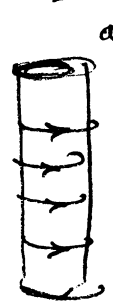


infinitely long.

superposition



an infinite solenoid

case 1

$$\underline{J_s} = K_0 \cos \theta_0 \underline{a_\phi}$$

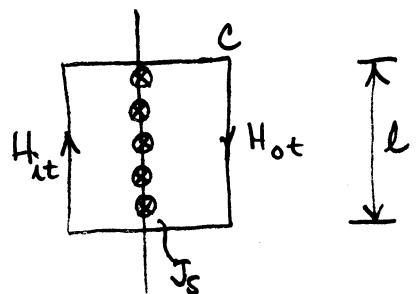


a hollow wire

Case 2.

$$\underline{J_s} = K_0 \sin \theta_0 \underline{a_z}$$

<case 1>



for an infinitely long cylinder there will be no radial fields. what does this mean?

$$\oint \underline{H} \cdot d\underline{l} = \int \underline{J} \cdot d\underline{S} \quad \text{amperes/meter.}$$

$$H_{it} l - H_{ot} l = J_s l.$$

$$H_{it} - H_{ot} = J_s$$

$$B_{it} - B_{ot} = \mu_0 J_s.$$

Argument: vary only  $B_{it}$  or  $B_{ot}$  radially the other is constant hence both must be constant.

ampers  
m.

oooo I.

from our previous studies of the finite length solenoid we know that the field at the center is  $H = \frac{NI}{L}$

$$\begin{aligned} & \# \frac{\text{wires}}{\text{meter}} \times \frac{\text{current}}{\text{wire}} \\ & = \frac{\text{current}}{\text{meter}} \end{aligned}$$

$\therefore$  we know that here the current  $\frac{\text{meter}}{\text{meter}} = J_s$

so that for this case

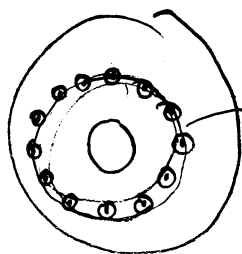
$H$  is simply the current flowing on the surface.

$$\text{i.e. } H = K_o \cos \theta_o.$$

but if  $H_{rt} = J_s \Rightarrow H_{ot} = \phi$ . which we could have argued anyway because how could we have an exterior field.

<case 2>

again use Ampere's Law



surface current  $J_s = K_o \sin \theta_o$

$$\oint H \cdot dl = \int J \cdot ds$$

for  $r < R$   
outside  $r > R$

$$H = 0 \Rightarrow B = 0$$

$$H_{o\phi} \cdot 2\pi r = K_o \sin \theta_o \cdot 2\pi R$$

$$B_{o\phi} = \mu_o K_o \sin \theta_o \frac{R}{r}$$

### Energy stored in the electric field

As we assemble a field, work is done - hence, it is an energy storage device.

simple proof: ① bring  $Q_1$  in from infinity

no work done.

② now bring in charge  $Q_2$

$$\text{work done} = Q_2 V_{21} \triangleq W_{21}$$

[Recall: voltage  $\triangleq \frac{\text{work}}{\text{unit charge}}$ .]

③ bring in charge  $Q_3$

$$\begin{aligned} \text{work done} &= Q_3 V_{31} + Q_3 V_{32} \\ &= W_{31} + W_{32} \end{aligned}$$

④ In general,  $W_e = W_{21} + W_{31} + W_{32} + \dots$

⑤ Order is not important so assemble it in another order.

$$W_e = W_{12} + W_{13} + W_{23} + \dots$$

bring in charge  $Q_1$  with  $Q_3$  first  
then bring in  $Q_2$  with  $Q_2$  and  $Q_3$  present.

⑥ Add together

$$\begin{aligned} 2W_e &= W_{12} + W_{21} + W_{31} + W_{13} + W_{32} + W_{23} + \dots \\ &= \underbrace{Q_1(V_{12} + V_{13}) + Q_2(V_{21} + V_{23}) + Q_3(V_{31} + V_{32}) + \dots}_{\substack{3 \\ \sum_{i=1}^3 Q_i V_i}} \quad \text{where } V_i = \sum_{\substack{j=1 \\ i \neq j}}^3 V_{ij} \\ &= \sum_{i=1}^3 Q_i V_i \end{aligned}$$

total potential on that charge.

discretely:  $W_e = \frac{1}{2} \sum_{i=1}^3 Q_i V_i$

continuously:  $W_e = \frac{1}{2} \int \rho V dv$

for electrostatic fields

$$\nabla \cdot \underline{D} = \rho.$$

$$W_e = \frac{1}{2} \int (\nabla \cdot \underline{D}) \underline{V} \, dv$$

use vector identity  $(\nabla \cdot \underline{D}) \underline{V} = \nabla \cdot (\underline{V} \underline{D}) - \underline{D} \cdot (\nabla \underline{V})$   
sort of the chain rule for the gradient

$$W_e = \frac{1}{2} \int \underbrace{\nabla \cdot (\underline{V} \underline{D})}_{\text{goes to zero}} \, dv - \int \underbrace{\underline{D} \cdot (\nabla \underline{V})}_{\text{goes to } -\epsilon |\underline{E}|^2} \, dv$$

argument consider point charges

$$\underline{E} \sim \frac{1}{r^2}$$

$$\underline{D} \sim \frac{1}{r^2}$$

$$\underline{V} \sim \frac{1}{r}$$

and convert to a surface integral

$$\oint_S \underline{V} \underline{D} \cdot d\underline{S}$$

where  $S \sim 4\pi r^2$

then  $\int \underline{V} \underline{D} \cdot d\underline{S} \sim \int \frac{1}{r} \cdot \frac{1}{r^2} r^2 = \frac{1}{r} \rightarrow 0 \text{ as } r \rightarrow \infty$

The magnetic field is exactly the same, except we use  $\underline{A} \cdot \underline{J}$

in assembling the fields to give.  $W_m = \frac{1}{2} \int \underline{A} \cdot \underline{J} \, dv$

$$W_m = \frac{1}{2} \int \mu |\underline{H}|^2 \, dv$$

Example

energy stored in a uniformly charged sphere.



$$\underline{E} = \begin{cases} \frac{r\rho}{3\epsilon} & 0 \leq r \leq R \\ \frac{R^3\rho}{3\epsilon r^2} & r > R \end{cases}$$

$$W_e = \frac{1}{2}\epsilon \int |\underline{E}|^2 d\tau$$

$$= \frac{1}{2}\epsilon \left\{ \int_0^R \int_0^\pi \int_0^{2\pi} \frac{r^2\rho^2}{9\epsilon^2} r^2 \sin\theta d\theta d\phi dr + \int_R^\infty \int_0^\pi \int_0^{2\pi} \frac{R^6\rho^2}{9\epsilon^2 r^4} r^2 \sin\theta d\theta d\phi dr \right\}$$

$$= \frac{1}{2}\epsilon \left\{ \int_0^R \frac{r^2\rho^2}{9\epsilon^2} 4\pi dr r^2 + \int_R^\infty \frac{R^6\rho^2}{9\epsilon^2 r^4} 4\pi dr r^2 \right\}$$

$$= \frac{1}{2}\epsilon \left\{ \frac{4\pi\rho^2}{9\epsilon^2} \int_0^R r^4 dr + \frac{4\pi R^6\rho^2}{9\epsilon^2} \int_R^\infty \frac{dr}{r^2} \right\}$$

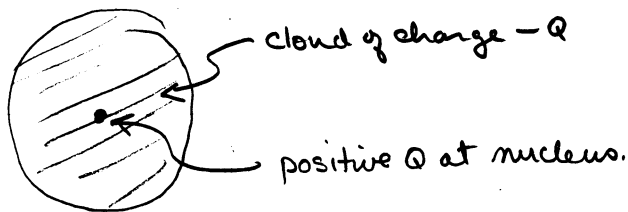
$$= \frac{1}{2}\epsilon \left\{ \frac{4\pi\rho^2}{9\epsilon^2} \frac{R^5}{5} + \frac{4\pi R^6\rho^2}{9\epsilon^2} \frac{1}{R} \right\}$$

$$= \frac{1}{2}\epsilon \frac{4\pi\rho^2}{9\epsilon^2} \left\{ \frac{R^5}{5} + R^5 \right\} = \frac{2\pi\rho^2}{9\epsilon} \left\{ \frac{6R^5}{5} \right\}$$

if we note  $Q = \frac{4}{3}\pi R^3\rho$        $Q^2 = \frac{16}{9}\pi^2 R^6\rho^2$

$$W_e = \frac{Q^2}{20\pi\epsilon R}$$

(2) Energy in assembling an atom?



Assemble electron cloud first?

$$W_e = \frac{3Q^2}{20\pi\epsilon R}$$

How about the positive charge?

What is the energy expended in bringing the  $+Q$  in from  $\infty$ ?  
From our original definition

$$W_e = QV$$

What are the fields and potential from a charged sphere?

The  $\underline{E}$  fields were given above, so the potential is given by

$$\phi_- = \begin{cases} -\frac{3Q}{8\pi\epsilon R^3} (R^2 - \frac{r^2}{3}) & r < R \\ -\frac{Q}{4\pi\epsilon R} & r > R \end{cases}$$

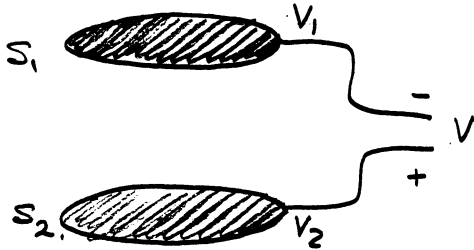
$$\text{Then } W_e = Q\phi_-(r=0) \quad \text{as } \phi_-(\infty) = 0$$

$$= -\frac{3Q^2}{8\pi\epsilon R}$$

$$W_e(\text{total}) = \frac{3Q^2}{20\pi\epsilon R} - \frac{3Q^2}{8\pi\epsilon R} = \frac{3Q^2}{\pi\epsilon R} \left[ \frac{1}{20} - \frac{1}{8} \right]$$

$$= \frac{3Q^2}{\pi\epsilon R} \left[ \frac{8-20}{160} \right] = \frac{3Q^2}{\pi\epsilon R} \left[ -\frac{3}{40} \right] = -\frac{9Q^2}{40\pi\epsilon R}$$

example of capacitor:



best done from definition  $C = \frac{Q}{V}$

$$W_e = \frac{1}{2} \int \rho V \, d\tau$$

$$= \frac{1}{2} \int_{S_1} \rho_s V_1 \, dS_1 + \frac{1}{2} \int_{S_2} \rho_s V_2 \, dS_2$$

surfaces are equipotentials

$$= \frac{1}{2} V_1 \underbrace{\int_{S_1} \rho_s \, dS_1}_{-Q} + \frac{1}{2} V_2 \underbrace{\int_{S_2} \rho_s \, dS_2}_{+Q}$$

total charges

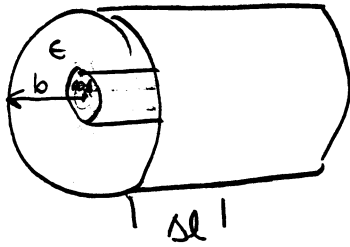
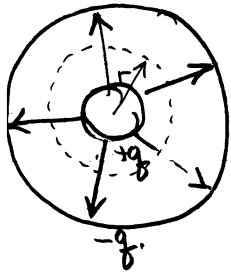
$$= \frac{1}{2} (V_2 - V_1) Q = \frac{1}{2} QV$$

but  $C = \frac{Q}{V}$

$$\therefore W_e = \frac{1}{2} CV^2$$

energy in a capacitor.

a sneaky way of finding capacitance is to use these definitions



$$\oint \mathbf{D} \cdot d\mathbf{S} = \frac{q}{\Delta l}$$

$$\epsilon E \cdot 2\pi r \Delta l = \frac{q}{\Delta l} \Delta l$$

$$E = \frac{q}{\Delta l} \frac{1}{2\pi \epsilon r}$$

what's the energy stored in the line

$$W_e = \frac{1}{2} \epsilon \int |\mathbf{E}|^2 d\mathbf{v} = \frac{1}{2} \epsilon \int_a^b \int_0^{\Delta l} \int_0^{2\pi} \left(\frac{q}{\Delta l}\right)^2 \frac{1}{4\pi^2 \epsilon^2} \frac{1}{r^2} r dr d\phi dz$$

$$= \frac{1}{2} \epsilon \left(\frac{q}{\Delta l}\right)^2 \frac{1}{4\pi^2 \epsilon^2} 2\pi \Delta l \int_a^b \frac{dr}{r}$$

$$\frac{W_e}{\Delta l} = \left(\frac{q}{\Delta l}\right)^2 \frac{1}{4\pi \epsilon} [\ln b - \ln a]$$

but  $W_e = \frac{1}{2} C V^2$

if  $E = \frac{q}{\Delta l} \frac{1}{2\pi \epsilon_0}$   $E = -\nabla \phi$   $\phi = -\int_a^R \mathbf{E} \cdot d\mathbf{l}$

so  $V = -\int_a^b \frac{q}{\Delta l} \frac{1}{2\pi \epsilon} \frac{dr}{r} = \frac{q}{\Delta l} \frac{1}{2\pi \epsilon} (\ln b - \ln a)$

$\therefore \left(\frac{q}{\Delta l}\right)^2 \frac{1}{4\pi \epsilon} [\ln b - \ln a] = \frac{1}{2} C \left(\frac{q}{\Delta l}\right)^2 \frac{1}{4\pi \epsilon^2} [\ln b - \ln a]^2$

$\therefore C = \frac{2\pi \epsilon}{\ln b - \ln a}$

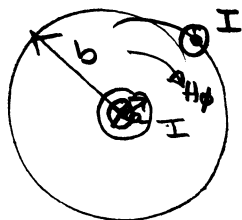


A coaxial cable also carries inductance:

Recall we used Amperes law in class

$$\text{to get } H\phi = \frac{I}{2\pi r}$$

just as for the capacitor  $W_m = \frac{1}{2} L I^2$



again integrate the field over all space.

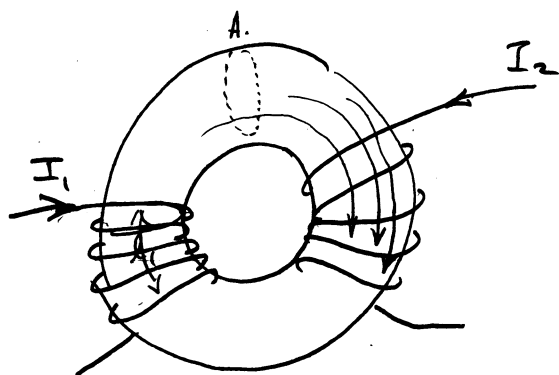
$$\begin{aligned} W_m &= \frac{1}{2} \mu \int_b^b \int_{\Delta l} \int_{2\pi} |H|^2 \, d\tau \\ &= \frac{1}{2} \mu \int_a^b \int_0^{\Delta l} \int_0^{2\pi} \frac{I^2}{4\pi^2 r^2} r \, dr \, d\phi \, dz \\ &= \frac{1}{2} \mu \int_a^b \frac{I^2}{4\pi^2 r^2} r \, 2\pi \Delta l \, dr \\ &= \frac{\mu I^2 \Delta l}{4\pi} \int_a^b \frac{dr}{r} \end{aligned}$$

$$\frac{W_m}{\Delta l} = \frac{\mu I^2}{4\pi} (\ln b - \ln a)$$

$$\therefore \frac{W_m}{\Delta l} = \frac{1}{2} \left( \frac{L}{\Delta l} \right) I^2 = \frac{\mu I^2}{4\pi} (\ln b - \ln a)$$

$$\left( \frac{L}{\Delta l} \right) = \frac{2\mu}{4\pi} (\ln b - \ln a) = \frac{\mu}{2\pi} [\ln b - \ln a]$$

What is inductance? Inductance refers to flux linkage.



What is the flux due to coil  $I_1$

$$\Phi_m = \frac{\mu N I}{l_1} dS$$

the flux linked by a particular coil

the flux linkage is defined as  $\lambda = N \Phi_m$ .

the inductance is then defined to be.  $L = \frac{\lambda}{I}$

For this toroid 
$$L = \frac{\lambda}{I} = \frac{N \Phi_m}{I} = \frac{N \mu N I dS}{I l_1} = \frac{\mu N^2 dS}{l_1}$$

How about the second coil

$$\lambda_2 = N_2 \Phi_m$$

$$L_{21} = \frac{\lambda_2}{I_1} = \frac{N_2}{I_1} \mu N_1 I_1 dS_2 = \mu N_1 N_2 dS_2$$

this is usually called the mutual inductance

but  $L_2$  also exists as  $L_2 = \frac{\mu N_2^2 dS_2}{l_1}$

in general we say  $L_{21} = M_{21}$  which is the coupling coefficient.

$$M_{21} = k \sqrt{L_2 L_1}$$

## Electromagnetic forces

magnetic system → input electric energy = mechanical work done + increase in stored energy.

$$\underline{I d\lambda} = F dx + dW_m.$$

how do you know this  
this we can't prove yet!

electric system

$$\underline{V I dt} = \underbrace{F dx}_{\text{mechanical work done}} + \underbrace{dW_m}_{\text{increase in stored energy.}}$$

$$v = - \frac{d\Phi}{dt}$$

$v dt = - d\Phi$  this is energy being taken out of the system

$v dt = d\Phi$  putting energy into the system,

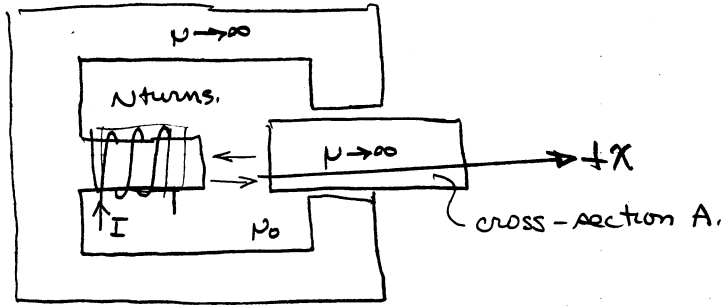
The inductance is handy here:

$$W_m = \frac{1}{2} L(x) i^2$$

$$dW_m = \frac{1}{2} i^2 L(x)$$

{ usually the current is constant  
but  $L$ , a function of geometry,  
changes.

(a) relay.



If we let the permeability of the core  $\rightarrow \infty$  then our magnetic circuit consists of only the source and the gap (a high reluctance).

what is the source  $\mathcal{F} = NI$

what is the reluctance of the gap?  $R_g = \frac{l}{\mu_0 A} = \frac{x}{\mu_0 A}$ .

$$\Phi = \frac{\mathcal{F}}{R_g} = \frac{NI}{x} \mu_0 A$$

flux linked by  $N$  turns:

$$L \triangleq \frac{N\Phi}{I} = \frac{N^2 \mu_0 A}{x}$$

$$W_m = \frac{1}{2} LI^2$$

$$F_x = \frac{dW_m}{dx} = \frac{1}{2} I^2 \frac{dL}{dx} = -\frac{1}{2} \frac{I^2 N^2 \mu_0 A}{x^2}$$

$\therefore$  piece is attracted to the coil

(b) magnetized material

for magnetic material  $w_m = \frac{1}{2} \int \mu_0 |M|^2 dv$

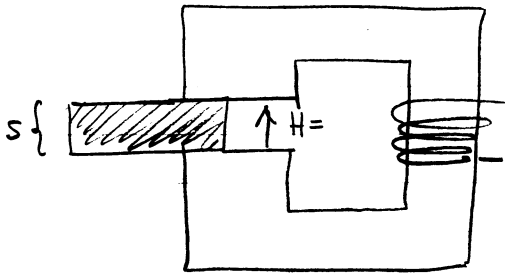
long way.

$\frac{\text{force}}{\text{unit volume}}$   
 $F = \int [\mu_0 (M \cdot \nabla) H + \mu_0 \underline{J}_f \times \underline{H}] dv$

this follows from  $\nabla \times B = \mu_0 \underline{J}_f + \nabla \times M$

$f = \text{curl} \times B$

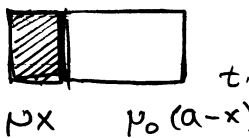
no free currents so  $F_{\text{total}} = \int [\mu_0 M \cdot \nabla H] dv$



$\mathcal{F} = NI$      $R_g = \frac{s}{\mu_0 A}$

$\Phi = \frac{\mathcal{F}}{R} = \frac{NI \mu_0 A}{s}$

except  $\mu$  is not constant.



$R_g = \frac{s}{\mu t x}$      $R_g' = \frac{s}{\mu_0 t (a-x)}$

$\Phi = \frac{NI (\mu t x)}{s}$      $\Phi' = \frac{NI \mu_0 t (a-x)}{s}$

$\Phi_{\text{total}} = \frac{NI t}{s} [\mu x + \mu_0 (a-x)]$

$L = \frac{N \Phi_{\text{total}}}{I} = \frac{N^2 t}{s} [\mu x + \mu_0 (a-x)]$

$f_x = \frac{d}{dx} \left( \frac{1}{2} L I^2 \right) = \frac{1}{2} I^2 \frac{N^2 t}{s} [\mu + \mu_0]$

since  $\mu > \mu_0$  force pulls magnet into gap.

## time dependent fields.

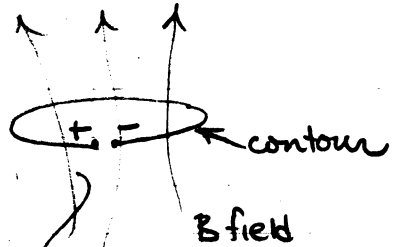
all boundary conditions, Gauss' Law, etc. remain the same.  
The big difference is something called the displacement current.  
and Faraday's law.

Faraday's law

$$\text{emf} = - \frac{d\Phi_m}{dt}$$

we use emf specifically because this is really a separation of charge to produce the potential. Because the loop is usually a conductor there is no E field across it and it all appears across the gap.

$$\oint_C \underline{E} \cdot d\underline{l} = - \frac{d}{dt} \int \underline{B} \cdot d\underline{s}$$



Use right hand rule,  $\frac{d\Phi}{dt} > 0$  polarity as shown

what's really important is that we showed that the E field was conservative for static fields

$$\text{i.e. } \oint_C \underline{E} \cdot d\underline{l} = 0$$

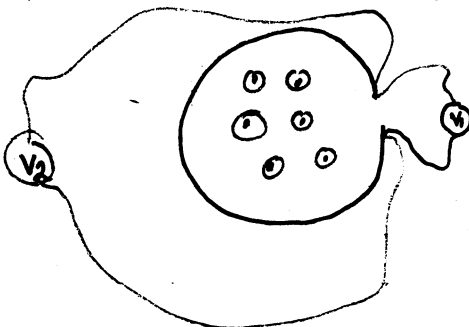
this is not true.  $\oint_C \underline{E} \cdot d\underline{l} = - \frac{d\Phi}{dt} \neq 0.$

specifically

$$\int_{P_1}^{P_2} \underline{E} \cdot d\underline{l} + \int_{P_2}^{P_1} \underline{E} \cdot d\underline{l} \neq 0$$

so there are not equal.

to show how important the choice of contour is:



for  $v_1$

$$v_1 + \int_{\text{leads}} \underline{E} \cdot d\underline{\ell} + \int_C \underline{E} \cdot d\underline{\ell} = - \frac{d}{dt} \left[ \int_{\text{meter loop}} \underline{B} \cdot d\underline{S} + \int_S \underline{B} \cdot d\underline{S} \right]$$

since there is no  $\underline{E}$  field along a conductor  
all  $\int \underline{E} \cdot d\underline{\ell} \rightarrow 0$

$$v_1 = - \frac{d}{dt} \left[ \int_{\text{meter loop}} \underline{B} \cdot d\underline{S} + \int_S \underline{B} \cdot d\underline{S} \right]$$

If the meter loop is small we will get approximately the correct result.

Even more importantly suppose  $v_1$  is as shown then the enclosed flux is what we wanted  
if  $v_2$  is as shown then the enclosed flux is zero.

You can convert Faraday's law to point form.

$$\oint_C \underline{E} \cdot d\underline{\ell} = - \frac{d}{dt} \int \underline{B} \cdot d\underline{S}$$

$$= - \int \frac{\partial}{\partial t} (\underline{B} \cdot d\underline{S})$$

partial because of the spatial coordinates

moving contour.

if  $S$  is stationary  $\oint \underline{E} \cdot d\underline{\ell} = - \int \frac{\partial \underline{B}}{\partial t} \cdot d\underline{S}$

use Stokes' theorem and this becomes

$$\int \nabla \times \underline{E} \cdot d\underline{S} = - \int \frac{\partial \underline{B}}{\partial t} \cdot d\underline{S}$$

$$\nabla \times \underline{E} = - \frac{\partial \underline{B}}{\partial t}$$

Faraday's law gives us time varying fields & Maxwell's eqns so let's review everything we've done to put it into a time dependent form.

Gauss' law (no change)

$$\nabla \cdot \underline{D} = \rho \quad \oint_s \underline{D} \cdot d\underline{s} = \int_v \rho dv$$

$$\nabla \cdot \underline{B} = 0 \quad \oint_s \underline{B} \cdot d\underline{s} = 0$$

Ampère's law

static  $\nabla \times \underline{H} = \underline{J}$

time dependent  $\nabla \times \underline{H} \stackrel{?}{=} \underline{J}$

$\nabla \cdot \nabla \times \underline{H} = 0$  vector identity  $\nabla \cdot \underline{J} \neq 0$  as shown below

from the continuity equation  $\nabla \cdot \underline{J} = -\frac{\partial \rho}{\partial t}$

but for time dependent fields the charge is not necessarily static, i.e.  $\frac{\partial \rho}{\partial t} \neq 0$ .

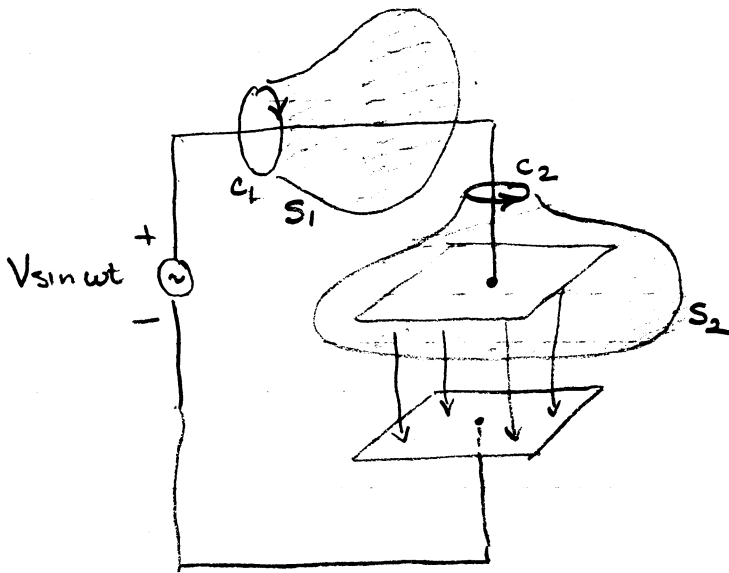
There is thus a missing term in this equation.

Maxwell chose to add that term on the right hand side

Displacement current  $\frac{\partial \underline{D}}{\partial t}$

This new term is called the displacement current even though it is not a physical current.





$$\oint \underline{H} \cdot d\underline{l} = \int_S \underline{j} \cdot d\underline{s} + \int_S \frac{\partial \underline{D}}{\partial t} \cdot d\underline{s}$$

$C_1 - S_1$

conduction current  $\underline{j}$  going through  $S_1$  gives rise to  $H_1$  about  $C_1$ .

$C_2 - S_2$

no conduction current  $\underline{j}$  going through  $S_2$  is there no  $H_2$  around  $C_2$ .

but free charge is transferred  $\Rightarrow$  there is an  $H_2$  but as this free charge is transferred it changes  $\underline{D}$  creating an induced current on the other plate.  $\therefore \frac{\partial \underline{D}}{\partial t}$  is due to the apparent motion of  $\frac{\partial}{\partial t}$  electrons.

to determine the ratio of these effects.

$$\nabla \times \underline{H} = \underline{j} + \frac{\partial \underline{D}}{\partial t}$$

$$\text{if } \underline{E} = E_0 e^{j\omega t} \quad \underline{D} = \epsilon \underline{E} = \epsilon E_0 e^{j\omega t}$$

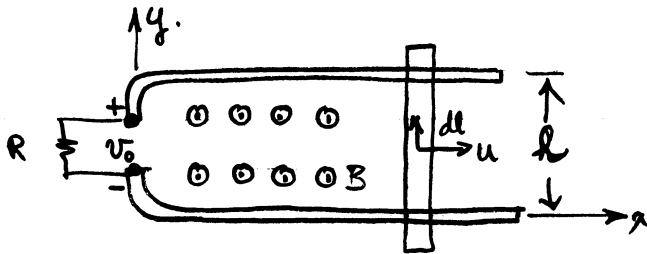
$$\underline{j} = \sigma E_0 e^{j\omega t} \quad \frac{\partial \underline{D}}{\partial t} = \frac{\epsilon(j\omega) E_0 e^{j\omega t}}$$

$$\therefore \frac{\frac{\partial \underline{D}}{\partial t}}{\underline{j}} = \frac{\sigma E_0 e^{j\omega t}}{j\omega \epsilon E_0 e^{j\omega t}} = \frac{\sigma}{j\omega \epsilon}$$

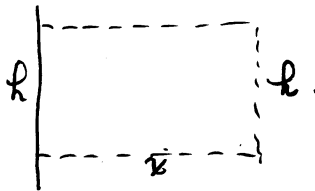
$$\left| \frac{\frac{\partial \underline{D}}{\partial t}}{\underline{j}} \right| = \frac{\sigma}{\omega \epsilon} \quad \leftarrow \text{conduction angle}$$

Example:

$$\mathcal{V}_0 = - \frac{d}{dt} \int \underline{B} \cdot d\underline{S}$$



A metal bar slides over a pair of conducting rails in a uniform magnetic field  $\underline{B} = B_0 \underline{a}_z$  with a constant velocity  $u$ .



(a)  $\int \underline{B} \cdot d\underline{S} = B l x$

$$\mathcal{V}_0 = - \frac{d}{dt} \int \underline{B} \cdot d\underline{S} = - \frac{d}{dt} (B l x) = - B l \frac{dx}{dt} = - B l u$$

(b) how much electrical power is developed.

$$I_{\text{out}} = \frac{\mathcal{V}_0}{R} = \frac{B l u}{R}$$

$$P_{\text{out}} = I^2 R = \frac{(B l u)^2}{R}$$

# properties of the medium

$$\nabla \times \underline{E} = -\frac{\partial \underline{B}}{\partial t}$$

$$\oint_C \underline{E} \cdot d\underline{l} = -\frac{d}{dt} \int_S \underline{B} \cdot d\underline{s}$$

$$\nabla \times \underline{H} = \underline{j} + \frac{\partial \underline{D}}{\partial t}$$

$$\oint_C \underline{H} \cdot d\underline{l} = \int_S \underline{j} \cdot d\underline{s} + \frac{d}{dt} \int_S \underline{D} \cdot d\underline{s}$$

$$\nabla \cdot \underline{D} = \rho$$

$$\oint_S \underline{D} \cdot d\underline{s} = \int_V \rho \, dv$$

$$\nabla \cdot \underline{B} = 0$$

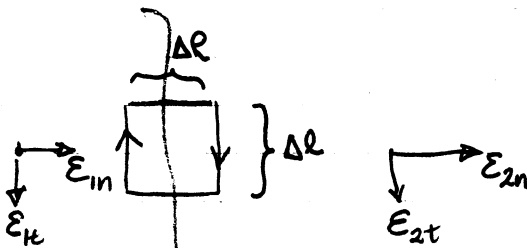
$$\oint_S \underline{B} \cdot d\underline{s} = 0$$

$$\underline{E} = \underline{j} \left( \frac{1}{\sigma} + \underline{u} \times \underline{B} \right)$$

$$\nabla \cdot \underline{j} = -\frac{\partial \rho}{\partial t}$$

Do any of our boundary conditions change?

the only thing that we added was Faraday's law?  
does this change the field B.C.'s.



re-call we used  $\oint_C \underline{E} \cdot d\underline{l} = 0$  as  $\Delta h \Delta l \rightarrow 0$

Fields are no longer conservative

$$\oint \underline{E} \cdot d\underline{l} = -\frac{d}{dt} \int_{S_b} \underline{B} \cdot d\underline{s}$$

if  $\underline{B}$  is finite  
then  $\underline{B}$

$$\therefore \underline{E}_{1t} = \underline{E}_{2t}$$

although its not a good argument as the  
surface  $\rightarrow 0$   
as  $\Delta h \rightarrow 0$   $\frac{d}{dt} \int \underline{B} \cdot d\underline{s} \rightarrow 0$ .

How about Ampère's law?

$$\oint_C \underline{H} \cdot d\underline{e} = \int_S \underline{j} \cdot d\underline{s} + \frac{d}{dt} \int_S \underline{D} \cdot d\underline{s}$$

same contour,

again, as  $\Delta h \Delta l \rightarrow 0$

$$\frac{d}{dt} \int_S \underline{D} \cdot d\underline{s} \rightarrow 0 \quad \text{so results are the same,}$$

$$\underline{H}_{1z} - \underline{H}_{2z} = \underline{K}_s$$

One important consequence of these laws is a perfect conductor,

as before  $\underline{j}_d = \sigma \underline{E}$

$$\sigma = \frac{\underline{j}_d}{\underline{E}}$$

if  $\sigma = \infty$ , then either  $\underline{j}_d = \infty$ , or  $\underline{E} = 0$

↑  
not physically  
realizable

↑  
use this

if  $\underline{E} = 0$  then  $\underline{D} = \epsilon \underline{E} = 0$  also,

use Faraday's Law  $\nabla \times \underline{E} = -\frac{\partial \underline{B}}{\partial t}$

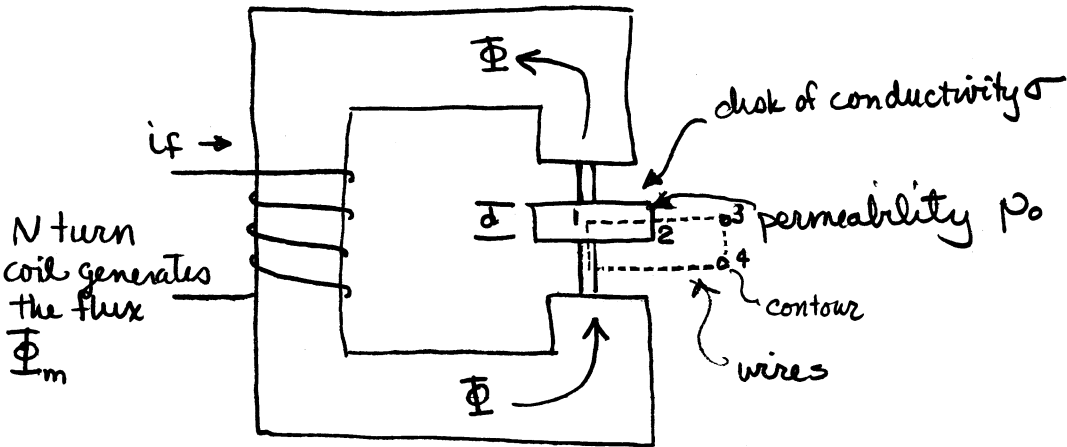
if  $\underline{E} = 0$ , then  $\frac{\partial \underline{B}}{\partial t} = 0$

$\therefore$  there is no time varying magnetic field.

$\therefore$  in a conductor  $\rightarrow$  no  $\underline{E}$  fields  
perfect  $\uparrow$  only a static  $\underline{H}$  field.

Occam's  
Razor.

# Faraday disk homopolar generator



what is the field across the gap? we did this problem already.

$$\mathcal{F} = NI$$

$$R_{\text{gap}} = \frac{s}{\mu_0 A}$$

$$\Phi_m = \frac{\mathcal{F}}{R_{\text{gap}}} = \frac{NI}{\frac{s}{\mu_0 A}} = \mu_0 \frac{NIA}{s}$$

$$\cancel{BA} = \mu_0 \frac{NIA}{s}$$

$$B_{\text{gap}} = \mu_0 \frac{NI}{s}$$

for moving fields

Lorentz  $\underline{F} = q(\underline{E} + \underline{v} \times \underline{B})$

if I travel with a velocity

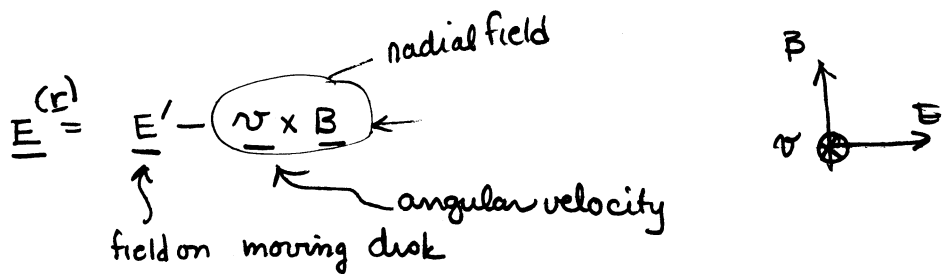
$\underline{v}$  I see only a

field  $q\underline{E}'$

where  $q\underline{E}' = q(\underline{E} + \underline{v} \times \underline{B})$

thus  $\underline{E}' = \underline{E} + \underline{v} \times \underline{B}$

for a charge  $q$  moving at velocity  $\underline{v}$  in  $\underline{E}, \underline{B}$  fields.



$$= \frac{J_r}{\sigma} - \omega r B_{gap} = \frac{i_r}{2\pi r d} - \omega r B_{gap}$$

the current is the same in all frames.

Now use Faraday's law on contour shown.....

$$\oint \underline{E} \cdot d\underline{l} = \int_1^2 E_r dr + \int_3^4 \underline{E} \cdot d\underline{l} = \tau \frac{dB}{dt} \text{ since } B \text{ is not changing}$$

$-\nu_r$

$$\therefore \nu_r = \int_1^2 E_r dr$$

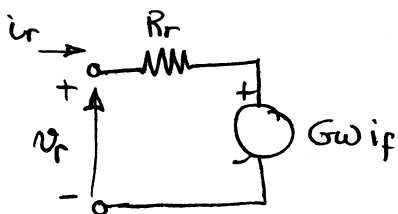
$$= \int_{R_1}^{R_2} \left[ \frac{i_r}{2\pi d r} - \omega r B_{gap} \right] dr$$

$$= \frac{i_r}{2\pi r d} [\ln R_2 - \ln R_1] - \omega B_{gap} \left[ \frac{R_2^2 - R_1^2}{2} \right]$$

$$\approx i_r R_r - G \omega i_f \leftarrow \text{speed coefficient}$$

$\leftarrow \text{rotor resistance}$

this is typically a very high current low voltage device.  $i_f$  is the field current.

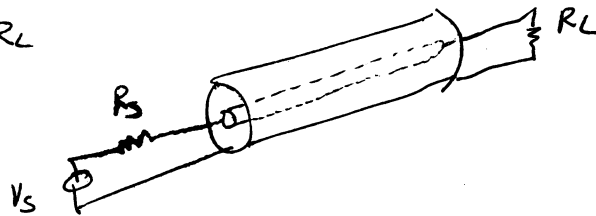
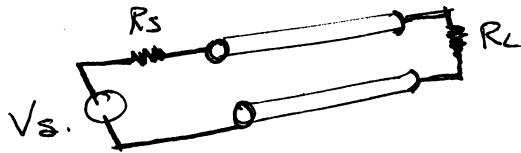


for  $\sigma = 6 \times 10^7$  siemens/m  
 $d = 1 \text{ mm}$   
 $\omega = [3600 \text{ rpm}] = 120\pi \text{ rad/sec.}$   
 $R_1 = 1 \text{ cm}$   
 $R_2 = 10 \text{ cm}$

$G \omega i_f = -1.9 \text{ volts.}$   
 slot circuit current  $\approx 350,000$  Amperes.

# TRANSMISSION LINES

guide propagation of energy from one point to another  
typically two conductors, (infinitely long at first)



these are uniform, i.e. cross-section is uniform,  
lossless  $\rightarrow$  no dielectric losses so Poynting  
vector is towards load.



as these are long, fields must only  
be in transverse coordinates

and uniform,

This has important results!

## Maxwell's Equations

$$\oint \underline{E} \cdot d\underline{l} = -\mu \frac{d}{dt} \int \underline{H} \cdot d\underline{s}$$

pick contour in  
transverse plane,

let  $d\underline{s}$  be in transverse  
plane

$$\oint \underline{H} \cdot d\underline{l} = \int \underline{j} \cdot d\underline{s} + \frac{\partial}{\partial t} \int \underline{D} \cdot d\underline{s}$$

pick  $x, y$  coordinates

$$\oint (E_x dx + E_y dy) = -\mu \frac{d}{dt} \int H_z dx dy$$

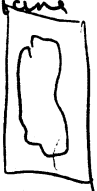
since  $d\underline{s} \neq dx dy \underline{a}_z$

$$\oint (H_x dx + H_y dy) = \int j_z dx dy + \epsilon \frac{\partial}{\partial t} \int E_z dx dy$$

but  $H_z = E_z = 0$  only transverse coordinates

$\therefore$  all time derivatives  $\rightarrow 0$

thus, the static solutions are valid.



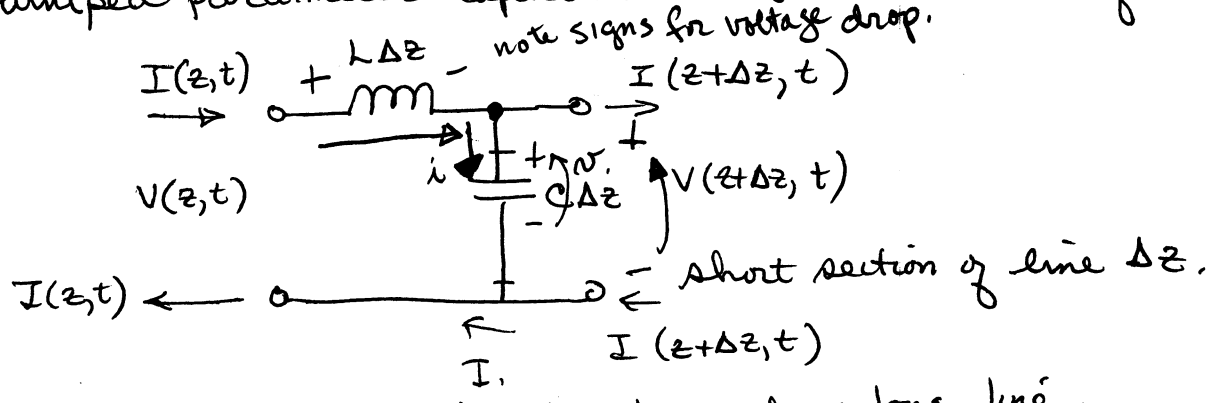
in plane.

i.e.

If the fields are the static fields we get some interesting results.

- ① electric field is conservative
- ② per unit length inductance is constant
- ③ per unit length capacitance is constant

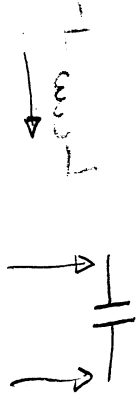
lumped parameter capacitance and inductance of lines.



I can stick these together to make a long line.  
 Note that these parameters are almost independent of frequency!

what do we know about circuits

for inductors  $v = L \frac{di}{dt}$



$v = \int i dt$

$$\frac{V(z+\Delta z, t) - V(z, t)}{\Delta z} = -L \frac{\partial I}{\partial t} = -L \Delta z \frac{\partial I(z, t)}{\partial t}$$

because of this relationship for capacitors  $i = C \frac{dv}{dt}$

$$\frac{I(z+\Delta z, t) - I(z, t)}{\Delta z} = -C \frac{\partial V}{\partial t} = -C \Delta z \frac{\partial V(z+\Delta z, t)}{\partial t}$$

- sign to indicate current out of capacitor

$$I(z+\Delta z, t) - I(z, t) = -C \Delta z \frac{\partial}{\partial t} \left[ V(z, t) - L \Delta z \frac{\partial I(z, t)}{\partial t} \right]$$

$$\frac{I(z+\Delta z, t) - I(z, t)}{\Delta z} = -C \Delta z \frac{\partial V(z, t)}{\partial t} + LC (\Delta z)^2 \frac{\partial^2 I(z, t)}{\partial t^2}$$



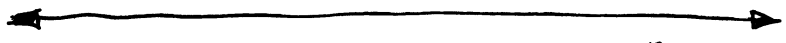
if  $\Delta z \rightarrow 0$  becomes

transmission  
line equations

$$\frac{\partial V}{\partial z} = -L \frac{\partial I}{\partial t}$$

$$\frac{\partial I}{\partial z} = -C \frac{\partial V}{\partial t}$$

second term goes to zero.



$$\begin{aligned} \frac{\partial^2 V}{\partial z^2} &= -L \frac{\partial^2 I}{\partial z \partial t} = -L \frac{\partial}{\partial t} \left( \frac{\partial I}{\partial z} \right) \\ &= -L \frac{\partial}{\partial t} \left( -C \frac{\partial V}{\partial t} \right) = LC \frac{\partial^2 V}{\partial t^2} \end{aligned}$$

like wise

$$\boxed{\frac{\partial^2 I}{\partial z^2} = LC \frac{\partial^2 I}{\partial t^2}}$$

$$\boxed{\frac{\partial^2 V}{\partial z^2} = LC \frac{\partial^2 V}{\partial t^2}}$$

where  $\frac{1}{\sqrt{LC}} = u$

the velocity of propagation

easy way to show this

$$V(z,t) = V^+(t - \frac{z}{u}) + V^-(t + \frac{z}{u})$$

$$I(z,t) = I^+(t - \frac{z}{u}) + I^-(t + \frac{z}{u})$$

don't know the form, but these are just like our phase functions

look at what happens.

$$\begin{aligned} \frac{\partial V}{\partial z} &= \frac{\partial V^+}{\partial s^+} \frac{\partial s^+}{\partial z} + \frac{\partial V^-}{\partial s^-} \frac{\partial s^-}{\partial z} = \frac{\partial V^+}{\partial s^+} \left( -\frac{1}{u} \right) + \frac{\partial V^-}{\partial s^-} \left( \frac{1}{u} \right) \\ \frac{\partial^2 V}{\partial z^2} &= -\frac{1}{u} \frac{\partial^2 V^+}{\partial s^{+2}} \frac{\partial s^+}{\partial z} + \frac{1}{u} \frac{\partial^2 V^-}{\partial s^{-2}} \frac{\partial s^-}{\partial z} = \frac{1}{u^2} \left[ \frac{\partial^2 V^+}{\partial s^{+2}} + \frac{\partial^2 V^-}{\partial s^{-2}} \right] \\ \frac{\partial^2 V}{\partial t^2} &= \frac{\partial V^+}{\partial s^+} \frac{\partial s^+}{\partial t} + \frac{\partial V^-}{\partial s^-} \frac{\partial s^-}{\partial t} = \frac{\partial V^+}{\partial s^+} + \frac{\partial V^-}{\partial s^-} \\ \frac{\partial^2 V}{\partial t^2} &= \frac{\partial^2 V^+}{\partial s^{+2}} + \frac{\partial^2 V^-}{\partial s^{-2}} \end{aligned}$$