

EEAP 210
ELECTROMAGNETIC FIELDS
SPRING SEMESTER 1983

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TEXT: PAUL & NASAR, INTRODUCTION TO ELECTROMAGNETIC FIELDS

COURSE OUTLINE (Approximately - SUBJECT TO SOME CHANGE)

LECTURES	TOPIC	CHAPTERS IN TEXT
3	VECTOR ANALYSIS	1, 2
1	Exam	—
6	Electrostatics	3
1	Exam	—
6	Magnetostatics	4
1	Exam	—
8	Maxwell's Equations	5
1	Exam	—
6	Waves and Radiation	6
1	Exam	—
6	Transmission Lines	7
1	Exam	—
3	Waveguides	8
2	Potential Functions	10
	Final Exam	

EEAP 210
REVISED SYLLABUS
&
GRADING POLICY

FRIDAY'S MEETING WITH THE COMMITTEE OF FOUR PRODUCED THE
REVISED GRADING POLICY SHOWN BELOW:

HOMEWORK	18 POINTS
EXAMS (5)	59 POINTS
FINAL	<u>23 POINTS</u>
	100 POINTS TOTAL

THE FINAL TWO (2) EXAMS WILL BE :

FRIDAY APRIL 15TH
FRIDAY APRIL 29TH.

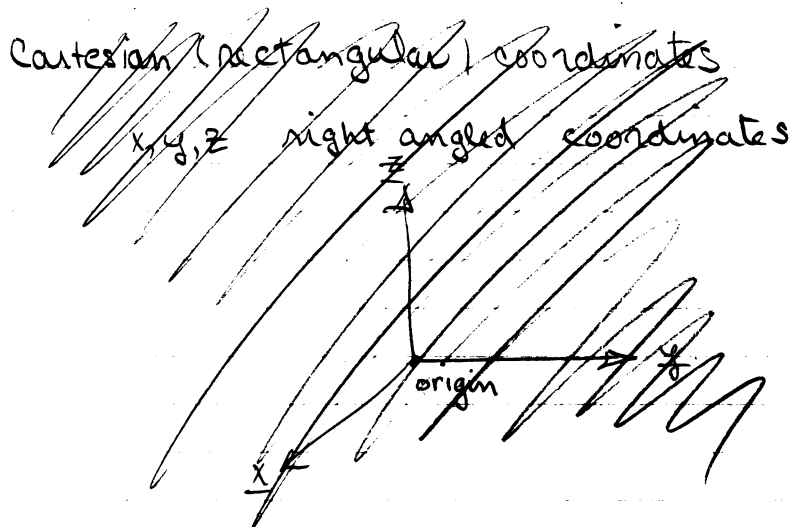
THESE EXAMS WILL BE EQUALLY WEIGHTED WITH THE PREVIOUS 3 EXAMS.

SYLLABUS

<u>DATE</u>	<u>LECTURE</u>
4/4	Time-dependent Maxwell's Equations, displacement current
4/6	Sinusoidal-steady state, Poynting vector
4/8	Wave equation, plane waves
4/11	Traveling waves, group & phase velocity, impedance
4/13	Conductors & dielectrics, reflection & transmission of plane waves
4/15	<u>EXAM # 4</u>
4/18	TEM waves, "transmission line" equations, traveling waves
4/20	Pulse transmission on a "transmission" line
4/22	reflection coefficient, impedance, load transformation
4/25	"lumped" versus "distributed" transmission lines
4/27	Waveguides <u>OR</u> quasi-statics
4/29	<u>EXAM # 5</u>

THERE WILL BE EVENING LECTURES APRIL 12TH and 26TH,
PROBABLY AT 7:00 IN GLENNAN, PROBABLY IN 713(?).

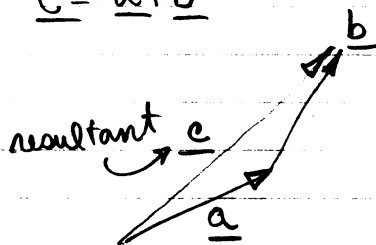
- Purpose:
- vector definitions & scalar operations ✓
 - Cartesian coordinates ✓
 - vector operations
 - coordinate systems
 - scalar vs. vector fields



vector - basic magnitude (quantity) with direction

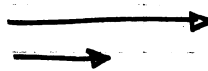
scalar operations on vectors operate in an algebraic manner (addition, subtraction, scalar multiplication)

addition $\underline{c} = \underline{a} + \underline{b}$



representations of vectors

magnitude by length.



direction by direction and arrow head.

unit vectors

The magnitude is one
indicate direction only.

For example:

$$\underline{a} = a \underline{a}_u$$

$$\underline{b} = b \underline{b}_u$$

↙ ↘
magnitude direction

vector components - represent vectors by sums of unit vectors

$$\underline{c} = \underline{a} + \underline{b} = a \underline{a}_u + b \underline{b}_u = [a, b]$$

where it is assumed we know what the unit vectors are.

$$\underline{a} = a \underline{a}_u = [a, 0]$$

$$\underline{b} = b \underline{b}_u = [0, b]$$

$$\underline{c} = a \underline{a}_u + b \underline{b}_u = [a, 0] + [0, b] = [a, b]$$

scalar multiplication

$$\underline{d} = k \underline{a} = k a \underline{a}_u = [ka, 0]$$

increases magnitude by k , does not change direction

$$\underline{d} = k \underline{c} = k [\underline{a} + \underline{b}] = k \underline{a} + k \underline{b} = [ka, 0] + [0, kb]$$

$$= [ka, kb]$$

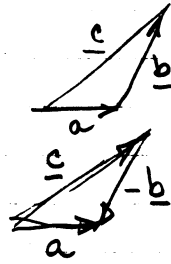
commutative ↗

subtraction

if $\underline{c} = \underline{a} + \underline{b}$

$\underline{a} = \underline{c} - \underline{b}$

$[a, 0]$



subtraction reverses the direction of \underline{b}

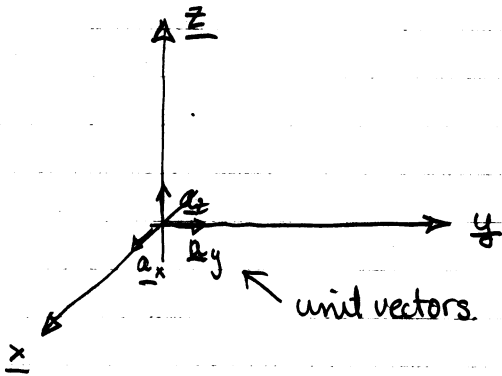
$\underline{c} = [a, b]$

$\underline{b} = [0, b]$

$-\underline{b} = [0, -b]$

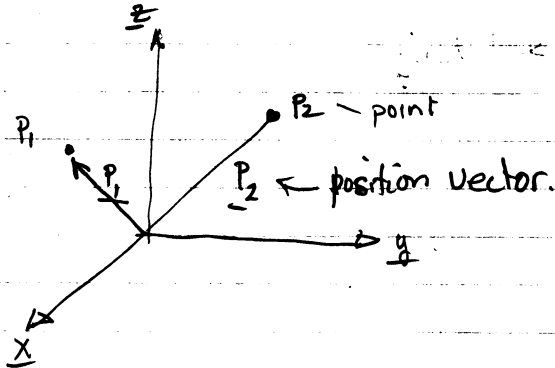
$\therefore \underline{c} - \underline{b} = [a, b] + [0, -b] = [a, 0] = \underline{a}$

Cartesian coordinates

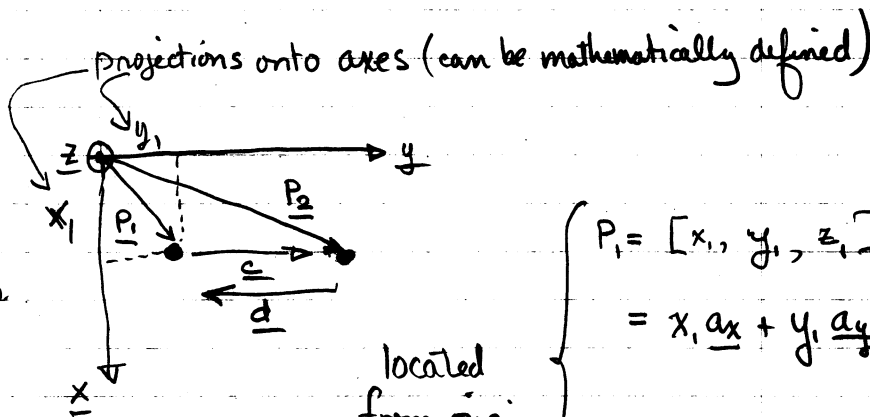


axes (unit vectors) at right angles.

we can use a vector to denote only position, location, distance, etc.



just
x, y
for example.



located
from origin

$$\left\{ \begin{aligned} P_1 &= [x_1, y_1, z_1] \\ &= x_1 \underline{a}_x + y_1 \underline{a}_y + z_1 \underline{a}_z \\ P_2 &= [x_2, y_2, z_2] \\ &= x_2 \underline{a}_x + y_2 \underline{a}_y + z_2 \underline{a}_z \end{aligned} \right.$$

since the vector indicates the location of an object
what is difference in locations between P_1 and P_2 .
Since this is a vector, the position from \underline{P}_1 from \underline{P}_2
is NOT the same as \underline{P}_2 from \underline{P}_1

the distance (magnitude & direction) from P_1 to P_2 is

$$\underline{P}_1 + \underline{c} = \underline{P}_2 \quad \text{or} \quad \underline{P}_2 + \underline{d} = \underline{P}_1$$

$$\underline{c} = \underline{P}_2 - \underline{P}_1$$

$$\underline{d} = \underline{P}_1 - \underline{P}_2$$

$$= -(\underline{P}_2 - \underline{P}_1)$$

$$= -\underline{c}$$

as we expected.

in vector notation

$$\underline{c} = \underline{P}_2 - \underline{P}_1 = [x_2, y_2, z_2] - [x_1, y_1, z_1] = [x_2 - x_1, y_2 - y_1, z_2 - z_1]$$

\underline{c} represents the vector distance from \underline{P}_1 to \underline{P}_2

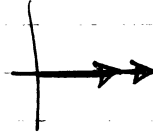
What is the scalar distance

if \underline{c} lay along one of the axes, say \underline{a}_x , only

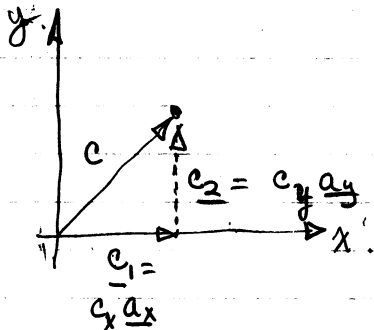
then $\underline{c} = [0, 0, c]$

and by inspection $|\underline{c}| = c$

means
scalar magnitude



if \underline{c} lay in the plane, say \underline{a}_x and \underline{a}_y



$$\underline{c} = \underline{c}_1 + \underline{c}_2$$

$$= c_x \underline{a}_x + c_y \underline{a}_y$$

what is $|\underline{c}|$? by inspection of graph. $|\underline{c}| = \sqrt{c_x^2 + c_y^2}$

x 5

using Pythagoras' theorem.

expanding to three dimensions.

$$|\underline{c}| = \sqrt{c_x^2 + c_y^2 + c_z^2}$$

differential lengths

an incremental distance in the x direction would be dx

↑
magnitude
since direction is
assumed.

the distance from x_1 to x_2 must be.

$$d = \int_{x_1}^{x_2} dx = x \Big|_{x_1}^{x_2} = x_2 - x_1$$

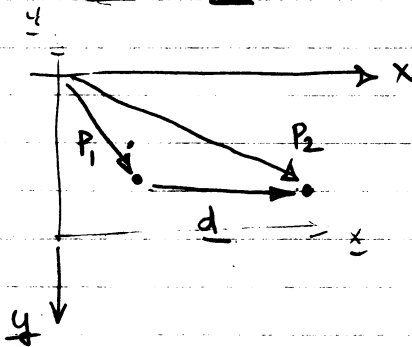
the distance from $\underline{P_1}$ to $\underline{P_2}$

$$\underline{d} = \int_{\underline{P_1}}^{\underline{P_2}} d\underline{l}$$

↑ what is \underline{d} ?

$d\underline{l}$ is a differential magnitude as we move along a vector from $\underline{P_1}$ to $\underline{P_2}$

Assume the $\underline{P_1}$ and $\underline{P_2}$ we had before



consider $\underline{d} = \underline{\Delta l_1} + \underline{\Delta l_2} + \underline{\Delta l_3} + \underline{\Delta l_4}$

$$\text{then } \underline{d} = \sum_{i=1}^N \underline{\Delta l_i} + \dots$$

as $|\underline{\Delta l_i}| \rightarrow 0$

$$\underline{d} = \int_{\underline{P_1}}^{\underline{P_2}} d\underline{l}$$

what is \underline{d} ? \underline{d} is the differential vector along \underline{d} and is not necessarily pointing in the same direction all the time.

however, in this case

$$d\underline{d} = dx \underline{a}_x + dy \underline{a}_y + dz \underline{a}_z$$

suppose we simply wanted the distance from P_1 to P_2
no vector.

i.e. $|\underline{d}|$

then

$$|\underline{d}| = \int_{\underline{P}_1}^{\underline{P}_2} |d\underline{d}| = \int_{\underline{P}_1}^{\underline{P}_2} \sqrt{dx^2 + dy^2 + dz^2}$$



if \underline{d} is a straight line then we can calculate

$$|\underline{d}| \text{ by } \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}$$

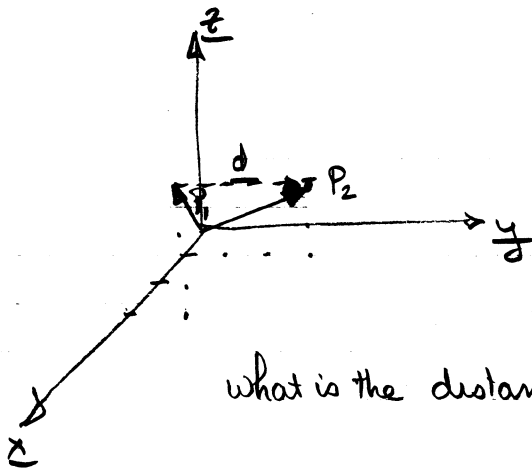
however, if we need the length along a specific
~~contour~~ contour we must use the above equation.

Example:

$$P_1 = [3, 1, 3]$$

$$P_2 = [1, 3, 2]$$

} rectangular coordinate system



what is the distance between P_1 and P_2

since there is no contour

$$\begin{aligned} |P_2 - P_1| = |d| &= \sqrt{(1-3)^2 + (3-1)^2 + (2-3)^2} \\ &= \sqrt{(-2)^2 + (2)^2 + (-1)^2} = \sqrt{4+4+1} = \sqrt{9} = 3 \end{aligned}$$

by contour integral

what is the vector from P_1 to P_2

$$\begin{aligned} \underline{d} &= \underline{P}_2 - \underline{P}_1 = (\underline{a}_x + 3\underline{a}_y + 2\underline{a}_z) - (3\underline{a}_x + \underline{a}_y + 3\underline{a}_z) \\ &= -2\underline{a}_x + 2\underline{a}_y - \underline{a}_z \end{aligned}$$

The problem in evaluating the integral this way is that we must write the equation of the line (\underline{d}) between \underline{P}_1 and \underline{P}_2 .

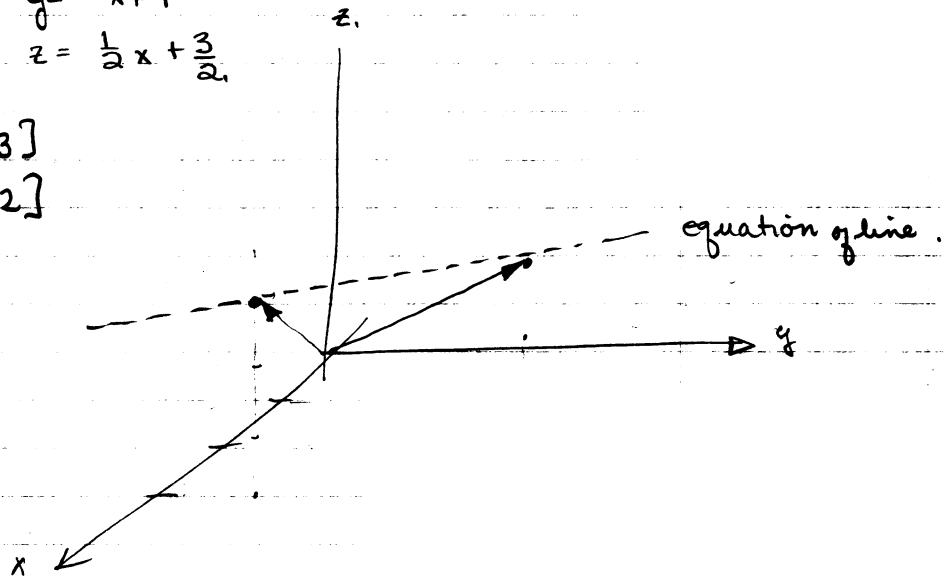
the vector $\underline{d} = -2\underline{a}_x + 2\underline{a}_y - \underline{a}_z$

$$y = -x + 4$$

$$z = \frac{1}{2}x + \frac{3}{2}$$

$$[x_1, y_1, z_1] = [3, 1, 3]$$

$$[x_2, y_2, z_2] = [1, 3, 2]$$



two-point form (see a text on analytic geometry)

$$\frac{y - y_1}{x - x_1} = \frac{y_2 - y_1}{x_2 - x_1}$$

$$\frac{y - 1}{x - 3} = \frac{3 - 1}{1 - 3}$$

$$\frac{y - 1}{x - 3} = \frac{2}{-2} = -1$$

$$y - 1 = -x + 3$$

$$\boxed{y = -x + 4}$$

$$\frac{z - z_1}{x - x_1} = \frac{z_2 - z_1}{x_2 - x_1}$$

$$\frac{z - 3}{x - 3} = \frac{2 - 3}{1 - 3} = \frac{-1}{-2} = \frac{1}{2}$$

$$z - 3 = \frac{1}{2}(x - 3)$$

$$z - 3 = \frac{1}{2}x - \frac{3}{2}$$

$$z = \frac{1}{2}x - \frac{3}{2} + \frac{6}{2} = \boxed{\frac{1}{2}x + \frac{3}{2}}$$

This is the equation
of the line.

example (cont.)

$$y = -x + 4$$

$$z = \frac{1}{2}x + \frac{\sqrt{3}}{2}$$

$$dy = -dx$$

$$dz = +\frac{1}{2} dx$$

$$\begin{aligned} \therefore dl &= \sqrt{dx^2 + dy^2 + dz^2} \\ &= \sqrt{dx^2 + (-dx)^2 + \left(\frac{1}{2}dx\right)^2} \\ &= \sqrt{dx^2 + dx^2 + \frac{1}{4}dx^2} \\ &= \sqrt{\left(1 + 1 + \frac{1}{4}\right)dx^2} = \sqrt{\frac{9}{4}dx^2} = \frac{3}{2}dx \end{aligned}$$

$$\underline{|dl|} = \int_{P_1}^{P_2} dl = \int_{x=3}^{x=1} \frac{3}{2} dx = \frac{3}{2}x \Big|_3^1 = \frac{3}{2}[1-3] = -3. \quad \blacksquare$$

Why is this answer wrong?

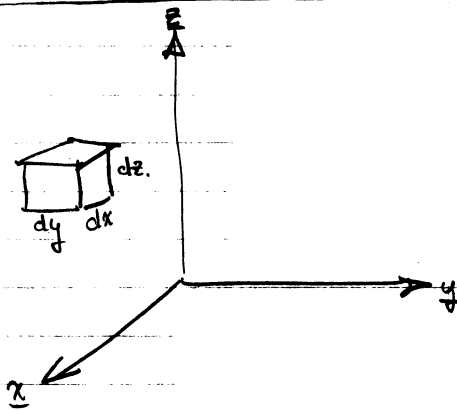
$$\text{because } dl = \pm \sqrt{dx^2 + dy^2 + dz^2}$$

and in this case we choose the minus sign

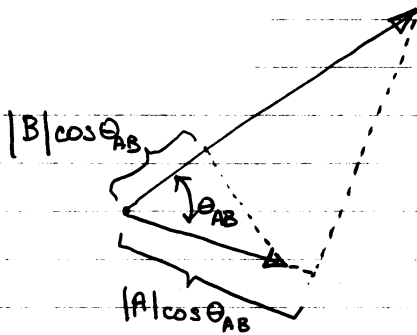
because $|dl|$ must always be positive or zero.

differential volume

$$dV = dx dy dz.$$



Vector operations (these appear in electromagnetic field equations)



dot product

$$\underline{A} \cdot \underline{B} \triangleq |\underline{A}| |\underline{B}| \cos \theta_{AB}$$

this is read A dot B.

The result is a scalar and this is often called the scalar product.

① The best geometric interpretation of $\underline{A} \cdot \underline{B}$ is that it is the projection of \underline{A} onto \underline{B} .

② A valuable property of the dot product is that we can, if we, know $\underline{A} \cdot \underline{B}$, compute the included angle.

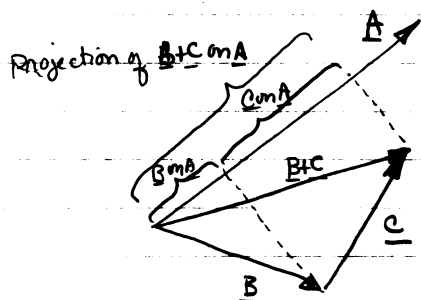
$$\text{If } \underline{A} \cdot \underline{B} = |\underline{A}| |\underline{B}| \cos \theta_{AB}$$

$$\theta_{AB} = \cos^{-1} \left[\frac{\underline{A} \cdot \underline{B}}{|\underline{A}| |\underline{B}|} \right]$$

This works if we know how to compute $\underline{A} \cdot \underline{B}$ by another method.

to develop how we can operate in terms of unit vectors consider the dot product of \underline{A} and the sum of two vectors \underline{B} and \underline{C}

$$\underline{A} \cdot (\underline{B} + \underline{C}) = \underline{A} \cdot \underline{B} + \underline{A} \cdot \underline{C}$$



extending this result

$$\underline{A} \cdot (\underline{B} + \underline{C} + \underline{D}) = \underline{A} \cdot \underline{B} + \underline{A} \cdot \underline{C} + \underline{A} \cdot \underline{D}$$

$$(\underline{A} + \underline{E}) \cdot (\underline{B} + \underline{C} + \underline{D}) = \underline{A} \cdot (\underline{B} + \underline{C} + \underline{D}) + \underline{E} \cdot (\underline{B} + \underline{C} + \underline{D})$$

$$= \underline{A} \cdot \underline{B} + \underline{A} \cdot \underline{C} + \underline{A} \cdot \underline{D} + \underline{E} \cdot \underline{B} + \underline{E} \cdot \underline{C} + \underline{E} \cdot \underline{D}$$

etc.

suppose $\underline{A} = A_x \underline{a}_x + A_y \underline{a}_y + A_z \underline{a}_z$

$$\underline{B} = B_x \underline{b}_x + B_y \underline{b}_y + B_z \underline{b}_z$$

$$\underline{A} \cdot \underline{B} = (A_x \underline{a}_x + A_y \underline{a}_y + A_z \underline{a}_z) \cdot (B_x \underline{b}_x + B_y \underline{b}_y + B_z \underline{b}_z)$$

$$= A_x B_x \underline{a}_x \cdot \underline{b}_x + A_y B_x \underline{a}_y \cdot \underline{b}_x + A_z B_x \underline{a}_z \cdot \underline{b}_x$$

$$+ A_x B_y \underline{a}_x \cdot \underline{b}_y + A_y B_y \underline{a}_y \cdot \underline{b}_y + A_z B_y \underline{a}_z \cdot \underline{b}_y$$

$$+ A_x B_z \underline{a}_x \cdot \underline{b}_z + A_y B_z \underline{a}_y \cdot \underline{b}_z + A_z B_z \underline{a}_z \cdot \underline{b}_z$$

but $\underline{a}_i \cdot \underline{b}_j = \delta_{ij}$ (use projections)

$$\therefore \underline{A} \cdot \underline{B} = A_x B_x + A_y B_y + A_z B_z$$

can I write $\underline{A} \cdot \underline{B} \cdot \underline{C}$

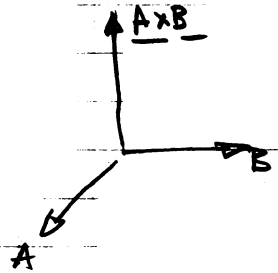
No! $\underline{A} \cdot \underline{B}$ is not a vector

and $(\underline{A} \cdot \underline{B}) \cdot \underline{C}$ makes no sense.

cross product

$$\underline{A} \times \underline{B} = |\underline{A}| |\underline{B}| \sin \theta_{AB} \underline{a}_N$$

$\underline{a}_N \perp$ to plane containing \underline{A} and \underline{B}



Right hand rule

Take your right hand, extend it along \underline{A} and rotate your hand from \underline{A} to \underline{B} , your thumb will point in the direction of $\underline{A} \times \underline{B}$

(this is also the way a screw operates, often operations in the plane produce operations \perp to the plane).

from the definition

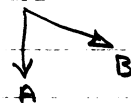
$$\theta_{AB} = \sin^{-1} \frac{\underline{A} \times \underline{B}}{|\underline{A}| |\underline{B}|}$$

This is a much more difficult operation to write in terms of unit vectors.

First;

$$\underline{A} \times \underline{B} = -\underline{B} \times \underline{A}$$

this can be seen in that the angle θ_{AB} changes sign and the sine changes accordingly



$$\underline{A} \times (\underline{B} + \underline{C}) = \underline{A} \times \underline{B} + \underline{A} \times \underline{C}$$

$$(\underline{A} + \underline{D}) \times (\underline{B} + \underline{C}) = \underline{A} \times (\underline{B} + \underline{C}) + \underline{D} \times (\underline{B} + \underline{C})$$

$$= \underline{A} \times \underline{B} + \underline{A} \times \underline{C} + \underline{D} \times \underline{B} + \underline{D} \times \underline{C}$$

etc.

$$\underline{A} \times \underline{B} = (A_x \underline{a}_x + A_y \underline{a}_y + A_z \underline{a}_z) \times (B_x \underline{b}_x + B_y \underline{b}_y + B_z \underline{b}_z)$$

$$= A_x B_x \underline{a}_x \times \underline{a}_x + A_y B_x \underline{a}_y \times \underline{a}_x + A_z B_x \underline{a}_z \times \underline{a}_x$$

$$+ A_x B_y \underline{a}_x \times \underline{a}_y + \cancel{A_y B_y} \underline{a}_y \times \underline{a}_y + A_z B_y \underline{a}_z \times \underline{a}_y$$

$$+ A_x B_z \underline{a}_x \times \underline{a}_z + A_y B_z \underline{a}_y \times \underline{a}_z + A_z B_z \underline{a}_z \times \underline{a}_z$$

any vector crossed with itself will be zero as $\underline{a} \times \underline{a} \rightarrow 0$.

$$\underline{a}_y \times \underline{a}_x = -\underline{a}_z$$

$$\underline{a}_z \times \underline{a}_x = \underline{a}_y$$

$$\underline{a}_x \times \underline{a}_y = \underline{a}_z$$

$$\underline{a}_z \times \underline{a}_y = -\underline{a}_x$$

$$\underline{a}_x \times \underline{a}_z = -\underline{a}_y$$

$$\underline{a}_y \times \underline{a}_z = \underline{a}_x$$

$$\underline{A} \times \underline{B} = \underline{a}_x (A_y B_z - A_z B_y) + \underline{a}_y (A_z B_x - A_x B_z) + \underline{a}_z (A_x B_y - A_y B_x)$$

$$= \begin{vmatrix} \underline{a}_x & \underline{a}_y & \underline{a}_z \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$$

be careful $\underline{A} \cdot (\underline{B} + \underline{C}) = \underline{A} \cdot \underline{B} + \underline{A} \cdot \underline{C}$
 these are dot products!

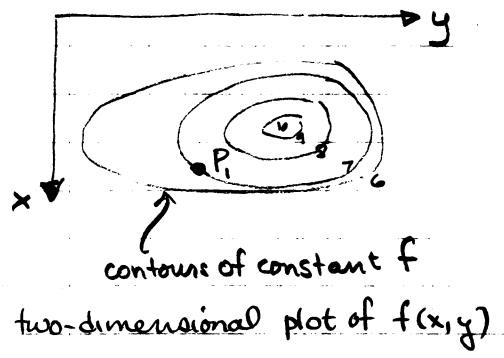
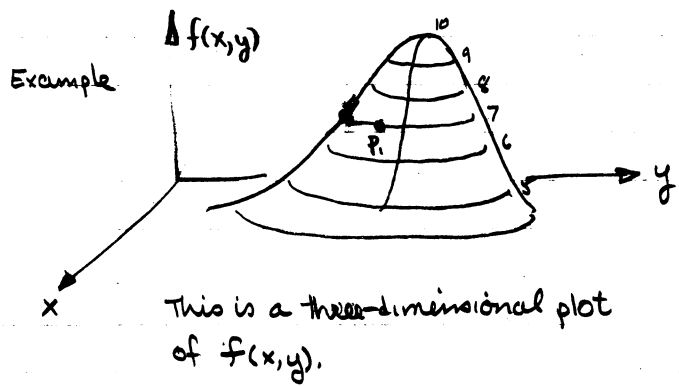
Objective: basic concepts of vector calculus

- 1. gradient
- 2. divergence
- 3. curl
- 4. Stoke's Theorem.

As will be shown in later lectures, the form of vector fields tells us about the sources of the fields. Basically, Maxwell's equations are the complete relationship between sources and fields. It turns out that the divergence and curl are the form that the source-field relationship takes.

GRADIENT - the gradient is the directional derivative of a scalar field.

A scalar field is one that is a simple function of position; the dependent variable is not a vector. Examples: temperature, pressure, humidity, etc.



Note that the derivative may be defined at P_1 , but its value depends upon the direction. In general, a small change in f will be given by

$$df = \frac{\partial f}{\partial x} dx + \frac{\partial f}{\partial y} dy + \frac{\partial f}{\partial z} dz \quad \text{This is in any direction. (1)}$$

lets re-write this in a vector form and look at its directional properties. The above looks a lot like a vector dot product - it's a sum of ~~two~~ operations in x, y , then z . So one part must be.

$$\frac{\partial f}{\partial x} \underline{a_x} + \frac{\partial f}{\partial y} \underline{a_y} + \frac{\partial f}{\partial z} \underline{a_z} \quad (2)$$

which we will call grad f or ∇f

If we define the rest of (1) to be

$$d\mathbf{l} = dx \mathbf{a}_x + dy \mathbf{a}_y + dz \mathbf{a}_z \quad (3)$$

We can write (1) as:

$$df = \nabla f \cdot d\mathbf{l} \quad (4)$$

Note that:

- ① ∇f is a vector result of a scalar function
- ② $d\mathbf{l}$ is a differential unit vector
- ③ the resulting dot product is a scalar, as we expected.

- ④ The operation ∇ is often called the del operator where

$$\nabla = \mathbf{a}_x \frac{\partial}{\partial x} + \mathbf{a}_y \frac{\partial}{\partial y} + \mathbf{a}_z \frac{\partial}{\partial z}$$

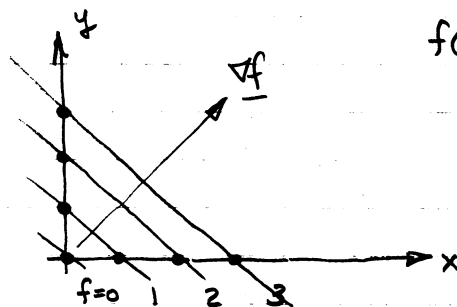
Returning to the original concept that the derivative is a function of direction, rewrite (4) as

$$df = |\nabla f| |d\mathbf{l}| \cos \theta$$

Note that ∇f then gives the MAXIMUM RATE OF CHANGE OF F.

Starting at P , if we follow the contour $df=0$ and hence ∇f must be perpendicular to the contour $d\mathbf{l}$ lies on.

Example:



$$f(x,y) = x+y = k \text{ (a constant)}$$

$$x+y=0$$

$$x+y=1$$

$$x+y=2$$

note that f is increasing along the 45° line between x and y most rapidly

what is the direction of ∇f

$$f(x,y,z) = x+y$$

$$\frac{\partial f}{\partial x} = 1$$

$$\frac{\partial f}{\partial y} = 1$$

$$\frac{\partial f}{\partial z} = 0$$

$$\Rightarrow \nabla f = \mathbf{a}_x + \mathbf{a}_y \text{ and } \nabla f \text{ perpendicular to the lines of constant } f \text{ as expected.}$$

The fact that $df = \nabla f \cdot d\mathbf{l}$ is a function of the contour, i.e. $d\mathbf{l}(x, y, z)$ leads to the idea of a contour integral, i.e.

$$f = \int_{P_1}^{P_2} df = \int_{P_1}^{P_2} \nabla f \cdot d\mathbf{l} \quad (5)$$

The most common example of this equation is Work where $\underline{W} = \underline{F} \cdot \underline{s}$ (force x distance). Unfortunately, the form of (5) corresponding to work is

$$W = \int_{P_1}^{P_2} \nabla f \cdot d\mathbf{l}$$

We must identify $\underline{F} = \nabla f$ and $\underline{s} = d\mathbf{l}$. The second is simple but what is the first. It turns out that for work f must be the energy but that is not important here. We can write

$$W = \int_{P_1}^{P_2} \underline{F} \cdot d\mathbf{l}$$

A very important result comes from (5) if we let $P_2 = P_1$. This is a special integral known as a contour integral and is denoted

$$\int_{P_1}^{P_1} \nabla f \cdot d\mathbf{l} = \oint_C \nabla f \cdot d\mathbf{l} \quad (6)$$

where the circle indicates a closed contour, i.e. no endpoints.

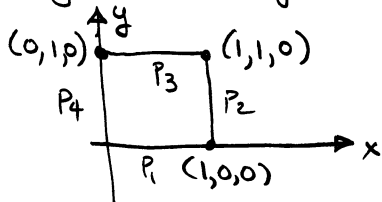
Recall, however, that $\int_{P_1}^{P_2} \nabla f \cdot d\mathbf{l} = \int_{P_1}^{P_2} df = f(P_2) - f(P_1)$.

As long as f is a single-valued function (usually) we have shown that

$$\oint_C \nabla f \cdot d\mathbf{l} = 0 \quad (7)$$

for any closed contour C .

Example: let $f(x, y, z) = 2xy + 3$ and evaluate the contour integral along the rectangular path shown below.



$$\underline{\nabla f} = \frac{\partial f}{\partial x} \underline{a}_x + \frac{\partial f}{\partial y} \underline{a}_y + \frac{\partial f}{\partial z} \underline{a}_z = 2y \underline{a}_x + 2x \underline{a}_y + 0 \cdot \underline{a}_z$$

$$\underline{\nabla f} \cdot \underline{dl} = 2y dx + 2x dy$$

path P_1 $\int_{(0,0,0)}^{(1,0,0)} \underline{\nabla f} \cdot \underline{dl} = \int_{x=0}^{x=1} 2y dx + \int_{y=0}^{y=0} 2x dy = 2y [1-0] = 2y \rightarrow 0$ as $y=0$ here.

path P_2 $\int_{(1,0,0)}^{(1,1,0)} \underline{\nabla f} \cdot \underline{dl} = \int_{x=1}^{x=1} 2y dx + \int_{y=0}^{y=1} 2x dy = 0 + 2x [1-0] \rightarrow 2$ as $x=1$ here.

path P_3 $\int_{(1,1,0)}^{(0,1,0)} \underline{\nabla f} \cdot \underline{dl} = \int_{x=1}^{x=0} 2y dx + \int_{y=1}^{y=1} 2x dy = 2y [0-1] + 0 = -2$ as $y=1$ here.

path P_4 $\int_{(0,1,0)}^{(0,0,0)} \underline{\nabla f} \cdot \underline{dl} = \int_{x=0}^{x=0} 2y dx + \int_{y=1}^{y=0} 2x dy = 0 + 2x [0-1] = 0$ as $x=0$ here.

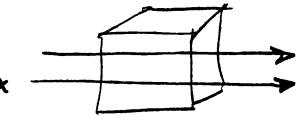
$$\oint \underline{\nabla f} \cdot \underline{dl} = \int_{P_1} + \int_{P_2} + \int_{P_3} + \int_{P_4} = 0 + 2 - 2 + 0 = 0.$$

DIVERGENCE

It is useful to think of the net flux entering or leaving a region of space. This is very useful to fields problems as the sources of flux are charges or currents and knowing fluxes allows us to locate field sources, or vice versa.

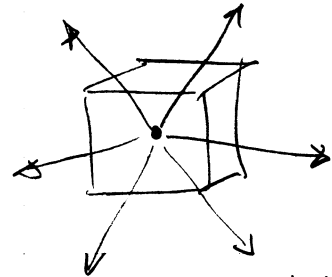
Example:

Electric field going through box



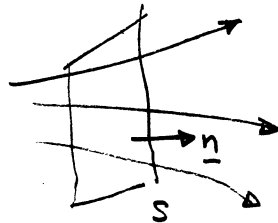
net in = net out
sum of flux = 0

source in box



net out \neq net in
source (or sink) in box.

How can I define the net flux through a surface S.



flux (vector field \underline{F})

Looking at S we see that the transverse components of \underline{F} on S do NOT contribute to the net flux only the normal components do. Transverse components are movements on S, not through \underline{S} .
scalar fields don't have flux

$$\therefore \psi = \int_S \underline{F} \cdot \underline{n} \, ds$$

differential element of surface area

To get to a box we use a closed surface and denote that integral by

$$\psi = \oint_S \underline{F} \cdot \underline{n} \, ds$$



(8)

Now we have not defined the direction of \underline{n} does it point in or out of the box. Convention is to pick \underline{n} pointing out so

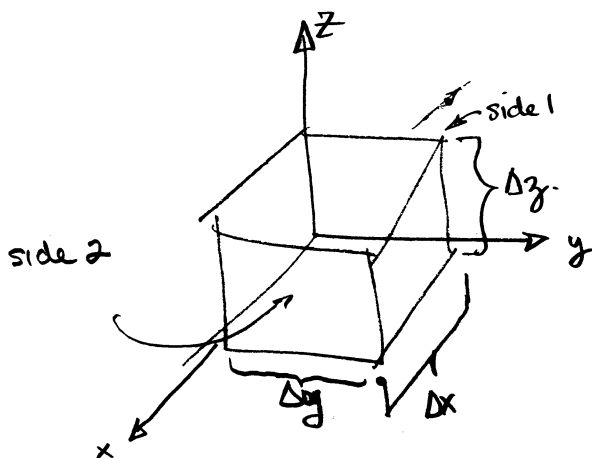
flux out > 0 and flux in < 0 .

start by →

Equation (8) is very common sense and tells us a lot about a large volume of space. On the other hand, can we localize just one source in a very tiny box. This is important in making a charge (a bunch of electrons) look mathematically like a bunch of electrons. This very tiny box operation has a special mathematical name, the DIVERGENCE, and is defined as

$$\text{div } \underline{F} = \lim_{\Delta V \rightarrow 0} \frac{\oint_S \underline{F} \cdot d\underline{s}}{\Delta V} \quad (9)$$

This is a nice definition but impractical to use. We can relate $\text{div } \underline{F}$ to the vector field \underline{F} in a easier to use manner by returning to our box, computing $\oint_S \underline{F} \cdot d\underline{s}$ and then taking the limit in (9).



\underline{F} is a vector so write it as $F_x \underline{a}_x + F_y \underline{a}_y + F_z \underline{a}_z$

We picked a special box where \underline{n} can only be \underline{a}_x , \underline{a}_y or \underline{a}_z depending upon the side.

suppose the center of our coordinate system is at (x, y, z) and that $\Delta x, \Delta y,$ and Δz are small. As $\Delta x, \Delta y, \Delta z \rightarrow 0$

F will eventually become constant over that side.

For side #1, the normal component is $F_x \underline{a_x}$
 the normal vector \underline{n} is $-\underline{a_x}$
 the differential surface ds is $\Delta y \Delta z$

so, the ~~flux~~ flux ψ_1 is through side 1 $F_x \underline{a_x} \cdot -\underline{a_x} \Delta y \Delta z = -F_x \Delta y \Delta z$

For side #2, the normal component is $(F_x + \frac{\partial F_x}{\partial x} \Delta x) \underline{a_x}$

the normal vector is $+\underline{a_x}$

the differential surface area is $\Delta y \Delta z$

the flux ψ_2 through side 2 is $(F_x + \frac{\partial F_x}{\partial x} \Delta x) \Delta y \Delta z.$

The net flux in the x direction is

$$\begin{aligned} \psi_1 + \psi_2 &= -F_x \Delta y \Delta z + F_x \Delta y \Delta z + \frac{\partial F_x}{\partial x} \Delta x \Delta y \Delta z \\ &= \frac{\partial F_x}{\partial x} \Delta x \Delta y \Delta z \end{aligned}$$

The same result can be done for the remaining sides

$$\psi_3 + \psi_4 = \frac{\partial F_y}{\partial y} \Delta x \Delta y \Delta z$$

$$\psi_5 + \psi_6 = \frac{\partial F_z}{\partial z} \Delta x \Delta y \Delta z.$$

so that we can re-write Eqn (9) as.

$$\text{div } \underline{F} = \lim_{\Delta V \rightarrow 0} \frac{\oint_S \underline{F} \cdot \underline{ds}}{\Delta V} = \lim_{\Delta V \rightarrow 0} \frac{\psi_1 + \psi_2 + \psi_3 + \psi_4 + \psi_5 + \psi_6}{\Delta V}.$$

$$\operatorname{div} \underline{F} = \lim_{\Delta V \rightarrow 0} \frac{\frac{\partial F_x}{\partial x} \Delta x \Delta y \Delta z + \frac{\partial F_y}{\partial y} \Delta x \Delta y \Delta z + \frac{\partial F_z}{\partial z} \Delta x \Delta y \Delta z}{\Delta V}$$

but $\Delta x \Delta y \Delta z = \Delta V$ so

$$\operatorname{div} \underline{F} = \lim_{\Delta V \rightarrow 0} \frac{\partial F_x}{\partial x} + \frac{\partial F_y}{\partial y} + \frac{\partial F_z}{\partial z} = \frac{\partial F_x}{\partial x} + \frac{\partial F_y}{\partial y} + \frac{\partial F_z}{\partial z}$$

This can be written as a vector operation by recalling our del operator ∇

$$\underline{\nabla} = \frac{\partial}{\partial x} \underline{a}_x + \frac{\partial}{\partial y} \underline{a}_y + \frac{\partial}{\partial z} \underline{a}_z$$

If $\underline{F} = F_x \underline{a}_x + F_y \underline{a}_y + F_z \underline{a}_z$ as we assumed, then

$$\underline{\nabla} \cdot \underline{F} = \frac{\partial F_x}{\partial x} + \frac{\partial F_y}{\partial y} + \frac{\partial F_z}{\partial z}$$

The general result is $\operatorname{div} \underline{F} = \underline{\nabla} \cdot \underline{F}$ and is a scalar representing net flux in a differential volume.

How about the net flux through a macroscopic volume, i.e. a volume V enclosed by a surface S . If $\operatorname{div} \underline{F}$ is the net flux from a differential volume we can guess that the total net flux must be given by

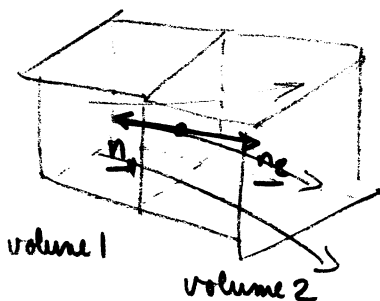
$$\int_V \underline{\nabla} \cdot \underline{F} \, dv$$

but the total net flux is $\oint_S \underline{F} \cdot d\underline{s}$

The result is the divergence theorem...

$$\oint_S \underline{F} \cdot d\underline{s} = \int_V \underline{\nabla} \cdot \underline{F} \, dv$$

Consider two ~~small~~ ^{differential} volumes



what happens in $\oint_{S_1} \underline{F} \cdot d\underline{S} + \oint_{S_2} \underline{F} \cdot d\underline{S}$

the contributions over the common surface cancel out
so that the sum equals

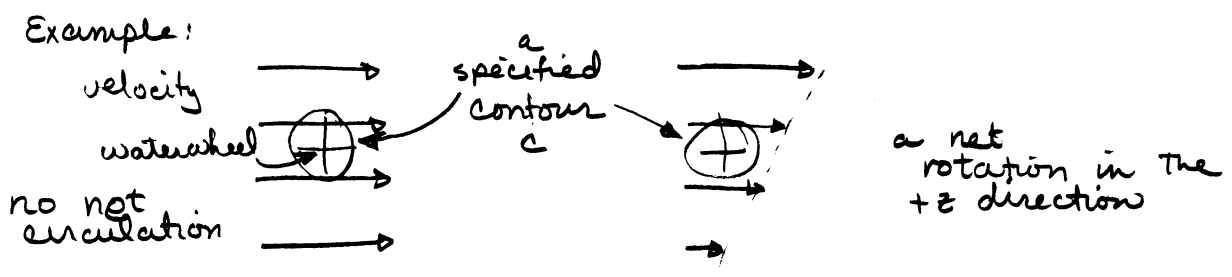
$$\oint_{S_1+S_2} \underline{F} \cdot d\underline{S} = \int_{V_1} \underline{\nabla} \cdot \underline{F} \, dV + \int_{V_2} \underline{\nabla} \cdot \underline{F} \, dV = \int_{V_1+V_2} \underline{\nabla} \cdot \underline{F} \, dV$$

so that we can generalize to arbitrary volumes simply summing

$$\oint_{\Sigma S_i} \underline{F} \cdot d\underline{S} = \int_{\Sigma V_i} \underline{\nabla} \cdot \underline{F} \, dV$$

$$\oint_S \underline{F} \cdot d\underline{S} = \int_V \underline{\nabla} \cdot \underline{F} \, dV$$

what is circulation? circulation indicates that a ~~vector field~~ ^{rotational force} is present to give a ^{net} non-zero result in the direction specified.



what is the net circulation of a vector field \underline{F} about some contour C ? It is the integral of F about the contour C .

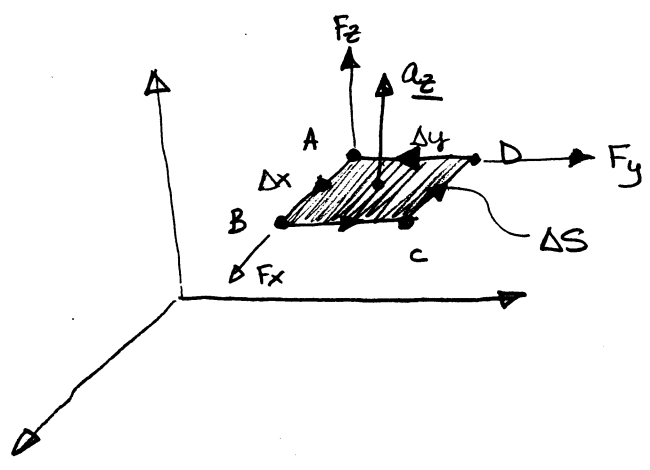
the curl $\underline{C} \triangleq \oint_C \underline{F} \cdot d\underline{l}$
only a force around C gives a contribution

How about the curl of \underline{F} at a microscopic point, Let

ΔS enclose a surface ΔS and let the contour and ΔS go to zero.

then $\text{curl } \underline{F} \cdot \underline{a}_n = \lim_{\Delta S \rightarrow 0} \frac{\oint_C \underline{F} \cdot d\underline{l}}{\Delta S}$

the direction of C and \underline{a}_n are related by the right-hand rule



we can evaluate this just as we did the divergence.

evaluate $\oint_C \underline{F} \cdot d\underline{r}$

what is F along AB, BC, CD, DA ?

$$F_x \underline{a}_x \cdot (-\underline{a}_x)$$

$$\oint_C \underline{F} \cdot d\underline{r} = F_x \Big|_{AB} \Delta x + F_y \Big|_{BC} \Delta y + (-F_x) \Big|_{CD} \Delta x + (-F_y) \Big|_{DA} \Delta y$$

$$= \cancel{F_x} \Delta x + \left[F_y + \frac{\partial F_y}{\partial x} \Delta x \right] \Delta y - \left[\cancel{F_x} + \frac{\partial F_x}{\partial y} \Delta y \right] \Delta x - F_y \Delta y$$

$$= \frac{\partial F_y}{\partial x} \Delta x \Delta y - \frac{\partial F_x}{\partial y} \Delta x \Delta y$$

$$\lim_{\Delta S \rightarrow 0} \frac{\oint_C \underline{F} \cdot d\underline{r}}{\Delta S} = \lim_{\Delta S \rightarrow 0} \frac{\left(\frac{\partial F_y}{\partial x} - \frac{\partial F_x}{\partial y} \right) \Delta x \Delta y}{\Delta x \Delta y} = \frac{\partial F_y}{\partial x} - \frac{\partial F_x}{\partial y}$$

this is the z component of $\text{curl } \underline{F}$ as given by right-hand rule

the x and y components are.

$$(\text{curl } \underline{F})_x = \frac{\partial F_z}{\partial y} - \frac{\partial F_y}{\partial z}$$

$$(\text{curl } \underline{F})_y = \frac{\partial F_x}{\partial z} - \frac{\partial F_z}{\partial x}$$

in three-dimensions
$$\text{curl } \underline{F} = \underline{a}_x \left(\frac{\partial F_z}{\partial y} - \frac{\partial F_y}{\partial z} \right) + \underline{a}_y \left(\frac{\partial F_x}{\partial z} - \frac{\partial F_z}{\partial x} \right) + \underline{a}_z \left(\frac{\partial F_y}{\partial x} - \frac{\partial F_x}{\partial y} \right)$$

inspecting this result

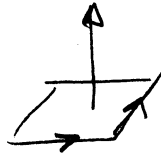
$$\text{curl } \underline{F} = \nabla \times \underline{F} \quad \text{where} \quad \nabla = \underline{a}_x \frac{\partial}{\partial x} + \underline{a}_y \frac{\partial}{\partial y} + \underline{a}_z \frac{\partial}{\partial z}$$

to show this write

$$\nabla \times \underline{F} = \begin{bmatrix} \underline{a}_x & \underline{a}_y & \underline{a}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ F_x & F_y & F_z \end{bmatrix}$$

Stokes' Theorem

Stokes' Theorem is simply the evaluation of $\text{curl } \underline{F}$ over an open surface

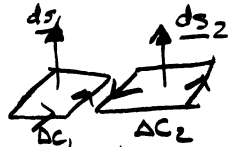


with contour ΔC

For an infinitesimal surface element \underline{dS} we have

$$(\nabla \times \underline{F}) \cdot \underline{dS} = \oint_{\Delta C} \underline{F} \cdot \underline{dl}$$

Suppose we generate a second \underline{dS}



note that the contours add $\Delta C_1 + \Delta C_2$ in a scalar manner
the curls (in directions \underline{dS}_1 and \underline{dS}_2) add in a vector manner, i.e. a vector sum.

so

$$\int_{\Delta S_1} (\nabla \times \underline{F}) \cdot \underline{dS}_1 + \int_{\Delta S_2} (\nabla \times \underline{F}) \cdot \underline{dS}_2 = \oint_{\Delta C_1} \underline{F} \cdot \underline{dl} + \oint_{\Delta C_2} \underline{F} \cdot \underline{dl}$$

as the ^{numbers} ΔS and ΔC becomes large,

$$\int_S (\nabla \times \underline{F}) \cdot \underline{dS} = \oint_C \underline{F} \cdot \underline{dl}$$

Lecture 3

① Electromagnetism is study of interactions among charges and currents. Original concept - action at a distance \Rightarrow Coulomb's Law

$$\underline{F} = k \frac{Q_1}{r_{12}^2} Q_2 \underline{a}_{r_{12}}$$

= force on Q_2 by Q_1 (directed along radius)

history

- Faraday suggested considering charge q_1 to be surrounded by "lines of force". Lines of force, or force field, indicate everywhere the direction and magnitude of force on unit positive charge if that charge were present.

field in absence of charge

- In Faraday concept, charge produces force field and field acts on other charges. This way effects can be discussed even if second charge is not present.

definition

- define the electric field intensity $\underline{E}(x, y, z)$

$$\underline{E}(x, y, z) = \frac{\underline{F}}{Q}$$

Q = magnitude of test charge.

\underline{E} = force / unit test charge. (assumed positive)

$$\underline{E} = k \frac{Q_1}{r^2} \underline{a}_r \quad \text{for single source charge } q_1$$

- in MKS units $k = \frac{1}{4\pi\epsilon_0}$

②. Lorentz force law

- charge in motion can be acted on by two types of electromagnetic forces.

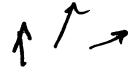
$$\underline{F} = q\underline{E} + q(\underline{v} \times \underline{B})$$

$\underbrace{\quad}_{\text{Coulomb force in terms of } \underline{E} \text{ field}}$
 $\underbrace{\quad}_{\text{velocity dependent force.}}$

- second term defines magnetic flux density \underline{B} in terms of force on moving charge.

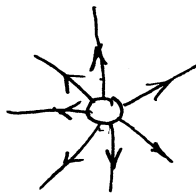
③ Any vector field can be represented graphically in one of two ways

a) array of vectors of appropriate lengths & directions



b) flux plot -- system of lines, called flux lines, drawn by two rules.

- 1) direction of flux lines correspond with direction of field vectors
- 2) transverse densities are same as magnitude of field vector.



flux lines for point charge.

Net flux through closed surface is

$$\Psi = \oint_{\partial V} \underline{E} \cdot d\underline{s}$$

④ Gauss' Law & The electric flux density vector displacement, or electric flux density

$$\oint_S \underline{D} \cdot d\underline{s} = Q_{\text{total}} \text{ enclosed by } S$$

closed surface.

proof: $\underline{E} \cdot d\underline{s} = \frac{Q}{4\pi\epsilon_0} \underline{a}_r \cdot d\underline{s}$

$d\underline{s} \underline{a}_n$
normal to surface

from solid geometry $d\Omega = \frac{ds \cos\theta}{R^2}$
↑
differential solid angle.

$$\oint_S \underline{E} \cdot d\underline{s} = \oint_S \frac{Q}{4\pi\epsilon_0 R^2} \underbrace{d\Omega}_{ds} \underbrace{\frac{R^2}{\cos\theta}}_{\text{dot product}} \cos\theta$$

$$= \oint_S \frac{Q}{4\pi\epsilon_0} d\Omega \Rightarrow \oint \frac{Q}{4\pi\epsilon_0} \cdot 4\pi$$

but, in solid geometry, $\oint_S d\Omega = 4\pi$

$\therefore \oint \underline{E} \cdot d\underline{s} = \frac{Q}{\epsilon_0}$

and re-writing $\oint_S \epsilon_0 \underline{E} \cdot d\underline{s} = Q$
↑
dimensions = $\frac{\text{coulombs}}{\text{m}^2}$

Furthermore, recall if $\Psi = \int_S \underline{F} \cdot d\underline{s} > 0$ source

$\Psi = \int_S \underline{F} \cdot d\underline{s} < 0$ sink

where Ψ was a flux so \underline{F} must be flux density

Electrostatic potential

electrostatic potential

How much work is done moving a charge in a static electric field?

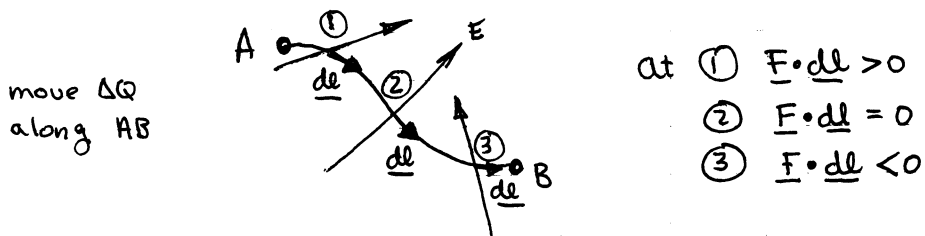
— force on a test charge ΔQ is given by Lorentz force law

$$\underline{F} = \frac{Q(\Delta Q)}{4\pi\epsilon_0 R^2} \underline{a}_R \quad (1)$$

— what is the incremental work dW done in moving ΔQ a distance $d\underline{l}$

$$dW = - \underline{F} \cdot d\underline{l} \quad (2)$$

Why a minus sign? The sign is negative so that if a positive test charge is moved against the field, the work done will be positive.



At ① the field is moving the charge, so the field is losing energy. At ② no work is being done. At ③ the charge is being moved against the field so real work is being done. Thus, we want case ③ to end up being a positive quantity of work.

Combining (1) and (2),

$$dW = - \frac{Q (\Delta Q)}{4\pi\epsilon_0 R^2} \underline{a_R} \cdot \underline{dl}$$

Note: This is work done in field of point charge.

- incremental work per charge moved is then

$$\frac{dW}{\Delta Q} = - \frac{Q}{4\pi\epsilon_0 R^2} \underline{a_R} \cdot \underline{dl}$$

But the first quantity on the right is \underline{E} , so.

$$\frac{dW}{\Delta Q} = - \underline{E} \cdot \underline{dl}$$

- define the voltage V [or electrostatic potential Φ] to be the incremental work / charge moved.

$$dV = \frac{dW}{\Delta Q} = - \underline{E} \cdot \underline{dl} \quad (3)$$

- The work done in moving ΔQ from P_1 to P_2 is given by integrating (3).

$$\int_{P_1}^{P_2} dV = \int_{P_1}^{P_2} - \underline{E} \cdot \underline{dl}$$

$$V(P_2) - V(P_1) = - \int_{P_1}^{P_2} \underline{E} \cdot \underline{dl} \quad (4)$$

- In passing, note that if $P_2 \rightarrow P_1$ and $V(P)$ is single valued (a requirement of a real field), then

$$- \int_{P_1}^{P_1} \underline{E} \cdot \underline{dl} = - \oint \underline{E} \cdot \underline{dl} = V(P_1) - V(P_1) = 0$$

This is the CONSERVATIVE PROPERTY OF AN ELECTRIC FIELD

$$\oint \underline{E} \cdot \underline{dl} = 0$$

(5)

Applying Stoke's Theorem to ~~the~~ (5)

$$\oint_C \underline{E} \cdot d\underline{l} = \int_S (\underline{\nabla} \times \underline{E}) \cdot d\underline{s}$$

But, as $\oint \underline{E} \cdot d\underline{l} = 0$, this implies that

$$\underline{\nabla} \times \underline{E} = 0 \quad (6)$$

This is actually one of Maxwell's equations.

— Returning to (3), let us rewrite dV .

$$dV = \frac{\partial V}{\partial x} dx + \frac{\partial V}{\partial y} dy + \frac{\partial V}{\partial z} dz \quad (7)$$

From (3), we can also write

$$\begin{aligned} dV &= -\underline{E} \cdot d\underline{l} \\ &= - (E_x \underline{a}_x + E_y \underline{a}_y + E_z \underline{a}_z) \cdot (dx \underline{a}_x + dy \underline{a}_y + dz \underline{a}_z) \\ &= - (E_x dx + E_y dy + E_z dz) \end{aligned} \quad (8)$$

Equating (7) and (8) we can make the identifications

$$\frac{\partial V}{\partial x} = -E_x \quad \frac{\partial V}{\partial y} = -E_y \quad \frac{\partial V}{\partial z} = -E_z$$

In vector form, this can be written

$$\begin{aligned} \underline{E} &= -\underline{\nabla} V \\ &= -\underline{\nabla} \Phi \end{aligned} \quad (9)$$

— Is Φ dependent upon the path?

No, because of the conservative property.

- Φ is only relative.

From the conservative property we can only calculate a potential difference, so we must define some point as zero potential. We often pick $r = \infty$ as the reference point and let $\Phi = 0$ there.

- Is Φ unique?

Consider. Let $\Phi' = \Phi + \text{constant}$

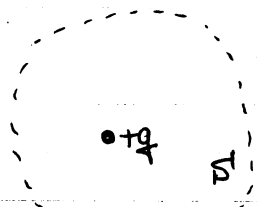
$$\underline{E} = -\nabla\Phi' = -\nabla(\Phi + \text{constant}) = -\nabla\Phi$$

Thus, both Φ and Φ' give the same \underline{E} . Φ is NOT unique; it is only defined to an additive constant

- methodology to solving electrostatic field problems.

- I. Use Gauss' Law to find \underline{E}
- II. Choose an appropriate coordinate system
- III. pick an appropriate surface.
- IV. Integrate to get \underline{E}

Example: Find \underline{E} , Φ of point charge.



I. Gauss' law $\oint \underline{E} \cdot \underline{dS} = \frac{Q_{\text{total}}}{\epsilon_0} = \frac{q}{\epsilon_0}$

II. choose a spherical coordinate system because of spherical symmetry, i.e.

$$\underline{E} = E_r \underline{a}_r + E_\theta \underline{a}_\theta + E_\phi \underline{a}_\phi$$

$$\underline{dS} = r^2 \sin \theta \, d\theta \, d\phi \, \underline{a}_r$$

$$\underline{E} \cdot \underline{dS} = E_r r^2 \sin \theta \, d\theta \, d\phi$$

III. Pick appropriate surface.

Actually we picked the surface already by selecting \underline{dS} .

IV. Integrate.

$$\oint \underline{E} \cdot \underline{dS} = \int_0^\pi \int_0^{2\pi} E_r r^2 \sin \theta \, d\theta \, d\phi$$

$\int_0^{2\pi}$ ϕ integration
 \int_0^π θ integration

$$= E_r r^2 2\pi \int_0^\pi \sin \theta \, d\theta = E_r r^2 2\pi \left(-\cos \theta \Big|_0^\pi \right)$$

$$= 2\pi r^2 E_r \left(-\cancel{\cos \pi}^1 + \cancel{\cos 0}^1 \right)$$

$$= 4\pi r^2 E_r$$

$$\therefore 4\pi r^2 E_r = \frac{q}{\epsilon_0} \quad ; \quad E_r = \frac{q}{4\pi r^2 \epsilon_0}$$

$$\underline{E} = \frac{q}{4\pi \epsilon_0 r^2} \underline{a}_r \quad \text{which is consistent with our earlier results and definitions.}$$

Now that we have \underline{E} , how about Φ ?

$$\underline{E} = -\nabla\Phi = -\frac{\partial\Phi}{\partial r} \underline{a}_r + \frac{1}{r} \frac{\partial\Phi}{\partial\theta} \underline{a}_\theta - \frac{1}{r\sin\theta} \frac{\partial\Phi}{\partial\phi} \underline{a}_\phi$$

only the first derivative for \underline{a}_r can be non-zero.

Equating terms in \underline{a}_r

$$\frac{q}{4\pi\epsilon_0 r^2} = -\frac{\partial\Phi}{\partial r} = -\frac{d\Phi}{dr} \quad \text{since no other dependence.}$$

Integrating

$$\int_{P_a}^{P_b} \frac{q}{4\pi\epsilon_0} \frac{dr}{r^2} = - \int_{P_a}^{P_b} d\Phi$$

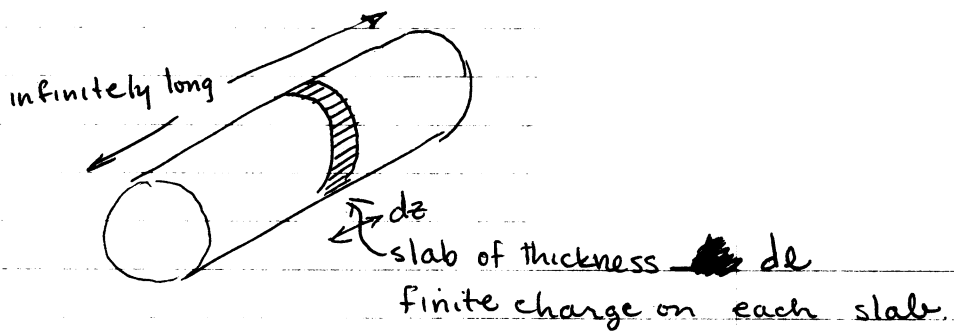
$$\frac{q}{4\pi\epsilon_0} \left. \frac{r^{-1}}{-1} \right|_{r=a}^{r=b} = -\Phi(r=b) + \Phi(r=a)$$

$$\therefore \Phi(r=a) = \frac{q}{4\pi\epsilon_0} \left(\frac{1}{a} - \frac{1}{b} \right) + \Phi(r=b)$$

Note the additive constant here. So, define $\Phi(r=\infty)=0$
and pick $b=\infty$

$$\text{Then } \Phi(r=a) = \frac{q}{4\pi\epsilon_0 a} \quad \square$$

Example: cylinder, charged on surface.



- ① since the cylinder is infinitely long its total charge is infinite; however, the charge on a short length of cylinder is finite
- ② as the cylinder is uniform, let the charge in any length of the cylinder be uniformly distributed. Let this charge density be ρ_s coulombs/m²

[what is a coulomb? unit of charge
 $e = 1.6 \times 10^{-19}$ C on an electron
 6.25×10^{18} electrons/coul.]

- ③ the total charge on any slab will be $\Lambda = \rho_s 2\pi r_c \Delta l$
 where $r_c =$ the radius, $2\pi r_c$ the circumference, and Δl the thickness

I. To find \underline{E} use Gauss' Law (given ρ , find \underline{E})

II. Choose the appropriate geometry because of symmetry.
 [pick a cylindrical volume, this means the source of charge and the surface integral can be described by a common set of coordinates making the integral easier.]

III. Write Gauss' Law in the cylindrical coordinate system and calculate Q_{total} , \underline{E}

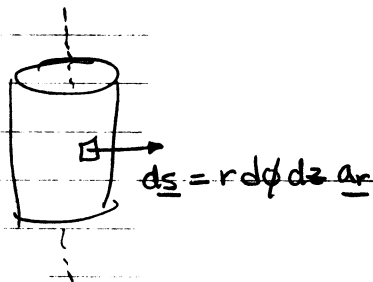
cylinder (cont.)

$$1. \oint_S \underline{E} \cdot d\underline{s} = \frac{Q_{\text{total}}}{\epsilon_0}$$

2. Pick cylindrical coordinates

$$d\underline{s} = r d\phi dz \underline{a}_r$$

$$\underline{E} = E_r \underline{a}_r + E_\phi \underline{a}_\phi + E_z \underline{a}_z$$



3. What is Q_{total} ?

Pick a length of the cylinder dz .

$$Q_t = \rho_s \cdot 2\pi r_c \cdot dz$$

How about the surface integral.

$$\begin{aligned} \oint_S \underline{E} \cdot d\underline{s} &= \iint (E_r \underline{a}_r + E_\phi \underline{a}_\phi + E_z \underline{a}_z) \cdot r d\phi dz \underline{a}_r \\ &= \int_0^{\Delta z} \int_0^{2\pi} E_r r d\phi dz \end{aligned}$$

\downarrow
 $0-2\pi$
 $0-\Delta z$

THINK: If the problem is radially symmetric it makes sense that all E_r 's are the same so assume $E_r = \text{constant}$.

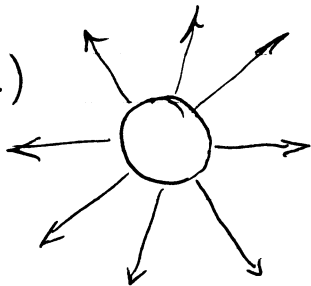
$$\oint_S \underline{E} \cdot d\underline{s} = E_r r \int_0^{\Delta z} \int_0^{2\pi} d\phi dz = 2\pi \Delta z r E_r$$

This must equal the total enclosed charge divided by ϵ_0

$$E_r r 2\pi \Delta z = \frac{\rho_s 2\pi r_c \Delta z}{\epsilon_0}$$

$$\therefore \underline{E} = \frac{\rho_s}{\epsilon_0} \left(\frac{r_c}{r} \right) \underline{a}_r$$

cylinder (cont.)

flux density goes down as $\frac{1}{2\pi r}$

How about Φ ?
$$\underline{E} = -\nabla\Phi = -a_r \frac{\partial\Phi}{\partial r} - a_\phi \frac{\partial\Phi}{\partial\phi} - a_z \frac{\partial\Phi}{\partial z}$$

$$\frac{\rho_s}{\epsilon_0} \left(\frac{r_c}{r}\right) a_r = -a_r \frac{\partial\Phi}{\partial r} = -\frac{d\Phi}{dr} a_r$$

$$\int_a^b \frac{\rho_s}{\epsilon_0} r_c \frac{dr}{r} = -\int_a^b d\Phi$$

what limits, $a \neq b$? Obviously $a > r_c$

$$\frac{\rho_s}{\epsilon_0} r_c \ln b - \ln a = -\Phi(b) + \Phi(a)$$

$$\Phi(a) = \Phi(b) + \frac{\rho_s}{\epsilon_0} r_c \ln\left(\frac{b}{a}\right)$$

Example: a charged sphere
(same as last problem except for geometry)

given: surface charge density ρ_s
total surface charge is $(4\pi r_s^2) \rho_s$.

I.
$$\oint_s \underline{E} \cdot d\underline{s} = \frac{Q_{\text{total}}}{\epsilon_0}$$

II. use spherical coordinates

$$d\underline{s} = r^2 \sin\theta d\theta d\phi \underline{a}_r \quad (\text{Figure 2.10})$$

$$\underline{E} = E_r \underline{a}_r + E_\theta \underline{a}_\theta + E_\phi \underline{a}_\phi$$

III. use a sphere of radius r

$$\oint \underline{E} \cdot d\underline{s} = \iint (E_r \underline{a}_r + E_\theta \underline{a}_\theta + E_\phi \underline{a}_\phi) \cdot r^2 \sin\theta d\theta d\phi \underline{a}_r$$

$$= \iint E_r r^2 \sin\theta d\theta d\phi$$

$$= E_r \cdot \underbrace{\int_0^\pi \int_0^{2\pi} r^2 \sin\theta d\theta d\phi}_{\text{surface of sphere}}$$

$$= E_r r^2 2\pi \int_{-\pi}^{\pi} \sin\theta d\theta = 2\pi E_r r^2 \left[-\cos\theta \Big|_0^\pi \right]$$

$$= 2\pi E_r r^2 \left[-\cos(\pi) + \cos(0) \right] = 2\pi E_r r^2 [1 + 1]$$

$$= 4\pi r^2 E_r$$

$$4\pi r^2 E_r = \frac{4\pi r_s^2 \rho_s}{\epsilon_0}$$

$$\boxed{\underline{E} = \frac{\rho_s}{\epsilon_0} \left(\frac{r_s}{r}\right)^2 \underline{a}_r}$$

as before $\underline{E} = -\nabla\phi = -\underline{a}_r \frac{d\phi}{dr}$ since only E_r component.

$$\frac{\rho_s r_s}{\epsilon_0} r^{-2} = -\frac{d\phi}{dr}$$

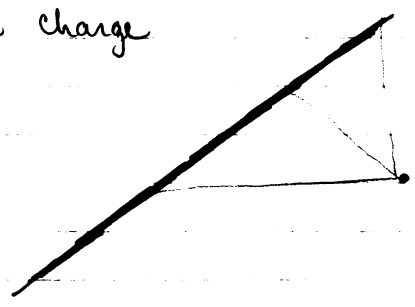
$$\leftarrow \frac{\rho_s r_s}{\epsilon_0} \frac{r^{-1}}{-1} \Big|_{r_a}^{r_b} = -\phi(b) + \phi(a)$$

$$\frac{\rho_s r_s}{\epsilon_0} \left(\frac{-1}{r_b} + \frac{1}{r_a} \right) = -\phi(b) + \phi(a)$$

pick $r_b = \infty$ then $\frac{\rho_s r_s}{\epsilon_0} \frac{1}{r_a} + \Phi(\infty) = \Phi(r_a)$
 \Downarrow
 \emptyset

6

line charge



do in cylindrical coordinates

result for charged cylinder $\underline{E} = \frac{\rho_s}{\epsilon_0} \left(\frac{r_c}{r}\right) \underline{a}_r$

as $r_c \rightarrow 0$ $\underline{E} \rightarrow 0$ because we used a surface charge density

use a linear charge density ρ_l

I. $\oint \underline{E} \cdot d\underline{s} = \frac{Q_{total}}{\epsilon_0}$

II. use cylindrical coordinates

III. $\oint (E_r \underline{a}_r + E_\phi \underline{a}_\phi + E_z \underline{a}_z) \cdot r d\phi dz \underline{a}_r$
 $= \int_0^{\Delta l} \int_0^{2\pi} E_r r d\phi dz = E_r r 2\pi \Delta l$

total charge: $Q_{total} = \rho_l \Delta l$

$E_r r 2\pi \Delta l = \frac{\rho_l \Delta l}{\epsilon_0}$

$\underline{E} = \frac{\rho_l}{2\pi\epsilon_0} \frac{1}{r}$

as before $\underline{E} = -\nabla\Phi = -\frac{d\Phi}{dr} \underline{a}_r$

$\frac{\rho_l}{2\pi\epsilon_0} \frac{1}{r} = -\frac{d\Phi}{dr}$

$\frac{\rho_l}{2\pi\epsilon_0} \int_{r_a}^{r_b} \frac{dr}{r} = -\int_{r_a}^{r_b} d\Phi$

$\frac{\rho_l}{2\pi\epsilon_0} \ln(r_b) - \ln(r_a) = -\Phi(r_b) + \Phi(r_a)$

$\Phi(r_a) = \frac{\rho_l}{2\pi\epsilon_0} \ln\left(\frac{r_b}{r_a}\right) + \Phi(r_b)$

(7)

in many problems it is impossible to pick a simple $\Phi(b)$ as shown in the cases of the cylinder and line. This is due to the charge being of infinite extent.

Boundary condition for potential



potential difference between A and B is

$$\begin{aligned}\Phi(B) - \Phi(A) &= - \int_A^B \underline{E} \cdot d\underline{\ell} \\ &= - (E_{2n} \delta - E_{1n} \delta)\end{aligned}$$

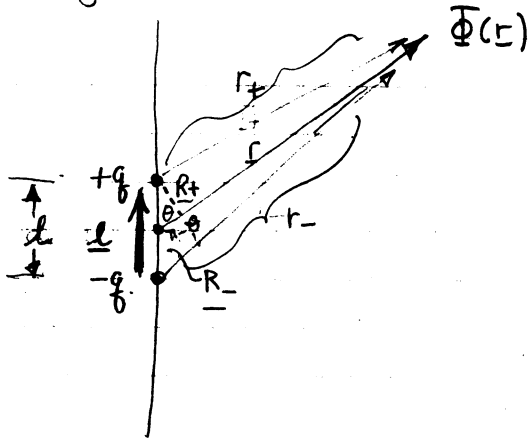
now, let $\delta \rightarrow 0$

$$\Phi(B) - \Phi(A) = \lim_{\delta \rightarrow 0} - [E_{2n} - E_{1n}] \delta$$

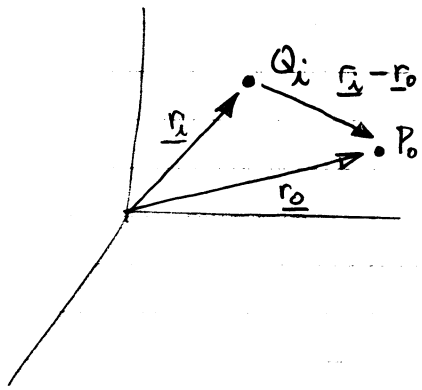
neglect components \parallel
to boundary as
 $\underline{E}_{\parallel} \cdot \underline{\delta} = 0$.

Φ, E for electric dipole

This is a very important and special example.



we can find this problem by considering the electric potential for a charge distribution of discrete charges Q_i



Φ_i is associated with each Q_i
 each $\Phi_i(r_o) = \frac{Q_i}{4\pi\epsilon_0 |r_i - r_o|}$
 at r_o
 since Φ_i is a scalar, and not influenced by other charges, the Φ_i 's must add.

$$\Phi(P_o) = \sum_{i=1}^N \frac{Q_i}{4\pi\epsilon_0 |r_i - r_o|} \rightarrow \int_V \frac{\rho(r') dV'}{4\pi\epsilon_0 |r' - r_o|}$$

for $\rho(r')$
a volume charge density

this gives us a powerful technique for solving problems such as the electric dipole in terms of previously solved solutions.

9

consider $\Phi(r) = \frac{+q}{4\pi\epsilon_0 |R_+ - r|} + \frac{-q}{4\pi\epsilon_0 |R_- - r|}$

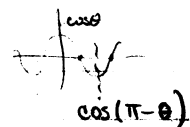
this assumes $\Phi(\infty) = 0$.

$$\Phi(r) = \frac{q}{4\pi\epsilon_0} \left(\frac{1}{r_+} - \frac{1}{r_-} \right)$$

make this simpler: by the law of cosines,

$$|r_+|^2 = |r|^2 + |R_+|^2 + 2|r||R_+|\cos\theta$$

$$|r_-|^2 = |r|^2 + |R_-|^2 + 2|r||R_-|\cos(\pi - \theta)$$



\downarrow
 $-\cos\theta$

$$r_+^2 = r^2 + \frac{l^2}{4} + 2r\frac{l}{2}\cos\theta$$

$$r_-^2 = r^2 + \frac{l^2}{4} - 2r\frac{l}{2}\cos\theta$$

$$r_+ = \left(r^2 + \frac{l^2}{4} + r l \cos\theta \right)^{\frac{1}{2}}$$

$$r_- = \left(r^2 + \frac{l^2}{4} - r l \cos\theta \right)^{\frac{1}{2}}$$

$$r_+ = r \left(1 + \frac{l^2}{4r^2} + \frac{l}{r} \cos\theta \right)^{\frac{1}{2}}$$

$$r_- = r \left(1 + \frac{l^2}{4r^2} - \frac{l}{r} \cos\theta \right)^{\frac{1}{2}}$$

expand this:

$$(1+x)^n \approx 1+nx$$

$$r_+ \approx r \left(1 - \frac{l^2}{8r^2} + \frac{l}{2r} \cos\theta \right)$$

$$r_- \approx r \left(1 - \frac{l^2}{8r^2} - \frac{l}{2r} \cos\theta \right)$$

it is reasonable that

$\frac{l}{r} \ll 1$ so neglect second order terms.

$$r_+ \approx r \left(1 + \frac{l}{2r} \cos\theta \right)$$

$$r_- \approx r \left(1 - \frac{l}{2r} \cos\theta \right)$$

$$\approx r + \frac{l}{2} \cos\theta$$

$$\approx r - \frac{l}{2} \cos\theta$$

substituting

$$\Phi(r) = \frac{q}{4\pi\epsilon_0} \left(\frac{1}{r_+} - \frac{1}{r_-} \right) \approx \frac{q}{4\pi\epsilon_0} \left(\frac{1}{r - \frac{l}{2} \cos\theta} - \frac{1}{r + \frac{l}{2} \cos\theta} \right)$$

$$\Phi(r) \approx \frac{q}{4\pi\epsilon_0} \frac{\left(-r + \frac{l}{2} \cos\theta - \left(r + \frac{l}{2} \cos\theta \right) \right)}{\left(r - \frac{l}{2} \cos\theta \right) \left(r + \frac{l}{2} \cos\theta \right)} \quad \text{since } \frac{l}{2} \ll r$$

$$\approx \frac{q l \cos\theta}{4\pi\epsilon_0 r^2}$$

this is the electric potential due to the electric dipole

define the electric dipole moment $\underline{p} = +q\underline{l} = +q l \underline{a}_z$

(vector points to + charge)

$$\text{if } \Phi(r) = \frac{1}{4\pi\epsilon_0} \frac{\underline{a}_r \cdot \underline{p}}{r^2} \quad \text{for } |r| \gg l$$

$$\underline{E} = -\nabla\Phi$$

use spherical coordinates

$$\nabla\Phi = \underline{a}_r \frac{\partial\Phi}{\partial r} + \underline{a}_\theta \frac{1}{r} \frac{\partial\Phi}{\partial\theta} + \underline{a}_\phi \frac{1}{r \sin\theta} \frac{\partial\Phi}{\partial\phi}$$

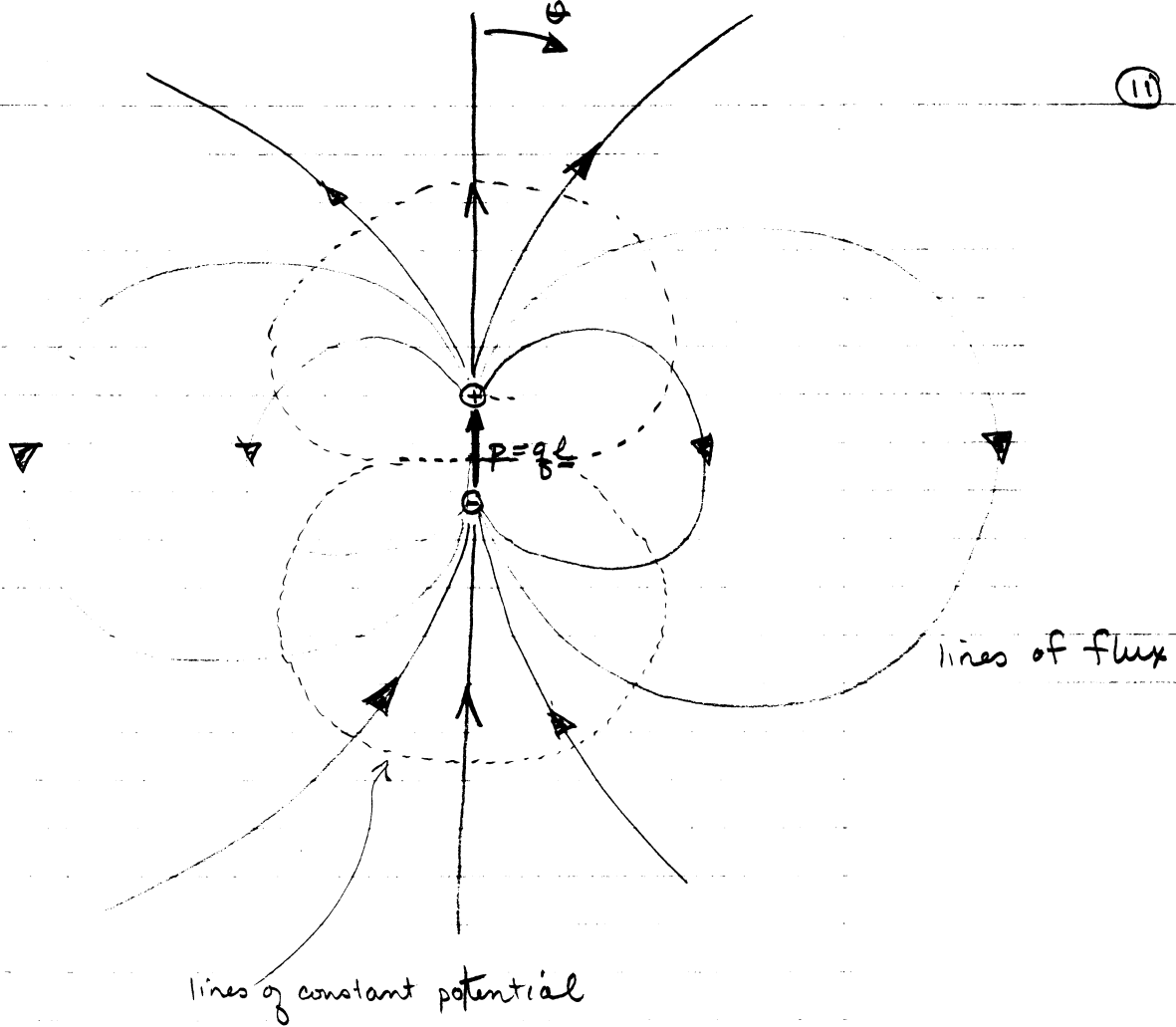
but a
 θ dependence

$$\frac{\partial\Phi}{\partial r} = - \frac{p \cos\theta}{4\pi\epsilon_0} \frac{2}{r^3}$$

$$\frac{1}{r} \frac{\partial\Phi}{\partial\theta} = - \frac{p \sin\theta}{4\pi\epsilon_0} \frac{1}{r^3}$$

$$\therefore \underline{E}(r) = \underline{E}(r, \theta, \phi) = + \frac{p \cos\theta}{4\pi\epsilon_0} \frac{2}{r^3} \underline{a}_r + \frac{p \sin\theta}{4\pi\epsilon_0} \frac{1}{r^3} \underline{a}_\theta$$

$$= \frac{p}{4\pi\epsilon_0} \frac{1}{r^3} \left(2 \cos\theta \underline{a}_r + \sin\theta \underline{a}_\theta \right)$$



topics in ~~the~~ electrostatics

① { electric field intensity
Lorentz force law
flux plots
Gauss' law

{ electrostatic potential
conservative property - ~~discrete charges~~
work in electrostatic fields
Example - E & Φ for point charge
Example - ∞ long cylinder
Example - charged sphere
Example - line charge
Example - electric dipole

{ conductors
Ohm's law
Example - fields in a wire

{ dielectrics
polarizability
electric flux density vector

{ boundary conditions
charge relaxation

conductors (revisited) - boundary conditions
~~the~~ energy density & electric field.

{ Laplace & Poisson's Eqns.
parallel plate ~~capacitor~~ capacitor
capacitance

Mike Nacci