{(s+1000)^2 + 1000000}$$

Since $G(s) = T(s) \frac{1}{s}$ multiply by s to get $T(s)$

$$T(s) = \frac{10000s}{(s+1000)^2 + 1000000}$$

Exercise 11-6 The impulse response of a circuit is

$$h(t) = 0.1 \delta(t) + 90e^{-100t} u(t)$$

$$H(s) = 0.1 + \frac{90}{s+100}$$

Since $H(s) = T(s) \cdot 1$ we have $T(s)$

$$T(s) = H(s) = 0.1 + \frac{90}{s+100}$$

If you present $T(j\omega)$ as a function of frequency in terms of $|T(j\omega)|$ and $\angle T(j\omega)$ this is called a Bode diagram.

In general,

$$T(j\omega) = A \frac{(j\omega + z_1)(j\omega + z_2) \dots (j\omega + z_k)}{(j\omega)^n (j\omega + p_1)(j\omega + p_2) \dots (j\omega + p_m)}$$

Rewrite each term as

$$(j\omega + z_i) = z_i \left(1 + j \frac{\omega}{z_i}\right)$$

$$(j\omega + p_j) = p_j \left(1 + j \frac{\omega}{p_j}\right)$$

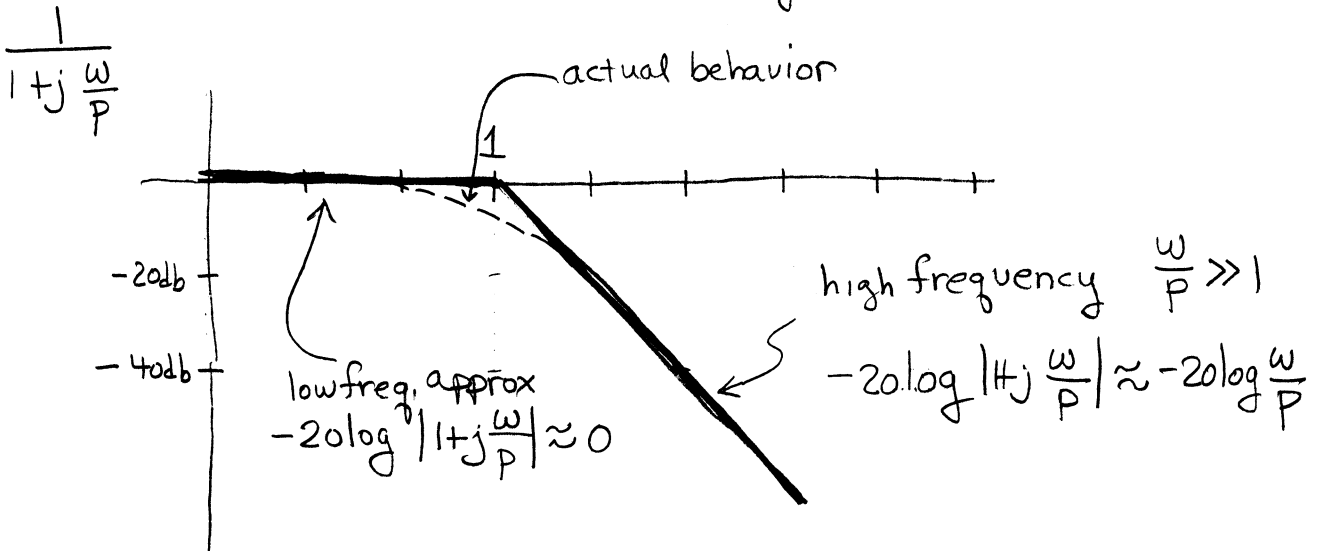
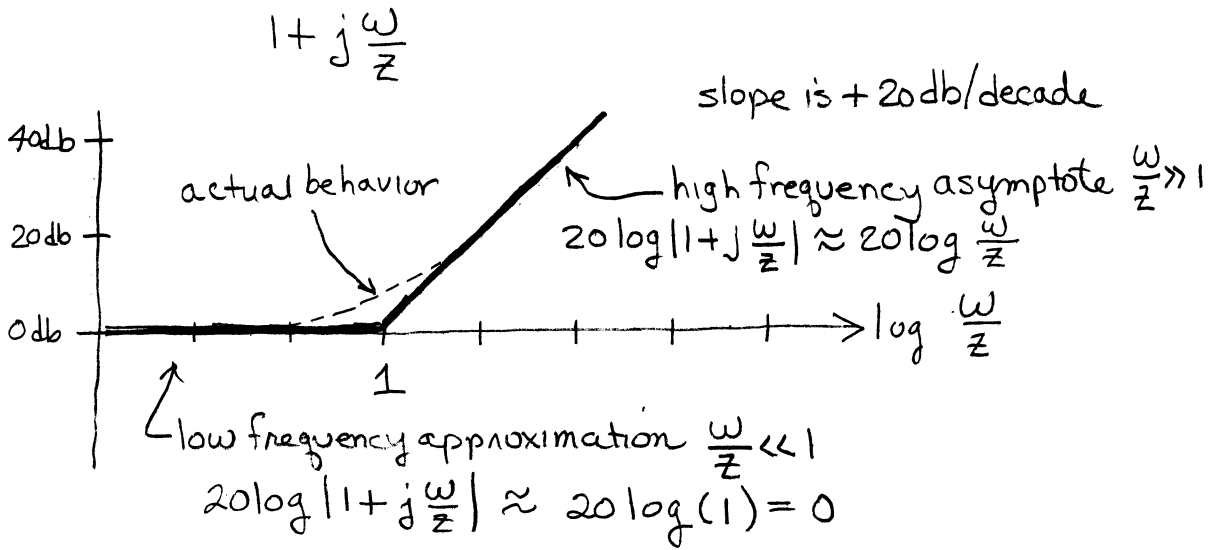
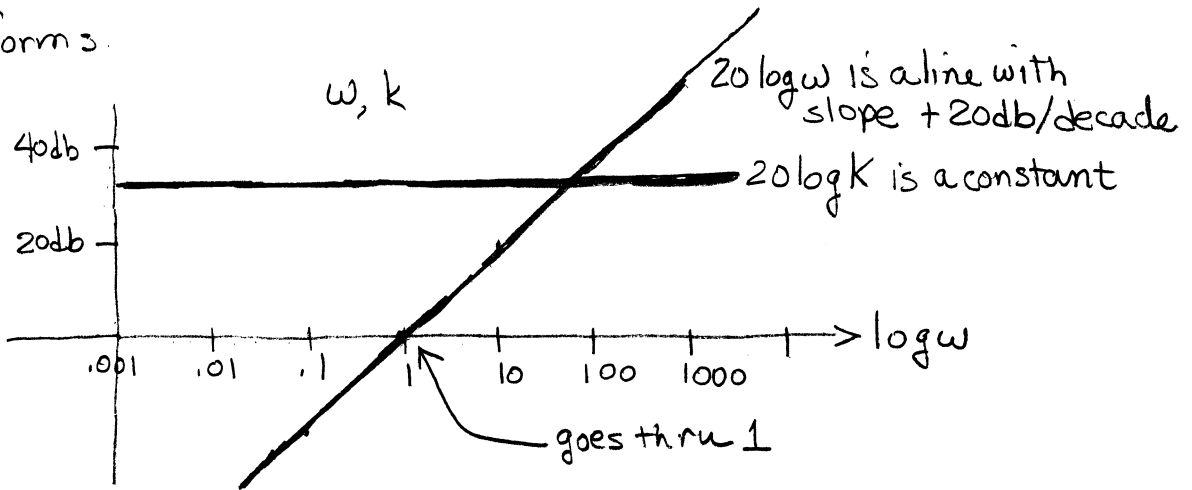
$$20 \log |T(j\omega)| = 20 \log K + \sum_{i=1}^k 20 \log \left|1 + j \frac{\omega}{z_i}\right| - 20n \log \omega - \sum_{j=1}^m 20 \log \left|1 + j \frac{\omega}{p_j}\right|$$

$$\text{where } K = A \frac{\prod_{i=1}^k z_i}{\prod_{j=1}^m p_j}$$

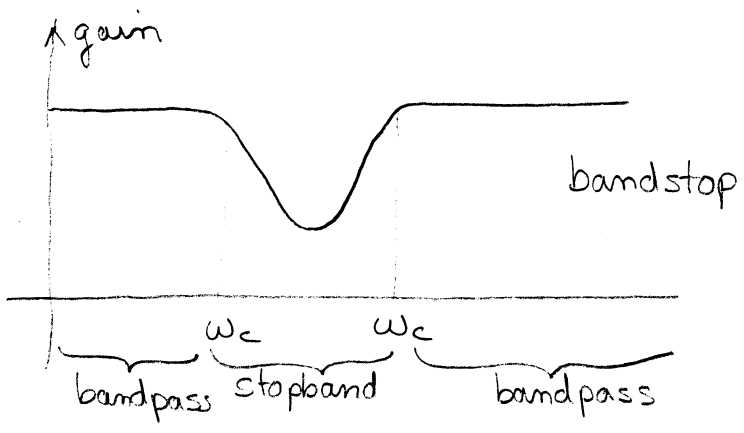
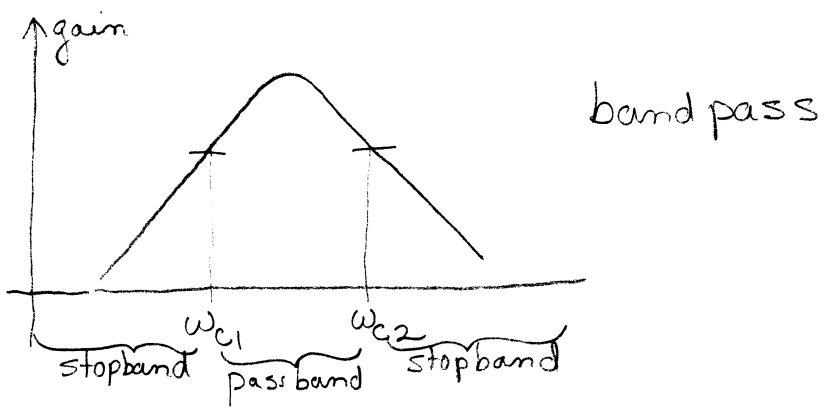
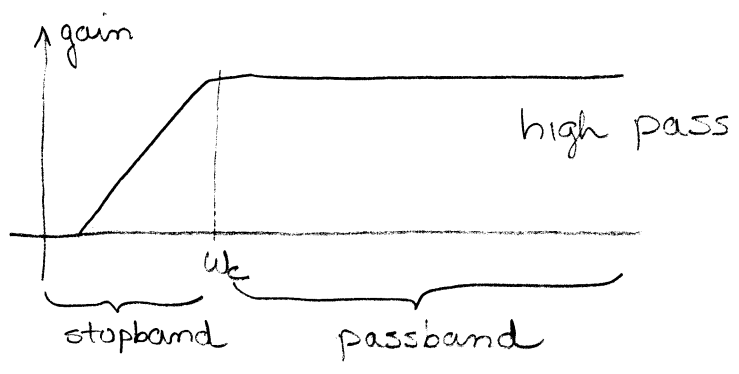
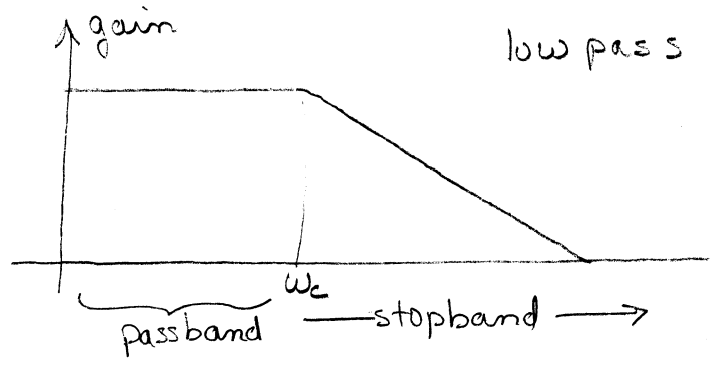
and

$$\angle T(j\omega) = \underbrace{\sum_{i=1}^k \tan^{-1}\left(\frac{\omega}{z_i}\right)}_{\angle(z+j\omega) = \tan^{-1}\left(\frac{\omega}{z}\right)} - \underbrace{90^\circ n}_{\text{from } (j\omega)^n} - \sum_{j=1}^m \tan^{-1}\left(\frac{\omega}{p_j}\right)$$

basic forms



Prototype gain responses



Example of how pole-zero placement affects response

$$\text{Consider } G_1(j\omega) = K \frac{(1 + j\frac{\omega}{z})}{(1 - j\frac{\omega}{p})}$$

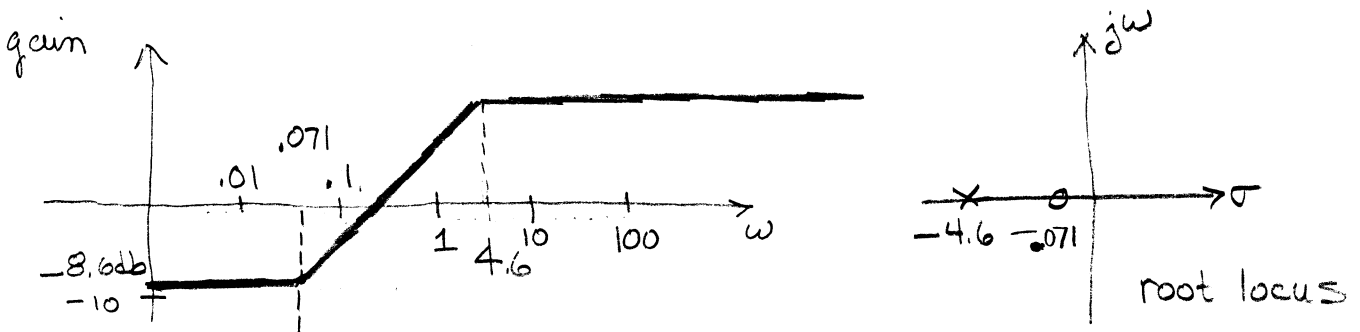
Taking logs

$$|G(j\omega)|_{\text{db}} = 20 \log K + 20 \log |1 + j\frac{\omega}{z}| - 20 \log |1 - j\frac{\omega}{p}|$$

Case I $z < p$

$$\text{Let } k = 0.37, z = 0.071, p = 4.6$$

$$|G(j\omega)|_{\text{db}} = \underbrace{20 \log |0.37|}_{-8.6\text{db}} + 20 \log |1 + j\frac{\omega}{0.071}| - 20 \log |1 - j\frac{\omega}{4.6}|$$



for small ω only have first term at -8.6db

since $z < p$, the zero comes in first adding

$$+20 \log |1 + j\frac{\omega}{0.071}|$$

@ $\omega = 0.071$ this term starts to add +20db/decade

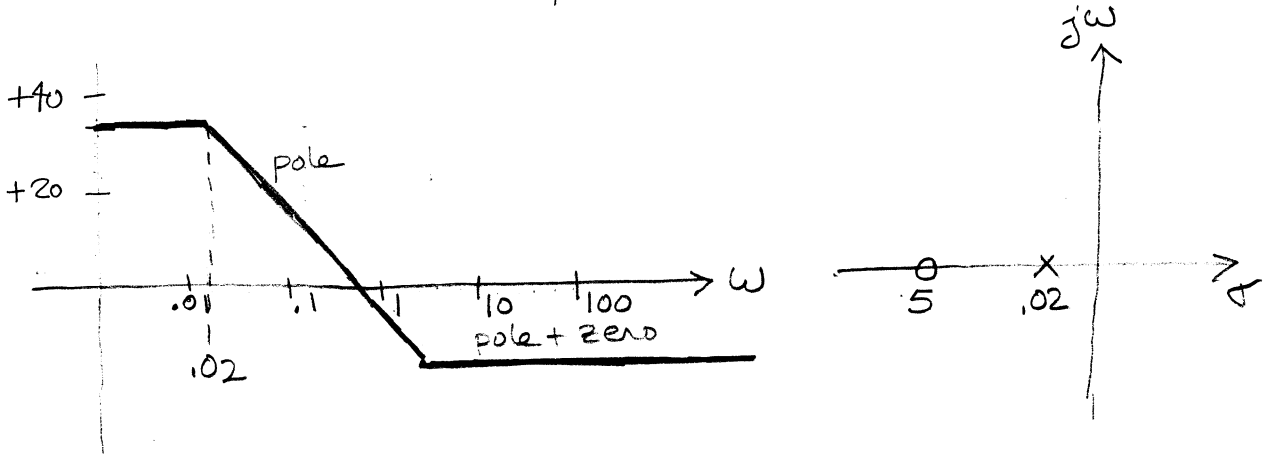
pole comes in at $\omega = 4.6$

$$-20 \log |1 + j\frac{\omega}{4.6}|$$

@ $\omega = 4.6$ this term begins adding -20db/decade

Case II. Same transfer function but $p < z$.

let $K = 40, z = 5, p = .02$



$$|G_1(j\omega)|_{db} = 20 \log 40 + 20 \log \left| 1 + j \frac{\omega}{5} \right| - 20 \log \left| 1 + j \frac{\omega}{.02} \right|$$

at low frequencies $20 \log 40 = +32 \text{ db}$

as ω increases pole at $\omega = .02$ comes in
at -20 db/decade

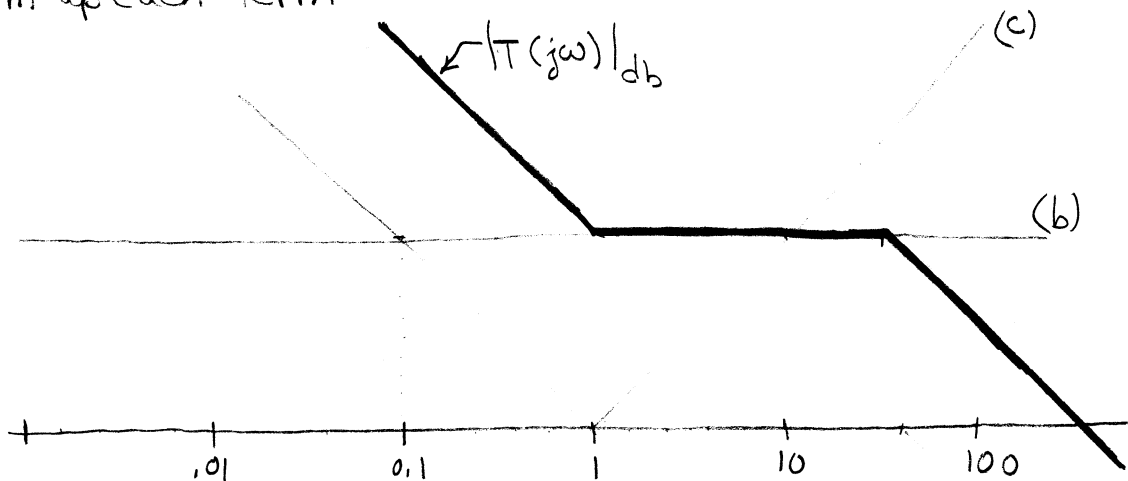
as ω continues to increase zero at
 $\omega = 5$ comes in giving
 $+20 \text{ db/decade}$ canceling out
effect of pole.

You can do more complex functions

Consider
$$T(j\omega) = \sqrt{10} \frac{1 + j\frac{\omega}{1}}{\omega(1 + j\frac{\omega}{50})}$$

Then $|T(j\omega)|_{db} = 20 \log \sqrt{10} + 20 \log |1 + j\frac{\omega}{1}| - 20 \log \omega - 20 \log |1 + j\frac{\omega}{50}|$

Sum up each term



(a) $-20 \log \omega$ term gives -20 dB/decade

(d)

(b) $20 \log \sqrt{10}$ term gives $+10 \text{ dB}$.

(c) @ $\omega = 1$ $+20 \text{ dB/decade}$.

(a)

(d) @ $\omega = 50$ -20 dB/decade .

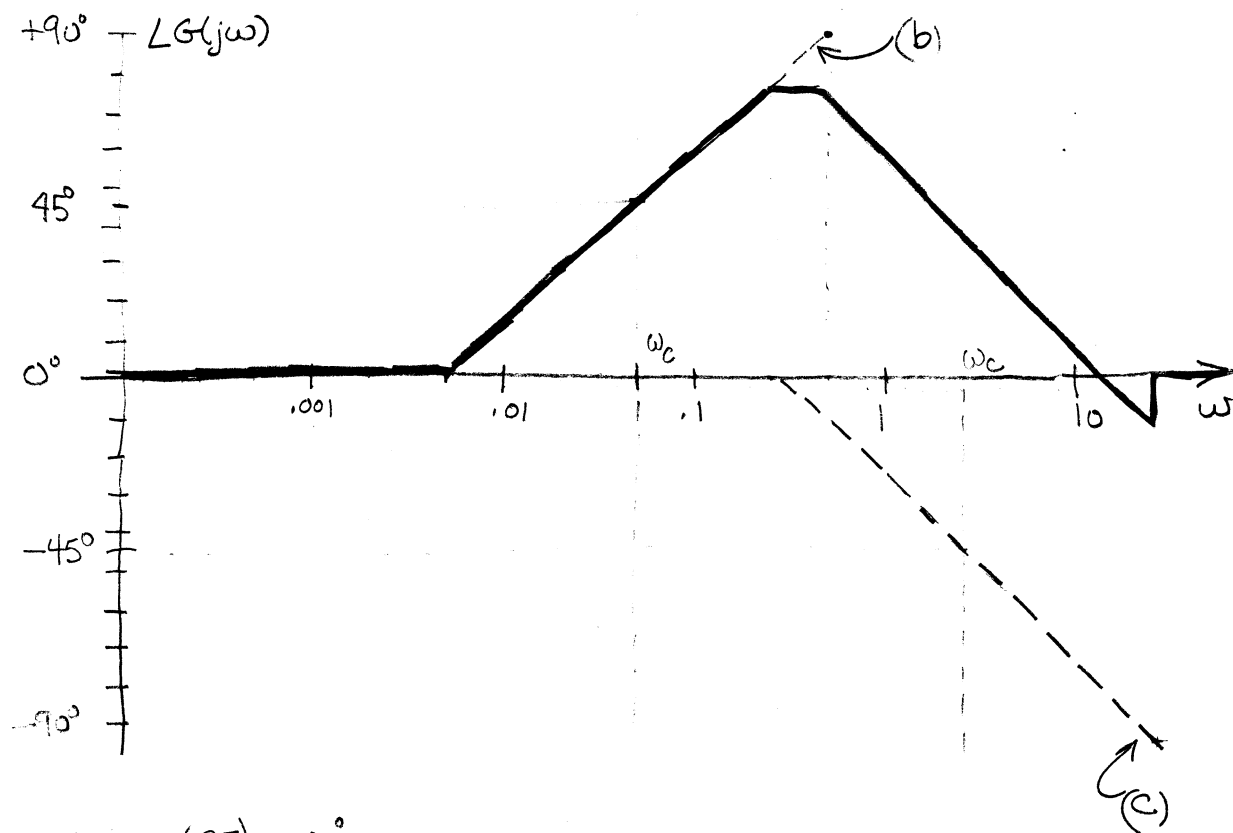
Let's do phase response of 1st order systems.

Phase gets plotted a little differently. It is $\pm 45^\circ$ at ω_c and goes between 0 and ± 90

Example

$$|G(j\omega)|_{dB} = 20 \log K + 20 \log \left| 1 + j \frac{\omega}{z} \right| - 20 \log \left| 1 + j \frac{\omega}{p} \right|$$

$$\angle G(j\omega) = \angle K + \angle \left(1 + j \frac{\omega}{.071} \right) - \angle \left(1 + j \frac{\omega}{4.6} \right)$$



(a) $\angle(.37) = 0^\circ$

(b) $\angle \left(1 + j \frac{\omega}{.071} \right)$

(c) $-\angle \left(1 + j \frac{\omega}{4.6} \right)$