

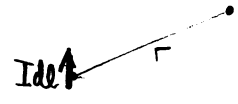
return to Lorentz Force Law.

$$\underline{F} = q \underline{E} + \underbrace{q \underline{v} \times \underline{B}}$$

Force due to charge in motion.

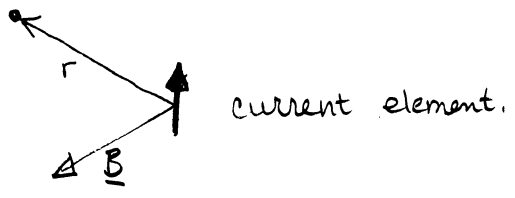
basically (without proof) the Biot - Savart Law

$$d\underline{H} = \frac{I d\underline{l} \times \underline{ar}}{4\pi r^2}$$



$H$  is the magnetic field intensity, it corresponds to  $E$ . There also is a  $\underline{B}$  which corresponds to  $D$ .

- ① Ampere' showed that currents exert forces on magnets.
- ② the next result was that electric currents exert forces on each other - and that a magnet could be replaced by a current.
- ③ the Biot - Savart Law involved determining the magnetic field from a magnet and an equivalent current.



④ the magnetic field intensity at  $\underline{r}$  is given mathematically by

$$\underline{H}(\underline{r}) = \frac{I d\underline{l} \times \underline{ar}}{4\pi r^2}$$

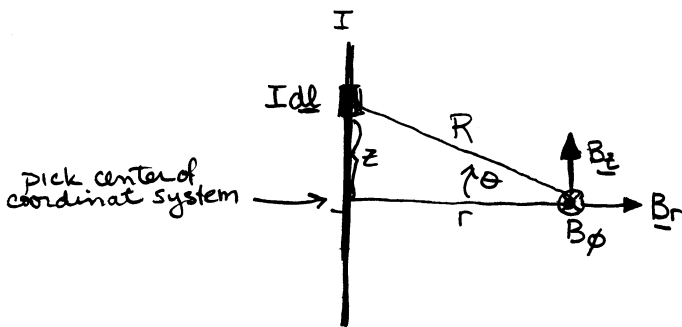
⑤ in general,  $I$  flows in a complex direction so we use the linear nature of the Biot-Savart Law and add up the contributions from many current elements.

$$H_{\text{tot}}(\underline{r}) = \int dH(\underline{r}) = \int \frac{I \underline{dl} \times \underline{a}_R}{4\pi r^2}$$

this is a contour integral

Three examples:

① current in a wire



Ⓐ use cylindrical coordinates

Ⓑ define the angle  $\theta$  as shown so that

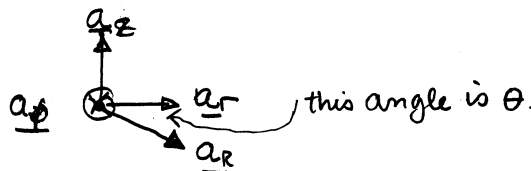
$$\underline{B} = B_r \underline{a}_r + B_\phi \underline{a}_\phi + B_z \underline{a}_z$$

Ⓒ Biot Savart Law

$$\underline{H}(\underline{r}, \phi, z) = \int \frac{I \underline{dl} \times \underline{a}_R}{4\pi R^2}$$

what is  $I \underline{dl}$ ?  $I dz \underline{a}_z$

what is  $\underline{a}_R$ ?



$$\text{let } \underline{a}_R = c_\phi \underline{a}_\phi + c_r \underline{a}_r + c_z \underline{a}_z$$

$$\text{dotting with } \underline{a}_r: \underline{a}_R \cdot \underline{a}_r = c_\phi \underline{a}_\phi \cdot \underline{a}_r + c_r \underline{a}_r \cdot \underline{a}_r + c_z \underline{a}_z \cdot \underline{a}_r$$

$$\underbrace{|\underline{a}_R| |\underline{a}_r| \cos \theta}_1 = 1$$

$$\therefore \cos \theta = c_r$$

dotting with  $\underline{a}_\phi$ :

$$\underline{a}_R \cdot \underline{a}_\phi = c_\phi \underbrace{\underline{a}_\phi \cdot \underline{a}_\phi}_1 + c_r \cancel{\underline{a}_\phi \cdot \underline{a}_r} + c_z \cancel{\underline{a}_z \cdot \underline{a}_\phi}$$

$$|\underline{a}_R| |\underline{a}_\phi| \cos \frac{\pi}{2}$$

this can also be seen to be zero as  $\underline{a}_R$  and  $\underline{a}_\phi$  are perpendicular.  $\therefore c_\phi = 0.$

dotting with  $\underline{a}_z$ :

$$\underline{a}_R \cdot \underline{a}_z = c_\phi \cancel{\underline{a}_\phi \cdot \underline{a}_z} + c_r \underline{a}_r \cdot \underline{a}_z + c_z \cancel{\underline{a}_z \cdot \underline{a}_z}$$

$$|\underline{a}_R| |\underline{a}_z| \cos(\frac{\pi}{2} + \theta)$$

$$1 \cdot 1 \cdot \cos \frac{\pi}{2} \cos \theta - \sin \frac{\pi}{2} \sin \theta$$

$$0 \cdot \cos \theta - 1 \cdot \sin \theta$$

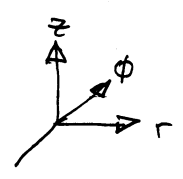
$\therefore c_z = -\sin \theta.$

and  $\underline{a}_R = \cos \theta \underline{a}_r - \sin \theta \underline{a}_z$

What is R?  $R = \sqrt{z^2 + r^2}.$

Ⓐ reduce integral

$$\underline{H}(r, \phi, z) = \int \frac{I dz \underline{a}_z \times (\cos \theta \underline{a}_r - \sin \theta \underline{a}_z)}{4\pi (z^2 + r^2)}$$



$$= \int \frac{I dz \cos \theta \underline{a}_\phi}{4\pi (z^2 + r^2)} - \int \frac{I dz \sin \theta \cancel{\underline{a}_z \times \underline{a}_z}}{4\pi (z^2 + r^2)}$$

note that  $\cos \theta = \frac{r}{R}$  and write integral only in terms of z and r.

i.e.  $\cos \theta = \frac{r}{R} = \frac{r}{\sqrt{z^2 + r^2}}$

$$\begin{aligned} \underline{H}(r, \phi, z) &= \int \frac{I r a \phi}{4\pi (z^2 + r^2)^{3/2}} dz \\ &= \int \frac{I r a \phi}{4\pi (z^2 + r^2)^{3/2}} dz \\ &= \frac{I r a \phi}{4\pi} \int \frac{dz}{(z^2 + r^2)^{3/2}} \end{aligned}$$

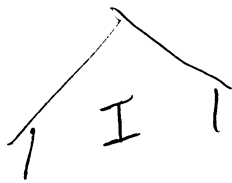
Ⓒ Now determine the exact contour and evaluate the integral. There is a trick here.

Let the wire extend from  $-\frac{L}{2}$  to  $+\frac{L}{2}$ .

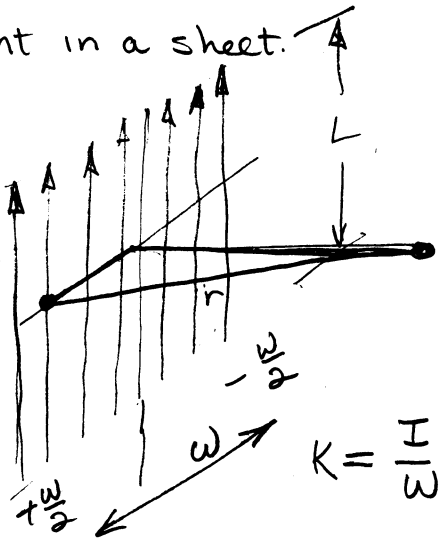
$$\begin{aligned} \int_{-\frac{L}{2}}^{+\frac{L}{2}} \frac{dz}{(z^2 + r^2)^{3/2}} &= \frac{z}{r^2 (z^2 + r^2)^{1/2}} \Big|_{-\frac{L}{2}}^{+\frac{L}{2}} \\ &= \frac{\frac{L}{2}}{r^2 (\frac{L^2}{4} + r^2)^{1/2}} - \frac{-\frac{L}{2}}{r^2 (\frac{L^2}{4} + r^2)^{1/2}} \\ &= \frac{L}{r^2 (\frac{L^2}{4} + r^2)^{1/2}} \end{aligned}$$

$$\begin{aligned} \therefore \underline{H}(r, \phi, z) &= \frac{I r a \phi}{4\pi} \frac{L}{r^2 (\frac{L^2}{4} + r^2)^{1/2}} \\ &= \frac{I}{4\pi r} a \phi \frac{L}{(\frac{L^2}{4} + r^2)^{1/2}} \end{aligned}$$

Note that if  $L \rightarrow 0$   $\underline{H}(r, \phi, z) \rightarrow \frac{I}{2\pi r} a \phi$



② current in a sheet.



a sheet looks like a lot of line currents.

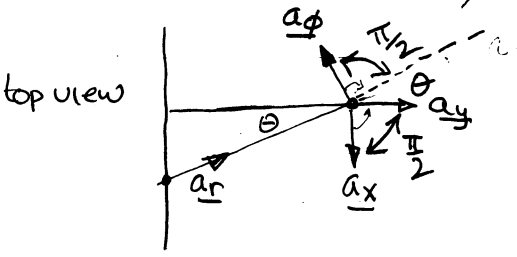
do this problem in x,y,z coordinates  
Why? easy to add vectors at point R.

we know  $H(r, \phi, z) = \frac{I}{4\pi r} \underline{a_\phi}$  as  $L \rightarrow \infty$

what is this in Cartesian coordinates

$$H_\phi \underline{a_\phi} = H_x \underline{a_x} + H_y \underline{a_y} + H_z \underline{a_z}$$

$$H_\phi \cdot \underline{a_\phi} \cdot \underline{a_x} = H_x \underline{a_x} \cdot \underline{a_x} + H_y \underline{a_y} \cdot \underline{a_x} + H_z \underline{a_z} \cdot \underline{a_x}$$



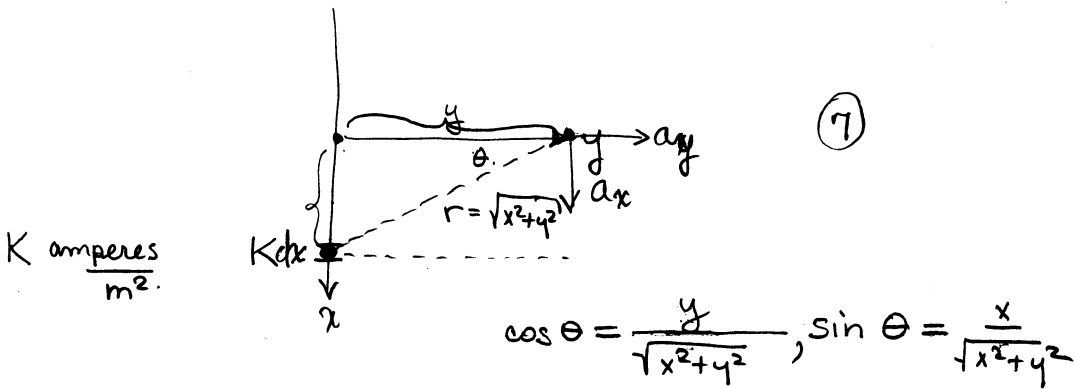
$$\begin{aligned} \underline{a_\phi} \cdot \underline{a_x} &= |\underline{a_\phi}| |\underline{a_x}| \cos\left(\frac{\pi}{2} + \frac{\pi}{2} + \theta\right) \\ &= \cos(\pi + \theta) \\ &= \cos \pi \cos \theta - \sin \pi \sin \theta \\ &= -\cos \theta \end{aligned}$$

$$H_\phi \underline{a_\phi} \cdot \underline{a_y} = H_x \underline{a_x} \cdot \underline{a_y} + H_y \underline{a_y} \cdot \underline{a_y} + H_z \underline{a_z} \cdot \underline{a_y}$$

$$\begin{aligned} \underline{a_\phi} \cdot \underline{a_y} &= |\underline{a_\phi}| |\underline{a_y}| \cos\left(\frac{\pi}{2} + \theta\right) \\ &= \cos \frac{\pi}{2} \cos \theta - \sin \frac{\pi}{2} \sin \theta = -\sin \theta \end{aligned}$$

$$\therefore H_x = \frac{I}{2\pi r} (-\cos\theta)$$

$$H_y = \frac{I}{2\pi r} (-\sin\theta)$$



$$\cos\theta = \frac{y}{\sqrt{x^2+y^2}}, \sin\theta = \frac{x}{\sqrt{x^2+y^2}}$$

$$H_x = \int \frac{(K dx)}{2\pi r} \left(-\frac{y}{(x^2+y^2)^{3/2}}\right) = \int -\frac{Ky}{2\pi (x^2+y^2)^{3/2}} dx$$

also  $\sqrt{x^2+y^2}$  →

$$= -\frac{Ky}{2\pi} \int_{-\frac{W}{2}}^{+\frac{W}{2}} \frac{dx}{(x^2+y^2)^{3/2}} = -\frac{Ky}{2\pi} \frac{1}{y} \tan^{-1}\left(\frac{x}{y}\right) \Big|_{-\frac{W}{2}}^{+\frac{W}{2}}$$

$$= -\frac{K}{2\pi y} \left[ \tan^{-1}\left(\frac{W}{2y}\right) - \tan^{-1}\left(-\frac{W}{2y}\right) \right]$$

this is equivalent to  $\tan^{-1}(\theta_{max}) - \tan^{-1}(-\theta_{max})$ .

$$2 \tan^{-1}(\theta_{max})$$

and as  $\theta_{max} \rightarrow \frac{\pi}{2}$   $H_x \rightarrow \infty$

$$H_y = \int \frac{K dx}{2\pi r} \left(-\frac{x}{\sqrt{x^2+y^2}}\right) = -\frac{K}{2 \cdot 2\pi} \int_{-\frac{W}{2}}^{+\frac{W}{2}} \frac{2x dx}{x^2+y^2} = -\frac{K}{4\pi} \left[ \ln(x^2+y^2) \right]_{-\frac{W}{2}}^{+\frac{W}{2}}$$

$$= -\frac{K}{4\pi} \frac{1}{(x^2+y^2)^2} \Big|_{-\frac{W}{2}}^{+\frac{W}{2}} \Rightarrow 0.$$

Math errors in integral!

Ampère Law (this is the magnetic equivalent of) Gauss' Law

the derivation of Ampère's Law follows from the Biot-Savart Law

Biot-Savart Law

$$d\mathbf{H} = \frac{I d\mathbf{l} \times \mathbf{a}_r}{4\pi r^2}$$

let  $I$  become a volume distribution of current  
not  $I d\mathbf{l}$   
but  $\mathbf{J} d\mathbf{v}$

$$d\mathbf{H}^{(r)} = \frac{\mathbf{J}^{(r')} d\mathbf{v}' \times \mathbf{a}_r}{4\pi r'^2}$$

include source & field coordinates

integrating

$$\mathbf{H}^{(r)} = \frac{1}{4\pi} \int_V \frac{\mathbf{J}^{(r')} d\mathbf{v}' \times \mathbf{a}_r}{r'^2}$$
$$= \frac{1}{4\pi} \int \frac{\mathbf{J}^{(r')} \times \mathbf{a}_r}{r'^2} d\mathbf{v}'$$

note that  $\frac{\mathbf{a}_r}{r^2} = \nabla' \left( \frac{1}{r} \right) = \frac{\partial}{\partial r} (r^{-1}) = -r^{-2}$

$$\mathbf{H}^{(r)} = -\frac{1}{4\pi} \int \mathbf{J}^{(r')} \times \nabla' \left( \frac{1}{r} \right) d\mathbf{v}'$$

where  $\nabla$  operates on source coordinates

taking the divergence of both sides

$$\nabla \cdot \mathbf{H} = -\frac{1}{4\pi} \int_V \nabla \cdot (\mathbf{J}^{(r')} \times \nabla' \left( \frac{1}{r} \right)) d\mathbf{v}'$$

operates on  $r$ , not  $r'$

use the vector identity

$$\nabla \cdot (\mathbf{A} \times \mathbf{B}) = \mathbf{B} \cdot (\nabla \times \mathbf{A}) - \mathbf{A} \cdot (\nabla \times \mathbf{B})$$

rewrite the integrand as

$$\nabla \cdot (\mathbf{J} \times \nabla \left( \frac{1}{r} \right)) = \nabla \left( \frac{1}{r} \right) \cdot (\nabla \times \mathbf{J}) - \mathbf{J} \cdot \underbrace{\nabla \times \nabla \left( \frac{1}{r} \right)}_{\nabla \times \nabla f \equiv 0 \text{ for any } f}$$

$$\underline{\nabla} \times \underline{H} = -\frac{1}{4\pi} \int \underline{\nabla}^2 \left( \frac{1}{r} \right) \underline{J} \, dv$$

This is a special integral.

$$\int \underline{\nabla}^2 \left( \frac{1}{r} \right) \underline{J}(r') \, dr' =$$

$$\nabla^2 \left( \frac{1}{r} \right) = 0 \text{ for all finite values of } r$$

thus, if  $(x, y, z)$  is outside a finite source region  $r$  is always  $> 0$  and  $\nabla^2 \left( \frac{1}{r} \right) \equiv 0$  so that  $\underline{\nabla} \times \underline{H} \equiv 0$ .

If  $(x, y, z)$  is in a source region, then  $r$  is sometimes zero and  $\nabla^2 \left( \frac{1}{r} \right) \neq 0$ .

Basically  $\nabla^2 \left( \frac{1}{r} \right)$  is a delta function of  $r$  and  $r'$

$$\int 4\pi \delta(\underline{r} - \underline{r}') \underline{J}(\underline{r}') \, dv' = -4\pi \underline{J}(\underline{r})$$

$$\underline{\nabla} \times \underline{H} = -\frac{1}{4\pi} \cdot -4\pi \underline{J}(\underline{r})$$

$$\underline{\nabla} \times \underline{H}(\underline{r}) = \underline{J}(\underline{r})$$

Applying Stokes Theorem

$$\int_S \underline{\nabla} \times \underline{H} \cdot d\underline{S} = \oint_C \underline{H} \cdot d\underline{l}$$

$$\int_S \underline{\nabla} \times \underline{H} \cdot d\underline{S} = \int_S \underline{J} \cdot d\underline{S}$$

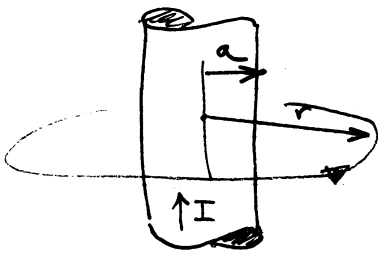
$$\text{or } \oint_C \underline{H} \cdot d\underline{l} = \int_S \underline{J} \cdot d\underline{S}$$



Now that we have Ampère's Law how can we use it.

Just like Gauss Law

Example 1 Field from an infinite wire of finite radius.



consider  $\underline{H} \cdot \underline{dl}$

pick a contour  $C$  outside any sources.

$$\underline{H} = H_r \underline{a}_r + H_\phi \underline{a}_\phi + H_z \underline{a}_z$$

$$\underline{dl} = r d\phi \underline{a}_\phi \quad \text{pick a circular contour}$$

$$\underline{H} \cdot \underline{dl} = H_\phi r d\phi$$

$$\oint_C \underline{H} \cdot \underline{dl} = \int_0^{2\pi} H_\phi r d\phi = 2\pi r H_\phi \quad (7)$$

$$\int \underline{J} \cdot \underline{dS} = I \quad \therefore \quad 2\pi r H_\phi = I \quad \text{and} \quad H_\phi = \frac{I}{2\pi r} \quad \text{for } r \geq a$$



suppose  $r < a$   
 then only a part of  $I$

$$\int \underline{J} \cdot \underline{dS} = \int_0^r \frac{I}{\pi a^2} r dr d\phi = \frac{I \cdot \frac{r^2}{2} \cdot 2\pi}{\pi a^2}$$

$$= I \frac{r^2}{a^2}$$

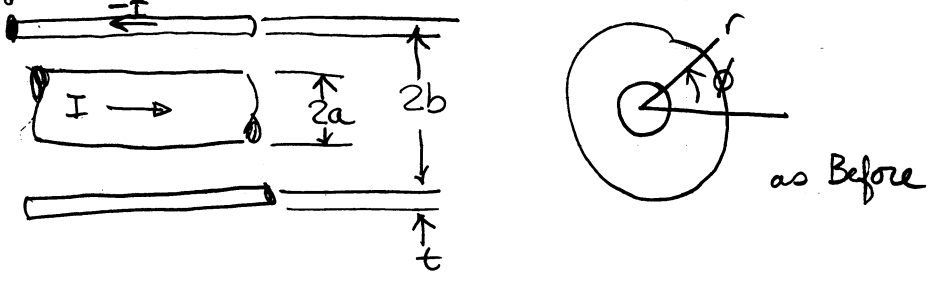
$$2\pi r H_\phi = I \frac{r^2}{a^2}$$

$$H_\phi = \frac{I}{2\pi} \frac{r}{a^2} \quad r < a$$

$$= \frac{I}{2\pi r} \quad r > a$$

Example #2

Magnetic field in a coaxial line.

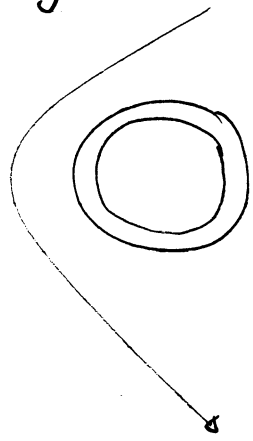


the field is the same as before for  $r < b$

$$H_\phi = \begin{cases} \frac{I}{2\pi r} \frac{r}{a^2} & r < a \\ \frac{I}{2\pi r} & r > a \end{cases}$$

consider now what happens between  $b$  and  $b+t$ .

$$\int \underline{J} \cdot \underline{ds} = \underbrace{\int_0^a \underline{J} \cdot \underline{ds}}_I + \int_b^r \frac{-I}{\pi(2bt+t^2)} \cdot r dr d\phi$$



$$J = \frac{-I}{\pi(2bt+t^2)}$$

$$\begin{aligned} \text{area} &= \pi(b+t)^2 - \pi(b)^2 \\ &= \pi(b^2 + 2bt + t^2 - b^2) \\ &= \pi(2bt + t^2) \end{aligned}$$

$$\begin{aligned} &= I - I \frac{1}{\pi(2bt+t^2)} \int_b^r r dr d\phi \\ &= I \left( 1 - \frac{1}{\pi(2bt+t^2)} 2\pi \frac{r^2}{2} \Big|_b^r \right) \\ &= I \left( 1 - \frac{\pi(r^2 - b^2)}{\pi(b+t)^2 - b^2} \right) \\ &= I \left( 1 - \frac{r^2 - b^2}{(b+t)^2 - b^2} \right) \end{aligned}$$

$$2\pi r H_\phi = I \left( \frac{(b+t)^2 - b^2 - r^2 + b^2}{(b+t)^2 - b^2} \right)$$

$$H_\phi = \frac{I}{2\pi r} \left[ \frac{(b+t)^2 - r^2}{(b+t)^2 - b^2} \right] \quad b \leq r < b+t$$

For  $r > b+t$        $\int \underline{J} \cdot \underline{dS} = I - I = 0$

$H_\phi = 0$        $b+t \leq r$

Now that we have Ampère's law in integral form we need to think about the differential form.

$$\oint_C \underline{H} \cdot d\underline{l} = \int_S \underline{J} \cdot d\underline{s}$$

Recall that  $\text{curl } \underline{F} \triangleq \lim_{\Delta S \rightarrow 0} \frac{\oint_C \underline{F} \cdot d\underline{l}}{\Delta S} \underline{a}_n = \underline{\nabla} \times \underline{F}$

i.e. the contribution to a vector circulation from a differential surface.

consider for Ampère's Law.

$$\lim_{\Delta S \rightarrow 0} \frac{\oint_C \underline{H} \cdot d\underline{l}}{\Delta S} \underline{a}_n = \text{curl } \underline{H} = \text{also } \lim_{\Delta S \rightarrow 0} \frac{\int \underline{J} \cdot d\underline{a}}{\Delta S} \underline{a}_n$$

$$= \lim_{\Delta S \rightarrow 0} \frac{\underline{J} \Delta S}{\Delta S} \underline{a}_n$$

$$= \underline{J} \cdot \underline{a}_n$$

the curl and  $\underline{J}$  are in the same direction

$$\underline{\nabla} \times \underline{H} = \underline{J}$$

Question: can we define any functions (potentials) for the magnetic field that are easier to find and from which we can obtain the field vectors.

Yes, both vector and scalar.

For a source-free region of space  $\nabla \times \underline{H} = \underline{J} \rightarrow 0$

$\nabla \times (-\nabla \mathcal{F}) = 0$  is true for any scalar field  $\mathcal{F}$ .

so let  $\underline{H} = -\nabla \mathcal{F}$

$$\oint \underline{H} \cdot d\underline{l} \text{ then becomes } \oint_{P_1}^{P_2} -\nabla \mathcal{F} = \mathcal{F}(P_2) - \mathcal{F}(P_1) = 0$$

just as from conservative electric field.

$\mathcal{F}$  is called the magnetomotive potential

finally, note that the flux

$$\Phi_m = \oint_S \mu_0 \underline{H} \cdot d\underline{s} = 0 \text{ over any closed surface.}$$

why? because there is no magnetic monopole.

a sink or source of magnetic flux.

$$\oint_S \underline{H} \cdot d\underline{s} = \int_V \nabla \cdot \underline{H} dV = 0$$

since  $\nabla \cdot \underline{H} = \rho_m$  a magnetic charge density.

## Magnetic vector potential

The magnetomotive potential was defined for a source free region of space.  
Suppose  $\underline{J} \neq 0$ .

we noted that  $\underline{B} = \mu_0 \underline{H}$  just as  $\underline{D} = \epsilon_0 \underline{E}$  defines a flux density

let us examine a vector potential.

$$\text{starting with } \underline{\nabla} \cdot \underline{B} = 0$$

$$\underline{\nabla} \cdot \underline{\nabla} \times \underline{A} = 0$$

$$\text{so let } \underline{B} = \underline{\nabla} \times \underline{A}$$

↑ magnetic vector potential

Ampère's Law

$$\underline{\nabla} \times \underline{H} = \underline{J}$$

$$\text{becomes } \underline{\nabla} \times \mu_0 \underline{H} = \mu_0 \underline{J}$$

↑  
 $\underline{B}$

consider our definition and taking the ~~divergence~~ <sup>curl</sup> of both sides

$$\begin{aligned} \underline{\nabla} \times \underline{B} &= \underline{\nabla} \times \underline{\nabla} \times \underline{A} \\ &= \underline{\nabla} (\underline{\nabla} \cdot \underline{A}) - \nabla^2 \underline{A} \end{aligned}$$

To simplify our results let's require  $\underline{\nabla} \cdot \underline{A} = 0$ . This is not arbitrary — it's related to something called the Lorentz condition. — and as we have not specified  $\underline{A}$  is just another condition:

$$\therefore \underline{\nabla} \times \underline{B} = -\nabla^2 \underline{A}$$

$$\nabla^2 \underline{A} = -\mu \underline{J} \quad \& \quad \underline{\nabla} \cdot \underline{A} = 0$$

The vector potential is then specified by

$$-\nabla^2 \underline{A} = \mu \underline{J}$$

(Eqn. 31 p.150 should have a minus sign in it)

$$\nabla^2 \underline{A} = -\mu \underline{J}$$

$$\underline{\nabla} \cdot \underline{A} = 0$$

How to solve this set of equations in integral form.

Recall that the electric potential obeyed a similar equation

$$\nabla^2 \Phi = 0$$

and had a general solution 
$$\Phi = \int_v \frac{\rho_v du}{4\pi\epsilon r}$$

By analogy, we shall use the same solution

$$\underline{A} = \int \frac{\mu \underline{J} dv}{4\pi r}$$

We can then operate on this equation to show that the Biot-Savart and Ampère's law can be derived from this solution.

Properties of the vector potential:

- A is not unique

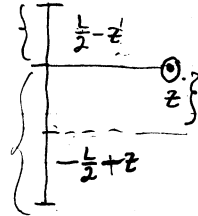
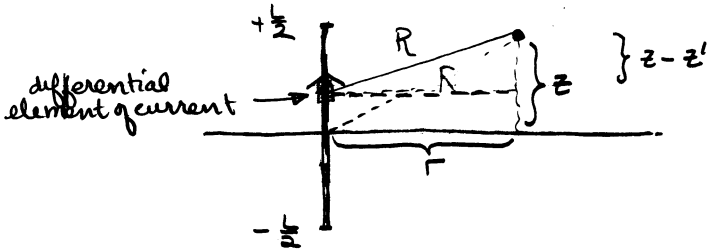
$$\text{let } \underline{A}' = \underline{A} + \nabla f$$

$$\underline{B} = \underline{\nabla} \times \underline{A}' = \underline{\nabla} \times (\underline{A} + \underline{\nabla} f) = \underline{\nabla} \times \underline{A} + 0$$

$$\text{as } \underline{\nabla} \times \underline{\nabla} f = 0$$

Examples of vector and scalar potential

Example 1: Vector potential of a finite length line current.



$\nabla^2 \Phi = -\frac{\rho}{\epsilon}$  Poisson's Eqn.

$\underline{A} = \int \frac{\mu \underline{J} d\mathbf{v}}{4\pi R}$  this is almost identical to defn for  $\Phi = \int \frac{\rho}{4\pi \epsilon R} d\mathbf{v}$

$\nabla^2 \underline{A} = -\mu \underline{J}$

$\underline{A} = \int \frac{\mu \underline{J} d\mathbf{v}}{4\pi R}$

Note:  $\underline{J} d\mathbf{v} \rightarrow \underline{K} dS \rightarrow I d\mathbf{l} \rightarrow q\mathbf{v}$   
 These are all just current elements.

$\underline{A} = \int \frac{\mu I d\mathbf{l}}{4\pi R} = \int \frac{\mu I dz' \underline{a}_z}{4\pi \sqrt{(z-z')^2 + r^2}}$   $dz'$  are the coordinates of the current element.

$= \frac{\mu I}{4\pi} \underline{a}_z \int_{z'=-l/2}^{z'=l/2} \frac{dz'}{\sqrt{(z-z')^2 + r^2}} = \frac{\mu I}{4\pi} \underline{a}_z$

let  $z'' = z - z'$   
 $dz'' = -dz'$   
 $z'' = z - \frac{l}{2}$   
 $z'' = z + \frac{l}{2}$

limits are  $\pm \frac{l}{2}$

$\int_{z+l/2}^{z-l/2} \frac{-dz''}{\sqrt{z''^2 + r^2}} = \int_{z-l/2}^{z+l/2} \frac{dz''}{(z''^2 + r^2)^{1/2}} = \ln(z'' + \sqrt{z''^2 + r^2})$

$= \ln(z + \frac{l}{2} + \sqrt{(z + \frac{l}{2})^2 + r^2})$

$- \ln(z - \frac{l}{2} + \sqrt{(z - \frac{l}{2})^2 + r^2})$

$= \ln r \left\{ \frac{z + \frac{l}{2}}{r} + \sqrt{\left(\frac{z + \frac{l}{2}}{r}\right)^2 + 1} \right\} - \ln r \left\{ \left(\frac{z - \frac{l}{2}}{r}\right) + \sqrt{\left(\frac{z - \frac{l}{2}}{r}\right)^2 + 1} \right\}$

$= \cancel{\ln r} + \ln\left(\frac{z + \frac{l}{2}}{r} + \sqrt{\left(\frac{z + \frac{l}{2}}{r}\right)^2 + 1}\right) - \cancel{\ln r} - \ln\left(\frac{z - \frac{l}{2}}{r} + \sqrt{\left(\frac{z - \frac{l}{2}}{r}\right)^2 + 1}\right)$



$$A = \frac{\mu I}{4\pi} a_z \left[ \ln \left( \frac{z + \frac{l}{2}}{r} \right) + \sqrt{\left( \frac{z + \frac{l}{2}}{r} \right)^2 + 1} \right] - \ln \left( \frac{z - \frac{l}{2}}{r} \right) + \sqrt{\left( \frac{z - \frac{l}{2}}{r} \right)^2 + 1} \right]$$

$$= \frac{\mu I}{4\pi} a_z \left[ \sinh^{-1} \left( \frac{z + \frac{l}{2}}{r} \right) - \sinh^{-1} \left( \frac{z - \frac{l}{2}}{r} \right) \right]$$

$$\underline{B} = \underline{\nabla} \times \underline{A} = \left( \frac{1}{r} \frac{\partial A_z}{\partial \phi} - \frac{\partial A_\phi}{\partial z} \right) \underline{a}_r + \left( \frac{\partial A_r}{\partial z} - \frac{\partial A_z}{\partial r} \right) \underline{a}_\phi + \frac{1}{r} \left( \frac{\partial (r A_\phi)}{\partial r} - \frac{\partial A_r}{\partial \phi} \right) \underline{a}_z$$

$$= - \frac{\partial A_z}{\partial r} \underline{a}_\phi$$

need  $\underline{\nabla} \times \underline{A} \rightarrow$

Recalling  $\frac{\partial}{\partial x} \sinh^{-1} u = \frac{1}{\sqrt{u^2 + 1}} \frac{\partial u}{\partial x}$

$$= - \frac{\mu I}{4\pi} a_\phi \left[ \frac{1}{\sqrt{\left( \frac{z + \frac{l}{2}}{r} \right)^2 + 1}} \left( \frac{z + \frac{l}{2}}{r} \right) \left( \frac{1}{r^2} \right) - \frac{1}{\sqrt{\left( \frac{z - \frac{l}{2}}{r} \right)^2 + 1}} \left( \frac{z - \frac{l}{2}}{r} \right) \left( \frac{-1}{r^2} \right) \right]$$

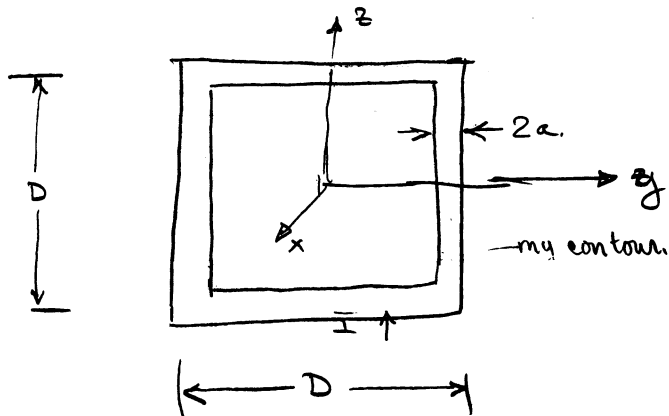
$$= - \frac{\mu I}{4\pi} a_\phi \left[ \frac{\left( \frac{z + \frac{l}{2}}{r} \right) \left( \frac{-1}{r^2} \right)}{\frac{1}{r} \sqrt{\left( \frac{z + \frac{l}{2}}{r} \right)^2 + r^2}} - \frac{\left( \frac{z - \frac{l}{2}}{r} \right) \left( \frac{-1}{r^2} \right)}{\frac{1}{r} \sqrt{\left( \frac{z - \frac{l}{2}}{r} \right)^2 + r^2}} \right]$$

$$= \frac{\mu I}{4\pi r} a_\phi \left[ \frac{z + \frac{l}{2}}{\sqrt{\left( \frac{z + \frac{l}{2}}{r} \right)^2 + r^2}} - \frac{z - \frac{l}{2}}{\sqrt{\left( \frac{z - \frac{l}{2}}{r} \right)^2 + r^2}} \right]$$

if  $\frac{l}{2} \rightarrow \infty$

$$\underline{B} \rightarrow \frac{\mu I}{4\pi r} a_\phi \left[ \frac{\frac{l}{2}}{\frac{l}{2}} - \frac{-\frac{l}{2}}{\frac{l}{2}} \right] = \frac{\mu I}{2\pi r} a_\phi$$

Example 2: Flux through a square loop.



Use the result for a finite length current along the  $z$ -axis.

$$\underline{A} = \frac{\mu I}{4\pi} a_z \left[ \sinh^{-1}\left(\frac{z+\frac{D}{2}}{r}\right) - \sinh^{-1}\left(\frac{z-\frac{D}{2}}{r}\right) \right]$$

To find the flux we recall that

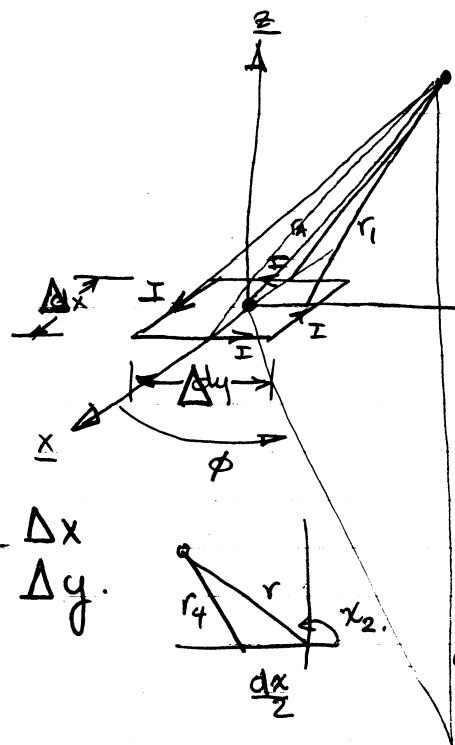
$$\Phi = \int_S \underline{B} \cdot d\underline{s} = \int_S \nabla \times \underline{A} \cdot d\underline{s} = \oint_C \underline{A} \cdot d\underline{l}$$

by Stokes theorem.

Note that the contour integral consists of four parts - all identical. All currents are in the same direction as the contour so all add.

$$\begin{aligned} \Phi &= 4 \int_{-\left(\frac{D}{2}-a\right)}^{\left(\frac{D}{2}-a\right)} A_z dz \\ &= 4 \int_{-\left(\frac{D}{2}-a\right)}^{\left(\frac{D}{2}-a\right)} \frac{\mu I}{4\pi} \left[ \sinh^{-1}\left(\frac{z+\frac{D}{2}}{a}\right) - \sinh^{-1}\left(\frac{z-\frac{D}{2}}{a}\right) \right] dz. \end{aligned}$$

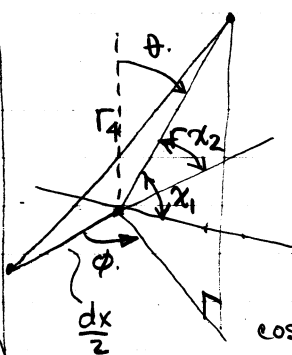
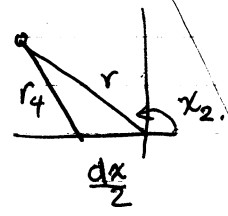
Example 3 Magnetic dipole (square)



$$\underline{A} = \int \frac{\mu_0 I}{4\pi} d\mathbf{v}$$

$$\underline{A} = \frac{\mu_0 I}{4\pi} \frac{dy}{r^3} \mathbf{y}$$

use  $\Delta x$   
 $\Delta y$ .

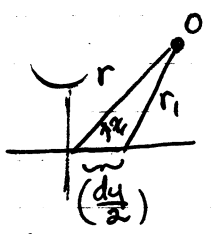


where

$$r_4^2 = r^2 + \left(\frac{dx}{2}\right)^2 - 2(r)\left(\frac{dx}{2}\right) \cos(\pi - \alpha_2)$$

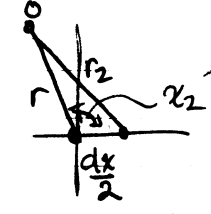
$$= r^2 + \frac{dx^2}{4} + r dx \cos \alpha_2$$

$$\cos(\pi - \frac{\alpha}{2}) = \cos \pi \cos \frac{\alpha}{2} + \sin \pi \sin \frac{\alpha}{2}$$



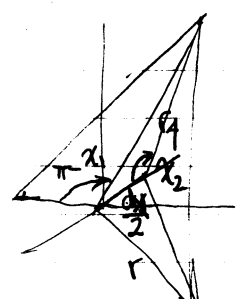
$$\underline{A}_1 = -\frac{\mu_0 I}{4\pi} \frac{dy}{r_1^3} \mathbf{y}$$

where  $r_1 = r^2 + \left(\frac{dy}{2}\right)^2 - 2(r)\left(\frac{dy}{2}\right) \cos \alpha_1$



$$\underline{A}_2 = -\frac{\mu_0 I}{4\pi} \frac{dx}{r_2^3} \mathbf{x}$$

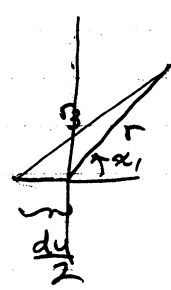
where  $r_2 = r^2 + \left(\frac{dx}{2}\right)^2 - 2(r)\left(\frac{dx}{2}\right) \cos \alpha_2$



$$\underline{A}_3 = \frac{\mu_0 I}{4\pi} \frac{dx}{r_3^3} \mathbf{x}$$

where  $r_3 = r^2 + \left(\frac{dy}{2}\right)^2 - 2(r)\left(\frac{dy}{2}\right) \cos(\pi - \alpha_1)$

$$= r^2 + \frac{dy^2}{4} + r dy \cos \alpha_1$$



consider  $\lim_{\frac{dx}{r} \rightarrow 0} \underline{A}$   
 $\frac{dy}{r} \rightarrow 0$

consider  $\underline{A}_1$  in this limit

$$\frac{dx}{\sqrt{r^2 + \left(\frac{dy}{2}\right)^2 - r dy \cos \alpha_1}} = \frac{dx}{r \left[ 1 + \left(\frac{dy}{2r}\right)^2 - \frac{dy}{r} \cos \alpha_1 \right]^{1/2}}$$

$$\approx \frac{\frac{dx}{r}}{1 - \frac{1}{2} \frac{dy}{r} \cos \alpha_1}$$

$$\approx \frac{dx}{r} \left( 1 + \frac{1}{2} \frac{dy}{r} \cos \alpha_1 \right)$$

$$\therefore \text{in the limit } \underline{A}_1 \approx - \frac{\mu_0 I}{4\pi r} \underline{ax} \left[ \frac{dx}{r} + \frac{dx dy}{2r^2} \cos \alpha_1 \right]$$

for  $\underline{A}_3$ ,

$$\frac{dx}{r^2 + \left(\frac{dy}{2}\right)^2 + r dy \cos \alpha_1} = \frac{dx}{r \left[ 1 + \left(\frac{dy}{2r}\right)^2 + \frac{dy}{r} \cos \alpha_1 \right]^{1/2}}$$

$$\approx \frac{\frac{dx}{r}}{1 + \frac{1}{2} \frac{dy}{r} \cos \alpha_1} = \frac{dx}{r} \left[ 1 - \frac{1}{2} \frac{dy}{r} \cos \alpha_1 \right]$$

$$\underline{A}_3 \approx \frac{\mu_0 I}{4\pi r} \underline{ax} \frac{dx}{r} \left[ 1 - \frac{1}{2} \frac{dy}{r} \cos \alpha_1 \right]$$

$$\underline{A}_1 + \underline{A}_3 = \frac{\mu_0 I}{4\pi} \underline{ax} \left[ -\cancel{\frac{dx}{r}} - \frac{1}{2} \frac{dx dy}{r^2} \cos \alpha_1 + \cancel{\frac{dx}{r}} - \frac{1}{2} \frac{dx dy}{r^2} \cos \alpha_1 \right]$$

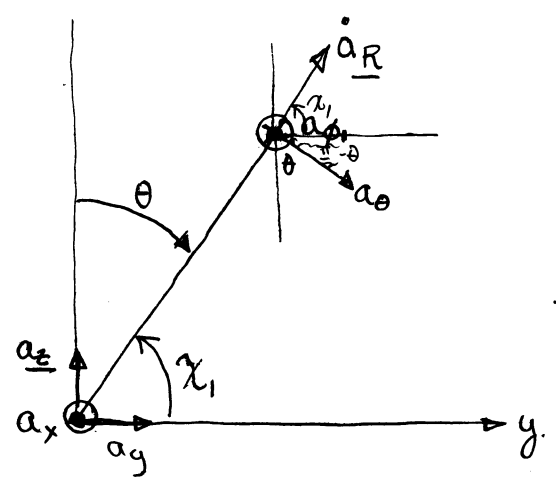
$$= - \frac{\mu_0 I}{4\pi r^2} \left[ dx dy \cos \alpha_1 \underline{ax} \right]$$

Similarly

$$\underline{A}_2 + \underline{A}_4 = - \frac{\mu_0 I}{4\pi r^2} dx dy \cos \alpha_2 \underline{ay}$$

$$\underline{A} = -\frac{\mu_0 I}{4\pi r^2} dx dy [\cos \chi_1 \underline{a}_x + \cos \chi_2 \underline{a}_y]$$

lets put this in spherical coordinates.



this is in plane.

$$\underline{a}_R \cdot \underline{a}_y = |\underline{a}_R| |\underline{a}_y| \cos \chi_1 = \cos \chi_1$$

$$\underline{a}_R \cdot \underline{a}_x = |\underline{a}_R| |\underline{a}_x| (-\cos \chi_2) = -\cos \chi_2$$

recall direction of  $\chi_2$

$$\begin{aligned} \text{by inspection } \cos \chi_1 &= \cos\left(\frac{\pi}{2} - \theta\right) \\ &= \cos \frac{\pi}{2} \cos \theta + \sin \frac{\pi}{2} \sin \theta \\ &= + \sin \theta \end{aligned}$$

This is however only for  $\phi = \frac{\pi}{2}$ .

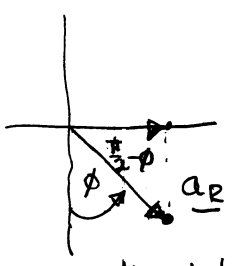
For  $\phi \neq \frac{\pi}{2}$  this is reduced by  $\sin \phi$ .

$$\text{so } \cos \chi_1 = + \sin \theta \sin \phi.$$

similarly

$$+\cos \chi_2 = -\sin \theta \cos \phi.$$

sign.



this dot product is

$$\begin{aligned} &|| \cos\left(\frac{\pi}{2} - \phi\right) \\ &\Downarrow \\ &\sin \phi \end{aligned}$$

$$\underline{A} \rightarrow -\frac{\mu_0 I}{4\pi r^2} dx dy [\cos \chi_1 \underline{a}_x + \cos \chi_2 \underline{a}_y]$$

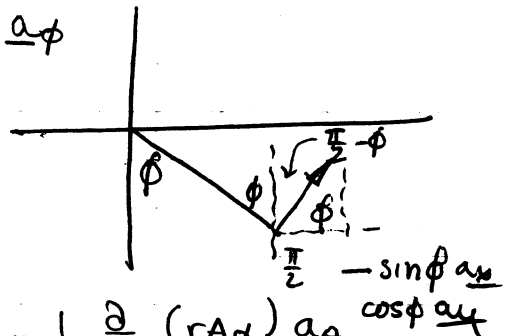
$$\text{but } \underline{a}_R \cdot \underline{a}_y = \cos \chi_1 = \sin \theta \sin \phi$$

$$\underline{a}_R \cdot \underline{a}_x = -\cos \chi_2 = +\sin \theta \cos \phi$$

$$\underline{A} \hat{=} -\frac{\mu_0 I}{4\pi r^2} dx dy [\sin \theta \sin \phi \underline{a}_x + \sin \theta \cos \phi \underline{a}_y]$$

$$= \frac{\mu_0 I}{4\pi r^2} \underbrace{dx dy}_{dS} \sin \theta \underbrace{[-\sin \phi \underline{a}_x + \cos \phi \underline{a}_y]}_{\underline{a}_\phi}$$

$$\underline{A} = \frac{\mu_0 I}{4\pi r^2} dS \sin \theta \underline{a}_\phi$$



$$\underline{B} = \nabla \times \underline{A} = \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (A_\phi \sin \theta) \underline{a}_r - \frac{1}{r} \frac{\partial}{\partial r} (r A_\phi) \underline{a}_\theta$$

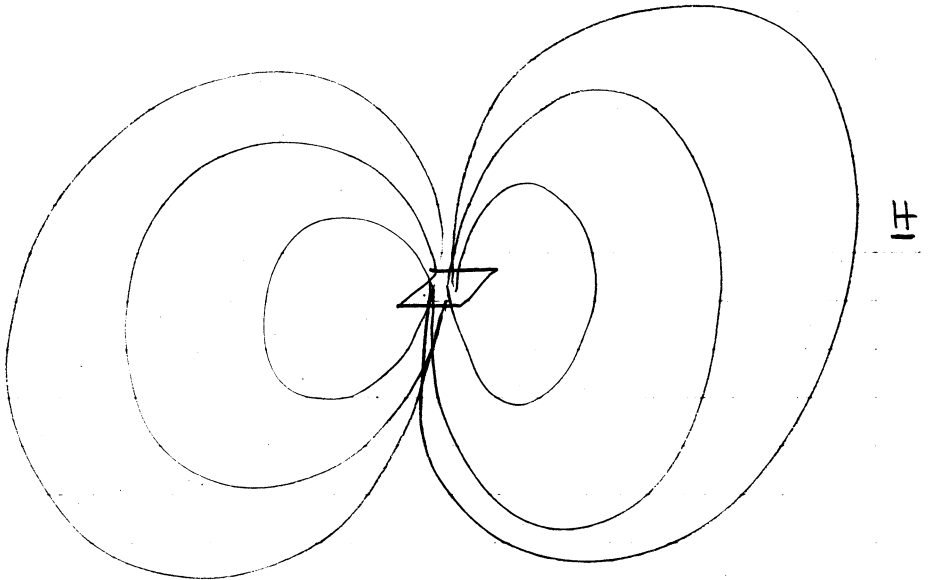
$$= \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} \left[ \frac{\mu_0 I}{4\pi r^2} dS \sin^2 \theta \underline{a}_r \right] - \frac{1}{r} \frac{\partial}{\partial r} \left[ \frac{\mu_0 I}{4\pi} r^{-1} dS \sin \theta \right] \underline{a}_\theta$$

$$= \frac{\mu_0 I dS}{4\pi} \left[ \frac{1}{r \sin \theta} \frac{1}{r^2} 2 \sin \theta \cos \theta \underline{a}_r - \frac{1}{r} \left( \frac{-1}{r^2} \right) dS \sin \theta \underline{a}_\theta \right]$$

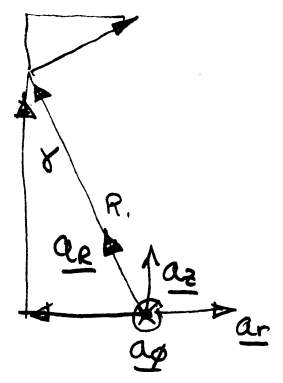
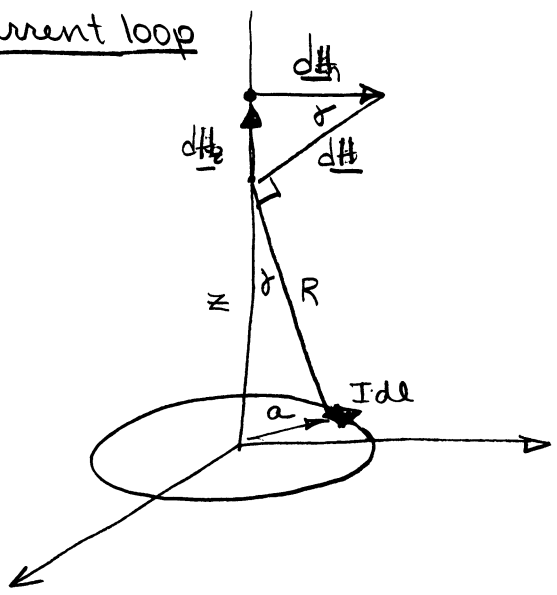
$$= \frac{\mu_0 I dS}{4\pi} \left[ \frac{2}{r^3} \cos \theta \underline{a}_r + \frac{1}{r^3} \sin \theta \underline{a}_\theta \right]$$

$$= \frac{\mu_0 I}{4\pi r^3} dS \left[ 2 \cos \theta \underline{a}_r + \sin \theta \underline{a}_\theta \right]$$

This is the same field as for the electric dipole.



single current loop



$$\underline{dH} = \frac{I \underline{dl} \times \underline{ar}}{4\pi R^2}$$

$$I \underline{dl} = I a d\phi \underline{a}_\phi$$

$$\underline{a}_R = c_1 \underline{a}_\phi + c_2 \underline{a}_z + c_3 \underline{a}_r$$

$$\underline{a}_R \cdot \underline{a}_\phi = 0 \quad \therefore c_1 = 0$$

$$c_2 = \underline{a}_R \cdot \underline{a}_z = |\underline{a}_R| |\underline{a}_z| \cos \gamma = \cos \gamma$$

$$c_3 = \underline{a}_R \cdot \underline{a}_r = |\underline{a}_R| |\underline{a}_r| \cos(\pi/2 + \gamma) = \cos \frac{\pi}{2} \cos \gamma - \sin \frac{\pi}{2} \sin \gamma = -\sin \gamma$$

$$\underline{a}_R = \cos \gamma \underline{a}_z - \sin \gamma \underline{a}_r$$

$$R^2 = a^2 + z^2$$

$$dH = \frac{I a d\phi \underline{a}_\phi \times (\cos \gamma \underline{a}_z - \sin \gamma \underline{a}_r)}{4\pi (a^2 + z^2)}$$



$$dH = \frac{Ia \, d\phi}{4\pi (a^2 + z^2)} \cdot (\cos \gamma \, \underline{a}_r + \sin \gamma \, \underline{a}_z)$$

$$= \frac{Ia}{4\pi} \left[ \frac{\cos \gamma}{a^2 + z^2} d\phi \, \underline{a}_r + \frac{\sin \gamma}{a^2 + z^2} d\phi \, \underline{a}_z \right]$$

$$\cos \gamma = \frac{z}{(a^2 + z^2)^{1/2}}$$

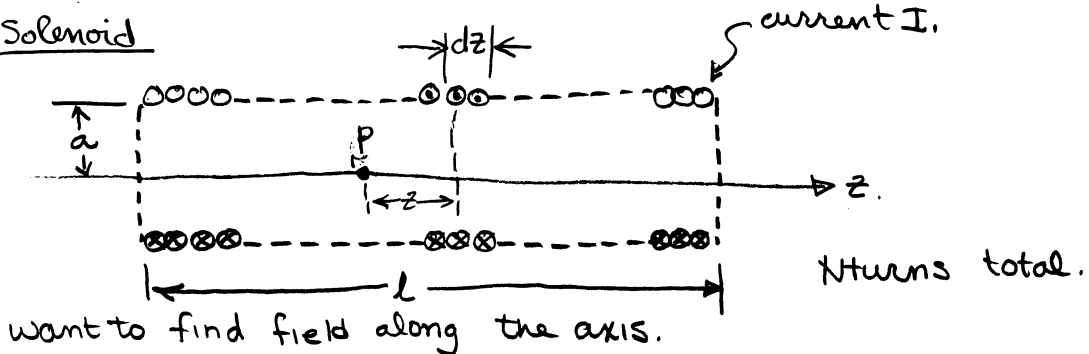
$$\sin \gamma = \frac{a}{(a^2 + z^2)^{1/2}}$$

$$H_r = \int dH_r = \frac{Ia}{4\pi} \int_0^{2\pi} \frac{z \, d\phi}{(a^2 + z^2)^{1/2}} \, \underline{a}_r \left. \vphantom{\int} \right\} \begin{array}{l} \text{I cannot do this because} \\ \text{the } \underline{a}_r\text{'s are not the} \\ \text{same, they will cancel.} \end{array}$$

$$H_z = \int dH_z = \frac{Ia}{4\pi} \frac{a}{(a^2 + z^2)^{3/2}} \cdot 2\pi$$

$$= \frac{Ia^2}{2(a^2 + z^2)^{3/2}}$$

Solenoid



what is the field from a single loop?

$$dH_z = \frac{(dI)a^2}{2(a^2+z^2)^{3/2}} = \frac{a^2}{2(a^2+z^2)^{3/2}} \left( \frac{N}{l} I dz \right)$$

# of turns / length  $\times$  current / turn  $\times$  length

what is the total field at point P.

$$H_z = \int \frac{a^2}{2(a^2+z^2)^{3/2}} \frac{N}{l} I dz$$

$$= \frac{a^2 NI}{2l} \int_{-\frac{l}{2}}^{+\frac{l}{2}} \frac{dz}{(a^2+z^2)^{3/2}}$$

$$= \frac{a^2 NI}{2l} \left[ \frac{z}{a^2(z^2+a^2)^{1/2}} \right]_{-\frac{l}{2}}^{+\frac{l}{2}}$$

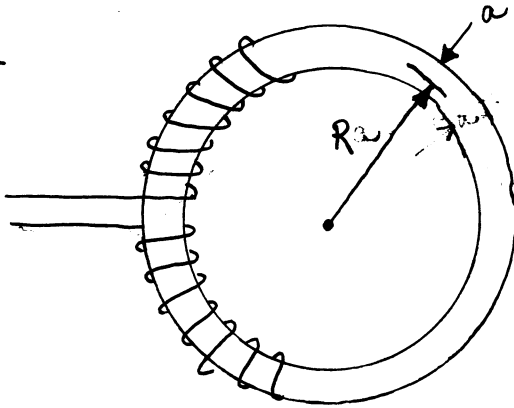
$$H_z = \frac{NI}{2l} \frac{\frac{l}{2} - (-\frac{l}{2})}{\left(\left(\frac{l}{2}\right)^2 + a^2\right)^{1/2}} = \frac{NI}{2l} \frac{l}{\left(\frac{l^2}{4} + a^2\right)^{1/2}} = \frac{NI}{2\left(\frac{l^2}{4} + a^2\right)^{1/2}}$$

Note that if  $l \gg a$  this becomes

$$H_z \approx \frac{NI}{2 \frac{l}{2}} = \frac{NI}{l}$$

in fact as long as  $\frac{l}{a} > 4$  this is a pretty good result.

toroid



a toroid is simply a solenoid in which the ends are brought together.

what is the length of this solenoid

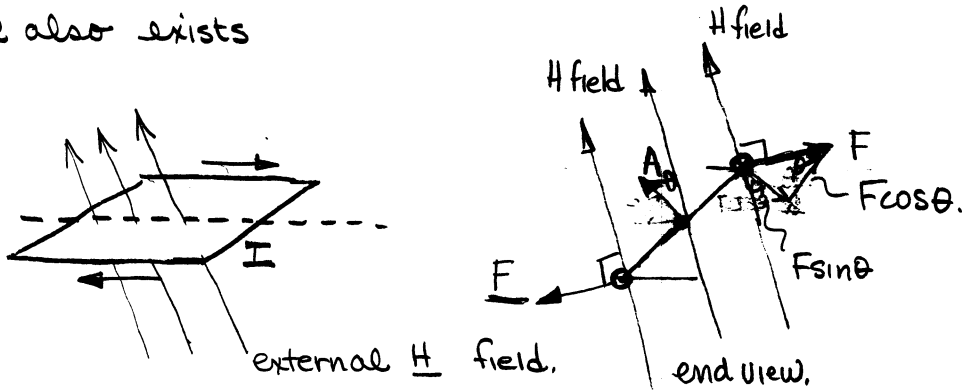
$$l = 2\pi R$$

$$\therefore H_{\phi} = \frac{NI}{2\left(\frac{4\pi^2 R^2}{4} + a^2\right)^{1/2}} = \frac{NI}{2(\pi^2 R^2 + a^2)^{1/2}}$$

materials

(7)

torque also exists



recall 
$$\underline{F} = q \underline{v} \times \underline{B} \approx \underline{I} \times \underline{B}$$

note that  $\underline{F}$  will pull the loop to align it perpendicular with the field.

this is like an <sup>electric</sup> dipole moment; however, because of the cross products we define the magnetic moment to be

$$\underline{m} = \underline{I} \underline{A}$$

the force acting on the loop is then

$$\underline{F} = |\underline{I} \times \underline{B}|$$

torque =  $2(\underline{F} \times \text{moment arm})$  since two arms.

$$T = 2 F I B l \frac{d}{2} \sin \theta.$$

← actually  $F \sin \theta$ .

⑧

in general we define

$$\underline{m} = I \underline{A}$$

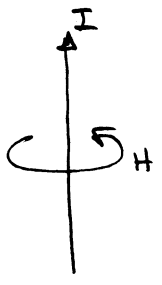
and 
$$\underline{T} = \underline{m} \times \underline{B}$$

Recalling. 
$$\underline{H} = \frac{I}{4\pi r^3} d\underline{S} \left[ 2 \cos \theta \underline{a}_r + \sin \theta \underline{a}_\theta \right]$$

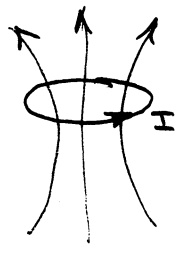
for a magnetic dipole.

Note that 
$$\underline{m} = I \underline{dS}$$

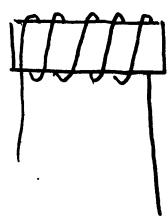
common shapes which produce magnetic fields.



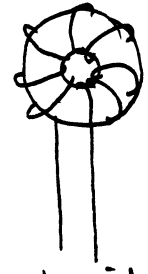
wire



loop

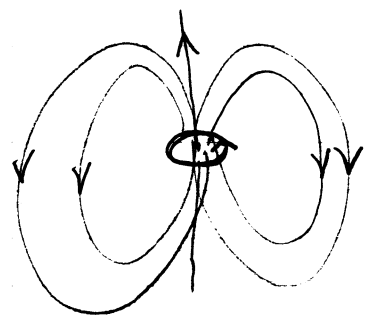
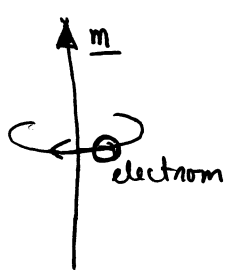
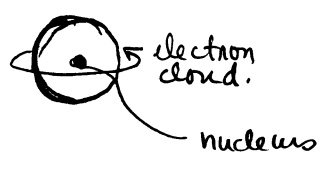


solenoid



toroid.

matter has several natural dipole moments.

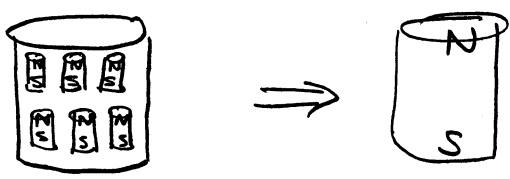


just as we defined 
$$\underline{P} = \lim_{\Delta v \rightarrow 0} \frac{\sum_i \underline{P}_i}{\Delta v}$$

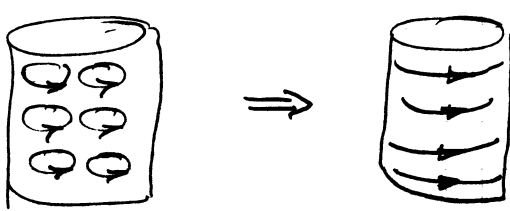
$$\underline{M} = \lim_{\Delta v \rightarrow 0} \frac{\sum_i \underline{m}_i}{\Delta v}$$

the situation for  $\underline{m}$  is very complex

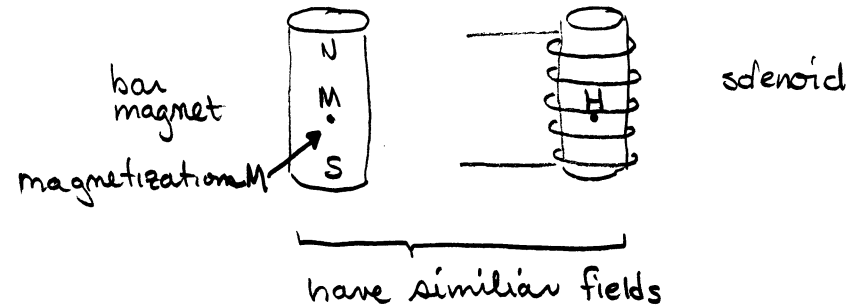
① small bar magnets



② small current loops



equivalent currents



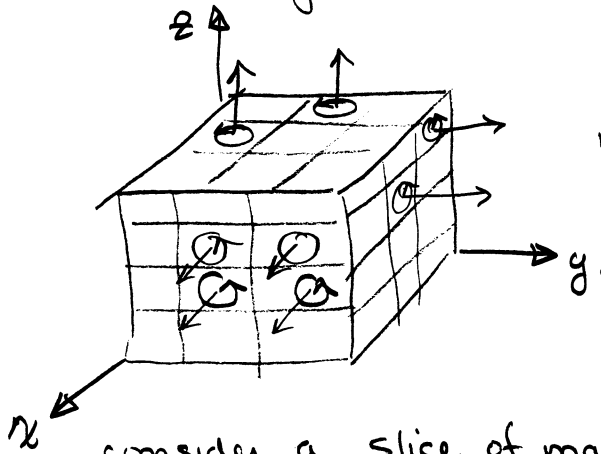
field is  $H = \frac{NI_m}{l}$

where  $I_m$  is the equivalent magnetic current,

$$\therefore M = \frac{NI_m}{l}$$

# Magnetization of matter

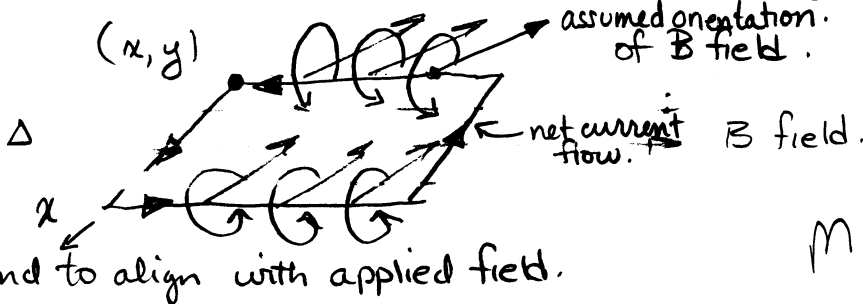
consider matter as composed of a number of magnetic dipoles. These dipoles may be permanent or induced by the applied magnetic field.



notice these are not random.

consider a slice of matter. Why?

$$\oint_C \underline{H} \cdot d\underline{l} = \int_S \underline{J} \cdot d\underline{s}$$



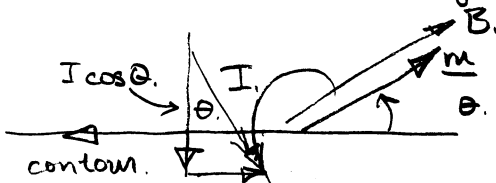
dipoles tend to align with applied field.

$$M = \lim_{\Delta V \rightarrow 0} \frac{\sum m_i}{\Delta V}$$

We define the dipole moment as  $\underline{m} = I d\underline{S}$  due to individual atoms

the overall magnetization  $\underline{M} = N \underline{m} = NI d\underline{S}$

What is the normal component of  $\underline{I}$  relative to the contour  $C$ ? Ans: zero in the interior. Only net contribution is from the layer near the edge of the loop.




z direction of current is

$$I dS \cos \theta / x$$

If field not uniform  $\theta$  is a function of  $x$ .



# of dipoles / volume. length of contour.



need to know # of dipoles along contour.

$$N \left( \underbrace{-I \Delta S \cos \theta}_x \right) \Delta y = I_z$$

current due to one dipole

- sign because of direction only that part inside loop contributes.

but by our earlier definitions This is also.

$$- \underbrace{m_y}_x |_{x} \Delta y = I_z$$

the y component of M at x

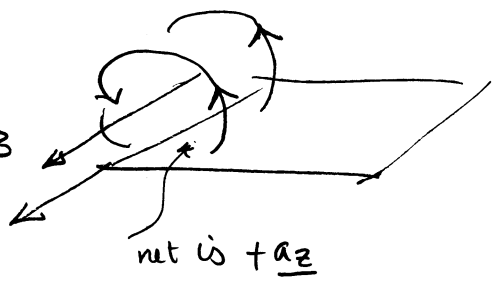
at the  $x + \Delta x$  edge of contour.

$$+ m_y |_{x+\Delta x} \Delta y = I_z$$

If the field is aligned along the x axis we can get contributions along the x-axis. in the same manner.

$$+ m_x |_y \Delta x = I_z$$

$$- m_x |_{y+\Delta y} \Delta x = I_z$$



overall

$$I_z \text{ total} = (m_y |_{x+\Delta x} - m_y |_x) \Delta y - (m_x |_{y+\Delta y} - m_x |_y) \Delta x$$

$$= \frac{m_y |_{x+\Delta x} - m_y |_x}{\Delta x} \Delta x \Delta y - \frac{m_x |_{y+\Delta y} - m_x |_y}{\Delta y} \Delta x \Delta y$$

$$\frac{I_z \text{ total}}{\Delta x \Delta y} = \left[ \frac{m_y |_{x+\Delta x} - m_y |_x}{\Delta x} - \frac{m_x |_{y+\Delta y} - m_x |_y}{\Delta y} \right]$$

taking limits as  $\Delta x \Delta y \rightarrow 0$

$$I_z \text{ total} = \frac{\partial m_y}{\partial x} - \frac{\partial m_x}{\partial y}$$

what do we do with this?

note that  $(\nabla \times \underline{m})_z = \underline{a_z} \cdot \begin{vmatrix} \underline{a_x} & \underline{a_y} & \underline{a_z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ m_x & m_y & m_z \end{vmatrix} = \frac{\partial m_y}{\partial x} - \frac{\partial m_x}{\partial y}$

$$J_z = (\nabla \times \underline{m})_z$$

In general, I could orient my loop in all directions and get

$$\underline{J} = \nabla \times \underline{m}$$

Tie this in with the magnetic field intensity. To do so go to historical form of Ampère's Law.

$$\oint \underline{H} \cdot d\underline{l} = \int \underline{J} \cdot d\underline{S}$$

$$\oint \underline{E} \cdot d\underline{S} = \frac{Q}{\epsilon_0}$$

$$\int (\nabla \times \underline{H}) \cdot d\underline{S} = \int \underline{J} \cdot d\underline{S}$$

$$\nabla \times \underline{H} = \underline{J}$$

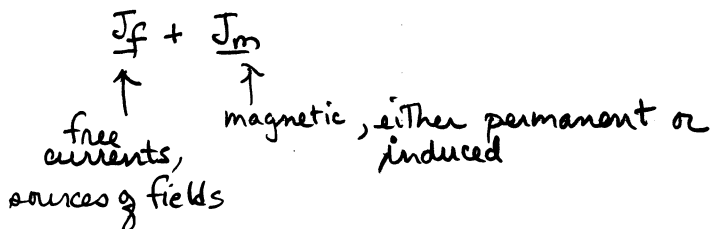
~~$B = \mu_0 H$  free space~~

this is not natural, actually.

$$\nabla \times \underline{B} = \mu_0 \underline{J}$$

$$\nabla \times \left( \frac{\underline{B}}{\mu_0} \right) = \underline{J}$$

we have studied free space & magnetic materials



Then,

$$\nabla \times \left( \frac{\underline{B}}{\mu_0} \right) = \underline{J}_f + \underline{J}_m = \underline{J}_f + \nabla \times \underline{m}$$

total magnetic flux density due to  
free & magnetic terms

$$\nabla \times \left( \frac{\underline{B}}{\mu_0} \right) = \underline{J}_f + \nabla \times \underline{M}$$

$$\nabla \times \left( \frac{\underline{B}}{\mu_0} - \underline{M} \right) = \underline{J}_f$$


 magnetic intensity due to free currents.

$$\underline{H} = \frac{\underline{B}}{\mu_0} - \underline{M}$$

$$\therefore \underline{B} = \mu_0 (\underline{H} + \underline{M})$$

the magnet flux density vector  $\underline{B}$

Recall  $\underline{D} = \epsilon \underline{E}$

In an analogous manner

$$\underline{B} = \mu \underline{H}$$

↑
↑

webers
amperes

meter<sup>2</sup>
meter

for free space  $\mu_0 = 4\pi \times 10^{-7}$  Hennys  
meter

The relationship between  $\underline{H}$  and  $\underline{M}$  is not as simple as that given since

$\underline{B} = \mu(H) \underline{H}$ , i.e.  $\mu$  is not necessarily linear.

The above results can be shown very accurately to describe materials

Depending on the material, there are three general forms of magnetization

diamagnetic  $\mu \lesssim \mu_0$  due to orbital motion of electrons

paramagnetic  $\mu \gtrsim \mu_0$  } spin motion of electron itself

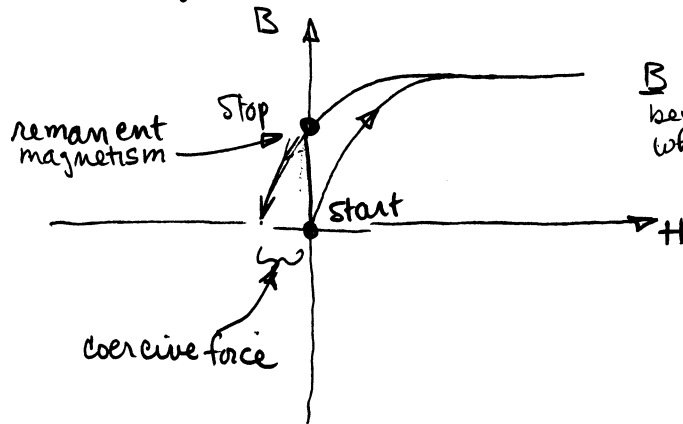
ferrimagnetic and ferrimagnetic  $\mu \gg \mu_0$

ferrites

hard  
soft.  
contain metallic ions.  
ferrites  
have nice high freq.  
 $\mu$  characteristics.

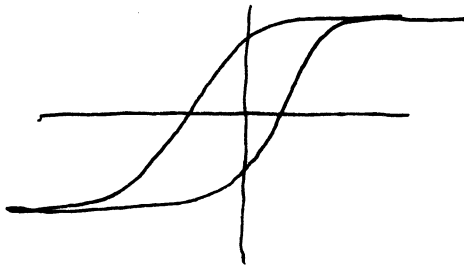
hard  
soft  
permanent magnets  
speaker magnets  
iron, etc.

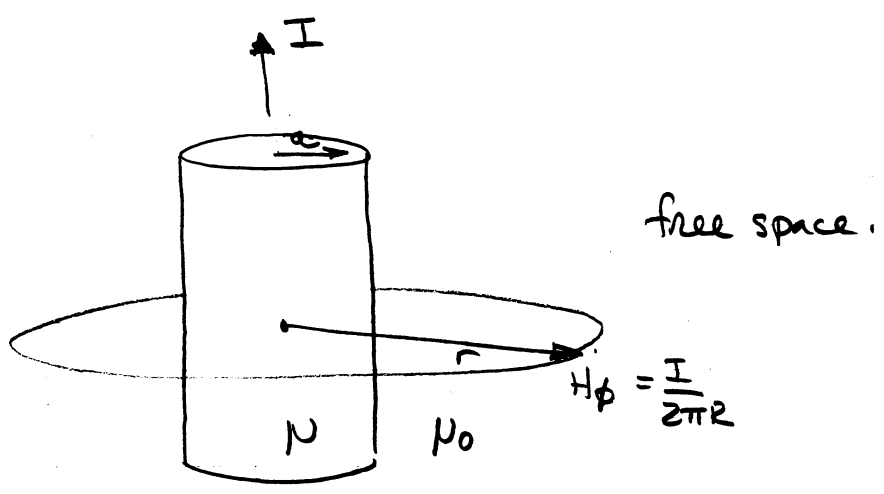
unusual property of ferromagnets  $\rightarrow$  HYSTERESIS



$B$  field saturates when  $H$  goes beyond a certain limit, when  $H$  is removed  $B$  is not zero.

overall,  $B$ - $H$  curve is cyclic and closed





current flows in a cylinder of radius  $a$  and permeability  $\mu$ .

What are  $\underline{B}$ ,  $\underline{H}$  and  $\underline{M}$  everywhere

use Ampère's law just as before.

$$\oint \underline{H} \cdot d\underline{l} = H_\phi 2\pi r = I \Rightarrow H_\phi = \frac{I}{2\pi r}$$

does the magnetic flux differ. You bet!

$$H_\phi = \begin{cases} \frac{I}{2\pi r} & r > a \\ \frac{I}{2\pi r} \frac{\pi r^2}{\pi a^2} = \frac{I}{2\pi r} \left(\frac{r}{a}\right)^2 & 0 < r < a \end{cases}$$

$$B_\phi = \frac{\mu_0 I}{2\pi r} \quad r > a$$

$$B_\phi = \mu \frac{I}{2\pi r} \left(\frac{r}{a}\right)^2 \quad 0 < r < a$$

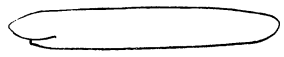
How about the magnetization?

$$B = \mu_0 (H + M) = \mu H.$$

$$H + M = \frac{\mu H}{\mu_0} \\ M = \left(\frac{\mu}{\mu_0} - 1\right) H$$

$$M = \left(\frac{\mu}{\mu_0} - 1\right) H_\phi \quad 0 < r < a \\ = 0 \quad r > a$$

$$\underline{J}_m = \nabla \times \underline{M} = - \frac{\partial M_\phi}{\partial z} \underline{a}_r + \frac{1}{r} \frac{\partial}{\partial r} (r M_\phi) \underline{a}_z$$



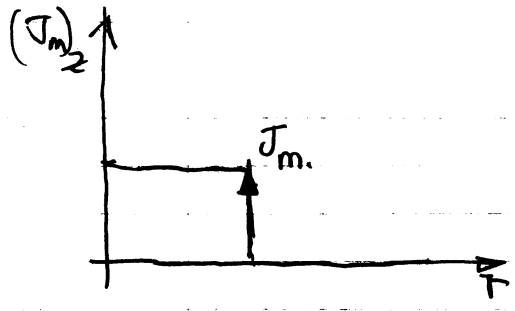
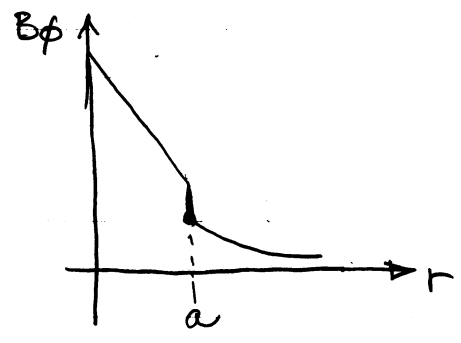
$$\underline{m} = \left(\frac{\mu}{\mu_0} - 1\right) \frac{I}{2\pi r} \left(\frac{r^2}{\pi a^2}\right) \underline{a}_\phi$$

$$\frac{\partial M_\phi}{\partial z} = 0$$

$$\begin{aligned} \frac{1}{r} \frac{\partial}{\partial r} [r m_\phi] &= \frac{1}{r} \frac{\partial}{\partial r} \left[ \left(\frac{\mu}{\mu_0} - 1\right) \frac{I}{2\pi a^2} r^2 \right] = \cancel{\frac{1}{r}} \left(\frac{\mu}{\mu_0} - 1\right) \frac{I}{\cancel{2\pi} a^2} \\ &= \left(\frac{\mu}{\mu_0} - 1\right) \frac{I}{\pi a^2} \end{aligned}$$

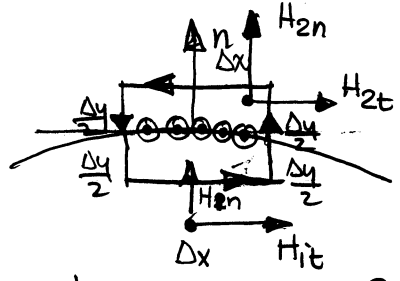
$$\therefore \underline{J}_m = \left(\frac{\mu}{\mu_0} - 1\right) \frac{I}{\pi a^2} \underline{a}_z$$

This says that the discontinuity in the B field is due to the magnetization current  $\underline{J}_m$ .



# Magnetic Boundary Conditions

(done just like E fields) tangential & normal components.



Apply Ampère's law

$$\oint \underline{H} \cdot d\underline{\ell} = \int \underline{J}_f \cdot d\underline{S}$$

↑  
for emphasis

$$\oint \underline{H} \cdot d\underline{\ell} = H_{1t} \Delta x + H_{1n} \frac{\Delta y}{2} + H_{2n} \frac{\Delta y}{2} - H_{2t} \Delta x - H_{2n} \frac{\Delta y}{2} - H_{1n} \frac{\Delta y}{2}$$

cancel

$$= (H_{1t} - H_{2t}) \Delta x$$

$$\oint \underline{J}_f \cdot d\underline{S} = J_n \Delta x \Delta y$$

$$\therefore J_n \Delta y = H_{1t} - H_{2t}$$

as  $\Delta y \rightarrow 0$   $J_n \Delta y \rightarrow K_s$  the surface current

$$\therefore (H_{1t} - H_{2t}) = K_n \quad \text{or} \quad \underline{n} \times (\underline{H}_2 - \underline{H}_1) = \underline{K}$$

vector

How about  $J_m$ ? Exactly the same except replace  $\underline{H}$  by  $\underline{m}$ !

$$(m_{1t} - m_{2t}) = (K_m)_n \quad \text{or} \quad \underline{n} \times (\underline{m}_2 - \underline{m}_1) = \underline{K}_m$$

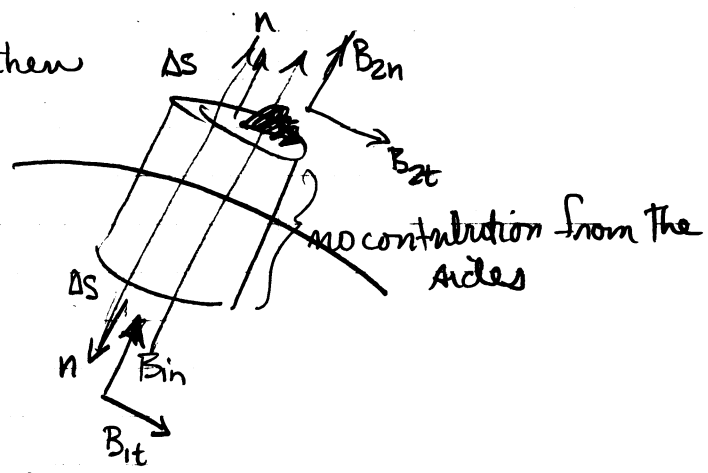


How about the normal components?

to do this we need to recall  $\Psi_m = \oint \underline{B} \cdot \underline{n} \, dS = 0$   
for a closed surface.

Why? There is no point charge on which field lines can terminate.

If  $\oint \underline{B} \cdot \underline{n} \, dS = 0$ . then



$$\oint \underline{B} \cdot \underline{n} \, dS = -(B_{in}) \Delta S + (B_{2n}) \Delta S = 0$$

$\therefore B_{2n} = B_{1n}$  and normal B is continuous.

# Scalar magnetic potential

lumped parameter analysis  
distributed parameter analysis

for a source-free region

$$\nabla \times \underline{H} = 0$$

$$\nabla \times \nabla \mathcal{F} = 0$$

this is a general vector identity  
for scalar fields

$$\therefore \underline{H} = -\nabla \mathcal{F}$$

↑  
choose the - sign only to make this the same  
as for electric potential

we can integrate this to get

$$\mathcal{F}_2 - \mathcal{F}_1 = - \int_{P_1}^{P_2} \underline{H} \cdot d\underline{l}$$

↑  
units of amperes.

this is often called the magnetomotive force or mmf.

by doing more math I can show that  $\nabla^2 \mathcal{F} = 0$   
in a source-free region

$$\Psi_m = \int_S \underline{B} \cdot d\underline{s} \quad \left. \vphantom{\int_S \underline{B} \cdot d\underline{s}} \right\} \text{this is similar to the electric potential}$$

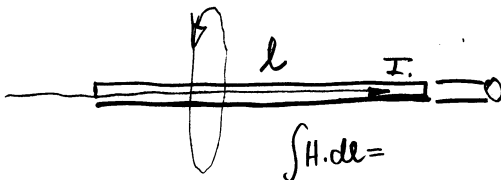
flux density.

write ohm's law for magnetic circuits

$$\mathcal{F} = R \Psi_m \quad R = \frac{\mathcal{F}}{\Psi_m}$$

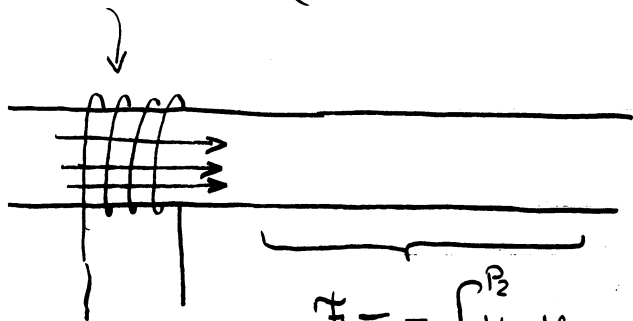
↑  
reluctance

← magnetomotive force  
← flux



$$ds = A.$$

source of flux (just like current)



magnetic circuit

$$\mathcal{F} = - \int_{P_1}^{P_2} \underline{H} \cdot d\underline{l}$$

this is really the beginning of Ohm's Law

If we define  $\Phi_m = \int \underline{B} \cdot d\underline{s}$

then we have

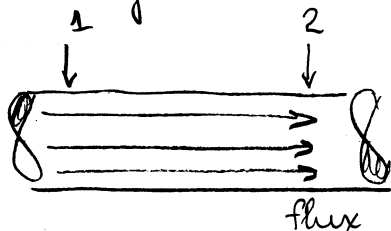
$$\mathcal{F} = R \Phi_m$$

$$[v = iR]$$

what is  $R$ ?

the reluctance

how can we get the Reluctance

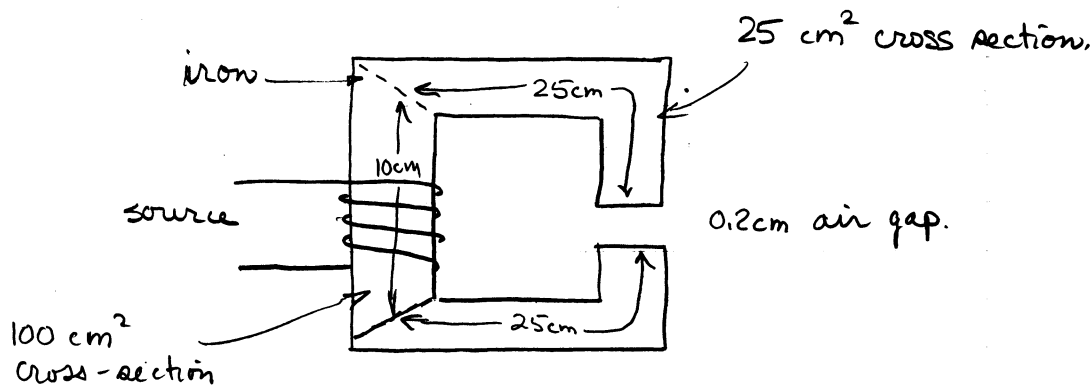


for a simple uniform geometry

$$\Phi_m = \int \underline{B} \cdot d\underline{s} = \int \mu \underline{H} \cdot d\underline{s} = \mu H A$$

$$\mathcal{F} = \int_1^2 \underline{H} \cdot d\underline{l} = H l$$

$$\therefore R = \frac{\mathcal{F}}{\Phi_m} = \frac{H l}{\mu H A} = \frac{l}{\mu A}$$



given the field I want in the gap how many turns do I need to get a field of  $1 \text{ Wb/m}^2$ .

air-gap reluctance

$$R_g = \frac{l}{\mu_0 \mu_r A} = \frac{2 \times 10^{-3}}{4\pi \times 10^{-7} \times 25 \times 10^{-4}} = 6.36 \times 10^5 \frac{\text{A-t}}{\text{Wb}}$$

$H = \text{amperes/m}$ .

$B = \text{webers/m}^2$

$\mu = \text{henrys/m}$

$R = \frac{\text{amperes (turns)}}{\text{weber, not really}}$

$\mathcal{F} = \text{ampere turns}$ .

$\Psi = \text{webers}$ .

air-gap flux

$$\Phi_m = \int B \cdot dS = \int 1 \frac{\text{Wb}}{\text{m}^2} ds = 1 \frac{\text{Wb}}{\text{m}^2} \cdot 25 \times 10^{-4} \text{m}^2 = 25 \times 10^{-4} \text{Wb}$$

by "ohm's law"

$$\mathcal{F}_g = \Psi_m R_g = 6.36 \times 10^5 \times 25 \times 10^{-4} = 1.590 \times 10^3 \text{ Ampere turns}$$

How about the rest of the circuit?

for the two "steel arms"

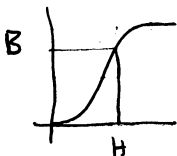
$$\mathcal{F}_{\text{steel}} = (25 \text{ cm} + 25 \text{ cm}) \cdot H$$

but what is H?

we know B

$$B = 1 \frac{\text{Wb}}{\text{m}^2} \text{ since normal B is continuous}$$

From chart



$$B = 1 \frac{\text{Wb}}{\text{m}^2} \rightarrow 200 \frac{\text{Amperes (turns)}}{\text{m}}$$

$$\mathcal{H}_{\text{steel}} = (0.50 \text{ meters}) \cdot \frac{200 \text{ Amperes} \cdot \text{turns}}{\text{meter}} = 100 \text{ At}$$

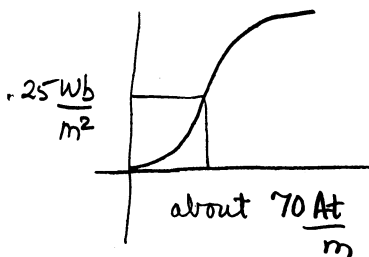
How about the steel transformer section?

$$\mathcal{H} = (0.10 \text{ meters}) (H)$$

but what is  $H$ ?  $\Phi = 25 \times 10^{-4}$  Webers as before.

$$\text{but } \Phi = \int B ds = B \cdot 100 \text{ cm}^2$$

$$B = \frac{25 \times 10^{-4}}{.01 \text{ m}^2} = 0.25 \frac{\text{Wb}}{\text{m}^2}$$



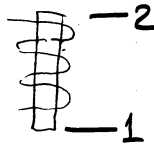
$$\therefore \mathcal{H} = (0.10 \text{ m}) (70 \frac{\text{At}}{\text{m}}) = 7.0 \text{ A-t.}$$

∴ we have the total circuit mmf.

$$\begin{aligned} \mathcal{H}_{\text{total}} &= \mathcal{H}_{\text{gap}} + \mathcal{H}_{\text{steel}} + \mathcal{H}_{\text{transformer}} \\ &= 1590 + 100 + 7 \\ &= 1697 \text{ A-t.} \end{aligned}$$

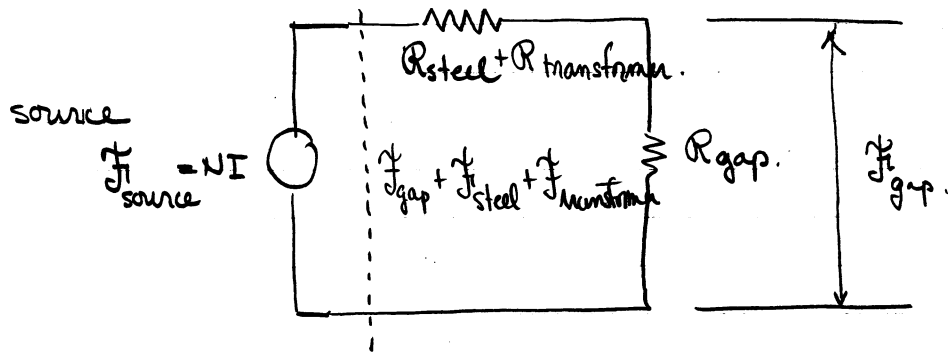
How about the source? This is a solenoid.

$$\text{Recall } H = \frac{NI}{l}$$



$$\mathcal{H}_{\text{source}} = \int_1^2 H \cdot dl = \frac{NI}{l} \cdot l = NI$$

This problem now has a solution



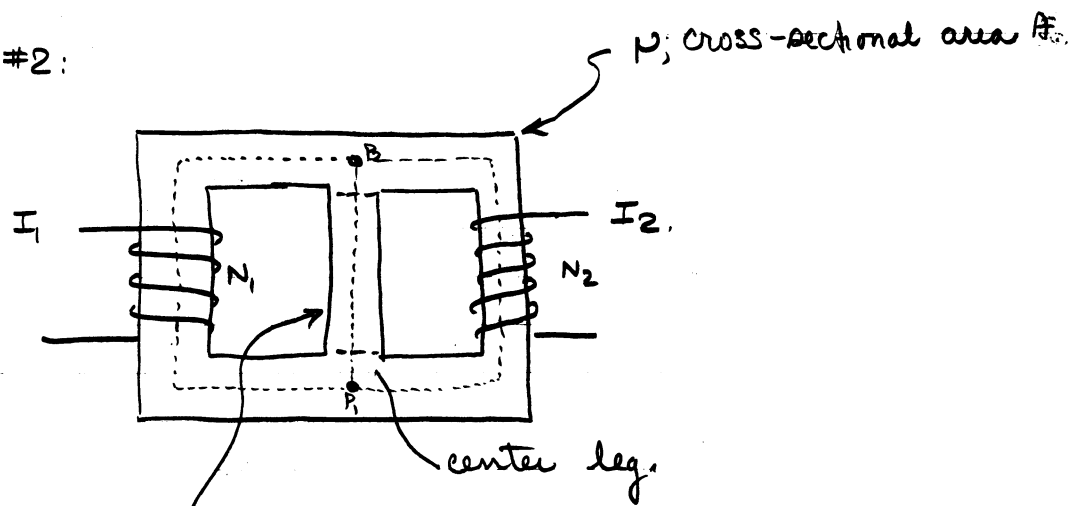
given  $F_{gap}$ , what was needed  $F_{source}$ ?

$$\therefore F_{source} = 1697 \text{ A} \cdot t = NI.$$

If  $I = 10 \text{ A}$ .  $N = 169.7$

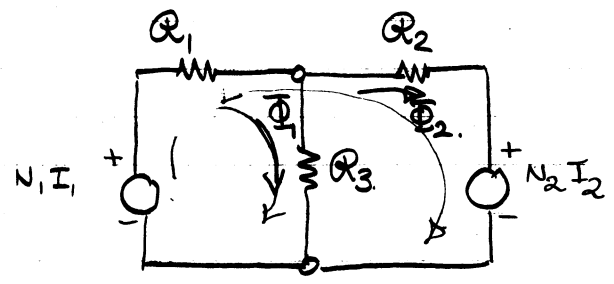
hence the use of the name Ampere-turns.

Example #2:



what is  $\Psi_m$  here.

draw electrical equivalent.



$$R_1 \triangleq \text{reluctance thru coil 1 from } P_1 \text{ to } P_2.$$

$$= \frac{l_1}{\mu A}$$

$$R_2 \triangleq \text{ " coil 2 " }$$

$$= \frac{l_2}{\mu A}$$

$$R_3 \triangleq \text{reluctance thru center leg.} = \frac{l_3}{\mu A}.$$

loop equations:  $N_1 I_1 = R_1 (\Phi_1 + \Phi_2) + R_3 \Phi_1$

$$N_1 I_1 - N_2 I_2 = R_1 (\Phi_1 + \Phi_2) + R_2 \Phi_2$$

(6)

$$\begin{aligned}
 (R_1 + R_3) \Phi_1 + R_1 \Phi_2 &= N_1 I_1 \\
 R_1 \Phi_1 + (R_1 + R_2) \Phi_2 &= N_1 I_1 - N_2 I_2
 \end{aligned}$$

$$\Phi_1 = \frac{\begin{bmatrix} N_1 I_1 & R_1 \\ N_1 I_1 - N_2 I_2 & R_1 + R_2 \end{bmatrix}}{\begin{bmatrix} R_1 + R_3 & R_1 \\ R_1 & R_1 + R_2 \end{bmatrix}}$$

$$= \frac{(N_1 I_1) \cancel{R_1} + R_2 N_1 I_1 - \cancel{R_1} N_1 I_1 + N_2 I_2 R_1}{\dots}$$

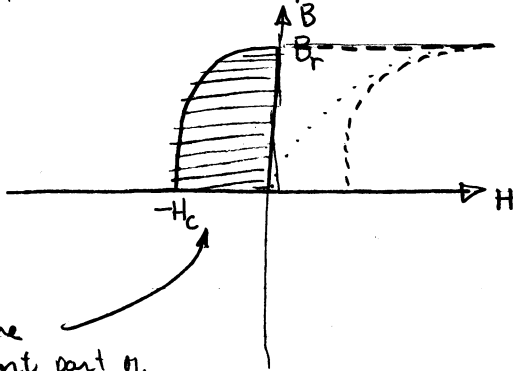
$$\left[ \cancel{R_1^2} + R_1 R_3 + R_1 R_2 + R_2 R_3 - \cancel{R_1^2} \right]$$

$$\Phi_1 = \frac{R_2 N_1 I_1 + R_1 N_2 I_2}{R_1 R_3 + R_1 R_2 + R_2 R_3}$$



How about a Permanent magnet.

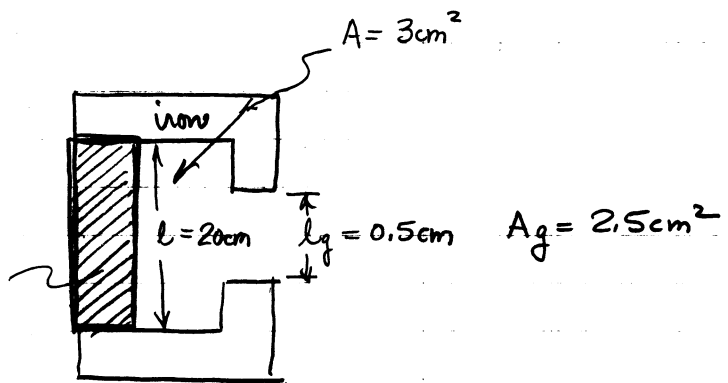
No real problem except we must use a second quadrant curve.



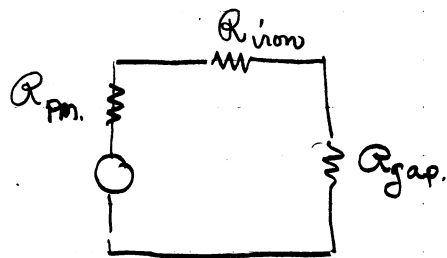
this is the permanent part of the magnet.

(this is actually the demagnetization curve)

say uniform M  
 $B = \mu_0 M$



as before



How about the magnet?

$$\oint_{PM} H \cdot dl = Ml$$

$$\Phi_{PM} = \int B \cdot dS = B \cdot A$$

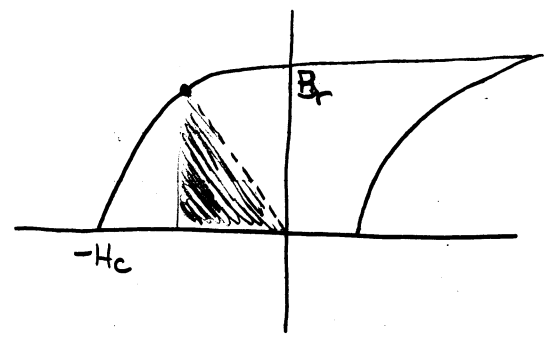
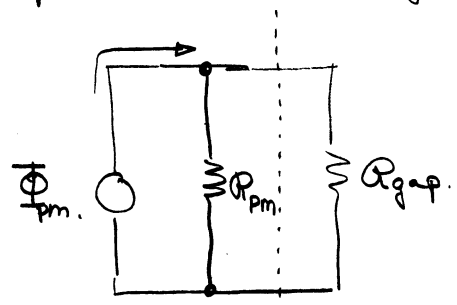
$$R_{PM} = \frac{\oint_{PM} H}{\Phi_{PM}} = \frac{Ml}{B \cdot A} = \frac{M}{Bt} = \frac{M}{\mu M t} = \frac{1}{\mu t}$$

typically,  $t = 1cm.$

$$\mu = \frac{B}{H} = \frac{1 \text{ Wb/m}^2}{25000 \text{ A/m}} = \frac{1}{25000} \frac{\text{W}}{\text{A-m}} = 4 \times 10^{-5} \frac{\text{W}}{\text{A-m}}$$

$$R_{pm} \approx \frac{1}{\frac{4 \times 10^{-5} \text{ W}}{\text{A-m}} \times 10^{-2}} = \frac{1}{4 \times 10^{-7} \text{ W}} \approx 10^7 \frac{\text{A}}{\text{W}}$$

neglecting the reluctance of iron.



this is a current source  $R_{pm} \gg R_{gap}$  and can be neglected.

$$\Phi_{pm} \approx \frac{\mathcal{F}_{gap}}{R_{gap}}$$

$$R_{gap} = \frac{l_g}{\mu A_g} = \frac{0.5 \times 10^{-2} \text{ m}}{4\pi \times 10^{-7} \frac{\text{Hy}}{\text{m}} \cdot \frac{5 \times 10^{-4} \text{ m}^2}{2}} = \frac{\text{A-t}}{\text{Weber}}$$

$$= \frac{1}{48\pi \cdot \frac{5}{2} \times 10^{-11}} = \frac{1}{20\pi} \times 10^9 \frac{\text{A-t}}{\text{weber}}$$

the magnet is at  $B = 0.95 \text{ Wb/m}^2$   
 $H = -24,000 \text{ A/m}$

$$\begin{array}{r} .95 \\ - .3 \\ \hline 2.85 \end{array}$$

$$\Phi = \int B \cdot dS = 0.95 \frac{\text{Wb}}{\text{m}^2} \times 3 \times 10^{-4} \text{ m}^2 = 2.85 \times 10^{-4} \text{ Wb}$$

$$\mathcal{F}_{gap} = \Phi_{pm} R_{gap} = 2.85 \times 10^{-4} \text{ Wb} \cdot \frac{10^9}{2\pi} \times 10^9$$

$$= \frac{2.85}{2\pi} \times 10^4 \approx 3 \times 10^4 \frac{\text{A-t}}{\text{weber}}$$