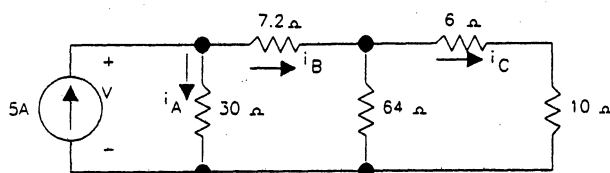


Simple Resistive Circuits

Drill Exercises

DE 3.1



$$16//64 = 12.8\Omega, \quad 12.8 + 7.2 = 20\Omega, \quad 20//30 = 12\Omega$$

[a] $v = 5(12) = 60\text{ V}$

[b] $p_{5A(\text{del})} = (5)(60) = 300\text{ W}$

[c] $i_A = 60/30 = 2\text{ A}$ $i_C = 3(64)/(80) = 2.4\text{ A}$
 $i_B = 5 - 2 = 3\text{ A}$ $p_{10\Omega} = (2.4)^2 10 = 57.6\text{ W}$

DE 3.2 [a] $v_o(\text{no load}) = 120(50)/80 = 75\text{ V}$

[b] $50//450 = 45\text{ k}\Omega$, therefore $v_o = 120(45)/75 = 72\text{ V}$

[c] $i = 120/30 = 4\text{ mA}$, $p_{30k} = (4 \times 10^{-3})^2 (30,000) = 0.48\text{ W}$

[d] Maximum dissipation at no load since v_o is maximum,

$$p = \frac{v_o^2}{50,000} = 0.1125\text{ W}$$

DE 3.3 [a] $i = 0.5/80 = 6.25\text{ mA}$

[b] $i_{\text{meas}} = 0.5/85 = 5.88\text{ mA}$

DE 3.4 [a] $v = 40(75)/80 = 37.5 \text{ V}$

[b] $R_m = 150/10^{-3} = 150 \text{ k}\Omega$, $150 \text{ k}\Omega // 75 \text{ k}\Omega = 50 \text{ k}\Omega$
 Therefore $v_{\text{meas}} = 50(40)/55 = 36.36 \text{ V}$

DE 3.5 [a] $1.5 = 50 \times 10^{-6}(23,000 + R)$, $R = 7 \text{ k}\Omega$

[b] At midscale: $v_{R_x} = 1.5 - 25 \times 10^{-6}(30,000) = 0.75 \text{ V}$
 Therefore $i_{11\Omega} = 0.75/11 = 68,181.818 \mu\text{A}$,
 Therefore $i_{R_x} = 68,206.818 \mu\text{A}$, $R_x = 0.75/i_{R_x} \cong 11 \Omega$

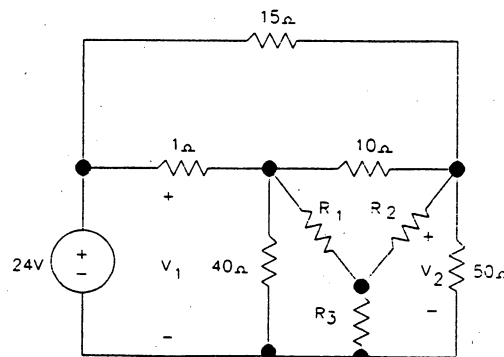
DE 3.6 [a] $100R_x = (1000)(150)$, $R_x = 1.5 \text{ k}\Omega$

[b] The current supplied by the 5-V source is $i_s = \frac{5}{250} + \frac{5}{2500} = 0.022 \text{ A} = 22 \text{ mA}$

Therefore $p_{5\text{V}}(\text{delivered}) = 5(22) = 110 \text{ mW}$

Since total power delivered to bridge is less than 250 mW, bridge will not be damaged.

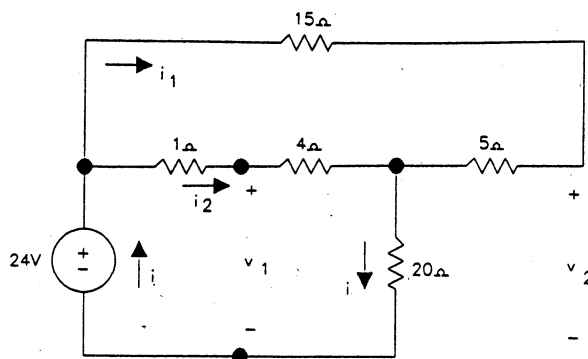
DE 3.7 [a] $R_1 = \frac{(40)(10)}{100} = 4 \Omega$; $R_2 = \frac{(50)(10)}{100} = 5 \Omega$; $R_3 = \frac{(40)(50)}{100} = 20 \Omega$



The resistance seen by the 24-V source is

$$R = (15 + 5) // (4 + 1) + 20 = 20 // 5 + 20 = 4 + 20 = 24 \Omega$$

$$i = 24/24 = 1 \text{ A}$$

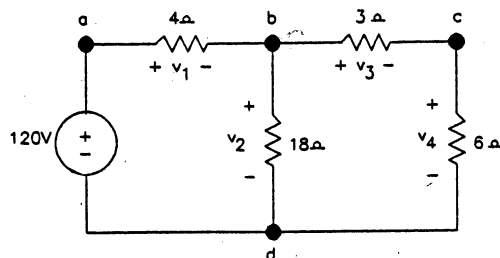


[b] $i_1 = (5/25)i = 0.2 \text{ A}, \quad i_2 = 1 - 0.2 = 0.8 \text{ A}$
 $v_1 = 4i_2 + 20i + 3.2 + 20 = 23.2 \text{ V}$
 $v_2 = 5i_1 + 20i = 1.0 + 20 = 21.0 \text{ V}$

Problems

P3.1 [a] From Ex. 3-1: $i_1 = 4 \text{ A}, \quad i_2 = 8 \text{ A}, \quad i_s = 12 \text{ A}$
 at node x: $-12 + 4 + 8 = 0$, at node y: $12 - 4 - 8 = 0$

[b]



$v_1 = 4i_s = 48 \text{ V} \quad v_3 = 3i_2 = 24 \text{ V}$
 $v_2 = 18i_1 = 72 \text{ V} \quad v_4 = 6i_2 = 48 \text{ V}$
 loop abda: $-120 + 48 + 72 = 0$,
 loop bcdb: $-72 + 24 + 48 = 0$,
 loop abcda: $-120 + 48 + 24 + 48 = 0$

P3.2 [a] $p_{4\Omega} = i_s^2 4 = (12)^2 4 = 576 \text{ W} \quad p_{18\Omega} = (4)^2 18 = 288 \text{ W},$
 $p_{3\Omega} = (8)^2 3 = 192 \text{ W} \quad p_{6\Omega} = (8)^2 6 = 384 \text{ W}$

[b] $p_{120\text{V}(\text{delivered})} = 120i_s = 120(12) = 1440 \text{ W}$

[c] $p_{\text{diss}} = 576 + 288 + 192 + 384 = 1440 \text{ W}$

P3.3 [a] $5\Omega // 20\Omega = 4\Omega \quad \therefore R_{ab} = 10 + 4 + 6 = 20\Omega$

[b] $200\Omega // 50\Omega = 40\Omega$

$20\Omega + 40\Omega = 60\Omega$

$\frac{1}{R_{ab}} = \frac{1}{30} + \frac{1}{60} + \frac{1}{60} = \frac{4}{60} = \frac{1}{15} \text{ U}$

$\therefore R_{ab} = 15\Omega$

P3.4 [a] $R_{ab_a} = 4\Omega // 12\Omega = 3\Omega$

$R_{ab_b} = [2.5 // 7.5 // 5 // 15 // 5 + 7] // 8 + 8 = 4 + 8 = 12\Omega$

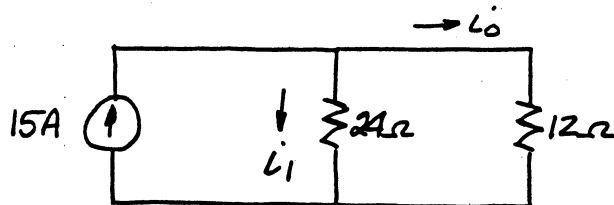
$R_{ab_c} = [6 // 3 + 3] // 20 + 7 = 11\Omega$

[b] $P_{15V} = \frac{15^2}{3} = 75 \text{ W}$

$P_{48V} = \frac{48^2}{12} = 192 \text{ W}$

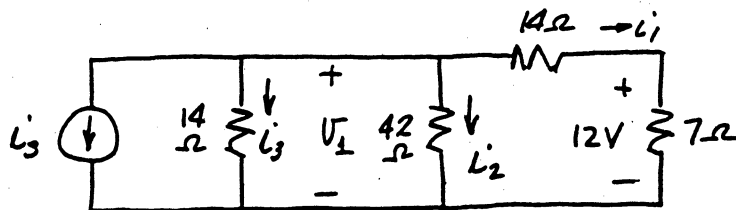
$P_{22V} = \frac{22^2}{11} = 44 \text{ W}$

P3.5 $40\Omega // 60\Omega = 24\Omega$



$i_o = \frac{(15)(24)}{(24 + 12)} = \frac{2}{3}(15) = 10 \text{ A}; \quad p_{12\Omega} = (10)^2(12) = 1200 \text{ W}$

P3.6



$i_1 = \frac{12}{7} \text{ A}; \quad v_1 = (21) \left(\frac{12}{7} \right) = 36 \text{ V}$

$i_2 = \frac{36}{42} = \frac{6}{7} \text{ A}; \quad i_3 = \frac{36}{14} = \frac{18}{7} \text{ A}$

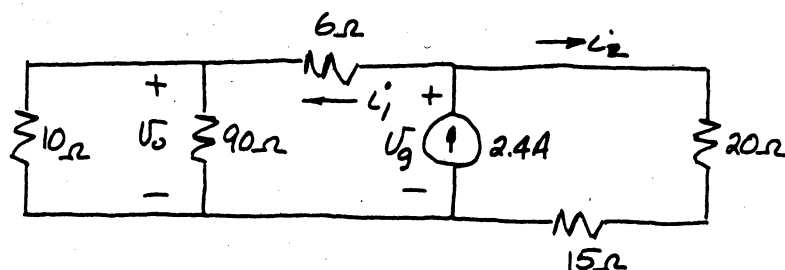
$i_s = -i_1 - i_2 - i_3 = -\frac{12}{7} - \frac{6}{7} - \frac{18}{7} = -\frac{36}{7} \text{ A} = -5.14 \text{ A}$

P3.7 [a] $5//20 = 100/25 = 4\ \Omega$ $5//20 + 9//18 + 10 = 20\ \Omega$
 $9//18 = 162/27 = 6\ \Omega$ $20//30 = 600/50 = 12\ \Omega$
 $R_{ab} = 5 + 12 + 3 = 20\ \Omega$

[b] $5 + 15 = 20\ \Omega$ $30//20 = 600/50 = 12\ \Omega$
 $20//60 = 1200/80 = 15\ \Omega$ $3//6 = 18/9 = 2\ \Omega$
 $15 + 10 = 25\ \Omega$ $3//6 + 30//20 = 2 + 12 = 14\ \Omega$
 $25//75 = 1875/100 = 18.75\ \Omega$ $26//14 = 364/40 = 9.1\ \Omega$
 $18.75 + 11.25 = 30\ \Omega$ $R_{ab} = 2.5 + 9.1 + 3.4 = 15\ \Omega$

[c] $3 + 5 = 8\ \Omega$ $60//40 = 2400/100 = 24\ \Omega$
 $8//12 = 96/20 = 4.8\ \Omega$ $24 + 6 = 30\ \Omega$
 $4.8 + 5.2 = 10\ \Omega$ $30//10 = 300/40 = 7.5\ \Omega$
 $45 + 15 = 60\ \Omega$ $R_{ab} = 1.5 + 7.5 + 1.0 = 10\ \Omega$

P3.8 [a]



$$10//90 = 9\ \Omega, \quad 9 + 6 = 15\ \Omega, \quad 15 + 20 = 35\ \Omega$$

$$i_1 = \frac{(2.4)(35)}{(35 + 15)} = \frac{35}{50}(2.4) = 1.68\ \text{A}$$

$$v_o = (9)(1.68) = 15.12\ \text{V}$$

[b] $i_2 = 2.4 - 1.68 = 0.72\ \text{A}$
 $p_{20\Omega} = i_2^2(20) = (0.72)^2(20) = 10.368\ \text{W}$

[c] $v_g = 35i_2 = 35(0.72) = 25.20\ \text{V}$
 $p_g(\text{dev}) = (25.2)(2.4) = 60.48\ \text{W}$

P3.9 $24 + 16 = 40\ \Omega$; $40\ \Omega//10\ \Omega = 8\ \Omega$; $8\ \Omega + 12\ \Omega = 20\ \Omega$

$$\therefore i_{12\Omega} = \frac{80}{20} = 4\ \text{A}; \quad i_o = i_{12\Omega} \left(\frac{40}{50} \right) = 0.8(4) = 3.2\ \text{A}$$

$$i_{4\Omega} = \frac{80}{8} = 10\ \text{A}; \quad i_g = i_{4\Omega} + i_{12\Omega} = 10 + 4 = 14\ \text{A}$$

Check:

$$P_{\text{dev}} = (80)i_g = 1120\ \text{W}$$

$$\sum P_{\text{diss}} = (10)^2(8) + 16(12) + (3.2)^2(10) + (0.8)^2(40)$$

$$= 800 + 192 + 102.4 + 25.6 = 1120\ \text{W}$$

P3.10 $20 + 60//30 = 40\ \Omega$, $16 + 12 + 32 = 60\ \Omega$

$\therefore i_{16\Omega} = (15) \frac{(40)}{(100)} = 6\text{ A}; \quad v_o = (32)(6) = 192\text{ V}$

The voltage across the three series connected resistors is

$v_a = 6(16 + 12 + 32) = 360\text{ V}$

$\therefore v_g - 8(15) = 360; \quad v_g = 360 + 120 = 480\text{ V}$

Check:

$P_{\text{dev}} = (480)(15) = 7200\text{ W}$

$P_{\text{diss}} = (15)^2(8) + (6)^2(60) + \frac{(360)^2}{40} = 7200\text{ W}$

P3.11 [a] $20//80 = 16\ \Omega$

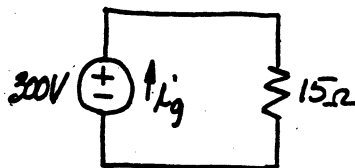
$16 + 4 = 20\ \Omega$

$20//30 = 12\ \Omega$

$12 + 8 = 20\ \Omega$

$20//60 = 15\ \Omega$

$i_g = 300/15 = 20\text{ A}$

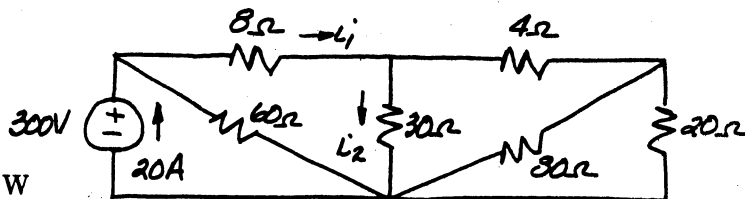


[b]

$i_1 = 20 \left(\frac{60}{80} \right) = 15\text{ A}$

$i_2 = 15 \left(\frac{20}{50} \right) = 6\text{ A}$

$p_{30\Omega} = 6^2(30) = 1080\text{ W}$



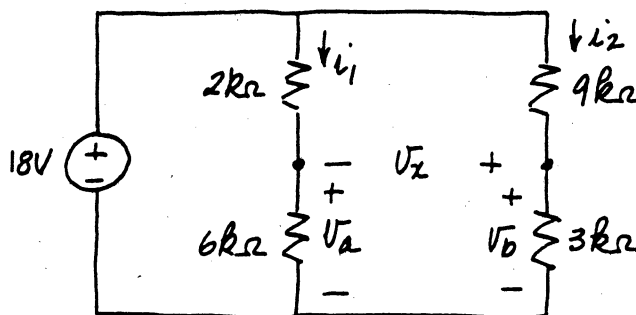
P3.12 [a]

$v_a = \frac{18}{8} \times 6 = 13.5\text{ V}$

$v_b = \frac{18}{12}(3) = 4.5\text{ V}$

$v_a + v_x = v_b$

$v_x = 4.5 - 13.5 = -9\text{ V}$

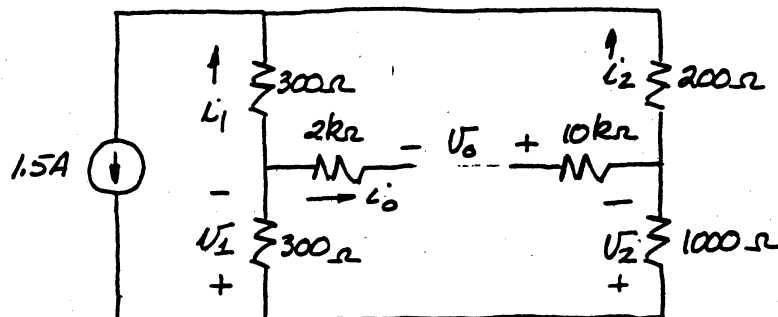


[b] $v_a = \frac{v_s}{8} \times 6 = 0.75v_s$

$v_b = \frac{v_s}{12}(3) = 0.25v_s$

$v_x = v_b - v_a = 0.25v_s - 0.75v_s = -0.5v_s$

P 3.13



Since $i_o = 0$

$$i_1 = \frac{1.5(1200)}{(1800)} = 1.0 \text{ A}, \quad \therefore v_1 = 300 \text{ V}$$

$$i_2 = \frac{1.5(600)}{(1800)} = 0.5 \text{ A}, \quad \therefore v_2 = 500 \text{ V}$$

$$v_1 - v_o - v_2 = 0, \quad \therefore v_o = 300 - 500 = -200 \text{ V}$$

P 3.14 [a] Voltage across $9\text{-}\Omega$ resistor is $1(12 + 6) = 18 \text{ V}$.

The current in the $9\text{-}\Omega$ resistor is $18/9 = 2 \text{ A}$. The current in the $2\text{-}\Omega$ resistor is $2 + 1$ or 3 A . Therefore the voltage across the $24\text{-}\Omega$ resistor is $(2)(3) + 18 = 24 \text{ V}$.

The current in the $24\text{-}\Omega$ resistor is 1 A . The current in the $3\text{-}\Omega$ resistor is $1 + 2 + 1$ or 4 A . Therefore, the voltage across the $72\text{-}\Omega$ resistor is $24 + 3(4) = 36 \text{ V}$.

The current in the $72\text{-}\Omega$ resistor is $36/72$ or 0.5 A .

The $20\text{-}\Omega // 5\text{-}\Omega$ resistors are equivalent to a $4\text{-}\Omega$ resistor. The current in this equivalent resistor is $0.5 + 1 + 3$ or 4.5 A . Therefore the voltage across the $108\text{-}\Omega$ resistor is $36 + 4.5(4) = 54 \text{ V}$.

The current in the $108\text{-}\Omega$ resistor is $54/108$ or 0.5 A . The current in the $1.2\text{-}\Omega$ resistor is $4.5 + 0.5$ or 5 A . Therefore $v_g = (1.2)(5) + 54 = 60 \text{ V}$.

[b] The current in the $20\text{-}\Omega$ resistor is $i_{20\Omega} = \frac{(4.5)(4)}{20} = \frac{18}{20} = 0.9 \text{ A}$

The power dissipated in the $20\text{-}\Omega$ resistor is $p_{20\Omega} = (0.9)^2(20) = 16.2 \text{ W}$

P 3.15 [a] $R_{\text{cond}} = 845(0.0397) = 33.5465 \text{ }\Omega$

$$R_{\text{total}} = 2(1/2)R_{\text{cond}} = 33.5465 \text{ }\Omega$$

$$P_{\text{loss}} = (2000)^2(33.5465) = 134.186 \text{ MW}$$

$$P_{\text{calif}} = 800(2) - 134.186 = 1465.814 \text{ MW}$$

$$\text{Efficiency} = (1465.814/1600) \times 100 = 91.61\%$$

$$[b] \quad P_{\text{calif}} = 2000 - 134.86 = 1865.814 \text{ MW}$$

$$\text{Efficiency} = 93.29\%$$

$$[c] \quad P_{\text{loss}} = (3000)^2 \cdot 2 \cdot (1/3) \cdot 845 \cdot (0.0397) = 201.279 \text{ MW}$$

$$P_{\text{oregon}} = 3000 \text{ MW}, \quad P_{\text{calif}} = 3000 - 201.279 = 2798.7 \text{ MW}$$

$$\text{Efficiency} = (2798.70/3000) \times 100 = 93.29\%$$

$$\text{P 3.16} \quad [a] \quad v_o = \frac{400(5.6)}{(39.2 + 5.6)} = 50 \text{ V}$$

$$[b] \quad v_{R_1} = 350 \text{ V}$$

$$P_{R_1} = (350)^2 / 39,200 = 3.125 \text{ W}$$

$$v_{R_2} = 50 \text{ V}$$

$$P_{R_2} = (50)^2 / 5600 = 0.4464 \text{ W}$$

$$[c] \quad \frac{R_2}{R_1 + R_2} = \frac{1}{8}, \quad \therefore 7R_2 = R_1, \quad R_2 = R_1/7$$

$$P_{R_1} = \frac{(350)^2}{R_1} = 1 \text{ W}$$

$$R_1 = 122.5 \text{ k}\Omega$$

$$R_2 = \frac{122.5}{7} = 17.50 \text{ k}\Omega$$

$$P_{R_2} = \frac{2500}{17,500} \cong 0.1429 \text{ W} < 1 \text{ W}$$

Note if R_2 is selected to be a 1-W resistor,

$$R_2 = 2500 \Omega$$

$$R_1 = 7R_2 = 17,500 \Omega$$

$$P_{R_1} = \frac{(350)^2}{17,500} = 7 \text{ W} > 1 \text{ W}$$

Therefore design must be based on R_1 dissipating 1 W.

$$\text{P 3.17} \quad [a] \quad v_o = \frac{80R_2}{(R_1 + R_2)} = 20$$

$$\therefore \frac{R_2}{R_1 + R_2} = \frac{20}{80} = \frac{1}{4}; \quad \therefore 3R_2 = R_1$$

$$\text{Let } R_e = R_2 // R_L = \frac{R_2 R_L}{R_2 + R_L}$$

$$v_o = \frac{80R_e}{R_1 + R_e} = 18; \quad \frac{R_e}{R_1 + R_e} = \frac{18}{80} = \frac{9}{40}$$

$$40R_e = 9R_1 + 9R_e; \quad 31R_e = 9R_1 = 27R_2; \quad R_e = \frac{(37.8)R_2}{R_2 + 37.8}$$

$$\frac{31(37.8)R_2}{R_2 + 37.8} = 27R_2$$

$$\therefore \frac{31(37.8)}{27} = R_2 + 37.8; \quad R_2 = 5.6 \text{ k}\Omega; \quad R_1 = 3(5.6) = 16.8 \text{ k}\Omega$$

- [b] Power dissipated in R_1 will be maximum when the voltage across R_1 is maximum. This will occur under load conditions.

$$v_{R_1} = 80 - 18 = 62 \text{ V}$$

$$P_{R_1} = \frac{(62)^2}{16.8} \times 10^{-3} = 228.81 \text{ mW}$$

- P 3.18** Refer to the solution of Problem 3.17. The divider will reach its dissipation limit when the power dissipated in R_1 equals 0.25 W.

Notes:

The dissipation in R_2 will be equal to or less than $P_{R_2} \leq \frac{400}{5.6} = 71.43 \text{ mW}$

The dissipation in R_1 can reach a maximum of $P_{R_1} = \frac{6400}{16.8} = 380.95 \text{ mW}$

When the dissipation in R_1 is 250 mW, the voltage across R_1 is

$$v_{R_1}^2 = 0.25(16.8 \times 10^3) = 4200, \quad v_{R_1} = 64.81 \text{ V}$$

$$\therefore v_o = 80 - 64.81 = 15.19 \text{ V}$$

$$\therefore \frac{80R_e}{R_1 + R_e} = 15.19, \quad \therefore R_e = 3.94 \text{ k}\Omega$$

$$\therefore \frac{5.6R_L}{5.6 + R_L} = 3.94, \quad R_L = 13.27 \text{ k}\Omega \quad (\text{minimum value})$$

$$\textbf{P 3.19} \quad \frac{(24)^2}{R_1 + R_2 + R_3} = 60, \quad \therefore R_1 + R_2 + R_3 = 9.6 \Omega$$

$$\frac{(R_1 + R_2)24}{(R_1 + R_2 + R_3)} = 12$$

$$\therefore 2(R_1 + R_2) = R_1 + R_2 + R_3$$

$$\therefore R_1 + R_2 = R_3; \quad 2R_3 = 9.6; \quad R_3 = 4.8 \Omega$$

$$\frac{R_2(24)}{R_1 + R_2 + R_3} = 5$$

$$4.8R_2 = R_1 + R_2 + 4.8 = 9.6$$

$$R_2 = 2 \Omega; \quad R_1 = 9.6 - R_2 - R_3 = 2.8 \Omega$$

- P 3.20** [a] When the circuits are connected, the 25-k Ω resistor is paralleled by a 100-k Ω resistor, thus the output voltage of the first divider is

$$v'_o = \frac{380}{(75 + 20)}(20) = 80 \text{ V}$$

$$\text{Therefore } v_o = \frac{80}{100}(60) = 48 \text{ V}$$

$$\begin{aligned}
 \text{[b]} \quad i &= \frac{380}{100} \times 10^{-3} = 3.8 \text{ mA} \\
 (3.8)(10^{-3})(25 \times 10^3) &= 95 \text{ V} \\
 v_o &= \frac{95}{(100)}(60) = 57 \text{ V}
 \end{aligned}$$

- [c] It removes the loading effect on the voltage divider connected to the 380-V source.

This can be seen by noting the no-load value of v'_o is 95 V, which is identical to the voltage applied to the second divider circuit in Fig. P3.20(c).

- P 3.21** [a] Let v_o be the voltage across the parallel branches, positive at the upper terminal, then

$$i_g = v_o G_1 + v_o G_2 + \cdots + v_o G_N = v_o (G_1 + G_2 + \cdots + G_N)$$

It follows that
$$v_o = \frac{i_g}{(G_1 + G_2 + \cdots + G_N)}$$

The current in the k^{th} branch is $i_k = v_o G_k$; $\therefore i_k = \frac{i_g G_k}{[G_1 + G_2 + \cdots + G_N]}$

[b] $G_1 + G_2 + G_3 + G_4 + G_5 + G_6 = 2.5 \text{ S}$

$$G_{5\Omega} = 0.2 \text{ S}$$

$$i_o = \frac{40(0.2)}{2.5} = 3.2 \text{ A}$$

$$\begin{aligned}
 \text{Check: } i_g &= \frac{16}{0.5} + \frac{16}{5} + \frac{16}{8} + \frac{16}{10} + \frac{16}{20} + \frac{16}{40} \\
 &= 32 + 3.2 + 2 + 1.6 + 0.8 + 0.4 = 40 \text{ A}
 \end{aligned}$$

P 3.22

$$i_4 = \frac{G_4}{\sum G} 10^{-3} \qquad i_2 = 2i_3 = \frac{4G_4}{\sum G} \times 10^{-3}$$

$$i_3 = 2i_4 = \frac{2G_4}{\sum G} \times 10^{-3} \qquad i_1 = 2i_2 = \frac{8G_4}{\sum G} \times 10^{-3}$$

$$i_1 + i_2 + i_3 + i_4 = 10^{-3} = \frac{G_4}{\sum G} \times 10^{-3}(8 + 4 + 2 + 1)$$

$$\therefore \frac{15G_4}{\sum G} = 1 \quad \text{or} \quad 15G_4 = \sum G$$

$$i_4 R_4 = 1$$

$$\therefore \left(\frac{G_4}{\sum G} \times 10^{-3} \right) \left(\frac{1}{G_4} \right) = 1$$

$$\therefore \sum G = 10^{-3}$$

$$\therefore G_4 = \frac{10^{-3}}{15}, \quad R_4 = \frac{1}{G_4} = 15,000 \, \Omega$$

$$i_3 = \frac{G_3 \times 10^{-3}}{\sum G} = \frac{2G_4}{\sum G} \times 10^{-3}$$

$$\therefore G_3 = 2G_4 = \frac{2 \times 10^{-3}}{15}, \quad R_3 = \frac{1}{G_3} = 7500 \Omega$$

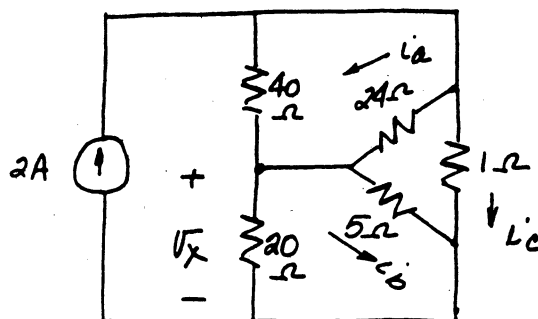
$$i_2 = \frac{G_2 10^{-3}}{\sum G} = \frac{4G_4 \times 10^{-3}}{\sum G}$$

$$\therefore G_2 = 4G_4, \quad R_2 = \frac{15}{4} \times 10^3 = 3750 \Omega$$

$$i_1 = \frac{G_1 \times 10^{-3}}{\sum G} = \frac{8G_4 \times 10^{-3}}{\sum G}$$

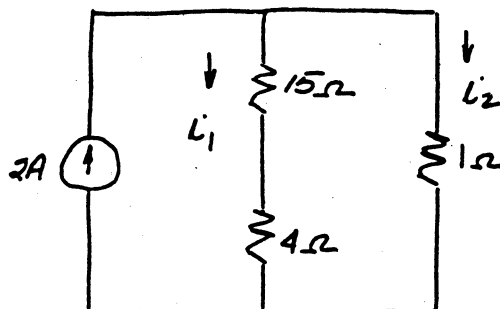
$$\therefore G_1 = 8G_4, \quad R_1 = \frac{15 \times 10^3}{8} = 1875 \Omega$$

P3.23 [a]



$$40 // 24 = 15 \Omega$$

$$20 // 5 = 4 \Omega$$



$$i_2 = \frac{2(19)}{20} = 1.9 \text{ A}$$

$$i_c = i_2 = 1.9 \text{ A}$$

$$i_1 = \frac{2(1)}{(19+1)} = 0.1 \text{ A}$$

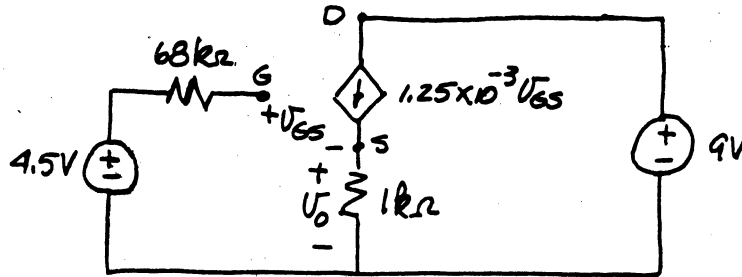
$$i_a = \frac{i_1(40)}{64} = 62.5 \text{ mA}$$

$$i_b = \frac{0.1(20)}{25} = 0.08 = 80 \text{ mA}$$

$$v_x = 5i_b = 0.40 \text{ V}$$

$$P_{\text{device}} = 24i_a^2 + 5i_b^2 + 1i_c^2 = 3.74 \text{ W}$$

P 3.24



$$4.5 = v_{GS} + 1000(1.25 \times 10^{-3} v_{GS}) = 2.25 v_{GS}, \quad \therefore v_{GS} = \frac{4.5}{2.25} = 2 \text{ V}$$

$$v_o = 1000(1.25 \times 10^{-3})(2) = 2.5 \text{ V}$$

$$v_{DS} + v_o = 9 \text{ V}, \quad \therefore v_{DS} = 6.5 \text{ V}$$

P 3.25 The current in the shunt resistor at full-scale deflection is $i_A = i_{\text{fullscale}} - 2 \times 10^{-3}$. The voltage across R_A at full-scale deflection is always 50mV, therefore

$$R_A = \frac{50 \times 10^{-3}}{i_{\text{fullscale}} - 2 \times 10^{-3}} = \frac{50}{1000i_{\text{fullscale}} - 2}$$

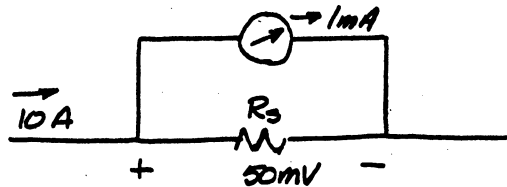
$$[a] \quad R_A = \frac{50}{10,000 - 2} = \frac{50}{9998} = 5.001 \text{ m}\Omega$$

$$[b] \quad R_A = \frac{50}{1000 - 2} = \frac{50}{998} = 50.10 \text{ m}\Omega$$

$$[c] \quad R_A = \frac{50}{48} = 1.042 \Omega$$

$$[d] \quad R_A = \infty \text{ (open)}$$

P 3.26



$$\text{Original meter: } R_e = \frac{50 \times 10^{-3}}{10} = 5 \times 10^{-3} = 0.005 \Omega$$

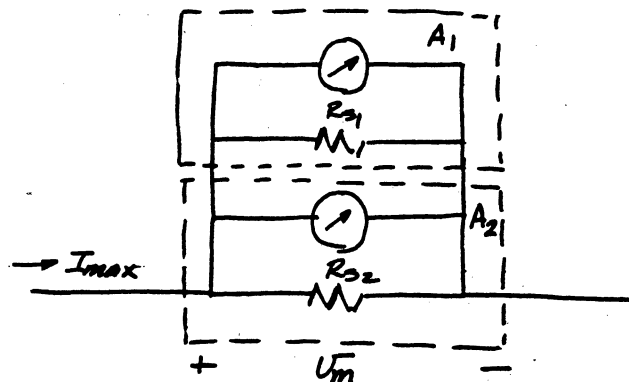
$$\text{Modified meter: } R_e = \frac{(0.005)(0.01)}{0.015} = \frac{0.05}{15} = \frac{1}{300} \Omega$$

$$\therefore (I_{\text{fullscale}}) \left(\frac{1}{300} \right) = 50 \times 10^{-3}$$

$$\therefore I_{\text{fullscale}} = (300)(50) \times 10^{-3} = 15 \text{ A}$$

$$I_{\text{fullscale}} = 15 \text{ A}$$

P 3.27



Note the maximum voltage across the parallel-connected ammeters is limited to $500 \mu\text{V}$, otherwise ammeter 1 exceeds its full-scale reading.

When $v_m = 500 \mu\text{V}$, A_1 reads $10 \mu\text{A}$ and ammeter 2 reads $(1/2)(5)$ or $2.5 \mu\text{A}$.

Therefore $I_{\max} = 12.5 \mu\text{A}$

$$\text{P 3.28 [a]} \quad i_m = \frac{i_{\text{meas}}(50/49)}{50 + (50/49)} = \frac{50i_{\text{meas}}}{2500} = \frac{1}{50}i_{\text{meas}} = \text{one fiftieth of } i_{\text{meas}}$$

$$\text{[b]} \quad R_s = \frac{50}{999} \Omega$$

$$i_m = \frac{i_{\text{meas}}(50/999)}{50 + (50/999)} = \frac{50i_{\text{meas}}}{50(999) + 50} = \frac{i_{\text{meas}}}{1000}$$

$\therefore i_m = \text{one-thousandth of } i_{\text{meas}}$

[c] Yes

P 3.29 Measured value:

$$i_g = \frac{400}{(16 + 64)} = 5 \text{ A}; \quad i_{\text{meas}} = (5) \frac{80}{100} = 4 \text{ A}$$

True value:

$$i_g = \frac{400}{\left[\frac{(80)(19)}{99} + 64\right]} = \frac{2475}{491} \cong 5.04 \text{ A}; \quad i_{\text{true}} = (5.04) \left(\frac{80}{99}\right) \cong 4.07 \text{ A}$$

$$\% \text{ error} = \left[\frac{4}{4.07} - 1 \right] \times 100 = -1.8\%$$

$$\text{P 3.30} \quad i_{\text{true}} = \frac{(300)(25)}{560} = 13.39 \mu\text{A}$$

$$R_{\text{meter 1}} = \frac{500 \times 10^{-6}}{10 \times 10^{-6}} = 50 \Omega$$

$$R_{\text{meter } 2} = \frac{1 \times 10^{-3}}{5 \times 10^{-6}} = 200 \Omega$$

$$\therefore \text{The resistance of the paralleled meters is } R_m = \frac{(50)(200)}{250} = 40 \Omega$$

$$i_{\text{meas}} = \frac{(300)(25)}{600} = 12.5 \mu\text{A}$$

$$\% \text{ error} = \left[\frac{12.5}{13.39} - 1 \right] 100 = -6.67\%$$

P 3.31 At full scale the voltage across the shunt resistor will be 20 mV; therefore the power dissipated will be

$$P_A = \frac{(20 \times 10^{-3})^2}{R_A}$$

$$\text{Therefore } R_A \text{ must be equal to or greater than } R_A \geq \frac{(20 \times 10^{-3})^2}{0.25} \geq 1600 \mu\Omega$$

Otherwise the power dissipated in R_A will exceed its power rating of 0.25 W

$$\text{When } R_A = 1600 \mu\Omega, \text{ the shunt current will be } i_A = \frac{20 \times 10^{-3}}{1600 \times 10^{-6}} = 12.5 \text{ A}$$

$$\text{The measured current will be } i_{\text{meas}} = 12.5 + 0.001 = 12.501 \text{ A}$$

$\therefore$ Full-scale reading is for practical purposes 12.5 A

P 3.32 For all full-scale readings the total resistance is $R_V + R_{\text{movement}} = \frac{\text{full-scale reading}}{10^{-3}}$

$$\therefore R_V = 1000 (\text{full-scale reading}) - 20$$

$$[a] \quad R_V = 1000(100) - 20 = 99,980 \Omega$$

$$[b] \quad R_V = 1000(1) - 20 = 980 \Omega$$

$$[c] \quad R_V = 200 - 20 = 180 \Omega$$

$$[d] \quad R_V = 20 - 20 = 0 \Omega$$

P 3.33 [a] $v_{\text{meter}} = 320 \text{ V}$

$$[b] \quad R_{\text{meter}} = (400)(600) = 240 \text{ k}\Omega$$

$$48 // 240 = 40 \text{ k}\Omega$$

$$v_{\text{meter}} = \frac{320}{56} \times 40 = 228.57 \text{ V}$$

$$[c] \quad 16 // 240 = 15 \text{ k}\Omega$$

$$v_{\text{meter}} = \frac{320}{63}(15) = 76.19 \text{ V}$$

- [d] $v_{\text{meter a}} = 320 \text{ V}$
 $v_{\text{meter b}} + v_{\text{meter c}} = 304.76$, no
 Because of the loading effect.

P3.34 [a] $R_{\text{movement}} = 50 \Omega$

$$R_1 + R_{\text{movement}} = \frac{30}{1 \times 10^{-3}} = 30 \text{ k}\Omega$$

$$\therefore R_1 = 29,950 \Omega$$

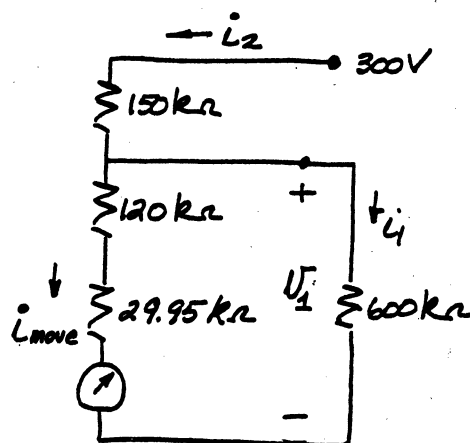
$$R_2 + R_1 + R_{\text{movement}} = \frac{150}{10^{-3}} = 150 \text{ k}\Omega$$

$$\therefore R_2 = 120 \text{ k}\Omega$$

$$R_3 + R_2 + R_1 + R_{\text{movement}} = \frac{300}{10^{-3}} = 300 \text{ k}\Omega$$

$$\therefore R_3 = 150 \text{ k}\Omega$$

[b]



$$i_{\text{move}} = \frac{240}{300}(1) = 0.8 \text{ mA}$$

$$v_1 = (0.8)(150) = 120 \text{ V}$$

$$i_1 = \frac{120}{600} = 0.2 \text{ mA}$$

$$i_2 = i_{\text{move}} + i_1 = 0.8 + 0.2 = 1 \text{ mA}$$

$$v_{\text{meas}} = v_x = v_1 + 150i_2 = 270 \text{ V}$$

[c]

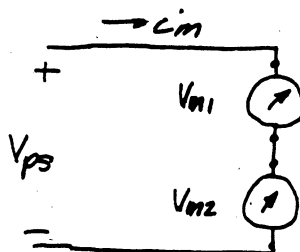
$$v_1 = 150 \text{ V}$$

$$i_1 = \frac{150}{600} = 0.25 \text{ mA}$$

$$i_2 = 1 + 0.25 = 1.25 \text{ mA}$$

$$v_{\text{meas}} = v_x = 150 + 150(1.25) = 337.50 \text{ V}$$

- P3.35 [a] Since the unknown voltage is greater than either voltmeter's maximum reading, the only possible way to use the voltmeters would be to connect them in series.



$$R_{m1} = (300)(900) = 270 \text{ k}\Omega$$

$$R_{m2} = (150)(1200) = 180 \text{ k}\Omega$$

$$\therefore R_{m1} + R_{m2} = 450 \text{ k}\Omega$$

$$i_m = \frac{400}{450 \times 10^3} = \frac{8}{9} \text{ mA}$$

$$V_{m1} = \frac{8}{9}(270) = 240 \text{ V}$$

$$V_{m2} = \frac{8}{9}(180) = 160 \text{ V}$$

Therefore the meters cannot be used since the reading of V_{m2} exceeds 150 V.

[b] The maximum current allowed in V_{m1} is $i_1(\text{max}) = \frac{300}{270} = \frac{10}{9} \text{ mA}$.

The maximum current allowed in V_{m2} is $i_2(\text{max}) = \frac{150}{180} = \frac{5}{6} \text{ mA}$.

$\therefore$ The 150-V meter limits the maximum voltage that can be measured. Thus

$$v_{\text{max}} = \frac{5}{6}(270) + \frac{5}{6}(180) = 225 + 150 = 375 \text{ V}$$

[c] $i_m = \frac{320}{450 \times 10^3} = 0.711 \text{ mA}$

$$V_{m1} = (0.711)(270) = 192 \text{ V}$$

$$v_{m2} = (0.711)(180) = 128 \text{ V}$$

P 3.36 The current in the series-connected voltmeters is

$$i_m = \frac{205.2}{270} = \frac{136.8}{180} = 0.76 \text{ mA}$$

$$v_{50\text{k}\Omega} = (0.76)(50) = 38 \text{ V}$$

$$V_{\text{power supply}} = 205.2 + 136.8 + 38 = 380 \text{ V}$$

P 3.37 [a] $R_{\text{meter}} = 400 \text{ k}\Omega + 200 \text{ k}\Omega // 200 \text{ k}\Omega = 500 \text{ k}\Omega$

$$500 // 125 = 100 \text{ k}\Omega$$

$$V_{\text{meter}} = \frac{750}{125}(100) = 600 \text{ V}$$

[b] What is the percent error in the measured voltage?

$$\text{True value} = \frac{750}{150}(125) = 625$$

$$\% \text{ error} = \left(\frac{600}{625} - 1 \right) 100 = -4\%$$

P 3.38 $R_{\text{meter}} = R_m + R_{\text{movement}} = 500 \text{ k}\Omega$

$$v_{\text{meas}} = 30 \times 10^{-3} R_e$$

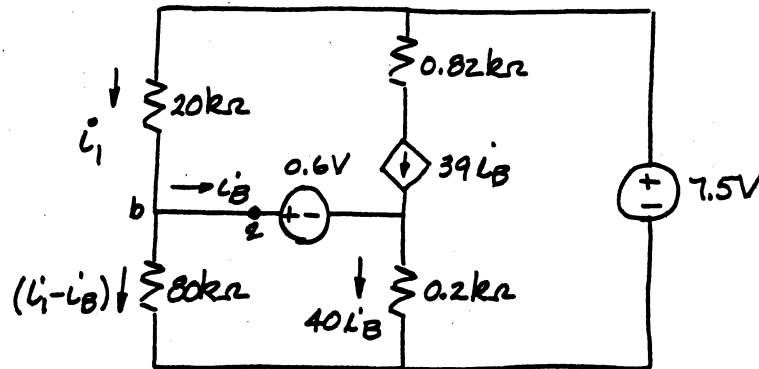
$$R_e = 25 \text{ k}\Omega // 125 \text{ k}\Omega // 500 \text{ k}\Omega = 20 \text{ k}\Omega$$

$$v_{\text{meas}} = 30(20) = 600 \text{ V}$$

$$v_{\text{true}} = (30 \times 10^{-3}) \frac{(25)(125)}{150} \times 10^3 = 625 \text{ V}$$

$$\% \text{ error} = \left(\frac{600}{625} - 1 \right) 100 = -4\%$$

P3.39 [a]



$$20 \times 10^3 i_1 + 80 \times 10^3 (i_1 - i_B) = 7.5$$

$$80 \times 10^3 (i_1 - i_B) = 0.6 + 40 i_B (0.2) \times 10^3$$

$$\therefore 100 i_1 - 80 i_B = 7.5 \times 10^{-3}$$

$$80 i_1 - 88 i_B = 0.6 \times 10^{-3}$$

$$\therefore \Delta = \begin{vmatrix} 100 & -80 \\ 80 & -88 \end{vmatrix} = -2400$$

$$N_B = \begin{vmatrix} 100 & 7.5 \times 10^{-3} \\ 80 & 0.6 \times 10^{-3} \end{vmatrix} = -540 \times 10^{-3}$$

$$i_B = \frac{N_B}{\Delta} = \frac{-540 \times 10^{-3}}{-2400} = 0.225 \times 10^{-3} = 225 \times 10^{-6} = 225 \mu\text{A}$$

[b] With the insertion of the ammeter the equations become

$$100 i_1 - 80 i_B = 7.5 \times 10^{-3} \quad (\text{no change})$$

$$80 \times 10^3 (i_1 - i_B) = 10^3 i_B + 0.6 + 40 i_B (200)$$

$$80 i_1 - 89 i_B = 0.6 \times 10^{-3}$$

$$\Delta = \begin{vmatrix} 100 & -80 \\ 80 & -89 \end{vmatrix} = -8900 + 6400 = -2500$$

$$N_B = \begin{vmatrix} 100 & 7.5 \times 10^{-3} \\ 80 & 0.6 \times 10^{-3} \end{vmatrix} = -540 \times 10^{-3}$$

$$i_B = \frac{N_B}{\Delta} = \frac{-540 \times 10^{-3}}{-2500} = 0.216 \times 10^{-3} = 216 \mu\text{A}$$

$$[c] \quad \% \text{ error} = \left(\frac{216}{225} - 1 \right) 100 = -4\%$$

$$\text{P3.40 [a]} \quad 67.2 \times 10^{-3} = \frac{V_s (12 \times 10^6)}{R_s + 12 \times 10^6}$$

$$\therefore 67.2 \times 10^{-3} R_s + 806,400 = 12 \times 10^6 V_s$$

$$4 \text{ M}\Omega // 12 \text{ M}\Omega = 3 \text{ M}\Omega$$

$$\therefore 60 \times 10^{-3} = \frac{3 \times 10^6 V_s}{R_s + 3 \times 10^6}$$

$$\therefore 60 \times 10^{-3} R_s + 180,000 = 3 \times 10^6 V_s$$

Therefore the two simultaneous equations are

$$12 \times 10^6 V_s - 67.2 \times 10^{-3} R_s = 806,400$$

$$3 \times 10^6 V_s - 60 \times 10^{-3} R_s = 180,000$$

$$\therefore \Delta = \begin{vmatrix} 12 \times 10^6 & -67.2 \times 10^{-3} \\ 3 \times 10^6 & -60 \times 10^{-3} \end{vmatrix} = -720,000 + 201,600 = -518,400$$

$$N_V = \begin{vmatrix} 806,400 & -67.2 \times 10^{-3} \\ 180,000 & -60 \times 10^{-3} \end{vmatrix} = -48,384 + 12,096 = -36,288$$

$$V_s = \frac{N_V}{\Delta} = 0.07 = 70 \times 10^{-3} = 70 \text{ mV}$$

$$[b] \quad N_R = \begin{vmatrix} 12 \times 10^6 & 806,400 \\ 3 \times 10^6 & 180,000 \end{vmatrix} = 216 \times 10^{10} - 24,192 \times 10^8 = -2592 \times 10^8$$

$$R_s = \frac{N_R}{\Delta} = \frac{-2592 \times 10^8}{-518,400} = 500,000 \Omega$$

$$R_s = 500 \text{ k}\Omega$$

P 3.41 [a] $R_1 = (100/2)10^3 = 50 \text{ k}\Omega$

$$R_2 = (10/2)10^3 = 5 \text{ k}\Omega$$

$$R_3 = (1/2)10^3 = 500 \Omega$$

[b] Let i_a = actual current in the movement
 i_d = design current in the movement

$$\text{Then \% error} = \left(\frac{i_a}{i_d} - 1 \right) 100$$

$$\text{For the 100-V scale: } i_a = \frac{100}{50,000 + 25} = \frac{100}{50,025}, \quad i_d = \frac{100}{50,000}$$

$$\frac{i_a}{i_d} = \frac{50,000}{50,025} \cong 0.9995 \quad \% \text{ error} = (0.9995 - 1)100 = -0.05\%$$

For the 10-V scale:

$$\frac{i_a}{i_d} = \frac{5000}{5025} \cong 0.995 \quad \% \text{ error} = (0.995 - 1.0)100 = -0.4975\%$$

For the 1-V scale:

$$\frac{i_a}{i_d} = \frac{500}{525} \cong 0.9524 \quad \% \text{ error} = (0.9524 - 1.0)100 = -4.76\%$$

P 3.42 [a] $\frac{9}{250} \times 10^6 = 36 \text{ k}\Omega$

$$\therefore 12 + R = 36, \quad R = 24 \text{ k}\Omega$$

[b] @ 80% full scale: $i = 0.8(250) = 200 \mu\text{A}$

$$R_t = \frac{9}{200} \times 10^6 = 45 \text{ k}\Omega = 36 + R_x \quad \therefore R_x = 9 \text{ k}\Omega$$

50% full scale: $i = 0.5(250) = 125 \mu\text{A}$

$$R_t = \frac{9}{125} \times 10^6 = 72 \text{ k}\Omega = 36 + R_x \quad \therefore R_x = 36 \text{ k}\Omega$$

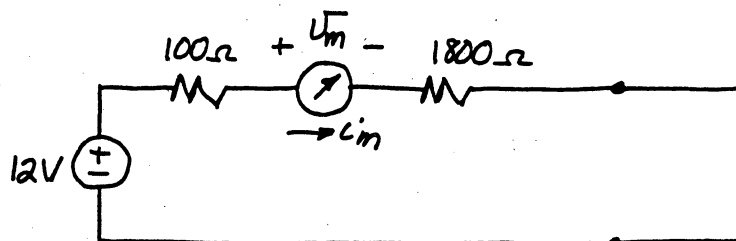
20% full scale: $i = 0.2(250) = 50 \mu\text{A}$

$$R_t = \frac{9}{50} \times 10^6 = 180 \text{ k}\Omega = 36 + R_x \quad \therefore R_x = 144 \text{ k}\Omega$$

0% full scale

$$R_x = \infty$$

P 3.43



When short circuited, $12 = 1900i_m + v_m$

When the short circuit is replaced with a $2000\text{-}\Omega$ resistor, the current is $0.5i_m$;

therefore $12 = 1900(0.5i_m) + 0.5v_m + 2000(0.5i_m) = 1950i_m + 0.5v_m$

or $24 = 3900i_m + v_m$

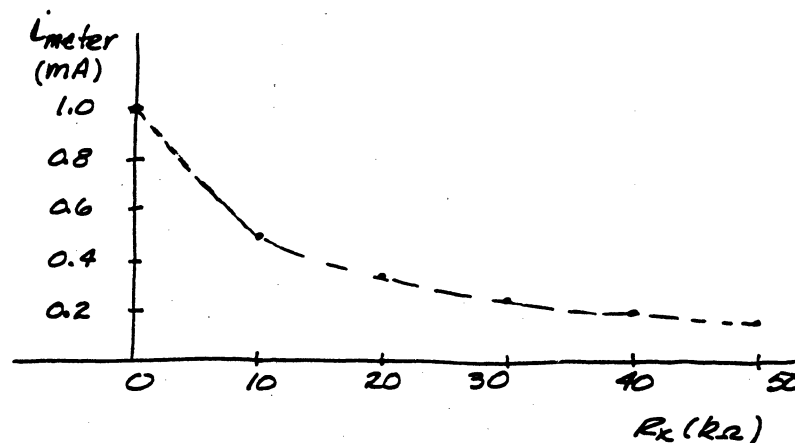
$\therefore 12 = 2000i_m, \quad i_m = 6 \text{ mA}$

$\therefore v_m = 0.6 \text{ V} = 600 \text{ mV}$

P 3.44 [a] $R_o = \frac{10}{10^{-3}} = 10 \text{ k}\Omega$

[b] $i_{\text{meter}} = \frac{10}{10 + R_x} \text{ mA}$

$R_x \text{ (k}\Omega\text{)}$	0	10	20	30	40	50
$i_{\text{meter}} \text{ (mA)}$	1.000	0.500	0.333	0.250	0.200	0.167

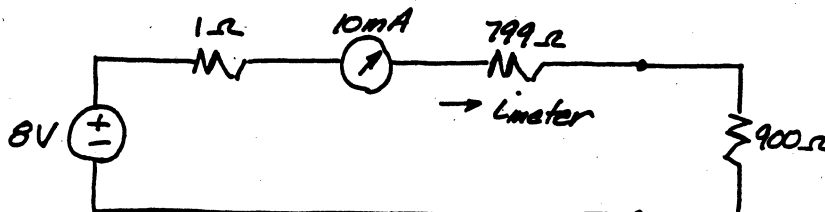


- [c] Because the meter current varies nonlinearly with respect to R_x but the deflection of the meter is proportional to i_{meter} .

P3.45 [a] $R_o + R_g = \frac{9}{10} \times 10^3 = 900 \quad \therefore R_o = 900 - 1 = 899 \Omega$

[b] $R_o + R_g = \frac{8}{10} \times 1000 = 800 \Omega \quad \therefore R_o = 800 - 1 = 799 \Omega$

[c]



$$i_{\text{meter}} = \frac{8}{800 + 900} = \frac{8}{1700} \text{ A}$$

The meter was calibrated using the relationship $i_{\text{meter}} = \frac{9}{900 + R_x}$.

$\therefore$ when $i_{\text{meter}} = \frac{8}{1700} \text{ A}$, the calibrated value of R_x is

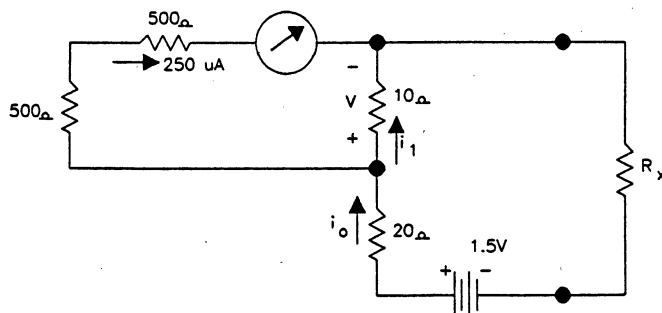
$$\frac{8}{1700} = \frac{9}{900 + R_x}$$

$$R_x = \frac{9(1700)}{8} - 900 = 1912.5 - 900 = 1012.5 \Omega$$

Therefore the ohmmeter would read 1012.5 Ω .

Note that R_o can be used to compensate for changes in R_g but not v_g .

- P3.46** [a] At midscale the microammeter carries 250 μA . With the switch in position 1, the circuit is



$$\begin{aligned}
 v &= 1000(250) \times 10^{-6} = 0.25 \text{ V}, & i_1 &= 0.25/10 = 25,000 \mu\text{A}, \\
 i_o &= i_1 + 250 = 25,250 \mu\text{A}, & 1.5/i_o &= 59.4 \Omega, \\
 R_T &= 20 + 1000//10 + R_x = 59.4 \Omega, & R_x &= 29.5 \Omega
 \end{aligned}$$

Similar analysis of the other positions yields

position #2:

$$\begin{aligned}
 i_1 &= 2272.73 \mu\text{A} & R_T &= 594.59 \Omega \\
 i_o &= 2522.73 \mu\text{A} & R_x &= 295.50 \Omega
 \end{aligned}$$

position #3:

$$\begin{aligned}
 i_1 &= 4629.63 \mu\text{A} & R_T &= 6148.01 \Omega \\
 i_o &= 4879.63 \mu\text{A} & R_x &= 3146.77 \Omega
 \end{aligned}$$

position #4:

$$\begin{aligned}
 i_1 &= 252.53 \mu\text{A} & R_T &= 59,698.49 \Omega \\
 i_o &= 502.53 \mu\text{A} & R_x &= 29,701.01 \Omega
 \end{aligned}$$

[b] Yes, the largest error is position #3, where the indicated value is 4.66% low.

$$\text{P3.47 } R_{\text{movement}} = \frac{100 \times 10^{-3}}{10 \times 10^{-6}} = 10 \text{ k}\Omega$$

$$R_{\text{movement}} + R_o = \frac{9}{10} \times 10^6 = 900 \text{ k}\Omega$$

$$R_o = 900 - 10 = 890 \text{ k}\Omega$$

$$20\% \text{ deflection } i_{\text{movement}} = 2 \mu\text{A}$$

$$\therefore v_{500\Omega} = (2 \times 10^{-6})(900 \times 10^3) = 1.8 \text{ V}$$

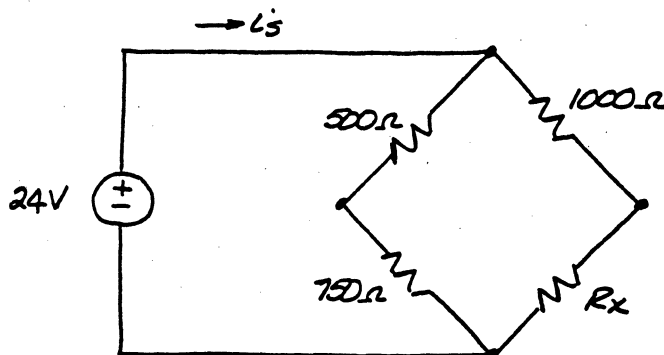
$$i_{500\Omega} = \frac{1.8}{500} = \frac{3.6}{1000} = 3.6 \text{ mA} = 3600 \mu\text{A}$$

$$i_x \cong i_{500} = 3600 \mu\text{A}$$

$$v_x = 9 - 1.8 = 7.2 \text{ V}$$

$$R_x \cong \frac{7.2}{3600} \times 10^6 = 2000 \Omega = 2 \text{ k}\Omega$$

P3.48 [a]



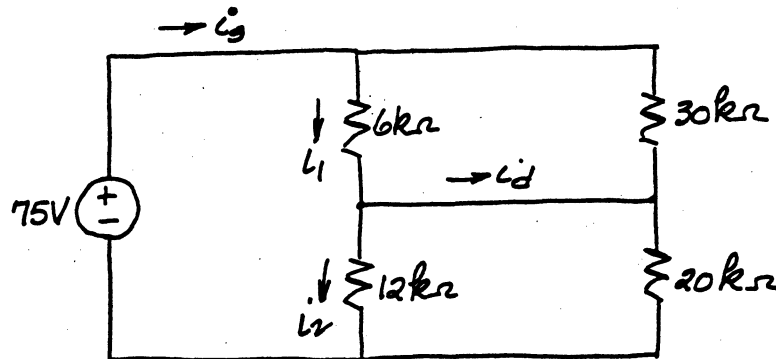
$$R_x = \frac{(1000)(750)}{500} = 1500 \Omega = 1.5 \text{ k}\Omega$$

$$[b] \quad i_s = \frac{24}{1.25} + \frac{24}{2.5} = 19.2 + 9.6 = 28.80 \text{ mA}$$

$$[c] \quad 750\text{-}\Omega \text{ resistor, } P = (19.2 \times 10^{-3})^2(750) = 276.48 \text{ mW}$$

$$[d] \quad 1000\text{-}\Omega \text{ resistor, } P = (9.6 \times 10^{-3})^2(1000) = 92.16 \text{ mW}$$

P 3.49 Redraw the circuit, replacing the detector branch with a short circuit.



$$6 \text{ k}\Omega // 30 \text{ k}\Omega = 5 \text{ k}\Omega$$

$$12 \text{ k}\Omega // 20 \text{ k}\Omega = 7.5 \text{ k}\Omega$$

$$i_g = \frac{75}{5 + 7.5} = 6 \text{ mA}$$

$$i_1 = 6 \frac{(30)}{36} = 5 \text{ mA}$$

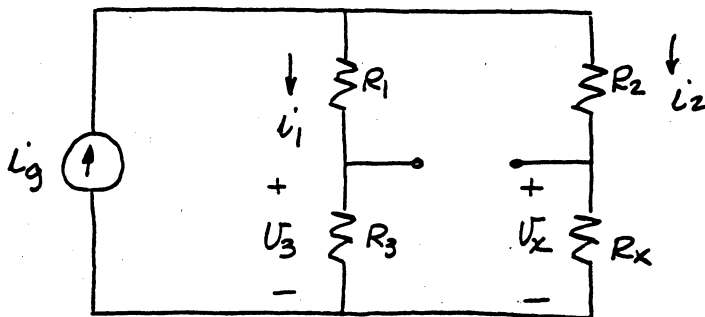
$$i_2 = 6 \frac{(20)}{32} = 3.75 \text{ mA}$$

$$i_1 = i_d + i_2$$

$$i_d = i_1 - i_2 = 5 - 3.75 = 1.25 \text{ mA}$$

$$\text{Check: } 6i_1 + 12i_2 = 30 + 45 = 75 \text{ V}$$

P 3.50 Since the bridge is balanced, we can remove the detector without disturbing the voltages and currents in the circuit.



It follows that

$$i_1 = \frac{i_g(R_2 + R_x)}{R_1 + R_2 + R_3 + R_x} = \frac{i_g(R_2 + R_x)}{\sum R}$$

$$i_2 = \frac{i_g(R_1 + R_3)}{R_1 + R_2 + R_3 + R_x} = \frac{i_g(R_1 + R_3)}{\sum R}$$

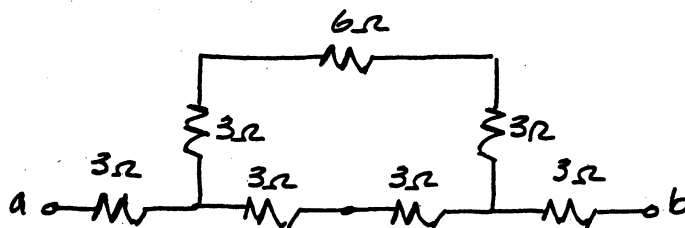
$$v_3 = R_3 i_3 = v_x = i_2 R_x$$

$$\therefore \frac{R_3 i_g(R_2 + R_x)}{\sum R} = \frac{R_x i_g(R_1 + R_3)}{\sum R}; \quad \therefore R_3(R_2 + R_x) = R_x(R_1 + R_3)$$

$$\text{From which } R_x = \frac{R_2 R_3}{R_1}$$

P 3.51 The top of the pyramid can be replaced by a resistor equal to $R_1 = \frac{(18)(9)}{27} = 6\ \Omega$

The lower left and right deltas can be replaced by wyes. Each resistance in the wye equals $3\ \Omega$. Thus our circuit can be reduced to

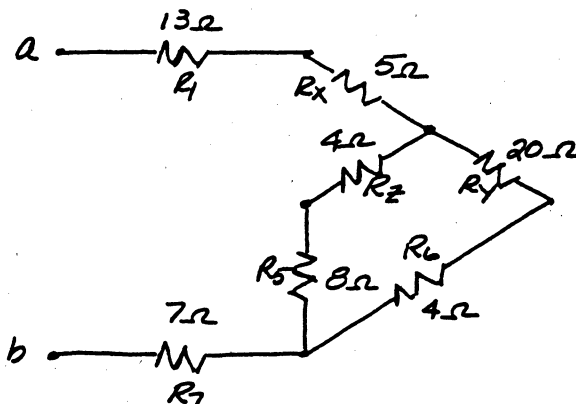


Now the $12\ \Omega$ in parallel with $6\ \Omega$ reduces to $R_2 = \frac{(12)(6)}{18} = 4\ \Omega$

$$\therefore R_{ab} = 3 + 4 + 3 = 10\ \Omega$$

P 3.52 [a] $R_X = \frac{(10)(50)}{100} = 5\ \Omega$; $R_Y = \frac{(40)(50)}{100} = 20\ \Omega$; $R_Z = \frac{(10)(40)}{100} = 4\ \Omega$

Replacing the R_2 - R_3 - R_4 delta with its equivalent Y gives



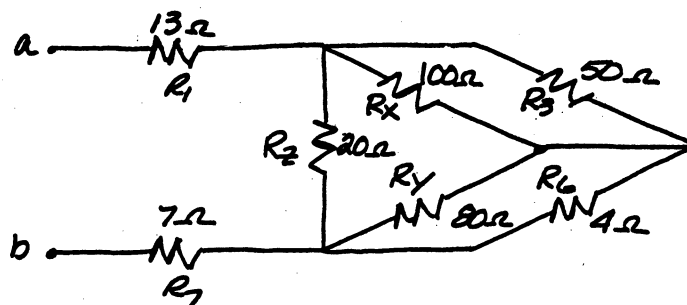
$$R_{ab} = 13 + 5 + 12//24 + 7 = 18 + 8 + 7 = 33 \Omega$$

$$[b] \quad R_X = \frac{(10)(40) + (40)(8) + (8)(10)}{8} = \frac{800}{8} = 100 \Omega$$

$$R_Y = \frac{800}{10} = 80 \Omega$$

$$R_Z = \frac{800}{40} = 20 \Omega$$

Replacing the R_2, R_4, R_5 wye with its equivalent Δ gives



$$\text{Now note that } 100//50 = \frac{5000}{150} = \frac{100}{3} \Omega; \quad 80//4 = \frac{320}{84} = \frac{80}{21} \Omega$$

$$\therefore 100//50 + 80//4 = \frac{100}{3} + \frac{80}{21} = \frac{780}{21} \Omega$$

$$\therefore \frac{780}{21} // 20 = \frac{(20)(780)}{21[20 + (780/21)]} = 13 \Omega$$

$$\therefore R_{ab} = 13 + 13 + 7 = 33 \Omega$$

- [c] Convert the delta connection R_4 - R_5 - R_6 to its equivalent wye.
Convert the wye connection R_3 - R_4 - R_6 to its equivalent delta.

P 3.53 In order that all four decades (1, 10, 100, 1000) that are used to set R_3 contribute to the balance of the bridge, the ratio R_2/R_1 should be set to 0.001.

P 3.54 Subtracting Eq. 3.44 from Eq. 3.45 gives

$$R_1 - R_2 = (R_c R_b - R_c R_a) / (R_a + R_b + R_c).$$

Adding this expression to Eq. 3.43 and solving for R_1 gives

$$R_1 = R_c R_b / (R_a + R_b + R_c).$$

To find R_2 , subtract Eq. 3.45 from Eq. 3.43 and add this result to Eq. 3.44. To find R_3 , subtract Eq. 3.43 from Eq. 3.44 and add this result to Eq. 3.45. Using the hint, Eq. 3.45 becomes

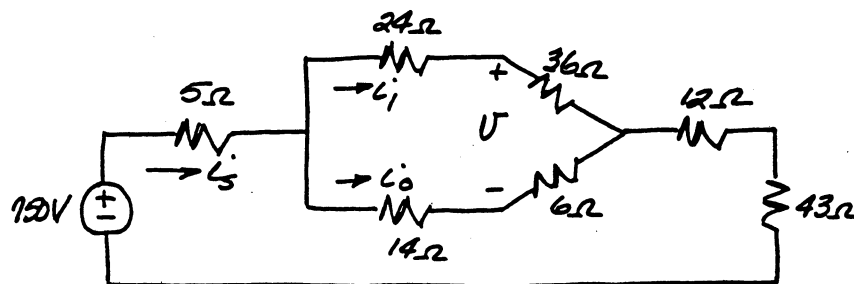
$$R_1 + R_3 = \frac{R_b[(R_2/R_3)R_b + (R_2/R_1)R_b]}{(R_2/R_1)R_b + R_b + (R_2/R_3)R_b} = \frac{R_b(R_1 + R_3)R_2}{(R_1 R_2 + R_2 R_3 + R_3 R_1)}$$

Solving for R_b gives $R_b = (R_1 R_2 + R_2 R_3 + R_3 R_1) / R_2$. To find R_a : First use Eqs. 3.37–3.39 to obtain the ratios $(R_1 / R_3) = (R_c / R_a)$ or $R_c = (R_1 / R_3) R_a$ and $(R_1 / R_2) = (R_b / R_a)$ or $R_b = (R_1 / R_2) R_a$. Now use these relationships to eliminate R_b and R_c from Eq. 3.44. To find R_c , use Eqs. 3.37–3.39 to obtain the ratios $R_b = (R_3 / R_2) R_c$ and $R_a = (R_3 / R_1) R_c$. Now use the relationships to eliminate R_b and R_a from Eq. 3.43.

$$\begin{aligned} \text{P 3.55 } G_a &= \frac{1}{R_a} = \frac{R_1}{R_1 R_2 + R_2 R_3 + R_3 R_1} \\ &= \frac{1/G_1}{(1/G_1)(1/G_2) + (1/G_2)(1/G_3) + (1/G_3)(1/G_1)} \\ &= \frac{(1/G_1)(G_1 G_2 G_3)}{G_1 + G_2 + G_3} = \frac{G_2 G_3}{G_1 + G_2 + G_3} \end{aligned}$$

Similar manipulations generate the expressions for G_b and G_c .

P 3.56 [a] Replace the 60–120–20- Ω delta with a wye equivalent to get



$$24 + 36 = 60 \Omega; \quad 14 + 6 = 20 \Omega$$

$$60 \Omega // 20 \Omega = 15 \Omega$$

$$\therefore i_s = \frac{750}{5 + 15 + 12 + 43} = \frac{750}{75} = 10 \text{ A}$$

$$\therefore i_1 = (10) \left(\frac{20}{80} \right) = 2.5 \text{ A}$$

$$[b] \quad i_o = 10 \left(\frac{60}{80} \right) = 7.5 \text{ A}$$

$$24i_1 + v - 14i_o = 0; \quad \therefore v = 14(7.5) - 24(2.5) = 45 \text{ V}$$

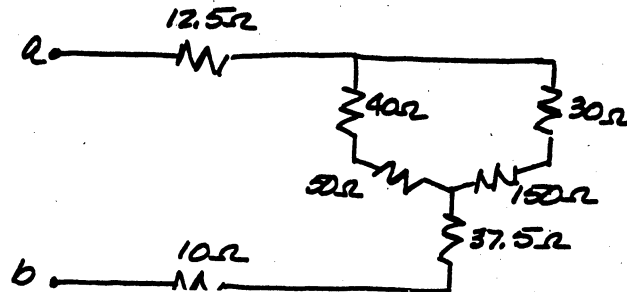
$$\therefore i_{60\Omega} = \frac{45}{60} = 0.75 \text{ A}; \quad i_2 = i_o + i_{60\Omega} = 7.5 + 0.75 = 8.25 \text{ A}$$

$$[c] \quad v = 45 \text{ V} \quad [\text{See calculation in part (b).}]$$

$$[d] \quad P_{\text{supplied}} = (750)(i_s) = 7500 \text{ W} = 7.5 \text{ kW}$$

P 3.57 Replace the lower delta with an equivalent wye.

$$R_1 = \frac{(100)(400)}{800} = 50 \Omega; \quad R_2 = \frac{(400)(300)}{800} = 150 \Omega; \quad R_3 = \frac{(100)(300)}{800} = 37.5 \Omega$$

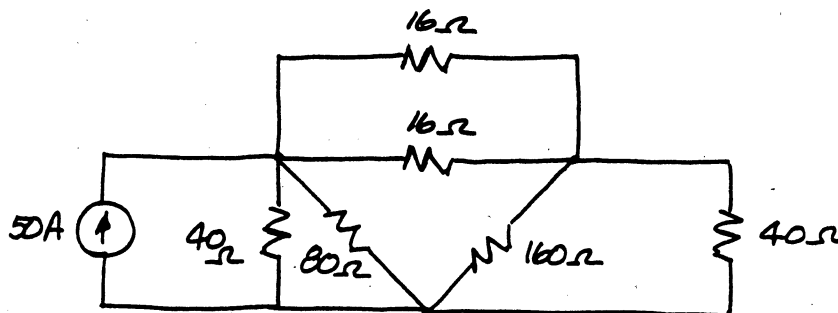


$$50 \Omega + 40 \Omega = 90 \Omega, \quad 150 \Omega + 30 \Omega = 180 \Omega$$

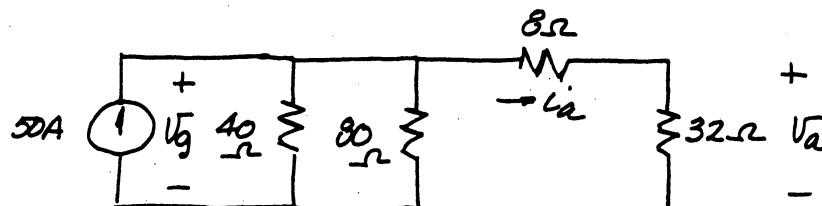
$$90 \Omega // 180 \Omega = 60 \Omega$$

$$R_{ab} = 12.5 + 60 + 37.5 + 10 = 120 \Omega$$

P 3.58 [a] After the 5Ω - 10Ω - 50Ω wye is replaced by its equivalent delta, the circuit reduces to



Now the circuit can be reduced to



Now $40\ \Omega // 80\ \Omega // 40\ \Omega = 16\ \Omega$.

Therefore $v_g = (50)(16) = 800\text{ V}$

$$i_a = \frac{800}{40} = 20\text{ A}$$

$$v_a = (32)(20) = 640\text{ V}$$

It follows that $i_o = \frac{640}{40} = 16\text{ A}$

[b] The voltage across the $16\text{-}\Omega$ resistor is $v_{16} = 8i_a = 160\text{ V}$

$$\text{Therefore } i_1 = \frac{160}{16} = 10\text{ A}$$

[c] It follows that the current in the $10\text{-}\Omega$ resistor is

$$i_{10\Omega} = i_o - i_1 = 16 - 10 = 6\text{ A}$$

Therefore the voltage across the $50\text{-}\Omega$ resistor is

$$v_{50\Omega} = v_a + 10i_{10\Omega} = 640 + 60 = 700\text{ V}$$

$$\therefore i_2 = \frac{v_{50\Omega}}{50} = 14\text{ A}$$

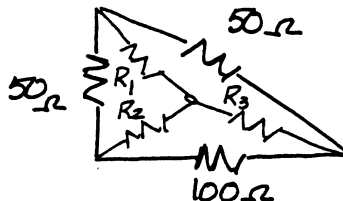
[d] $P_{\text{del}} = (50)(800) = 40,000\text{ W} = 40\text{ kW}$

P 3.59 [a] Convert the upper delta to a wye.

$$R_1 = \frac{(50)(50)}{200} = 12.5\ \Omega$$

$$R_2 = \frac{(50)(100)}{200} = 25\ \Omega$$

$$R_3 = \frac{(50)(100)}{200} = 25\ \Omega$$

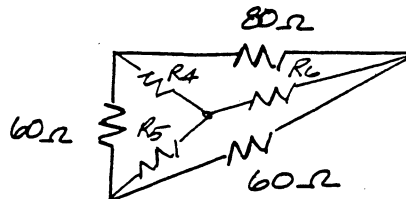


Convert the lower delta to a wye.

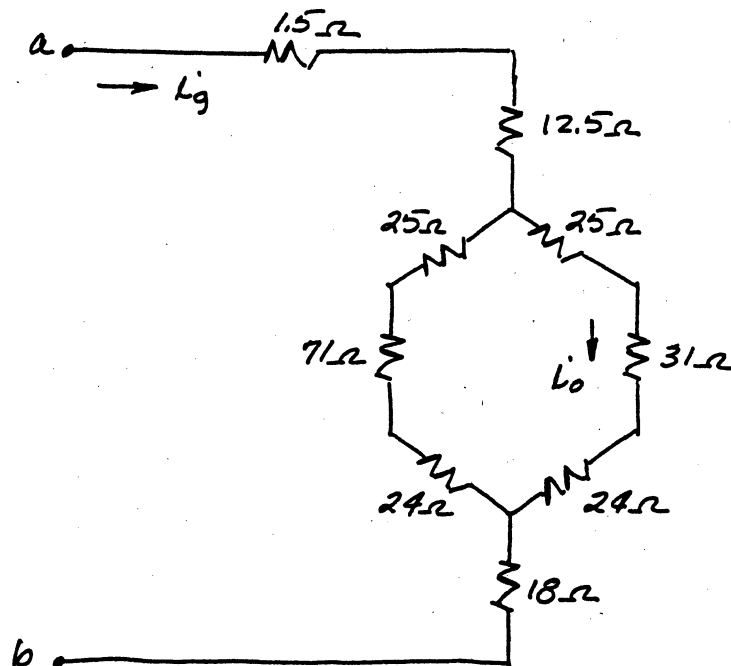
$$R_4 = \frac{(60)(80)}{200} = 24\ \Omega$$

$$R_5 = \frac{(60)(60)}{200} = 18\ \Omega$$

$$R_6 = \frac{(60)(80)}{200} = 24\ \Omega$$



Now redraw the circuit using the wye equivalents.



$$R_{ab} = 1.5 + 12.5 + \frac{(120)(80)}{200} + 18 = 14 + 48 + 18 = 80 \Omega$$

[b] When $v_{ab} = 400$ V

$$i_g = \frac{400}{80} = 5 \text{ A}$$

$$i_o = \frac{(5)(120)}{200} = 3 \text{ A}$$

$$p_{31\Omega} = (9)(31) = 279 \text{ W}$$

P3.60 [a] At no load: $v_o = kv_s = \frac{R_2}{R_1 + R_2}v_s$.

At full load: $v_o = \alpha v_s = \frac{R_e}{R_1 + R_e}v_s$, where $R_e = \frac{R_o R_2}{R_o + R_2}$

Therefore $k = \frac{R_2}{R_1 + R_2}$ and $R_1 = \frac{(1-k)}{k}R_2$

$\alpha = \frac{R_e}{R_1 + R_e}$ and $R_1 = \frac{(1-\alpha)}{\alpha}R_e$

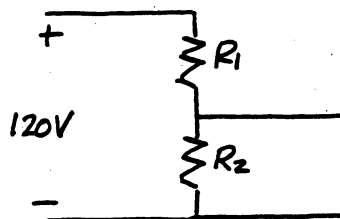
Therefore $\left(\frac{1-\alpha}{\alpha}\right) \left[\frac{R_2 R_o}{R_o + R_2}\right] = \frac{(1-k)}{k}R_2$

Solving for R_2 yields $R_2 = \frac{(k-\alpha)}{\alpha(1-k)}R_o$

$$[b] \quad R_1 = \left(\frac{0.15}{0.675} \right) R_o = \frac{2}{9}(36) = 8 \text{ k}\Omega$$

$$R_2 = \left(\frac{0.15}{0.075} \right) R_o = 2(36) = 72 \text{ k}\Omega$$

[c]



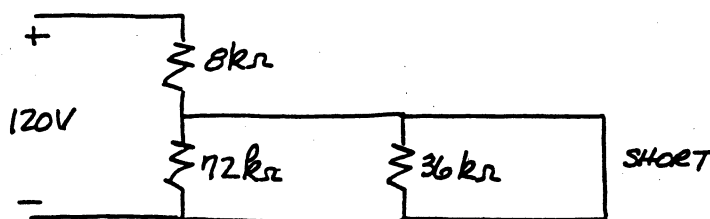
Maximum dissipation in R_2 occurs at no load, $\therefore$

$$P_{R_2(\max)} = \frac{[(120)(0.9)]^2}{72,000} = 162 \text{ mW}$$

Maximum dissipation in R_1 occurs at full load.

$$P_{R_1(\max)} = \frac{[120 - 0.75(120)]^2}{8000} = 112.50 \text{ mW}$$

[d]



$$P_{R_1} = \frac{(120)^2}{8000} = 1.8 \text{ W} = 1800 \text{ mW}$$

$$P_{R_2} = \frac{(0)^2}{72,000} = 0 \text{ W}$$

P 3.61 [a] $R_{ab} = 2R_1 + \frac{R_2(2R_1 + R_L)}{2R_1 + R_2 + R_L} = R_L$

$$\text{Therefore } 2R_1 - R_L + \frac{R_2(2R_1 + R_L)}{2R_1 + R_2 + R_L} = 0$$

$$\text{Therefore } R_L^2 = 4R_1^2 + 4R_1R_2 = 4R_1(R_1 + R_2)$$

When $R_{ab} = R_L$, the current into terminal a of the attenuator will be $\frac{v_i}{R_L}$

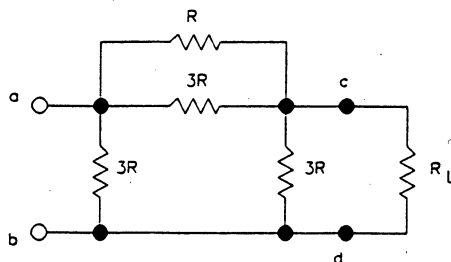
Using current division, the current in the R_L branch will be

$$\frac{v_i}{R_L} \cdot \frac{R_2}{2R_1 + R_2 + R_L}$$

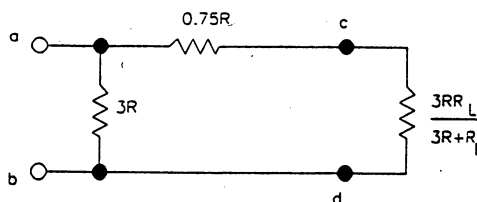
$$\text{Therefore } v_o = \frac{v_i}{R_L} \cdot \frac{R_2}{2R_1 + R_2 + R_L} R_L \quad \text{and} \quad \frac{v_o}{v_i} = \frac{R_2}{2R_1 + R_2 + R_L}$$

$$\begin{aligned}
[b] \quad (600)^2 &= 4(R_1 + R_2)R_1 \\
9 \times 10^4 &= R_1^2 + R_1R_2 \\
\frac{v_o}{v_i} &= 0.6 = \frac{R_2}{2R_1 + R_2 + 600} \\
\therefore 1.2R_1 + 0.6R_2 + 360 &= R_2 \\
0.4R_2 &= 1.2R_1 + 360 \\
R_2 &= 3R_1 + 900 \\
\therefore 9 \times 10^4 &= R_1^2 + R_1(3R_1 + 900) = 4R_1^2 + 900R_1 \\
\therefore R_1^2 + 225R_1 - 22,500 &= 0 \\
R_1 &= -112.5 \pm \sqrt{(112.5)^2 + 22,500} = -112.5 \pm 187.5 \\
\therefore R_1 &= 75 \, \Omega \\
\therefore R_2 &= 3(75) + 900 = 1125 \, \Omega
\end{aligned}$$

P3.62 [a] After making the Y-to- Δ transformation, the circuit in Fig. P3.62 reduces to



Combining the parallel resistors reduces the circuit to



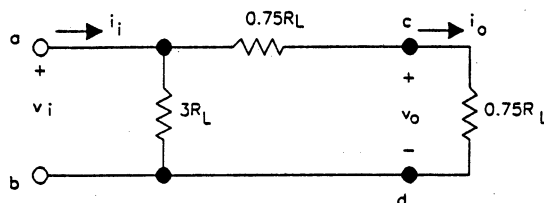
$$\text{Now note: } 0.75R + \frac{3RR_L}{3R + R_L} = \frac{2.25R_L^2 + 3.75RR_L}{3R + R_L}$$

$$\text{Therefore } R_{ab} = \frac{3R \left(\frac{2.25R_L^2 + 3.75RR_L}{3R + R_L} \right)}{3R + \left(\frac{2.25R_L^2 + 3.75RR_L}{3R + R_L} \right)} = \frac{3R(3R + 5R_L)}{15R + 9R_L}$$

$$\text{When } R_{ab} = R_L, \text{ we have } 15RR_L + 9R_L^2 = 9R^2 + 15RR_L$$

$$\text{Therefore } R_L^2 = R^2 \text{ or } R_L = R$$

[b] When $R = R_L$, the circuit reduces to

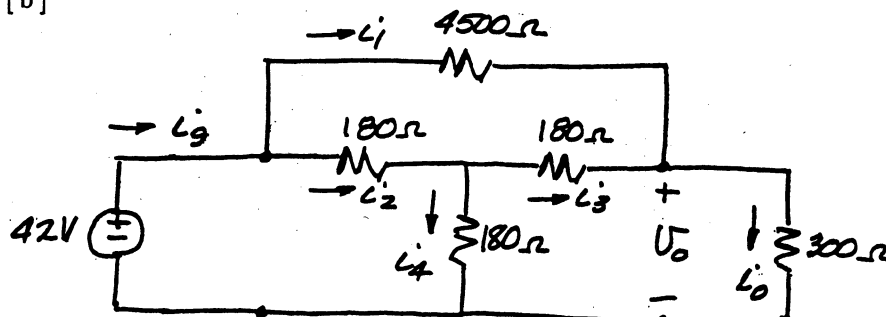


$$i_o = \frac{i(3R_L)}{4.5R_L} = \frac{1}{1.5}i = \frac{1}{1.5} \frac{v_i}{R_L}, \quad v_o = 0.75R_L i_o = \frac{1}{2}v_i,$$

$$\text{Therefore } \frac{v_o}{v_i} = 0.5$$

P3.63 [a] $3.5(3R - R_L) = 3R + R_L$
 $10.5R - 1050 = 3R + 300$
 $7.5R = 1350, \quad R = 180 \Omega$
 $R_2 = \frac{2(180)(300)^2}{3(180)^2 - (300)^2} = 4500 \Omega$

[b]



$$v_o = \frac{v_i}{3.5} = \frac{42}{3.5} = 12 \text{ V}$$

$$i_o = \frac{12}{300} = 40 \text{ mA}$$

$$i_1 = \frac{42 - 12}{4500} = \frac{30}{4500} = 6.67 \text{ mA}$$

$$i_g = \frac{42}{300} = 140 \text{ mA}$$

$$i_2 = 140 - 6.67 = 133.33 \text{ mA}$$

$$i_3 = 40 - 6.67 = 33.33 \text{ mA}$$

$$i_4 = 133.33 - 33.33 = 100 \text{ mA}$$

$$P_{4500\Omega} = (6.67 \times 10^{-3})^2 (4500) = 0.20 \text{ W}$$

$$P_{180\Omega \text{ left}} = (133.33 \times 10^{-3})^2 (180) = 3.20 \text{ W}$$

$$p_{180\Omega \text{ right}} = (33.33 \times 10^{-3})^2(180) = 0.20 \text{ W}$$

$$p_{180\Omega \text{ vertical}} = (100 \times 10^{-3})^2(180) = 1.8 \text{ W}$$

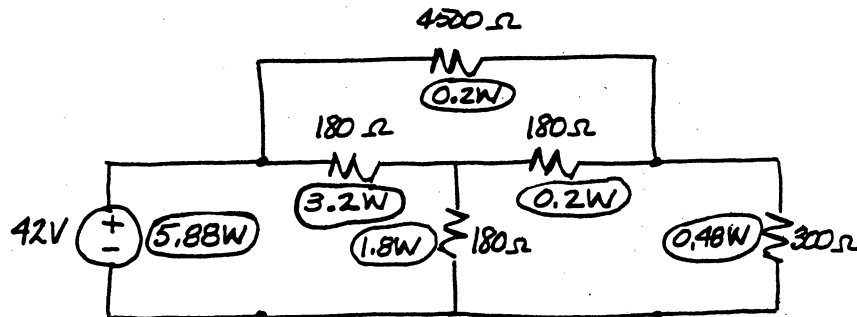
$$p_{300\Omega} = (40 \times 10^{-3})^2(300) = 0.48 \text{ W}$$

The 180- Ω resistor carrying i_2

[c] $p_{180\Omega \text{ left}} = 3.20 \text{ W}$

[d] Two resistors dissipate minimum power, the 4500- Ω and the 180- Ω carrying i_3 .

[e] Both resistors dissipate 0.20 W or 200 mW



Check:

$$\sum P_{\text{diss}} = 0.2 + 3.2 + 1.8 + 0.2 + 0.48 = 5.88 \text{ W}$$

$$\sum P_{\text{dev}} = 42(0.14) = 5.88 \text{ W}$$

Techniques of Circuit Analysis

Drill Exercises

DE 4.1 [a] 11,8 resistors, 2 independent sources, 1 dependent source

[b] 9

[c] 9, $R_4 - R_5$ forms an essential branch as does $R_8 - 10\text{ V}$. The remaining seven branches contain a single element.

[d] 7 [e] 6 [f] 4 [g] 6

DE 4.2 Solution given in text.

DE 4.3 Solution given in text.

DE 4.4 Solution given in text.

DE 4.5 [a] The two-node voltage equations are

$$\left. \begin{aligned} 5 + \frac{v_1}{16} + \frac{v_1 - v_2}{2} &= 0 \\ \frac{v_2 - v_1}{2} + \frac{v_2}{20} + \frac{v_2}{80} - 12 &= 0 \end{aligned} \right\} \begin{aligned} v_1 &= 48\text{ V} \\ v_2 &= 64\text{ V} \end{aligned}$$

$$i_1 = \frac{v_1 - v_2}{2} = -8\text{ A}$$

[b] $p_{12A}(\text{del}) = (12)(64) = 768 \text{ W}$

[c] $p_{5A} = 5(48) = 240 \text{ W}$, therefore 5-A source delivers -240 W to the circuit.

DE 4.6 Use the lower node as the reference node. Let v_1 = node voltage across $1\text{-}\Omega$ resistor and v_2 = node voltage across $12\text{-}\Omega$ resistor. Then

$$\left. \begin{aligned} \frac{v_1}{1} + \frac{v_1 - v_2}{8} &= 4.5 \\ \frac{v_2}{12} + \frac{v_2 - v_1}{8} + \frac{v_2 - 30}{4} &= 0 \end{aligned} \right\} \begin{aligned} v_1 &= 6 \text{ V} \\ v_2 &= 18 \text{ V} \\ i &= (v_1 - v_2)/8 = -1.5 \text{ A} \\ v &= v_2 + 2i = 15 \text{ V} \end{aligned}$$

DE 4.7 Use the lower node as the reference node. Let v_1 = node voltage across the $4\text{-}\Omega$ resistor, let v_2 = node voltage across the $20\text{-}\Omega$ resistor. Then

$$\left. \begin{aligned} \frac{v_1}{4} + \frac{v_1 - v_2}{2} + 6i_2 &= 1.5 \\ \frac{v_2}{20} + \frac{v_2 - v_1}{2} - 6i_2 + \frac{v_2 - 80}{5} &= 0 \\ i_2 &= \frac{80 - v_2}{5} \end{aligned} \right\} \begin{aligned} v_1 &= 10 \text{ V} \\ v_2 &= 60 \text{ V} \\ i_2 &= 4 \text{ A} \end{aligned}$$

$$p_{15A} = -1.5v_1 = -15 \text{ W} \quad (\text{delivering})$$

$$p_{80V} = -4(80) = -320 \text{ W} \quad (\text{delivering})$$

$$p_{6i_2} = -6i_2(v_2 - v_1) = -1200 \text{ W} \quad (\text{delivering})$$

DE 4.8 Use the lower node as the reference node. Let v_1 = node voltage across the $7.5\text{-}\Omega$ resistor and v_2 = node voltage across the $2.5\text{-}\Omega$ resistor. Place the dependent voltage source inside a supernode between the node voltages v and v_2 . The node voltage equations are

$$\text{node 1: } \frac{v_1}{7.5} + \frac{v_1 - v}{2.5} = 4.8$$

$$\text{supernode: } \frac{v - v_1}{2.5} + \frac{v}{10} + \frac{v_2}{2.5} + \frac{v_2 - 12}{1} = 0$$

We also have: $v + i_x = v_2$ and $i_x = v_1/7.5$. Solving this set of equations for v gives $v = 8 \text{ V}$.

$$\text{DE 4.9} \quad \frac{v_1 - 150}{25} + \frac{v_1}{80} + \frac{v_1 - (150 - 15i_\phi)}{40} = 0, \quad i_\phi = \frac{150 - v_1}{25}$$

$$\text{Therefore } v_1 = 120 \text{ V}$$

$$\text{DE 4.10} \quad \frac{v_o}{40} + \frac{v_o - 10}{10} + \frac{v_o + 20i_\Delta}{20} = 0, \quad i_\Delta = \frac{10 - v_o}{10} + \frac{10 + 20i_\Delta}{30}$$

$$\text{Therefore } v_o = 24 \text{ V}$$

DE 4.11 Define three clockwise mesh currents i_1 , i_2 , and i_3 in the lower left, upper, and lower right windows. The three mesh-current equations are

$$\begin{aligned}100 &= 45i_1 - 5i_2 - 40i_3 \\0 &= -5i_1 + 35i_2 - 10i_3 \\0 &= -40i_1 - 10i_2 + 65i_3\end{aligned}$$

- [a] Solve for i_1 and get $i_1 = 6$ A, therefore 100-V source is delivering 600 W to the circuit.
[b] Solve for i_3 and get $i_3 = 4$ A, therefore $p_{15\Omega} = (16)(15) = 240$ W.

DE 4.12 [a] $b = 8$, $n = 6$, $b - n + 1 = 3$

[b] $b_e = 6$, $n_e = 4$, $b_e - n_e + 1 = 3$

[c] Define three clockwise mesh currents i_1 , i_2 , and i_3 in the upper, lower left, and lower right windows. The three mesh-current equations are

$$\begin{aligned}-(-3v_\phi) + 19i_1 - 2i_2 - 3i_3 &= 0 \\25 - 10 &= -2i_1 + 7i_2 - 5i_3 \\10 &= -3i_1 - 5i_2 + 9i_3\end{aligned}$$

We also have $v_\phi = 3(i_3 - i_1)$

Solving for i_1 and i_3 gives $i_1 = -1$ A, $i_3 = 3$ A

Therefore $v_\phi = 12$ V and $p_{3v_\phi} = -(-3v_\phi)i_1 = -36$ W

DE 4.13 Let i_a = lower left mesh current cw, let i_b = upper mesh cw current, and i_c = lower right cw mesh current. Then

$$\begin{aligned}15 &= 10(i_a - i_b) + 40(i_a - i_c) \\0 &= 50i_b + 20(i_b - i_c) + 10(i_b - i_a) \\0 &= 40(i_c - i_a) + 20(i_c - i_b) - 40i_\phi \\i_\phi &= i_a, \quad i_a = -1 \text{ A}, \quad i_c = -1.5 \text{ A} \\v_o &= 40(i_a - i_c) = 20 \text{ V}\end{aligned}$$

DE 4.14 Define two mesh currents i_1 and i_2 (clockwise) in the left and center windows of the circuit. Then $30 = 11i_1 - 2i_2$ and $0 = -2i_1 + 19i_2 - 5(-16)$. Solving for i_1 and i_2 gives $i_1 = 2$ A and $i_2 = -4$ A. The current in the $2\text{-}\Omega$ resistor is $i_1 - i_2 = 6$ A, therefore $p_{2\Omega} = (6)^2(2) = 72$ W.

DE 4.15 $20 = (i_a - 30)1 + 2\left(i_a + \frac{v_\phi}{4}\right)$, $v_\phi = 2\left(i_a + \frac{v_\phi}{4}\right)$

Therefore $v_\phi = 4i_a$, $i_a = 10$ A

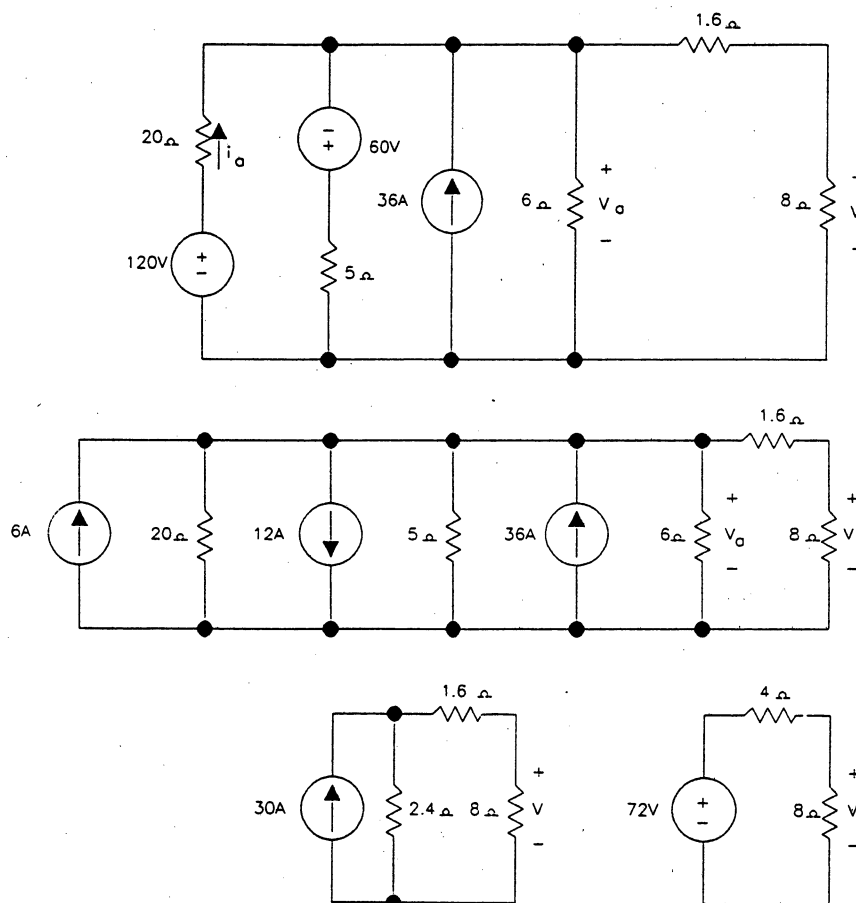
DE 4.16 Let v_1 denote the voltage across the 2-A source. Let v_1 be a voltage rise in the direction of the 2-A current.

$$\frac{v_1 - 20}{15} - 2 + \frac{v_1 - 25}{10} = 0, \quad v_1 = 35 \text{ V}$$

$$p_{2A} = -35(2) = -70 \text{ W}, \quad p_{2A}(\text{del}) = 70 \text{ W}$$

DE 4.17 Define two clockwise mesh currents i_1 and i_2 in the lower left and lower right windows. The two mesh equations are $128 = 12i_1 - 6i_2 - 4(4)$ and $0 = -6i_1 + 14i_2 - 3(4) + 30(i_1 - 4)$. The solutions for i_1 and i_2 are $i_1 = 9 \text{ A}$ and $i_2 = -6 \text{ A}$. The voltage drop across the 4-A source in the direction of the source current is $v_{4A} = 4(i_1 - 4) + 3(i_2 - 4) = 20 - 30 = -10 \text{ V}$, therefore $p_{4A} = 4(-10) = -40 \text{ W}$, therefore $p_{4A}(\text{del}) = 40 \text{ W}$.

DE 4.18

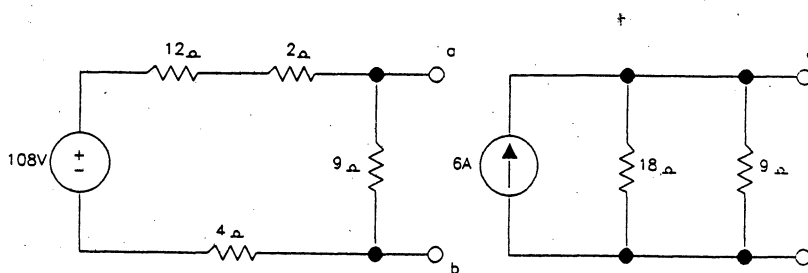


[a] $v = \frac{72}{12}(8) = 48 \text{ V}, \quad i_a = \frac{120 - 57.6}{20} = 3.12 \text{ A}$

[b] $v_a = 6(9.6) = 57.6 \text{ V}, \quad p_{120V}(\text{del}) = 120i_a = 374.40 \text{ W}$

DE 4.19 To find the Thévenin resistance, deactivate the independent voltage source and note that $R_{Th} = 12//[8 + 20//5] = 12//12 = 6\ \Omega$. With the terminals a, b open, the current delivered by the 72-V source is $72/24$ or 3 A. The current (left-to-right) in the 5- Ω resistor is $(20/25)(3) = 2.4$ A, and the current (left-to-right) in the 12- Ω resistor is $(5/25)3$ or 0.6 A. The Thévenin voltage $v_{Th} = v_{ab}$ is the drop across the 8- Ω resistor plus the drop across the 20- Ω resistor. Thus $v_{Th} = (8)(0.6) + (20)(3) = 64.8$ V.

DE 4.20 After one source transformation, the circuit becomes



Therefore $I_N = 6$ A, $R_N = 18//9 = 6\ \Omega$

DE 4.21 Find the Thévenin equivalent with respect to A, B.

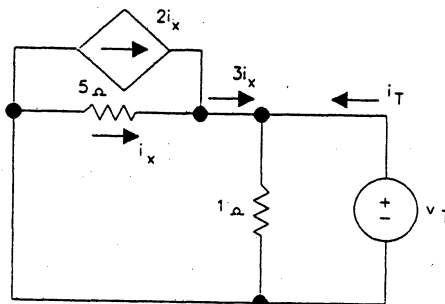
$$\frac{V_{Th} + 36}{12} + \frac{V_{Th}}{60} - 18 = 0, \quad V_{Th} = 150\text{ V}$$

$$R_{Th} = 15 + \frac{(60)(12)}{72} = 25\text{ k}\Omega, \quad \text{therefore } v_{meas} = \frac{150}{125}(100) = 120\text{ V}$$

DE 4.22 Summing the currents away from node a, where $v_{Th} = v_{ab}$, we have

$$\frac{v_{Th}}{1} - 8 - 2i_x + \frac{v_{Th} - 40}{5} = 0, \quad i_x = \frac{40 - v_{Th}}{5}$$

Solving for v_{Th} yields $v_{Th} = 20$ V.



$$v_T = 3i_x + i_T, \quad i_x = -v_T/5$$

Therefore $i_T = 1.6(v_T)$ and $R_{Th} = v_T/i_T = 0.625 \Omega$

DE 4.23 Use the bottom node as the reference. Let v_1 be the node voltage across the 60- Ω resistor. Then

$$\frac{v_1}{60} + \frac{v_1 - (v_{Th} + 160i_\Delta)}{20} - 4 = 0, \quad \frac{v_{Th}}{40} + \frac{v_{Th}}{80} + \frac{v_{Th} + 160i_\Delta - v_1}{20} = 0$$

$$i_\Delta = \frac{v_{Th}}{40}, \quad \text{therefore } v_{Th} = 30 \text{ V}$$

Let i_T be the test current into terminal a:

$$i_T = \frac{v_T}{80} + \frac{v_T}{40} + \frac{v_T + 160(v_T/40)}{80}, \quad \frac{i_T}{v_T} = \frac{1}{10}; \quad \text{therefore } R_{Th} = 10 \Omega$$

DE 4.24 First find the Thévenin equivalent circuit. To find v_{Th} , use the bottom node as the reference. Let $v_{Th} = v_{ab}$ and v_1 = node voltage across the 20-V – 4- Ω branch. The two node-voltage equations are

$$\frac{v_{Th} - 100 - v_\phi}{4} + \frac{v_{Th} - v_1}{4} = 0, \quad (v_\phi = v_1 - 20)$$

$$\frac{v_1 - 100}{4} - \frac{v_1 - 20}{4} + \frac{v_1 - v_{Th}}{4} = 0$$

Solving for v_{Th} gives $v_{Th} = 120 \text{ V}$. To find R_{Th} , deactivate the two independent sources and apply a test voltage source across a, b. Let v_T be positive at a and i_T directed into a. Then the two node-voltage equations are

$$\frac{v_T - v_\phi}{4} + \frac{v_{Th} - v_\phi}{4} = i_T, \quad \frac{v_\phi}{4} + \frac{v_\phi}{4} + \frac{v_\phi - v_T}{4} = 0$$

Therefore $v_\phi = v_T/3$ and $12i_T = 4v_T$

Therefore $R_{Th} = v_T/i_T = 3 \Omega$

[a] For maximum power transfer, $R_L = R_{Th} = 3 \Omega$

[b] $p_{\max} = (120/6)^2(3) = 1200 \text{ W}$

DE 4.25 When $R_L = 3 \Omega$, the voltage across R_L is 60 V. As before, let v_1 be the node voltage across the 20 – V = 4 – Ω branch, then $v_\phi = v_1 - 20$ and

$$\frac{60}{3} + \frac{60 - v_1}{4} + \frac{60 - 100 - v_\phi}{4} = 0$$

Therefore $v_1 = 60 \text{ V}$ and $v_\phi = 40 \text{ V}$. The current out of the plus terminal of the 100-V source is

$$i_1 = \frac{100 - 60}{4} + \frac{100 + 40 - 60}{4} = 10 + 20 = 30 \text{ A}$$

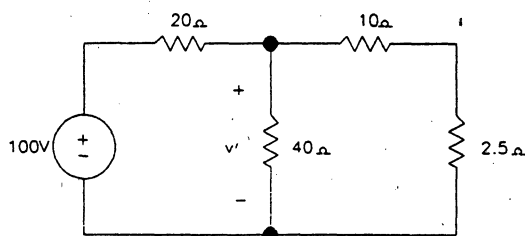
[a] Therefore 100 V is delivering 3000 W to the circuit.

[b] The current out of the plus terminal of the dependent source is 20 A. Therefore the dependent source is delivering 800 W to the circuit.

[c] The load power is $(1200/3800)100$ or 31.58% of this generated power.

DE 4.26 100-V source acting alone:

$$\frac{v'}{40} + \frac{v' - 100}{20} + \frac{v'}{12.5} = 0, \quad v' = \frac{100}{3.1} = 32.26 \text{ V}$$



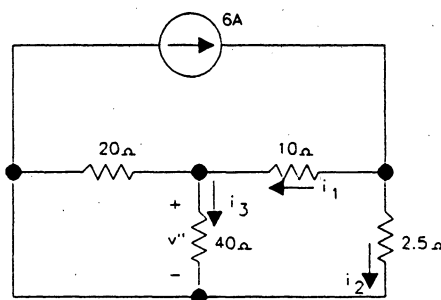
6-A source acting alone:

$$20 // 40 + 10 = \frac{70}{3} \Omega$$

$$\text{Therefore } i_1 = \frac{2.5(6)}{2.5 + 70/3} = \frac{18(2.5)}{77.5}$$

$$i_3 = \frac{20}{60} i_1 = \frac{15}{77.5}$$

$$v'' = 40 i_3 = \frac{600}{77.5} = 7.74 \text{ V}$$



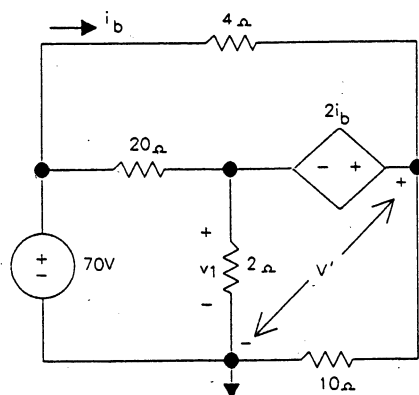
[a] $v = v' = v'' = 32.26 + 7.74 = 40 \text{ V}$

[b] $p_{40\Omega} = \frac{(40)^2}{40} = 40 \text{ W}$

DE 4.27 70-V source acting alone:

$$\frac{v'}{10} + \frac{v' - 70}{4} + \frac{v'_1 - 70}{20} + \frac{v'_1}{2} = 0, \quad i_b = \frac{70 - v'}{4}, \quad v'_1 + 2i'_b = v'$$

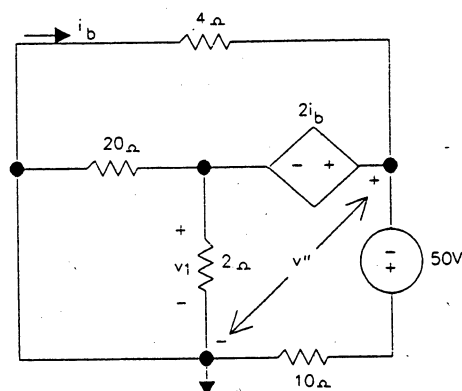
$$\text{Therefore } v' = \frac{805}{23.5} = 34.26 \text{ V}$$



50-V source acting alone:

$$\frac{v_1''}{2} + \frac{v_1''}{20} + \frac{v''}{4} + \frac{v'' + 50}{10} = 0, \quad v'' = v_1'' + 2i_b'', \quad i_b'' = \frac{-v''}{4}$$

$$\text{Therefore } v'' = \frac{-100}{23.5} = -4.6 \text{ V and } v = v' + v'' = 34.26 - 4.26 = 30 \text{ V}$$



Problems

P4.1 [a] Five.

[b] Three.

[c] Sum the currents at any three of the four essential nodes a, b, c, and d. Using nodes a, b, and c we get

$$-i_g + i_1 + i_2 = 0$$

$$-i_1 - i_4 + i_3 = 0$$

$$i_5 - i_2 - i_3 = 0$$

[d] Two.

- [e] Sum the voltages around two independent closed paths, avoiding a path that contains the independent current source since the voltage across the current source is not known. Using the upper and lower meshes formed by the five resistors gives

$$R_1 i_1 + R_3 i_3 - R_2 i_2 = 0$$

$$R_3 i_3 + R_5 i_5 + R_4 i_4 = 0$$

P 4.2 Use the lower terminal of the $25\text{-}\Omega$ resistor as the reference node.

$$\frac{v_o}{25} + 0.04 + \frac{v_o + 25}{125} = 0$$

$$5v_o + 5 + v_o + 25 = 0$$

$$6v_o = -30$$

$$v_o = -5\text{ V}$$

P 4.3 $\frac{v_1}{40} + \frac{v_1 - v_2}{8} = 6$

$$6v_1 - 5v_2 = 240$$

$$\frac{v_2 - v_1}{8} + \frac{v_2}{80} + \frac{v_2}{120} + 1 = 0$$

$$-30v_1 + 35v_2 = -240$$

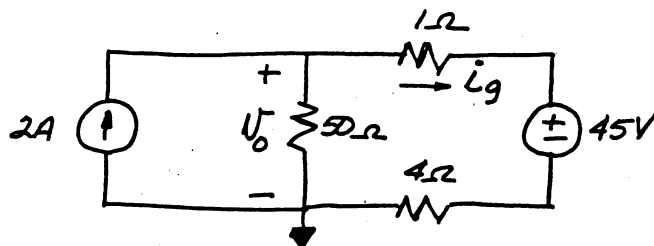
$$\Delta = \begin{vmatrix} 6 & -5 \\ -30 & 35 \end{vmatrix} = 210 - 150 = 60$$

$$N_1 = \begin{vmatrix} 240 & -5 \\ -240 & 35 \end{vmatrix} = 240(35 - 5) = (240)(30)$$

$$N_2 = \begin{vmatrix} 6 & 240 \\ -30 & -240 \end{vmatrix} = 240(-6 + 30) = 240(24)$$

$$v_1 = \frac{N_1}{\Delta} = 120\text{ V}; \quad v_2 = \frac{N_2}{\Delta} = 96\text{ V}$$

P 4.4



$$\frac{v_o}{50} + \frac{v_o - 45}{5} = 2$$

$$11v_o = 100 + 450 = 550$$

$$v_o = 50 \text{ V}$$

$$i_g = \frac{v_o - 45}{5} = 1 \text{ A}$$

$$p_{45\text{V}} = (45)(1) = 45 \text{ W (absorbing)}$$

$$\text{P4.5 } \frac{v_1}{10} + \frac{v_1 - 144}{4} + \frac{v_1 - v_2}{80} = 0$$

$$\frac{v_2 - v_1}{80} - 3 + \frac{v_2}{5} = 0$$

$$\therefore 29v_1 - v_2 = 2880; \quad -v_1 + 17v_2 = 240$$

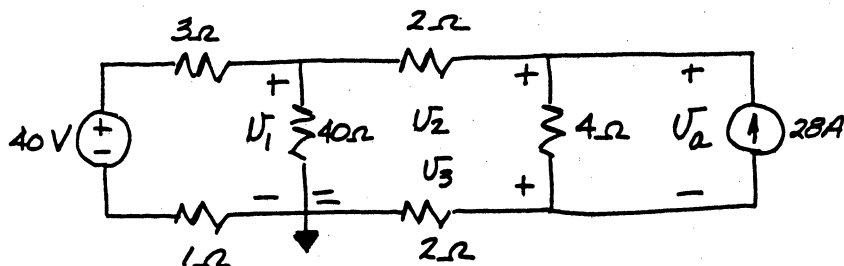
$$\Delta = \begin{vmatrix} 29 & -1 \\ -1 & 17 \end{vmatrix} = 492$$

$$N_1 = \begin{vmatrix} 2880 & -1 \\ 240 & 17 \end{vmatrix} = 49,200$$

$$N_2 = \begin{vmatrix} 29 & 2880 \\ -1 & 240 \end{vmatrix} = 9840$$

$$v_1 = (N_1/\Delta) = 100 \text{ V}; \quad v_2 = (N_2/\Delta) = 20 \text{ V}$$

P4.6 [a]



$$\frac{v_1}{40} + \frac{v_1 - 40}{4} + \frac{v_1 - v_2}{2} = 0$$

$$v_1 + 10v_1 + 20v_1 - 20v_2 = 400$$

$$\boxed{31v_1 - 20v_2 + 0v_3 = 400}$$

$$\frac{v_2 - v_1}{2} + \frac{v_2 - v_3}{4} - 28 = 0$$

$$\boxed{-2v_1 + 3v_2 - v_3 = 112}$$

$$\frac{v_3}{2} + \frac{v_3 - v_2}{4} + 28 = 0$$

$$\boxed{0v_1 - v_2 + 3v_3 = -112}$$

$$\Delta = \begin{vmatrix} 31 & -20 & 0 \\ -2 & 3 & -1 \\ 0 & -1 & 3 \end{vmatrix} = 31(9 - 1) + 2(-60) = 128$$

$$N_1 = \begin{vmatrix} 400 & -20 & 0 \\ 112 & 3 & -1 \\ -112 & -1 & 3 \end{vmatrix} = 1(-400 - 2240) + 3(1200 + 2240) = 7680$$

$$N_2 = \begin{vmatrix} 31 & 400 & 0 \\ -2 & 112 & -1 \\ 0 & -112 & 3 \end{vmatrix} = 31(336 - 112) + 2(1200) = 9344$$

$$N_3 = \begin{vmatrix} 31 & -20 & 400 \\ -2 & 3 & 112 \\ 0 & -1 & -112 \end{vmatrix} = 31(-336 + 112) + 2(2640) = -1664$$

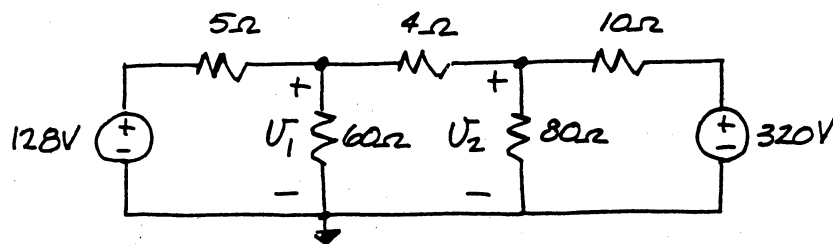
$$v_1 = \frac{N_1}{\Delta} = \frac{7680}{128} = 60 \text{ V}$$

$$v_2 = \frac{N_2}{\Delta} = \frac{9344}{128} = 73 \text{ V}$$

$$v_3 = \frac{N_3}{\Delta} = \frac{-1664}{128} = -13 \text{ V}$$

[b] $v_2 = v_a + v_3$
 $v_a = v_2 - v_3 = 73 - (-13) = 86 \text{ V}$
 $p_{28A} = v_a(28) = (86)(28)$
 $p_{28A} = 2408 \text{ W}$

P4.7 [a]



$$\frac{v_1}{60} + \frac{v_1 - 128}{5} + \frac{v_1 - v_2}{4} = 0$$

$$28v_1 - 15v_2 = 1536$$

$$\frac{v_2}{80} + \frac{v_2 - v_1}{4} + \frac{v_2 - 320}{10} = 10$$

$$-20v_1 + 29v_2 = 2560$$

$$\Delta = \begin{vmatrix} 28 & -15 \\ -20 & 29 \end{vmatrix} = 512$$

$$N_1 = \begin{vmatrix} 1536 & -15 \\ 2560 & 29 \end{vmatrix} = 82,944$$

$$N_2 = \begin{vmatrix} 28 & 1536 \\ -20 & 2560 \end{vmatrix} = 102,400$$

$$v_1 = \frac{N_1}{\Delta} = \frac{82,944}{512} = 162 \text{ V}$$

$$v_2 = \frac{N_2}{\Delta} = \frac{102,400}{512} = 200 \text{ V}$$

$$i_a = \frac{128 - 162}{5} = -6.8 \text{ A}$$

$$i_b = \frac{162}{60} = 2.7 \text{ A}$$

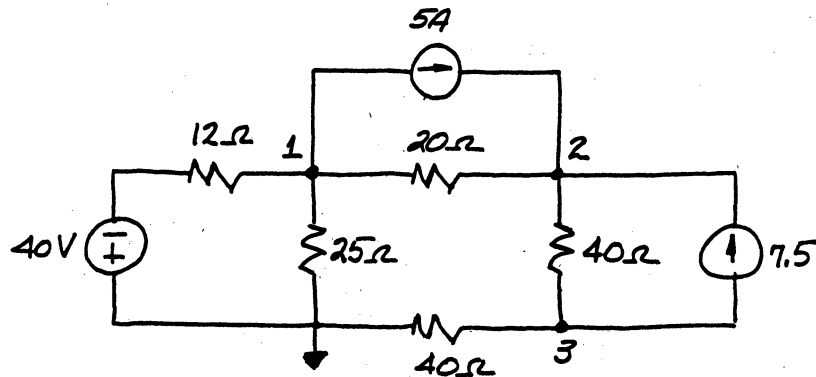
$$i_c = \frac{162 - 200}{4} = -9.5 \text{ A}$$

$$i_d = \frac{200}{80} = 2.5 \text{ A}$$

$$i_e = \frac{200 - 320}{10} = -12 \text{ A}$$

- [b] The only source developing power is the 320-V independent voltage source. Hence the total power developed is $P_{\text{dev}} = (320)(12) = 3840 \text{ W}$.

P4.8



$$\frac{v_1 + 40}{12} + \frac{v_1}{25} + \frac{v_1 - v_2}{20} + 5 = 0$$

$$25v_1 + 1000 + 12v_1 + 15v_1 - 15v_2 + 1500 = 0$$

$$52v_1 - 15v_2 + 0v_3 = -2500$$

$$\frac{v_2 - v_1}{20} + \frac{v_2 - v_3}{40} - 5 - 7.5 = 0$$

$$-2v_1 + 3v_2 - v_3 = 500$$

$$\frac{v_3}{40} + \frac{v_3 - v_2}{40} + 7.5 = 0$$

$$0v_1 - v_2 + 2v_3 = -300$$

$$\Delta = \begin{vmatrix} 52 & -15 & 0 \\ -2 & 3 & -1 \\ 0 & -1 & 2 \end{vmatrix} = 52(6 - 1) + 2(-30) = 200$$

$$N_1 = \begin{vmatrix} -2500 & -15 & 0 \\ 500 & 3 & -1 \\ -300 & -1 & 2 \end{vmatrix} = 1(2500 - 4500) + 2(-7500 + 7500) = -2000$$

$$N_2 = \begin{vmatrix} 52 & -2500 & 0 \\ -2 & 500 & -1 \\ 0 & -300 & 2 \end{vmatrix} = 52(1000 - 300) + 2(-5000) = 26,400$$

$$N_3 = \begin{vmatrix} 52 & -15 & -2500 \\ -2 & 3 & 500 \\ 0 & -1 & -300 \end{vmatrix} = 52(-900 + 500) + 2(4500 - 2500) \\ = 52(-400) + 4000 = -20,800 + 4000 = -16,800$$

$$v_1 = \frac{N_1}{\Delta} = \frac{-2000}{200} = -10 \text{ V}$$

$$v_2 = \frac{N_2}{\Delta} = \frac{26,400}{200} = 132 \text{ V}$$

$$v_3 = \frac{N_3}{\Delta} = \frac{-16,800}{200} = -84 \text{ V}$$

Now observe all three independent sources are developing power.

The current into the negative terminal of the voltage source is

$$i_g = \frac{-10 + 40}{12} = 2.5 \text{ A}$$

$$p_{40\text{V}} = -(2.5)(40) = -100 \text{ W (dev)}$$

The voltage rise across the 5-A source is

$$v_{5\text{A}} = 132 - (-10) = 142 \text{ V}$$

$$p_{5\text{A}} = -5(142) = -710 \text{ W (dev)}$$

The voltage rise across the 7.5-A source is

$$v_{7.5\text{A}} = 132 - (-84) = 216 \text{ V}$$

$$p_{7.5\text{A}} = -7.5(216) = -1620 \text{ W (dev)}$$

$$\sum P_{\text{dev}} = \sum P_{\text{diss}} = 100 + 710 + 1620 = 2430 \text{ W}$$

Check:

$$p_{12\Omega} = (2.5)^2(12) = 75 \text{ W}$$

$$p_{25\Omega} = \frac{(10)^2}{25} = 4 \text{ W}$$

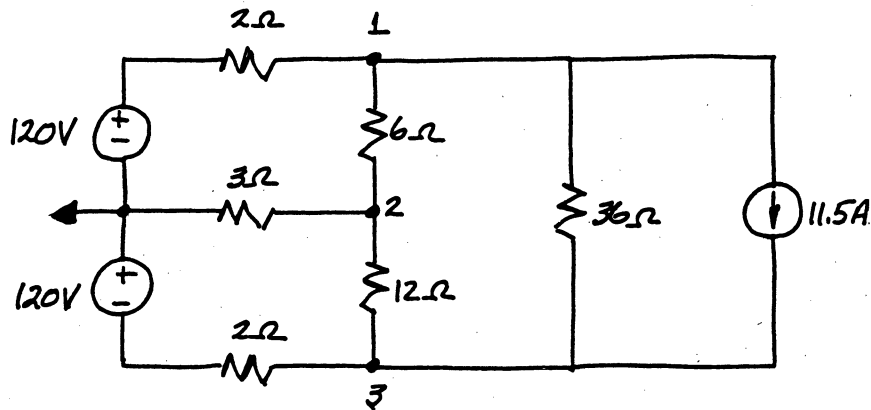
$$p_{20\Omega} = \frac{(142)^2}{20} = 1008.2 \text{ W}$$

$$p_{40\Omega} = \frac{(216)^2}{40} = 1166.4 \text{ W}$$

$$p_{40\Omega} = \frac{(84)^2}{40} = 176.4 \text{ W}$$

$$\sum P_{\text{diss}} = 2430 \text{ W}$$

P4.9 [a]



$$\frac{v_1 - 120}{2} + \frac{v_1 - v_2}{6} + \frac{v_1 - v_3}{36} + 11.5 = 0$$

$$18v_1 - 2160 + 6v_1 - 6v_2 + v_1 - v_3 + 414 = 0$$

$$25v_1 - 6v_2 - v_3 = 1746$$

$$\frac{v_2 - v_1}{6} + \frac{v_2}{3} + \frac{v_2 - v_3}{12} = 0$$

$$2v_2 - 2v_1 + 4v_2 + v_2 - v_3 = 0$$

$$-2v_1 + 7v_2 - v_3 = 0$$

$$\frac{v_3 + 120}{2} + \frac{v_3 - v_2}{12} + \frac{v_3 - v_1}{36} - 11.5 = 0$$

$$18v_3 + 2160 + 3v_3 - 3v_2 + v_3 - v_1 - 414 = 0$$

$$-v_1 - 3v_2 + 22v_3 = -1746$$

$$\Delta = \begin{vmatrix} 25 & -6 & -1 \\ -2 & 7 & -1 \\ -1 & -3 & 22 \end{vmatrix} = 25(151) + 2(-135) - 1(13) = 3492$$

$$N_1 = \begin{vmatrix} 1746 & -6 & -1 \\ 0 & 7 & -1 \\ -1746 & -3 & 22 \end{vmatrix} = 1746(151) - 1746(13) = 240,948$$

$$N_2 = \begin{vmatrix} 25 & 1746 & -1 \\ -2 & 0 & -1 \\ -1 & -1746 & 22 \end{vmatrix} = -1746(-45) + 1746(-27) = 31,428$$

$$N_3 = \begin{vmatrix} 25 & -6 & 1746 \\ -2 & 7 & 0 \\ -1 & -3 & -1746 \end{vmatrix} = 1746(13) - 1746(163) = -261,900$$

$$v_1 = \frac{N_1}{\Delta} = \frac{240,948}{3492} = 69 \text{ V}$$

$$v_2 = \frac{N_2}{\Delta} = \frac{31,428}{3492} = 9 \text{ V}$$

$$v_3 = \frac{N_3}{\Delta} = \frac{-261,900}{3492} = -75 \text{ V}$$

$$i_1 = \frac{120 - v_1}{2} = \frac{120 - 69}{2} = 25.50 \text{ A}$$

$$i_2 = \frac{v_2}{3} = \frac{9}{3} = 3 \text{ A}$$

$$i_3 = \frac{v_3 + 120}{2} = \frac{-75 + 120}{2} = 22.5 \text{ A}$$

$$i_4 = \frac{v_1 - v_2}{6} = \frac{69 - 9}{6} = 10 \text{ A}$$

$$i_5 = \frac{v_2 - v_3}{12} = \frac{9 + 75}{12} = 7 \text{ A}$$

$$i_6 = \frac{v_1 - v_3}{36} = \frac{69 + 75}{36} = 4 \text{ A}$$

$$[b] \quad P_{120V \text{ upper}} = -120(25.5) = -3060 \text{ W} \quad (\text{dev})$$

$$P_{120V \text{ lower}} = -120(22.5) = -2700 \text{ W} \quad (\text{dev})$$

$$P_{11.5A} = (36)(4)(11.5) = 1656 \text{ W} \quad (\text{diss})$$

$$P_{2\Omega(\text{upper})} = (25.5)^2(2) = 1300.5 \text{ W} \quad (\text{diss})$$

$$P_{3\Omega} = (3)^2(3) = 27 \text{ W} \quad (\text{diss})$$

$$P_{2\Omega(\text{lower})} = (22.5)^2(2) = 1012.50 \text{ W} \quad (\text{diss})$$

$$P_{6\Omega} = (10)^2(6) = 600 \text{ W}$$

$$P_{12\Omega} = (7)^2(12) = 588 \text{ W}$$

$$P_{36\Omega} = (4)^2(36) = 576 \text{ W}$$

$$\sum P_{\text{dev}} = 5760 \text{ W}$$

$$\sum P_{\text{diss}} = 5760 \text{ W}$$

P4.10 Let v_2 be the node voltage across the $150\text{-}\Omega$ resistor, positive at the upper terminal.

Then $2 + \frac{v_1}{50} + \frac{v_2}{150} + \frac{v_2}{75} = 0$ Note we have created a super node in writing this expression.

$$300 + 3v_1 + v_2 + 2v_2 = 0$$

$$3v_1 + 3v_2 = -300$$

$$v_1 + v_2 = -100$$

$$v_1 = v_2 + 25$$

$$\therefore 2v_2 = -125$$

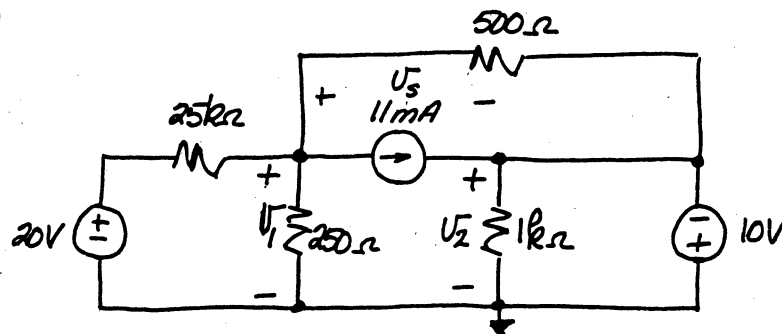
$$v_2 = -62.5 \text{ V}$$

$$v_1 = -37.5 \text{ V}$$

$$p_{2A} = 2v_1 = -75 \text{ W}$$

$$\therefore p_{2A(\text{del})} = 75 \text{ W}$$

P4.11 [a]



$$\frac{v_1}{0.25} + \frac{v_1 - 20}{25} + \frac{v_1 + 10}{0.50} + 11 = 0$$

$$100v_1 + v_1 - 20 + 50v_1 + 500 + 275 = 0$$

$$151v_1 = -755$$

$$v_1 = -5 \text{ V}$$

$$i_1 = \frac{20 - v_1}{25} = \frac{20 + 5}{25} = 1 \text{ mA}$$

$$i_2 = \frac{v_1}{0.25} = \frac{-5}{0.25} = -20 \text{ mA}$$

$$i_3 + \frac{v_2}{1} - 11 + \frac{v_2 - v_1}{0.5} = 0$$

$$i_3 = 11 - v_2 + \frac{v_1 - v_2}{0.5}$$

$$i_3 = 11 - (-10) + \frac{(-5 + 10)}{0.5} = 31 \text{ mA}$$

$$[b] \quad p_{20\text{V}} = -20i_1 = -20 \text{ mW} \quad (\text{del})$$

$$p_{10\text{V}} = -10i_3 = -310 \text{ mW} \quad (\text{del})$$

$$v_1 = v_s + v_2, \quad v_s = v_1 - v_2 = -5 + 10 = 5 \text{ V}$$

$$p_{11 \text{ mA}} = 11v_s = 55 \text{ mW} \quad (\text{abs})$$

$$p_{1 \text{ k}\Omega} = 10^2/1000 = 100 \text{ mW}$$

$$p_{25 \text{ k}\Omega} = (10^{-3})^2(25 \times 10^3) = 25 \text{ mW}$$

$$p_{250\Omega} = (20 \times 10^{-3})^2(0.25 \times 10^3) = 100 \text{ mW}$$

$$p_{500\Omega} = \frac{v_s^2}{500} = \frac{25}{0.50} = 50 \text{ mW}$$

$$\sum P_{\text{dev}} = 330 \text{ mW}$$

$$\sum P_{\text{diss}} = 55 + 25 + 200 + 50 = 330 \text{ mW}$$

P 4.12 [a] From the solution to Problem 4.2 we know $v_o = -5 \text{ V}$, therefore

$$p_{40 \text{ mA}} = 40 \times 10^{-3} v_o = -200 \text{ mW}$$

$$\therefore p_{40 \text{ mA}}(\text{developed}) = 200 \text{ mW}$$

[b] The current into the negative terminal of the 25-V source is

$$i_g = \frac{v_o + 25}{125} = \frac{20}{125} = 160 \text{ mA}$$

$$p_{25\text{V}} = -25i_g = -4000 \text{ mW}$$

$$\therefore p_{25\text{V}}(\text{developed}) = 4000 \text{ mW}$$

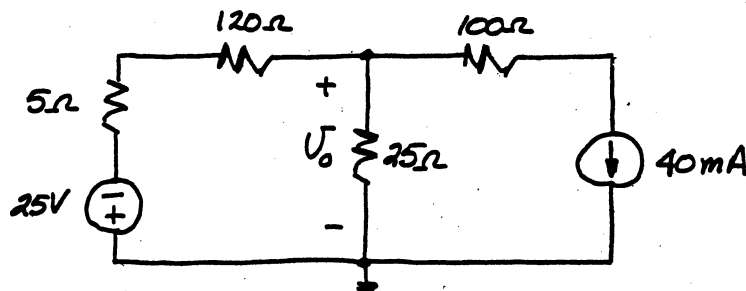
$$[c] \quad p_{25\Omega} = \frac{(-5)^2}{25} = 1 \text{ W} = 1000 \text{ mW}$$

$$p_{120\Omega} = 120i_g^2 = 3072 \text{ mW}$$

$$p_{5\Omega} = 5i_g^2 = 128 \text{ mW}$$

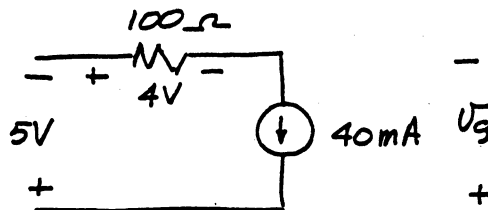
$$\sum P_{\text{diss}} = 4200 \text{ mW} = \sum P_{\text{dev}}$$

P4.13 [a]



$$\begin{aligned}\frac{v_o}{25} + \frac{v_o + 25}{125} + 0.04 &= 0 \\ 5v_o + v_o + 25 + 5 &= 0 \\ 6v_o &= -30; \quad v_o = -5 \text{ V}\end{aligned}$$

[b]



$$\begin{aligned}v_g &= +5 + 4 = 9 \text{ V} \\ p_{40 \text{ mA}} &= -40 \times 10^{-3} v_g = -360 \text{ mW} \\ \therefore p_{40 \text{ mA}}(\text{developed}) &= 360 \text{ mW}\end{aligned}$$

- [c] Since v_o is identical to its value in Problem 4.2, the 25-V voltage source develops the same power as calculated in Problem 4.12[b]:

$$P_{25\text{-V}}(\text{developed}) = 4000 \text{ mW}$$

- [d] The power dissipated in the 5-Ω, 120-Ω, and 25-Ω is the same as in Problem 4.12[c]; thus

$$\begin{aligned}p_{5\Omega} &= 128 \text{ mW} & \sum P_{\text{diss}} &= 4360 \text{ mW} \\ p_{120\Omega} &= 3072 \text{ mW} & \sum P_{\text{dev}} &= 4360 \text{ mW} \\ p_{25\Omega} &= 1000 \text{ mW} & \therefore \sum P_{\text{diss}} &= \sum P_{\text{dev}} \\ p_{100\Omega} &= (40 \times 10^{-3})^2 100 = 160 \text{ mW}\end{aligned}$$

- [e] None, since the node-voltage equation is not affected by such a resistance.

P4.14 Use d as the reference node

$$\begin{aligned}\frac{v_b}{10} + \frac{v_b - 33}{20} + \frac{v_b - v_c}{8} &= 0 \\ \frac{v_c - v_b}{8} - 4.95 + \frac{v_c}{26.4} + \frac{v_c - 33}{198} &= 0\end{aligned}$$

$$4v_b + 2v_b - 66 + 5v_b - 5v_c = 0$$

$$24.75v_c - 24.75v_b + 7.5v_c + v_c - 33 = 980.10$$

$$11v_b - 5v_c = 66$$

$$-24.75v_b + 33.25v_c = 980.10 + 33 = 1013.10$$

$$\Delta = \begin{vmatrix} 11 & -5 \\ -24.75 & 33.25 \end{vmatrix} = 242$$

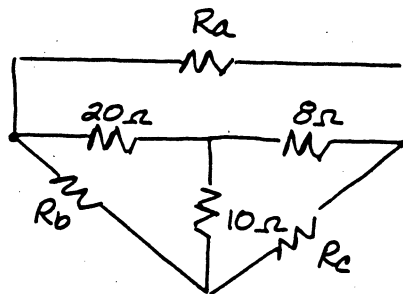
$$N_c = \begin{vmatrix} 11 & 66 \\ -24.75 & 1013.10 \end{vmatrix} = 12,777.60$$

$$v_c = \frac{N_c}{\Delta} = \frac{12,777.60}{242} = 52.80 \text{ V}$$

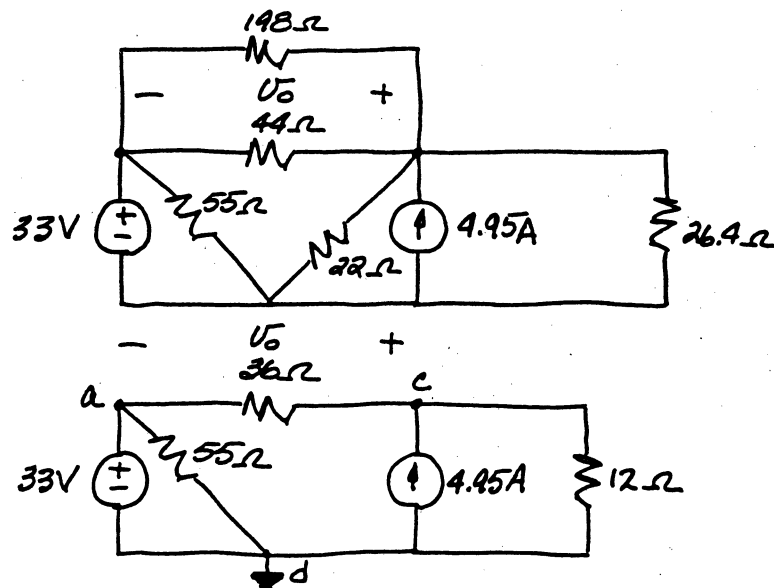
$$33 + v_o = 52.80$$

$$v_o = 19.80 \text{ V}$$

P4.15



$$R_a = \frac{(20)(8) + 8(10) + 10(20)}{10} = 44 \Omega; \quad R_b = \frac{440}{8} = 55 \Omega; \quad R_c = \frac{440}{20} = 22 \Omega$$



$$\frac{v_c}{12} - 4.95 + \frac{v_c - 33}{36} = 0$$

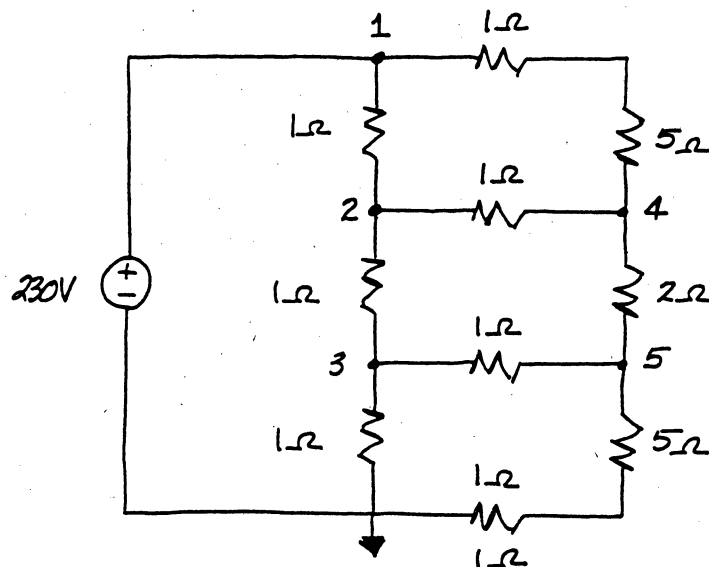
$$3v_c + v_c = 33 + 178.20$$

$$4v_c = 211.20$$

$$v_c = 52.80 \text{ V}$$

$$\therefore v_o = 52.80 - 33 = 19.8 \text{ V}$$

P4.16 [a]



$$\frac{v_2 - 230}{1} + \frac{v_2 - v_4}{1} + \frac{v_2 - v_3}{1} = 0$$

$$\frac{v_3 - v_2}{1} + \frac{v_3}{1} + \frac{v_3 - v_5}{1} = 0$$

$$\frac{v_4 - v_2}{1} + \frac{v_4 - 230}{6} + \frac{v_4 - v_5}{2} = 0$$

$$\frac{v_5 - v_3}{1} + \frac{v_5}{6} + \frac{v_5 - v_4}{2} = 0$$

$$3v_2 - v_3 - v_4 + 0v_5 = 230$$

$$-v_2 + 3v_3 + 0v_4 - v_5 = 0$$

$$-6v_2 + 0v_3 + 10v_4 - 3v_5 = 230$$

$$0v_2 - 6v_3 - 3v_4 + 10v_5 = 0$$

$$\Delta = \begin{vmatrix} 3 & -1 & -1 & 0 \\ -1 & 3 & 0 & -1 \\ -6 & 0 & 10 & -3 \\ 0 & -6 & 3 & 10 \end{vmatrix}$$

$$= 3 \begin{vmatrix} 3 & 0 & -1 \\ 0 & 10 & -3 \\ -6 & -3 & 10 \end{vmatrix} + 1 \begin{vmatrix} -1 & -1 & 0 \\ 0 & 10 & -3 \\ -6 & -3 & 10 \end{vmatrix} - 6 \begin{vmatrix} -1 & -1 & 0 \\ 3 & 0 & -1 \\ -6 & -3 & 10 \end{vmatrix}$$

$$= 3[(3)(91) - (6)(10)] + 1[(-1)(91) - (6)(3)] - 6[(1)(-3) + (10)(3)]$$

$$= (3)(213) - 109 - (6)(27) = 368$$

$$N_2 = \begin{vmatrix} 230 & -1 & -1 & 0 \\ 0 & 3 & 0 & -1 \\ 230 & 0 & 10 & -3 \\ 0 & -6 & -3 & 10 \end{vmatrix}$$

$$= 230(213) + 230(27) = (230)(240) = 55,200$$

$$N_3 = \begin{vmatrix} 3 & 230 & -1 & 0 \\ -1 & 0 & 0 & -1 \\ -6 & 230 & 10 & -3 \\ 0 & 0 & -3 & 10 \end{vmatrix} = -230 \begin{vmatrix} -1 & 0 & -1 \\ -6 & 10 & -3 \\ 0 & -3 & 10 \end{vmatrix} - 230 \begin{vmatrix} 3 & -1 & 0 \\ -1 & 0 & -1 \\ 0 & -3 & 10 \end{vmatrix}$$

$$= -230 [(-1)(91) + (6)(-3)] - 230 [(3)(-3) + 1(-10)]$$

$$= -230(-109) - 230(-19) = 230(128) = 29,440$$

$$N_4 = \begin{vmatrix} 3 & -1 & 230 & 0 \\ -1 & 3 & 0 & -1 \\ -6 & 0 & 230 & -3 \\ 0 & -6 & 0 & 10 \end{vmatrix} = 230 \begin{vmatrix} -1 & 3 & -1 \\ -6 & 0 & -3 \\ 0 & -6 & 10 \end{vmatrix} + 230 \begin{vmatrix} 3 & -1 & 0 \\ -1 & 3 & -1 \\ 0 & -6 & 10 \end{vmatrix}$$

$$= 230 [(-1)(-18) + (6)(24)] + 230 [(3)(24) + (1)(-10)]$$

$$= 230(162) + 230(62) = 230(224) = 51,520$$

$$N_5 = \begin{vmatrix} 3 & -1 & -1 & 230 \\ -1 & 3 & 0 & 0 \\ -6 & 0 & 10 & 230 \\ 0 & -6 & -3 & 0 \end{vmatrix} = -230 \begin{vmatrix} -1 & 3 & 0 \\ -6 & 0 & 10 \\ 0 & -6 & -3 \end{vmatrix} - 230 \begin{vmatrix} 3 & -1 & -1 \\ -1 & 3 & 0 \\ 0 & -6 & -3 \end{vmatrix}$$

$$= -230 [(-1)(60) + (6)(-9)] - 230 [(3)(-9) + (1)(-3)]$$

$$= -230(-114) - 230(-30) = 230(144) = 33,120$$

Therefore

$$v_2 = \frac{N_2}{\Delta} = \frac{55,200}{368} = 150 \text{ V}$$

$$v_3 = \frac{N_3}{\Delta} = \frac{29,440}{368} = 80 \text{ V}$$

$$v_4 = \frac{N_4}{\Delta} = \frac{51,520}{368} = 140 \text{ V}$$

$$v_5 = \frac{N_5}{\Delta} = \frac{33,120}{368} = 90 \text{ V}$$

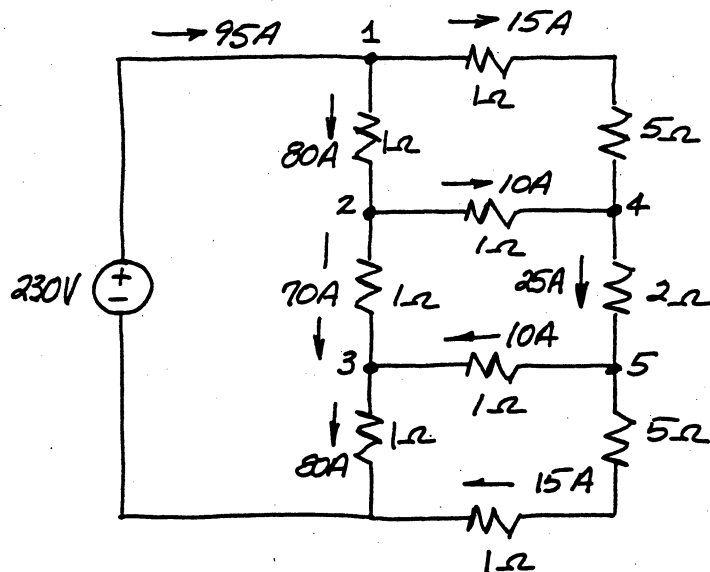
$$i_{2\Omega} = \frac{v_4 - v_5}{2} = \frac{140 - 90}{2} = 25 \text{ A}$$

$$p_{2\Omega} = (25)^2(2) = 1250 \text{ W}$$

$$[b] \quad i_{230V} = \frac{v_1 - v_2}{1} + \frac{v_1 - v_4}{6} = \frac{230 - 150}{1} + \frac{230 - 140}{6} = 80 + 15 = 95$$

$$p_{230V} = 21,850 \text{ W}$$

Check:



$$\begin{aligned}\sum P_{\text{diss}} &= (80)^2(1) + (70)^2(1) + (80)^2(1) + (15)^2(6) + (10)^2(1) + (25)^2(2) \\ &\quad + (10)^2(1) + (15)^2(6) \\ &= 6400 + 4900 + 6400 + 1350 + 100 + 1250 + 100 + 1350 = 21,850 \text{ W}\end{aligned}$$

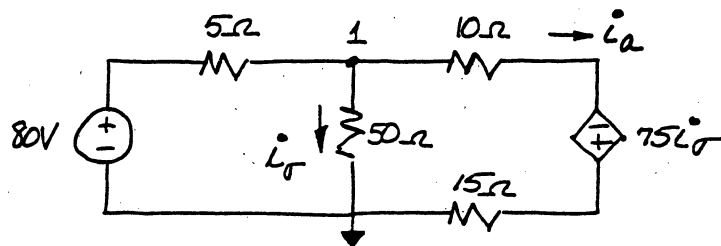
P4.17 $\frac{v_o - 186}{22} + \frac{v_o + 1.6i_\Delta}{14} + \frac{v_o + 43}{2} = 0$

$$i_\Delta = \frac{v_o + 43}{2}, \quad 1.6i_\Delta = 0.8v_o + 34.40$$

$$14v_o - 2604 + 22v_o + 17.6v_o + 756.80 + 154v_o + 6622 = 0$$

$$207.60v_o = -4774.8$$

$$v_o = -23 \text{ V}$$

P4.18

$$\frac{v_1 - 80}{5} + \frac{v_1}{50} + \frac{v_1 + 75i_\sigma}{25} = 0$$

$$i_\sigma = \frac{v_1}{50}, \quad 75i_\sigma = 1.5v_1$$

$$10v_1 - 800 + v_1 + 5v_1 = 0$$

$$16v_1 = 800$$

$$v_1 = 50 \text{ V}$$

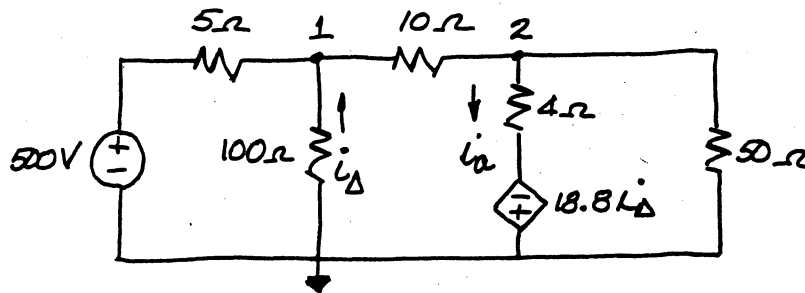
$$i_\sigma = \frac{50}{50} = 1 \text{ A}$$

$$i_a = \frac{v_1 + 75i_\sigma}{25} = \frac{125}{25} = 5 \text{ A}$$

$$p_{75i_\sigma} = -75i_\sigma i_a = -(75)(5) = -375 \text{ W}$$

$\therefore$ The dependent voltage source delivers 375 W to the circuit.

P4.19



$$\frac{v_1 - 500}{5} + \frac{v_1}{100} + \frac{v_1 - v_2}{10} = 0$$

$$\boxed{31v_1 - 10v_2 = 10,000}$$

$$\frac{v_2 - v_1}{10} + \frac{v_2 + 18.8(-v_1/100)}{4} + \frac{v_2}{50} = 0$$

$$\boxed{-14.7v_1 + 37v_2 = 0}$$

$$\Delta = \begin{vmatrix} 31 & -10 \\ -14.7 & 37 \end{vmatrix} = 1147 - 147 = 1000$$

$$N_1 = \begin{vmatrix} 10,000 & -10 \\ 0 & 37 \end{vmatrix} = 37 \times 10^4$$

$$N_2 = \begin{vmatrix} 31 & 10,000 \\ -14.7 & 0 \end{vmatrix} = 147 \times 10^3$$

$$v_1 = \frac{N_1}{\Delta} = \frac{37 \times 10^4}{1000} = 370 \text{ V}$$

$$v_2 = \frac{N_2}{\Delta} = \frac{147 \times 10^3}{1000} = 147 \text{ V}$$

$$i_\Delta = \frac{-v_1}{100} = -3.7 \text{ A}$$

$$18.8i_\Delta = -69.56 \text{ V}$$

$$i_a = \frac{v_2 + 18.8i_\Delta}{4} = \frac{147 - 69.56}{4} = 19.36 \text{ A}$$

$$p_{18.8i_\Delta} = -(18.8i_\Delta)(i_a) = -(-69.56)(19.36) = 1346.6816 \text{ W}$$

Therefore the dependent voltage source dissipates 1346.6816 W, or delivers -1346.6816 W.

P4.20 Place $5v_\Delta$ inside a supernode and use the lower node as a reference. Then

$$\begin{aligned}\frac{v_\Delta}{2} + \frac{v_\Delta - 15}{10} + \frac{v_1}{20} + \frac{v_1}{40} &= 0 \\ 20v_\Delta + 4v_\Delta - 60 + 2v_1 + v_1 &= 0 \\ v_\Delta = 5v_\Delta + v_1, \quad \therefore v_1 &= -4v_\Delta \\ \therefore 24v_\Delta + 3(-4v_\Delta) &= 60 \\ 12v_\Delta &= 60; \quad v_\Delta = 5 \text{ V}\end{aligned}$$

P4.21 [a] $-5\left(\frac{v_2}{40}\right) + \frac{v_1}{20} + \frac{v_1 - v_2}{5} = 0$

$$-5v_2 + 2v_1 + 8v_1 - 8v_2 = 0$$

$$\boxed{10v_1 - 13v_2 + 0v_3 = 0}$$

$$\frac{v_2}{40} + \frac{v_2 - v_1}{5} + \frac{v_2 - v_3}{10} = 0$$

$$v_2 + 8v_2 - 8v_1 + 4v_2 - 4v_3 = 0$$

$$\boxed{-8v_1 + 13v_2 - 4v_3 = 0}$$

$$\frac{v_3 - v_2}{10} + \frac{v_3 - 11.5(v_2/40)}{5} + \frac{v_3 - 96}{4} = 0$$

$$20v_3 - 20v_2 + 40v_3 - 11.5v_2 + 50v_3 = 4800$$

$$\boxed{0v_1 - 63v_2 + 220v_3 = 9600}$$

$$\Delta = \begin{vmatrix} 10 & -13 & 0 \\ -8 & 13 & -4 \\ 0 & -63 & 220 \end{vmatrix} = 10(2860 - 252) + 8(-2860) = 3200$$

$$N_1 = \begin{vmatrix} 0 & -13 & 0 \\ 0 & 13 & -4 \\ 9600 & -63 & 220 \end{vmatrix} = 9600(52)$$

$$N_2 = \begin{vmatrix} 10 & 0 & 0 \\ -8 & 0 & -4 \\ 0 & 9600 & 220 \end{vmatrix} = -9600(-40) = 9600(40)$$

$$N_3 = \begin{vmatrix} 10 & -13 & 0 \\ -8 & 13 & 0 \\ 0 & -63 & 9600 \end{vmatrix} = 9600(130 - 104) = 9600(26)$$

$$v_1 = \frac{N_1}{\Delta} = 156 \text{ V}; \quad v_2 = \frac{N_2}{\Delta} = 120 \text{ V}; \quad v_3 = \frac{N_3}{\Delta} = 78 \text{ V}$$

[b] From the numerical values of v_1 , v_2 , and v_3 we note the independent voltage source and the dependent current source will generate power. All other elements dissipate power. Thus

$$\begin{aligned}\sum P_{\text{gen}} &= \left(\frac{96 - 78}{4}\right)(96) + 5\left(\frac{120}{40}\right)(156) = (4.5)(96) + 15(156) \\ &= 432 + 2340 = 2772 \text{ W}\end{aligned}$$

$$\sum P_{\text{diss}} = \sum P_{\text{gen}} = 2772 \text{ W}$$

P 4.22 For the given values of v_3 and v_4 we have

$$v_{\Delta} = 120 - v_3 = 120 - 108 = 12 \text{ V}$$

$$1.75v_{\Delta} = 21 \text{ A}$$

$$i_{\phi} = \frac{v_4 - v_3}{8} = \frac{81.60 - 108}{8} = -3.3 \text{ A}$$

$$\left(\frac{40}{3}\right) i_{\phi} = -44 \text{ V}$$

$$v_1 = v_4 + \left(\frac{40}{3}\right) i_{\phi} = 81.60 - 44 = 37.60 \text{ V}$$

Let i_a be the current in the dependent voltage source. The reference direction for i_a is from right to left. Then

$$i_a = \frac{v_1}{20} + \frac{v_1 - v_2}{4} = \frac{37.60}{20} + \frac{37.60 - 120}{4} = 1.88 - 20.60 = -18.72 \text{ A}$$

Let i_b be the current supplied by the 120-V source, then

$$i_b = \frac{120 - 37.60}{4} + \frac{120 - 108}{2} = 20.60 + 6 = 26.60 \text{ A}$$

The power developed by the independent voltage source is

$$p_{120\text{V}} = (120)(26.60) = 3192 \text{ W}$$

The power developed by the dependent voltage source is

$$p_{(40/3)i_{\phi}} = (44)(18.72) = 823.68 \text{ W}$$

The power dissipated by the dependent current source is

$$p_{1.75v_{\Delta}} = (81.60)(21) = 1713.60 \text{ W}$$

The total power dissipated in the resistors is

$$p_R = \frac{(37.6)^2}{20} + \frac{(82.40)^2}{4} + \frac{(12)^2}{2} + \frac{(108)^2}{40} + (3.3)^2(8) + \frac{(81.60)^2}{80} = 2302.08 \text{ W}$$

Therefore

$$\sum P_{\text{dev}} = 3192 + 823.68 = 4015.68 \text{ W}$$

$$\sum P_{\text{diss}} = 2302.08 + 1713.60 = 4015.68$$

Her solution checks; yes, I agree.

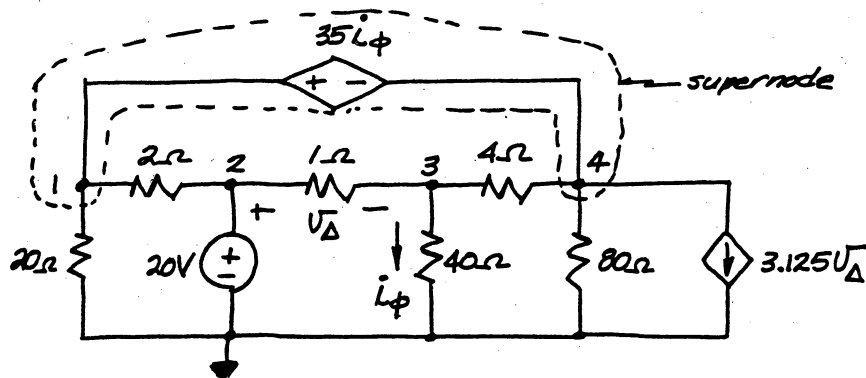
P 4.23 From Eq. 4.16, $i_B = v_c / (1 + \beta)R_E$

From Eq. 4.17, $i_B = (v_b - V_o) / (1 + \beta)R_E$

From Eq. 4.19,

$$\begin{aligned} i_B &= \frac{1}{(1 + \beta)R_E} \left[\frac{V_{CC}(1 + \beta)R_ER_2 + V_oR_1R_2}{R_1R_2 + (1 + \beta)R_E(R_1 + R_2)} - V_o \right] \\ &= \frac{V_{CC}R_2 - V_o(R_1 + R_2)}{R_1R_2 + (1 + \beta)R_E(R_1 + R_2)} = \frac{[V_{CC}R_2 / (R_1 + R_2)] - V_o}{[R_1R_2 / (R_1 + R_2)] + (1 + \beta)R_E} \end{aligned}$$

P4.24



$$\frac{v_1}{20} + \frac{v_1 - 20}{2} + \frac{v_4}{80} + \frac{v_4 - v_3}{4} + 3.125v_\Delta = 0$$

$$\frac{v_3}{40} + \frac{v_3 - 20}{1} + \frac{v_3 - v_4}{4} = 0$$

$$v_\Delta = 20 - v_3; \quad i_\phi = \frac{v_3}{40}$$

$$v_1 = 35i_\phi + v_4 = \frac{35}{40}v_3 + v_4$$

$$4v_1 + 40v_1 - 800 + v_4 + 20v_4 - 20v_3 + 250(20 - v_3) = 0$$

$$44v_1 - 270v_3 + 21v_4 = -4200$$

$$44\left(\frac{35}{40}v_3 + v_4\right) - 270v_3 + 21v_4 = -4200$$

$$\boxed{-231.50v_3 + 65v_4 = -4200}$$

$$v_3 + 40v_3 - 800 + 10v_3 - 10v_4 = 0$$

$$\boxed{51v_3 - 10v_4 = 800}$$

$$\Delta = \begin{vmatrix} -231.50 & 65 \\ 51 & -10 \end{vmatrix} = -1000$$

$$N_3 = \begin{vmatrix} -4200 & 65 \\ 800 & -10 \end{vmatrix} = -10,000$$

$$N_4 = \begin{vmatrix} -231.50 & -4200 \\ 51 & 800 \end{vmatrix} = 29,000$$

$$v_3 = \frac{N_3}{\Delta} = \frac{-10,000}{-1000} = 10 \text{ V}$$

$$v_4 = \frac{N_4}{\Delta} = \frac{29,000}{-1000} = -29 \text{ V}$$

$$v_1 = \frac{350}{40} - 29 = -20.25 \text{ V}$$

Let i_g be the current delivered by the 20-V source, then

$$i_g = \frac{20 - v_1}{2} + \frac{20 - v_3}{1} = \frac{40.25}{2} + 10 = 30.125 \text{ A}$$

$$p_g(\text{delivered}) = 20(30.125) = 602.50 \text{ W}$$

Check:

$$i_\phi = \frac{10}{40} = 0.25 \text{ A}, \quad 35i_\phi = 8.75 \text{ V}$$

$$v_\Delta = 10 \text{ V}, \quad 3.125v_\Delta = 31.25 \text{ A}$$

$$p_{3.125v_\Delta} = v_4(31.25) = -906.25 \text{ W}$$

$\therefore$ Dependent current source develops 906.25 W.

Let i_a represent the current left to right in the dependent voltage source. Then

$$i_a = \frac{v_4}{80} + \frac{v_4 - v_3}{4} + 3.125v_\Delta = 21.1375 \text{ A}$$

$$p_{35i_\phi} = (8.75)(21.1375) = 184.953125 \text{ W}$$

$\therefore$ Dependent voltage source absorbs power.

$$\begin{aligned} \sum P_{\text{diss}} &= 184.953125 + \frac{(20.25)^2}{20} + (20.125)^2(2) + \frac{10^2}{1} + \frac{10^2}{40} \\ &\quad + \left(\frac{39}{4}\right)^2(4) + \frac{(29)^2}{80} \\ &= 1508.75 \text{ W} \end{aligned}$$

$$\sum P_{\text{dev}} = 906.25 + 602.50 = 1508.75 \text{ W}$$

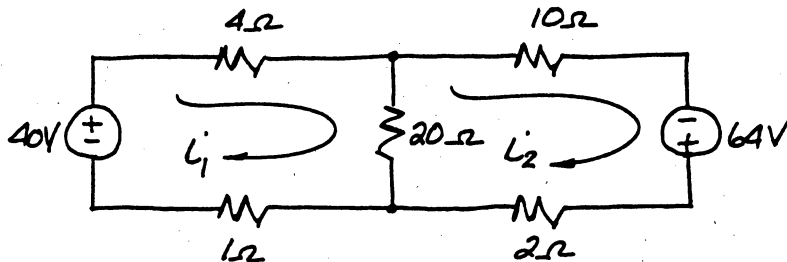
P4.25 [a] $\frac{v_o - v_1}{R} + \frac{v_o - v_2}{R} + \frac{v_o - v_3}{R} + \cdots + \frac{v_o - v_n}{R} = 0$

$$\therefore nv_o = v_1 + v_2 + v_3 + \cdots + v_n$$

$$v_o = \frac{1}{n}[v_1 + v_2 + v_3 + \cdots + v_n] = \frac{1}{n} \sum_{k=1}^n v_k$$

[b] $v_o = \frac{1}{3}(100 + 80 - 60) = 40 \text{ V}$

P4.26 [a]



$$40 = 25i_1 - 20i_2$$

$$64 = -20i_1 + 32i_2$$

$$\Delta = \begin{vmatrix} 25 & -20 \\ -20 & 32 \end{vmatrix} = 800 - 400 = 400$$

$$N_1 = \begin{vmatrix} 40 & -20 \\ 64 & 32 \end{vmatrix} = 1280 + 1280 = 2560$$

$$N_2 = \begin{vmatrix} 25 & 40 \\ -20 & 64 \end{vmatrix} = 1600 + 800 = 2400$$

$$i_1 = \frac{N_1}{\Delta} = \frac{2560}{400} = 6.4 \text{ A}$$

$$i_2 = \frac{N_2}{\Delta} = \frac{2400}{400} = 6.0 \text{ A}$$

$$i_a = i_1 = 6.4 \text{ A}, \quad i_b = i_1 - i_2 = 0.4 \text{ A}, \quad i_c = -i_2 = -6.0 \text{ A}$$

[b] If the polarity of the 64-V source is reversed, we have

$$40 = 25i_1 - 20i_2$$

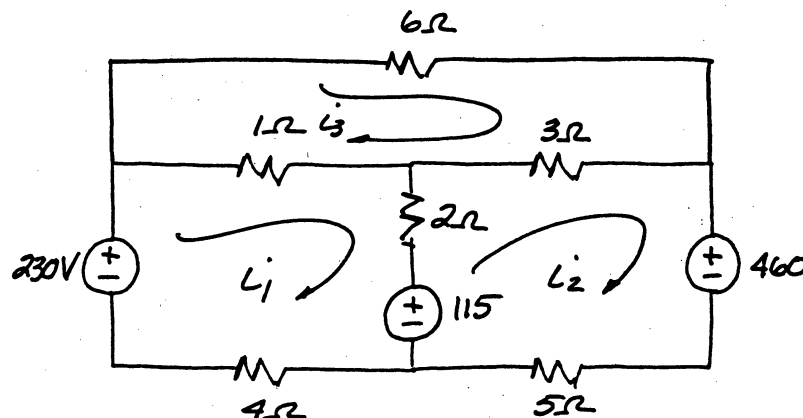
$$-64 = -20i_1 + 32i_2$$

$$\Delta = 400, \quad N_1 = 0, \quad N_2 = -800$$

$$i_1 = 0 \quad \text{and} \quad i_2 = -2 \text{ A}$$

$$i_a = i_1 = 0 \text{ A}, \quad i_b = i_1 - i_2 = 2 \text{ A}, \quad i_c = -i_2 = 2 \text{ A}$$

P4.27 [a]



$$115 = 7i_1 - 2i_2 - i_3$$

$$-345 = -2i_1 + 10i_2 - 3i_3$$

$$0 = -i_1 - 3i_2 + 10i_3$$

$$\Delta = \begin{vmatrix} 7 & -2 & -1 \\ -2 & 10 & -3 \\ -1 & -3 & 10 \end{vmatrix} = 7(100 - 9) + 2(-20 - 3) - 1(6 + 10) = 575$$

$$N_1 = \begin{vmatrix} 115 & -2 & -1 \\ -345 & 10 & -3 \\ 0 & -3 & 10 \end{vmatrix} = 115(91) + 345(-23) = 2530$$

$$N_2 = \begin{vmatrix} 7 & 115 & -1 \\ -2 & -345 & -3 \\ -1 & 0 & 10 \end{vmatrix} = -115(-23) - 345(69) = -21,160$$

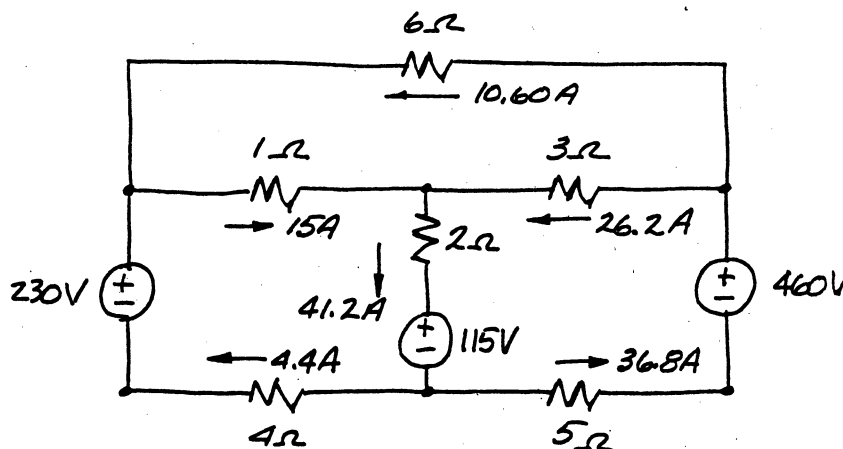
$$N_3 = \begin{vmatrix} 7 & -2 & 115 \\ -2 & 10 & -345 \\ -1 & -3 & 0 \end{vmatrix} = 115(16) + 345(-23) = -6095$$

$$i_1 = \frac{N_1}{\Delta} = \frac{2530}{575} = 4.40 \text{ A}$$

$$i_2 = \frac{N_2}{\Delta} = \frac{-21,160}{575} = -36.80 \text{ A}$$

$$i_3 = \frac{N_3}{\Delta} = \frac{-6095}{575} = -10.60 \text{ A}$$

The branch currents corresponding to these mesh currents are shown on the following diagram.

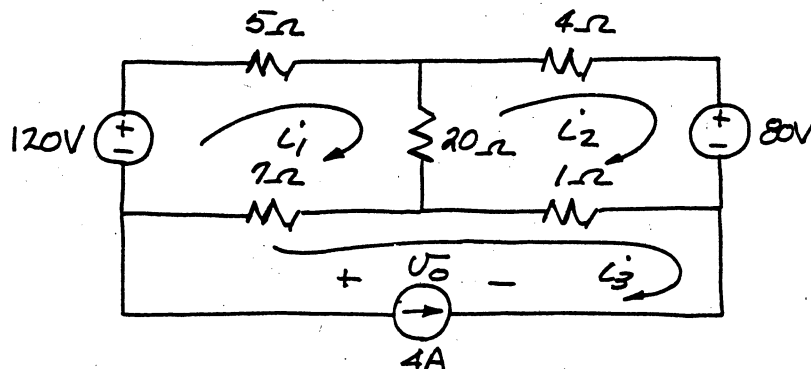


The 230-V and 460-V sources are developing power. Therefore

$$\sum P_{\text{dev}} = (230)(4.4) + 460(36.8) = 17,940 \text{ W}$$

$$\begin{aligned} [b] \quad P_{\text{diss}} &= (15)^2(1) + (26.2)^2(3) + (10.6)^2(6) + (41.2)^2(2) + (4.4)^2(4) \\ &\quad + (36.8)^2(5) + 41.2(115) \\ &= 17,940 \text{ W} \end{aligned}$$

P4.28 [a]



$$120 = 32i_1 - 20i_2 - 7(-4)$$

$$0 = -20i_1 + 25i_2 + 80 - 1(-4)$$

Therefore

$$92 = 32i_1 - 20i_2$$

$$-84 = -20i_1 + 25i_2$$

$$\Delta = \begin{vmatrix} 32 & -20 \\ -20 & 25 \end{vmatrix} = 800 - 400 = 400$$

$$N_1 = \begin{vmatrix} 92 & -20 \\ -84 & 25 \end{vmatrix} = 620$$

$$N_2 = \begin{vmatrix} 32 & 92 \\ -20 & -84 \end{vmatrix} = -848$$

$$i_1 = \frac{N_1}{\Delta} = \frac{620}{400} = 1.55 \text{ A}$$

$$i_2 = \frac{N_2}{\Delta} = \frac{-848}{400} = -2.12 \text{ A}$$

$$v_o = 7(i_3 - i_1) + 1(i_3 - i_2) = 7(-5.55) + 1(-1.88) = -40.73 \text{ V}$$

$$p_{4A} = (-40.73)(4) = -162.92 \text{ W}$$

Therefore the 4-A source is delivering 162.92 W to the circuit.

$$[b] \quad p_{120V} = -(120)(1.55) = -186 \text{ W (dev)}$$

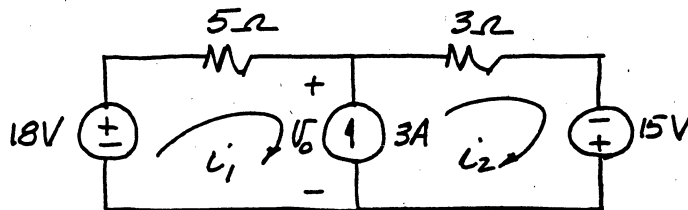
$$p_{80V} = 80(-2.12) = -169.60 \text{ W (dev)}$$

$$\therefore \sum P_{\text{dev}} = 162.92 + 186 + 169.60 = 518.52 \text{ W}$$

$$[c] \quad \begin{aligned} \sum P_{\text{diss}} &= i_1^2(5) + i_2^2(4) + (i_1 - i_2)^2(20) + (i_1 - i_3)^2(7) + (i_2 - i_3)^2(1) \\ &= (1.55)^2(5) + (2.12)^2(4) + (3.67)^2(20) + (5.55)^2(7) + (1.88)^2(1) \\ &= 518.52 \text{ W} \end{aligned}$$

$$\text{Therefore } \sum P_{\text{dev}} = \sum P_{\text{diss}} = 518.52 \text{ W}$$

P 4.29



Summing around the supermesh gives

$$18 = 5i_1 + 3i_2 - 15$$

$$33 = 5i_1 + 3i_1 + 9$$

$$33 = 5i_1 + 3i_2$$

$$\therefore 8i_1 = 24$$

$$i_1 - i_2 = -3$$

$$i_1 = 3 \text{ A}$$

$$\therefore i_2 = i_1 + 3$$

$$i_2 = 6 \text{ A}$$

$$p_{18V} = -18(3) = -54 \text{ W} \quad (\text{dev})$$

$$p_{15V} = -15(6) = -90 \text{ W} \quad (\text{dev})$$

$$v_o = 18 - 5i_1 = 18 - 15 = 3 \text{ V}$$

$$p_{3A} = -3(+3) = -9 \text{ W} \quad (\text{dev})$$

$$\sum P_{\text{dev}} = 54 + 90 + 9 = 153 \text{ W}$$

$$\therefore \sum P_{\text{diss}} = 153 \text{ W}$$

$$\text{Check: } \sum P_{\text{diss}} = 5(9) + 36(3) = 45 + 108 = 153 \text{ W}$$

P 4.30 Summing around the supermesh used in the solution to Problem 4.29 gives

$$6 = 5i_1 + 3i_2 - 15$$

$$21 = 5i_1 + 3(i_1 + 3)$$

$$\therefore 8i_1 = 12$$

$$i_1 = 1.5 \text{ A}$$

$$i_2 = 4.5 \text{ A}$$

$$p_{6V} = -6(1.5) = -9 \text{ W} \quad (\text{dev})$$

$$p_{15V} = -15(4.5) = -67.5 \text{ W} \quad (\text{dev})$$

$$p_{3A} = -3v_o$$

$$v_o = 6 - 5i_1 = 6 - 7.5 = -1.5 \text{ V}$$

$$p_{3A} = -3(-1.5) = 4.5 \text{ W} \quad (\text{diss})$$

$$p_{5\Omega} = (1.5)^2(5) = 11.25 \text{ W}$$

$$p_{3\Omega} = (4.5)^2(3) = 60.75 \text{ W}$$

$$\sum P_{\text{diss}} = 4.5 + 11.25 + 60.75 = 76.5 \text{ W}$$

$$\text{Check: } \sum P_{\text{dev}} = 9 + 67.5 = 76.5 \text{ W}$$

P 4.31 [a] Summing around the supermesh used in the solution to Problem 4.29 gives

$$10 = 5i_1 + 3i_2 - 15$$

$$25 = 5i_1 + 3(i_1 + 3)$$

$$\therefore 16 = 8i_1, \quad i_1 = 2 \text{ A}, \quad i_2 = 5 \text{ A}$$

$$\therefore v_o = 10 - 5(2) = 0 \text{ V}$$

$$\therefore \sum P_{\text{dev}} = \sum P_{\text{diss}} = (10)(2) + 15(5) = 95 \text{ W}$$

$$\text{Check: } \sum P_{\text{diss}} = 4(5) + 25(3) = 95 \text{ W}$$

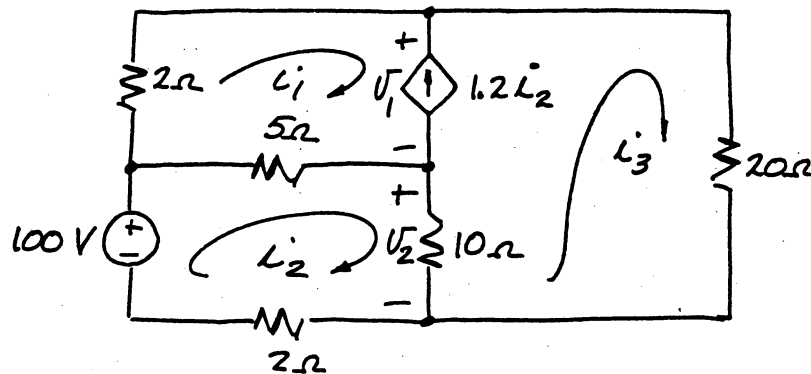
[b] With 3-A current source replaced with a short circuit

$$i_1 = 10/5 = 2 \text{ A}; \quad i_2 = 15/3 = 5 \text{ A}$$

$$\therefore \sum P_{\text{diss}} = (4)(5) + (25)(3) = 95 \text{ W}$$

- [c] A 3-A source with zero terminal voltage is equivalent to a short circuit carrying 3 A.

P 4.32 [a]



$$100 = 2i_1 + 20i_3 + 2i_2$$

$$100 = 5(i_2 - i_1) + 10(i_2 - i_3) + 2i_2$$

$$100 = 2i_1 + 2i_2 + 20i_3$$

$$100 = -5i_1 + 17i_2 - 10i_3$$

$$1.2i_2 = i_3 - i_1$$

$$\therefore i_3 = 1.2i_2 + i_1$$

$$20i_3 = 20i_1 + 24i_2$$

$$10i_3 = 10i_1 + 12i_2$$

$$\therefore 100 = 2i_1 + 2i_2 + 20i_1 + 24i_2$$

$$100 = -5i_1 + 17i_2 - 10i_1 - 12i_2$$

$$\therefore 100 = 22i_1 + 26i_2$$

$$100 = -15i_1 + 5i_2$$

$$\Delta = \begin{vmatrix} 22 & 26 \\ -15 & 5 \end{vmatrix} = 500$$

$$N_1 = \begin{vmatrix} 100 & 26 \\ 100 & 5 \end{vmatrix} = -2100$$

$$N_2 = \begin{vmatrix} 22 & 100 \\ -15 & 100 \end{vmatrix} = 3700$$

$$\therefore i_1 = \frac{N_1}{\Delta} = -4.20 \text{ A}$$

$$i_2 = \frac{N_2}{\Delta} = 7.40 \text{ A}$$

$$i_3 = 1.2i_2 + i_1 = 4.68 \text{ A}$$

$$i_a = i_1 = -4.20 \text{ A}$$

$$i_b = i_2 = 7.40 \text{ A}$$

$$i_c = i_3 = 4.68 \text{ A}$$

$$i_d = i_2 - i_1 = 7.4 + 4.2 = 11.6 \text{ A}$$

$$i_e = i_2 - i_3 = 7.4 - 4.68 = 2.72 \text{ A}$$

$$[b] \quad v_1 + v_2 = 20i_3 = 93.60 \text{ V}$$

$$v_2 = 10i_e = 27.20 \text{ V}$$

$$\therefore v_1 = 93.60 - 27.20 = 66.40 \text{ V}$$

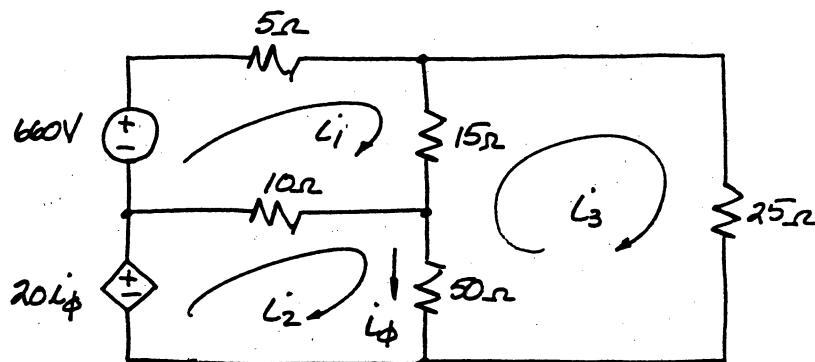
$$\sum P_{\text{dev}} = 100i_b + 1.2i_b v_1 = 740 + 589.632 = 1329.632 \text{ W}$$

$$\sum P_{\text{diss}} = 2i_a^2 + 5i_d^2 + 2i_b^2 + 10i_e^2 + 20i_c^2$$

$$= 2(4.2)^2 + 5(11.6)^2 + 2(7.4)^2 + 10(2.72)^2 + 20(4.68)^2 = 1329.632 \text{ W}$$

$$\therefore \sum P_{\text{dev}} = \sum P_{\text{diss}} = 1329.632 \text{ W}$$

P 4.33



$$660 = 30i_1 - 10i_2 - 15i_3$$

$$132 = 6i_1 - 2i_2 - 3i_3$$

$$0 = -20(i_2 - i_3) - 10i_1 + 60i_2 - 50i_3$$

$$0 = -10i_1 + 40i_2 - 30i_3$$

$$0 = -i_1 + 4i_2 - 3i_3$$

$$0 = -15i_1 - 50i_2 + 90i_3$$

$$0 = -3i_1 - 10i_2 + 18i_3$$

$$\Delta = \begin{vmatrix} 6 & -2 & -3 \\ -1 & 4 & -3 \\ -3 & -10 & 18 \end{vmatrix} = 6(72 - 30) + 1(-36 - 30) - 3(6 + 12) = 132$$

$$N_1 = \begin{vmatrix} 132 & -2 & -3 \\ 0 & 4 & -3 \\ 0 & -10 & 18 \end{vmatrix} = 132(42)$$

$$N_2 = \begin{vmatrix} 6 & 132 & -3 \\ -1 & 0 & -3 \\ -3 & 0 & 18 \end{vmatrix} = 132(27)$$

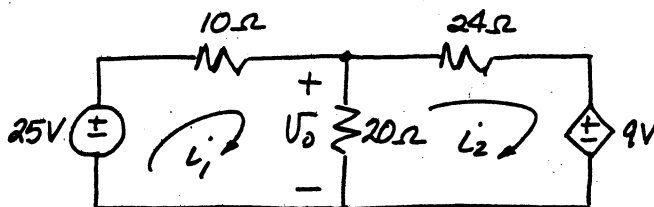
$$N_3 = \begin{vmatrix} 6 & -2 & 132 \\ -1 & 4 & 0 \\ -3 & -10 & 0 \end{vmatrix} = 132(22)$$

$$i_1 = \frac{N_1}{\Delta} = 42 \text{ A}, \quad i_2 = \frac{N_2}{\Delta} = 27 \text{ A}, \quad i_3 = \frac{N_3}{\Delta} = 22 \text{ A}$$

$$p_{20i_\Delta} = -27(20)(27 - 22) = -2700 \text{ W}$$

$$p_{20i_\Delta}(\text{developed}) = 2700 \text{ W}$$

P 4.34 [a] $i_\Delta = \frac{21}{14} = 1.5 \text{ A}, \quad 6i_\Delta = 9 \text{ V}$



$$25 = 30i_1 - 20i_2$$

$$-9 = -20i_1 + 44i_2$$

$$\Delta = \begin{vmatrix} 30 & -20 \\ -20 & 44 \end{vmatrix} = 920$$

$$N_1 = \begin{vmatrix} 25 & -20 \\ -9 & 44 \end{vmatrix} = 920$$

$$N_2 = \begin{vmatrix} 30 & 25 \\ -20 & -9 \end{vmatrix} = 230$$

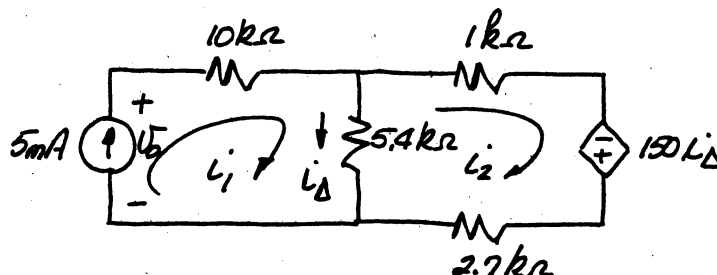
$$i_1 = \frac{N_1}{\Delta} = 1 \text{ A}, \quad i_2 = \frac{N_2}{\Delta} = 0.25 \text{ A}$$

$$v_o = 20(i_1 - i_2) = 20(1.0 - 0.25) = 15 \text{ V}$$

[b] $p_{9V} = 9i_2 = 2.25 \text{ W}$ (abs)

$$\therefore p_{9V}(\text{delivered}) = -2.25 \text{ W}$$

P 4.35 [a]



$$i_1 = 5 \text{ mA}, \quad i_\Delta = (i_1 - i_2)$$

$$5400(i_2 - i_1) + 3700i_2 - 150(i_1 - i_2) = 0$$

$$9250i_2 - 5550i_1 = 0$$

$$i_2 = \frac{(5550)(5 \times 10^{-3})}{9250} = 3 \text{ mA}$$

$$\therefore i_{\Delta} = 5 - 3 = 2 \text{ mA}$$

$$[b] \quad p_{5 \text{ mA}} = -v_o i_1$$

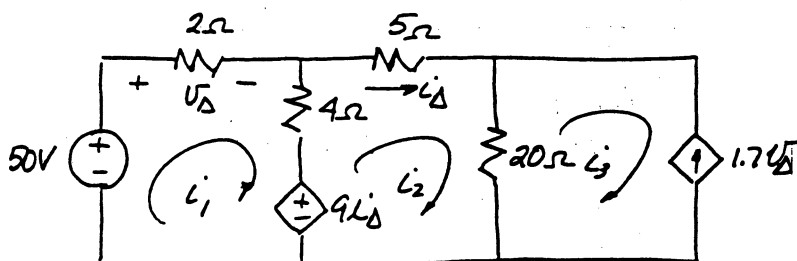
$$v_o = 10i_1 + 5.4(i_1 - i_2) = 50 + 10.8 = 60.8 \text{ V}$$

$$p_{5 \text{ mA}} = -60.8(5) = -304 \text{ mW}$$

$$p_{5 \text{ mA}}(\text{del}) = 304 \text{ mW}$$

$$[c] \quad p_{150i_{\Delta}} = -150i_{\Delta}i_2 = -150(2) \times 10^{-3}(3 \times 10^{-3}) = -900 \times 10^{-6} = 900 \mu\text{W}$$

$$p_{150i_{\Delta}}(\text{del}) = 900 \mu\text{W}$$

P 4.36


$$50 = 2i_1 + 4(i_1 - i_2) + 9i_2$$

$$0 = -9i_2 + 4(i_2 - i_1) + 5i_2 + 20(i_2 + 1.7v_{\Delta})$$

$$50 = 6i_1 + 5i_2$$

$$0 = -5i_2 - 4i_1 + 5i_2 + 20i_2 + 34(2i_1)$$

$$0 = 64i_1 + 20i_2$$

$$\Delta = \begin{vmatrix} 6 & 5 \\ 64 & 20 \end{vmatrix} = 120 - 320 = -200$$

$$N_1 = \begin{vmatrix} 50 & 5 \\ 0 & 20 \end{vmatrix} = 1000$$

$$N_2 = \begin{vmatrix} 6 & 50 \\ 64 & 0 \end{vmatrix} = -3200$$

$$i_1 = \frac{N_1}{\Delta} = -5 \text{ A}, \quad i_2 = \frac{N_2}{\Delta} = 16 \text{ A}, \quad i_a = i_1 = -5 \text{ A}$$

$$p_{50\text{V}} = -50i_a = 250 \text{ W} \quad (\text{abs})$$

$$i_b = i_1 - i_2 = -5 - 16 = -21 \text{ A}$$

$$p_{9i_{\Delta}} = 9i_{\Delta}i_b = 9(16)(-21) = -3024 \text{ W} \quad (\text{del})$$

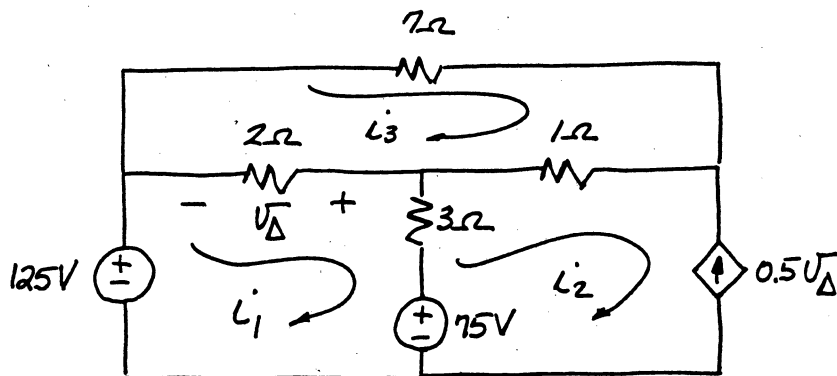
$$v_{1.7v_{\Delta}} = 20(i_2 - i_3)$$

$$i_3 = -1.7(2)(i_1) = -3.4(-5) = 17 \text{ A}$$

$$v_{1.7v_{\Delta}} = 20(16 - 17) = -20 \text{ V}$$

$$p_{1.7v_{\Delta}} = -(1.7v_{\Delta})v_{1.7v_{\Delta}} = -(-17)(-20) = 20(-17) = -340 \text{ W} \quad (\text{del})$$

P 4.37



$$125 - 75 = 5i_1 - 3(-0.5)(2)(i_3 - i_1) - 2i_3$$

$$0 = -2i_1 - i_2 + 10i_3$$

$$50 = 2i_1 + i_3$$

$$0 = -3i_1 + 11i_3$$

$$\Delta = \begin{vmatrix} 2 & 1 \\ -3 & 11 \end{vmatrix} = 22 + 3 = 25$$

$$N_1 = \begin{vmatrix} 50 & 1 \\ 0 & 11 \end{vmatrix} = 550$$

$$N_3 = \begin{vmatrix} 2 & 50 \\ -3 & 0 \end{vmatrix} = 150$$

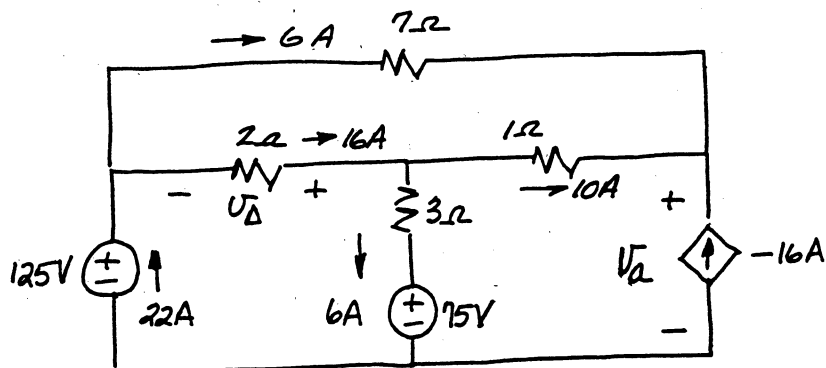
$$i_1 = \frac{N_1}{\Delta} = 22 \text{ A}$$

$$i_3 = \frac{N_3}{\Delta} = 6 \text{ A}$$

$$v_{\Delta} = 2(i_3 - i_1) = 2(-16) = -32 \text{ V}$$

$$i_2 = -0.5v_{\Delta} = 16 \text{ A}$$

$$i_1 - i_3 = 16 \text{ A}; \quad i_1 - i_2 = 6 \text{ A}; \quad i_2 - i_3 = 10 \text{ A}$$



$$v_a = 75 + 18 - 10 = 83 \text{ V}$$

Therefore the only source developing power is the 125-V source.

$$P_{\text{dev}} = (125)(22) = 2750 \text{ W}$$

Check:

$$p_{0.5v_\Delta} = (83)(16) = 1328 \text{ W (absorbed)}$$

$$p_{75V} = 6(75) = 450 \text{ W (absorbed)}$$

$$p_{7\Omega} = 36(7) = 252 \text{ W (absorbed)}$$

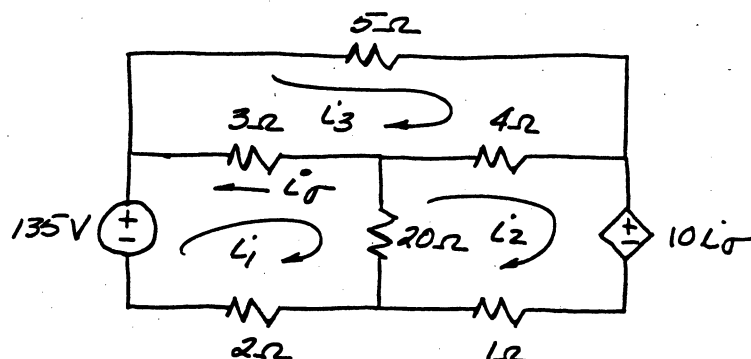
$$p_{2\Omega} = 256(2) = 512 \text{ W (absorbed)}$$

$$p_{1\Omega} = 100(1) = 100 \text{ W (absorbed)}$$

$$p_{3\Omega} = 36(3) = 108 \text{ W (absorbed)}$$

$$\sum P_{\text{abs}} = 2750 \text{ W}$$

P4.38



$$135 = 25i_1 - 20i_2 - 3i_3$$

$$0 = -20i_1 + 25i_2 - 4i_3 + 10(i_3 - i_1)$$

$$0 = -3i_1 - 4i_2 + 12i_3$$

$$135 = 25i_1 - 20i_2 - 3i_3$$

$$0 = -30i_1 + 25i_2 + 6i_3$$

$$0 = -3i_1 - 4i_2 + 12i_3$$

$$\Delta = \begin{vmatrix} 25 & -20 & -3 \\ -30 & 25 & 6 \\ -3 & -4 & 12 \end{vmatrix} = 25(300 + 24) + 30(-240 - 12) - 3(-120 + 75) = 675$$

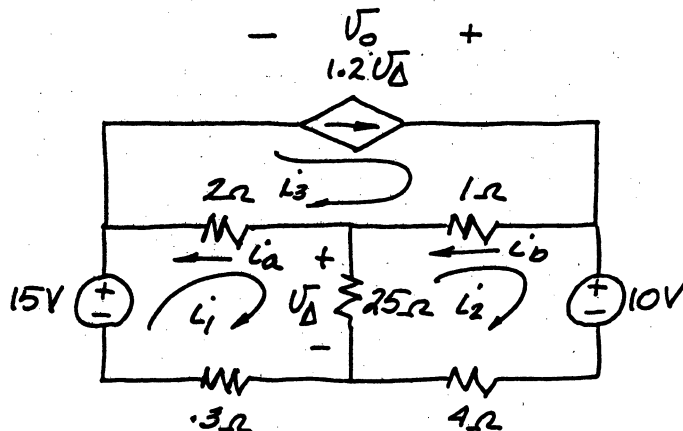
$$N_1 = \begin{vmatrix} 135 & -20 & -3 \\ 0 & 25 & 6 \\ 0 & -4 & 12 \end{vmatrix} = (324)(135) = 43,740$$

$$N_2 = \begin{vmatrix} 25 & 135 & -3 \\ -30 & 0 & 6 \\ -3 & 0 & 12 \end{vmatrix} = -135(-360 + 18) = (342)(135) = 46,170$$

$$i_1 = \frac{N_1}{\Delta} = 64.80 \text{ A}; \quad i_2 = \frac{N_2}{\Delta} = 68.40 \text{ A}; \quad i_2 - i_1 = 36 \text{ A}$$

$$p_{20\Omega} = (3.6)^2(20) = 259.20 \text{ W}$$

P4.39 [a]



$$15 = 30i_1 - 25i_2 - 2(1.2)(25)(i_1 - i_2)$$

$$15 = 30i_1 - 25i_2 - 60i_1 + 60i_2$$

$$15 = -30i_1 + 35i_2$$

$$0 = -25i_1 + 30i_2 + 10 - 1.2(25)(i_1 - i_2)$$

$$-10 = -25i_1 + 30i_2 - 30i_1 + 30i_2$$

$$-10 = -55i_1 + 60i_2$$

$$\Delta = \begin{vmatrix} -30 & 35 \\ -55 & 60 \end{vmatrix} = -1800 + 1925 = 125$$

$$N_1 = \begin{vmatrix} 15 & 35 \\ -10 & 60 \end{vmatrix} = 900 + 350 = 1250$$

$$N_2 = \begin{vmatrix} -30 & 15 \\ -55 & -10 \end{vmatrix} = 300 + 825 = 1125$$

$$i_1 = \frac{N_1}{\Delta} = \frac{1250}{125} = 10 \text{ A}$$

$$i_2 = \frac{N_2}{\Delta} = \frac{1125}{125} = 9.0 \text{ A}$$

$$i_1 - i_2 = 10 - 9 = 1 \text{ A}$$

$$p_{25\Omega} = (1)^2(25) = 25 \text{ W}$$

[b] $1.2v_\Delta = (1.2)(25) = 30 \text{ A} = i_3$

$$i_a = i_3 - i_1 = 20 \text{ A}$$

$$i_b = i_3 - i_2 = 30 - 9 = 21 \text{ A}$$

$$v_o = 2i_a + 1i_b = 40 + 21 = 61 \text{ V}$$

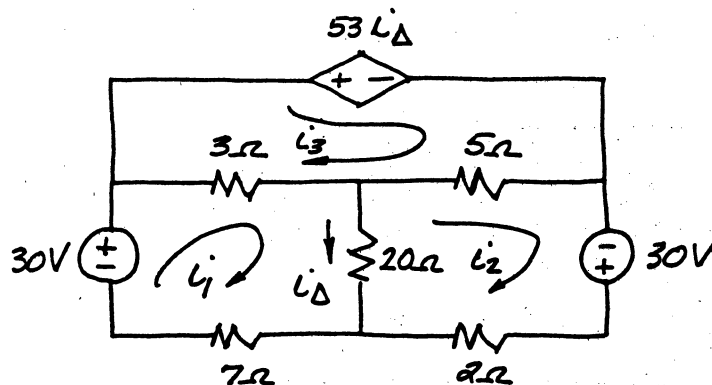
$$p_{1.2v_\Delta} = (1.2v_\Delta)v_o = i_3v_o = 30(61) = 1830 \text{ W}$$

$$p_{15V} = 15i_1 = 15(10) = 150 \text{ W}$$

$$\sum p_{\text{dev}} = 1830 + 150 = 1980 \text{ W}$$

$$\% \text{delivered} = \frac{25}{1980} \times 100 = 1.26\%$$

P 4.40



$$30 = 30i_1 - 20i_2 - 3i_3$$

$$30 = -20i_1 + 27i_2 - 5i_3$$

$$0 = -3i_1 - 5i_2 + 8i_3 + 53(i_1 - i_2)$$

$$0 = 50i_1 - 58i_2 + 8i_3$$

$$\Delta = \begin{vmatrix} 30 & -20 & -3 \\ -20 & 27 & -5 \\ 50 & -58 & 8 \end{vmatrix} = 30(216 - 290) + 20(-160 - 174) + 50(100 + 81) \\ = 30(-74) - 20(334) + 50(181) = 150$$

$$N_1 = \begin{vmatrix} 30 & -20 & -3 \\ 30 & 27 & -5 \\ 0 & -58 & 8 \end{vmatrix} = 30(-74) - 30(-334) = 7800$$

$$N_2 = \begin{vmatrix} 30 & 30 & -3 \\ -20 & 30 & -5 \\ 50 & 0 & 8 \end{vmatrix} = -30(-160 + 250) + 30(240 + 150)$$

$$N_3 = \begin{vmatrix} 30 & -20 & 30 \\ -20 & 27 & 30 \\ 50 & -58 & 0 \end{vmatrix} = 30(1160 - 1350) - 30(-1740 + 1000)$$

$$i_1 = \frac{N_1}{\Delta} = \frac{7800}{150} = 52 \text{ A}$$

$$i_2 = \frac{N_2}{\Delta} = \frac{9000}{150} = 60 \text{ A}$$

$$i_3 = \frac{N_3}{\Delta} = \frac{16,500}{150} = 110 \text{ A}$$

$$i_{\Delta} = i_1 - i_2 = 52 - 60 = -8 \text{ A}$$

$$p_{53i_{\Delta}} = (53i_{\Delta})(i_3) = (53(-8))(110) = -46,640 \text{ W}$$

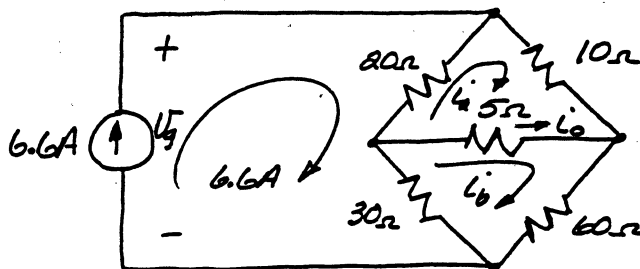
Therefore the dependent voltage source develops 46,640 W or 46.64 kW.

P4.41 [a] There are three unknown node voltages and only two unknown mesh currents. Use the mesh current method to minimize the number of simultaneous equations.

[b] See following figure for mesh currents

$$20(i_a - 6.6) + 10i_a + 5(i_a - i_b) = 0$$

$$30(i_b - 6.6) + 5(i_b - i_a) + 60i_b = 0$$



Our equations simplify to

$$7i_a - i_b = 26.4$$

$$-i_a + 19i_b = 39.6$$

$$\therefore \Delta = \begin{vmatrix} 7 & -1 \\ -1 & 19 \end{vmatrix} = 132$$

$$N_a = \begin{vmatrix} 26.4 & -1 \\ 39.6 & 19 \end{vmatrix} = 541.20$$

$$N_b = \begin{vmatrix} 7 & 26.4 \\ -1 & 39.6 \end{vmatrix} = 303.60$$

$$i_a = \frac{N_a}{\Delta} = 4.1 \text{ A}; \quad i_b = \frac{N_b}{\Delta} = 2.3 \text{ A}; \quad i_o = i_b - i_a = -1.8 \text{ A}$$

$$p_{5\Omega} = (-1.8)^2(5) = 16.20 \text{ W}$$

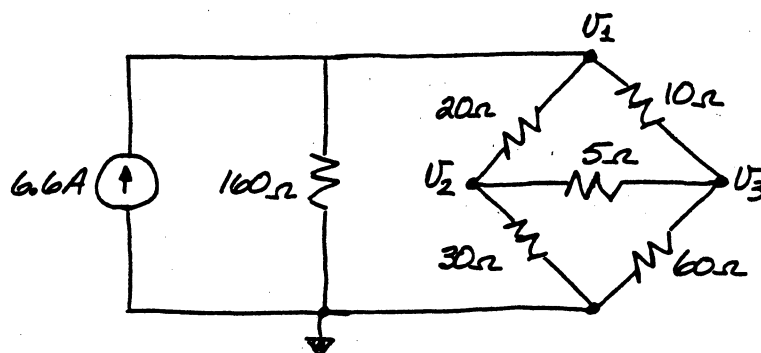
[c] No, the voltage across the 6.6-A current source is readily available from the mesh currents, and solving two simultaneous mesh-current equations is less work than solving three node voltage equations.

$$[d] \quad v_g = 10i_a + 60i_b = 41 + 138 = 179 \text{ V}$$

$$p_{6.6A}(\text{developed}) = (179)(6.6) = 1181.40 \text{ W}$$

P4.42 [a] There are three unknown node voltages and three unknown mesh currents, so the number of simultaneous equations required are the same for both methods. The node-voltage method has the advantage of having to solve the three simultaneous equations for one unknown voltage provided the connection at either the top or bottom of the circuit is used as the reference node. Therefore recommend the node-voltage method.

[b]



$$-6.6 + \frac{v_1}{160} + \frac{v_1 - v_2}{20} + \frac{v_1 - v_3}{10} = 0 \quad \text{or} \quad 25v_1 - 8v_2 - 16v_3 = 1056$$

$$\frac{v_2 - v_1}{20} + \frac{v_2 - v_3}{5} + \frac{v_3}{30} = 0 \quad \text{or} \quad -3v_1 + 17v_2 - 12v_3 = 0$$

$$\frac{v_3 - v_2}{5} + \frac{v_3}{60} + \frac{v_3 - v_1}{10} = 0 \quad \text{or} \quad -6v_1 - 12v_2 + 19v_3 = 0$$

$$\Delta = \begin{vmatrix} 25 & -8 & -16 \\ -3 & 17 & -12 \\ -6 & -12 & 19 \end{vmatrix} = 1235$$

$$N_1 = \begin{vmatrix} 1056 & -8 & -16 \\ 0 & 17 & -12 \\ 0 & -12 & 19 \end{vmatrix} = 189,024$$

$$v_1 = \frac{N_1}{\Delta} = 153.06 \text{ V}$$

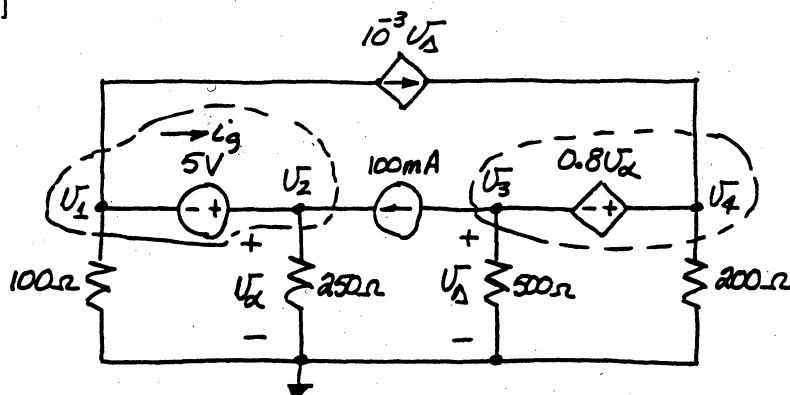
$$p_{\text{dev}} = (6.6)(153.06) = 1010.17 \text{ W}$$

P4.43 [a] The node-voltage method requires summing the currents at two supernodes in terms of four node voltages and using two constraint equations to reduce the system of equations to two unknowns. If the connection at the bottom of the circuit is used as the reference node, then the voltages controlling the dependent sources are node voltages. This makes it easy to formulate the constraint equations. The current in the 5-V source is obtained by summing the currents at either terminal of the source.

The mesh-current method requires summing the voltages around the two meshes not containing current sources in terms of four mesh currents. In addition the voltages controlling the dependent sources must be expressed in terms of the mesh currents. Thus the constraint equations are more complicated, and the reduction to two equations and two unknowns involves more algebraic manipulation. The current in the 5-V source is found by subtracting two mesh currents.

Because the constraint equations are easier to formulate in the node-voltage method, it is the preferred approach.

[b]



$$v_{\Delta} = v_3; \quad v_{\alpha} = v_2$$

$$\frac{v_1}{100} + \frac{v_2}{250} - 0.1 + 10^{-3}v_3 = 0 \quad \text{or} \quad 5v_1 + 2v_2 - 50 + 0.5v_3 = 0$$

$$v_1 = v_2 - 5, \quad \therefore 5v_1 = 5v_2 - 25$$

$$\therefore \boxed{7v_2 + 0.5v_3 = 75}$$

$$\frac{v_3}{500} + 0.1 + \frac{v_4}{200} - 10^{-3}v_3 = 0$$

$$\therefore 2v_3 + 100 + 5v_4 - v_3 = 0$$

$$v_4 = v_3 + 0.8v_2; \quad \therefore 5v_4 = 5v_3 + 4v_2$$

$$\therefore 4v_2 + 6v_3 = -100 \quad \text{or} \quad \boxed{2v_2 + 3v_3 = -50}$$

$$\therefore \Delta = \begin{vmatrix} 7 & 0.5 \\ 2 & 3 \end{vmatrix} = 21 - 1 = 20$$

$$N_2 = \begin{vmatrix} 75 & 0.5 \\ -50 & 3 \end{vmatrix} = 225 + 25 = 250$$

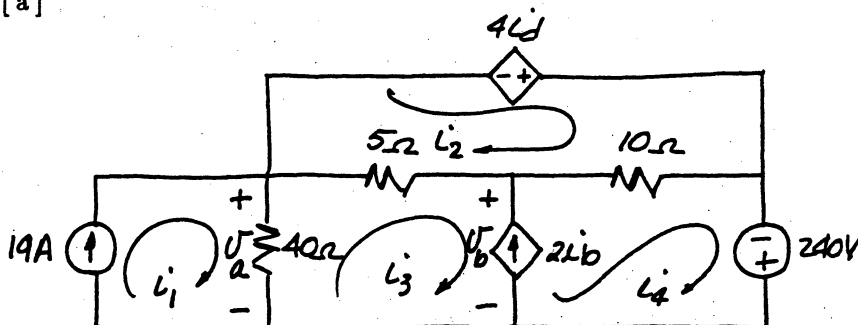
$$\therefore v_2 = \frac{250}{20} = 12.5 \text{ V}$$

$$i_g = \frac{v_2}{250} - 0.1 = \frac{12.5}{250} - 0.1 = -0.05 \text{ A} = -50 \text{ mA}$$

$$p_{5V} = -5i_g = -5(-50) = 250 \text{ mW}$$

$$\therefore p_{5V}(\text{absorbed}) = 250 \text{ mW}$$

P4.44 [a]



$$40(i_3 - 19) - 4i_4 - 240 = 0$$

$$40i_3 - 4i_4 = 1000$$

$$\boxed{10i_3 - i_4 = 250}$$

$$40(i_3 - 19) + 5(i_3 - i_2) + 10(i_4 - i_2) - 240 = 0$$

$$45i_3 - 15i_2 + 10i_4 = 1000$$

$$i_b = i_2 - i_3$$

$$2i_b = i_4 - i_3$$

$$2i_2 - 2i_3 = i_4 - i_3; \quad i_2 = 0.5i_4 + 0.5i_3$$

$$15i_2 = 7.5i_4 + 7.5i_3$$

$$45i_3 - 7.5i_4 - 7.5i_3 + 10i_4 = 1000$$

$$37.5i_3 + 2.5i_4 = 1000$$

$$\boxed{15i_3 + i_4 = 400}$$

$$\Delta = \begin{vmatrix} 10 & -1 \\ 15 & 1 \end{vmatrix} = 25$$

$$N_3 = \begin{vmatrix} 250 & -1 \\ 400 & 1 \end{vmatrix} = 650$$

$$N_4 = \begin{vmatrix} 10 & 250 \\ 15 & 400 \end{vmatrix} = +250$$

$$i_3 = \frac{N_3}{\Delta} = 26 \text{ A}; \quad i_2 = 18 \text{ A}$$

$$i_4 = \frac{N_4}{\Delta} = 10 \text{ A}; \quad i_1 = 19 \text{ A}$$

$$i_a = 19 - 26 = -7 \text{ A}$$

$$i_b = 18 - 26 = -8 \text{ A}$$

$$i_c = 18 - 10 = 8 \text{ A}$$

$$i_d = 10 \text{ A}$$

$$i_e = i_c + i_d = 8 + 10 = 18 \text{ A}$$

[b] $v_a = 40i_a = -280 \text{ V}; \quad v_b = -10i_c - 240 = -320 \text{ V}$

$$p_{19\text{A}} = -19v_a = -19(-280) = 5320 \text{ W (diss)}$$

$$p_{4i_d} = -4i_d i_e = -4(10)(18) = -720 \text{ W (gen)}$$

$$p_{2i_b} = -2i_b v_b = -2(-8)(-320) = -5120 \text{ W (gen)}$$

$$p_{240\text{V}} = -240i_d = -240(10) = -2400 \text{ W (gen)}$$

$$p_{40\Omega} = (-7)^2(40) = 1960 \text{ W (diss)}$$

$$p_{5\Omega} = (-8)^2(5) = 320 \text{ W (diss)}$$

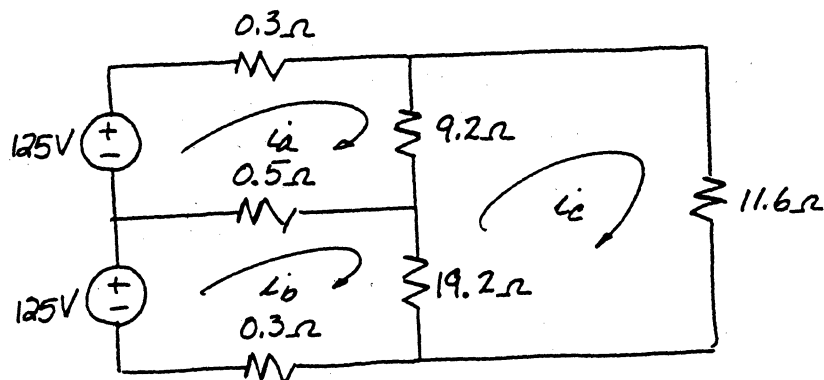
$$p_{10\Omega} = (8)^2(10) = 640 \text{ W (diss)}$$

$$\sum P_{\text{gen}} = 720 + 5120 + 2400 = 8240 \text{ W}$$

$$\sum P_{\text{diss}} = 5320 + 1960 + 320 + 640 = 8240 \text{ W}$$

$$\therefore \sum P_{\text{gen}} = \sum P_{\text{diss}} = 8240 \text{ W}$$

P4.45 [a]



$$125 = 10i_a - 0.5i_b - 9.2i_c$$

$$125 = -0.5i_a + 20i_b - 19.2i_c$$

$$0 = -9.2i_a - 19.2i_b + 40i_c$$

$$\Delta = \begin{vmatrix} 10 & -0.5 & -9.2 \\ -0.5 & 20 & -19.2 \\ -9.2 & -19.2 & 40 \end{vmatrix} = 2434.16$$

$$N_a = \begin{vmatrix} 125 & -0.5 & -9.2 \\ 125 & 20 & -19.2 \\ 0 & -19.2 & 40 \end{vmatrix} = (125)(628)$$

$$N_b = \begin{vmatrix} 10 & 125 & -9.2 \\ -0.5 & 125 & -19.2 \\ -9.2 & 0 & 40 \end{vmatrix} = (125)(512)$$

$$N_c = \begin{vmatrix} 10 & -0.5 & 125 \\ -0.5 & 20 & 125 \\ -9.2 & -19.2 & 0 \end{vmatrix} = 125(390.2)$$

$$i_a = \frac{N_a}{\Delta} = 32.25 \text{ A}; \quad i_b = \frac{N_b}{\Delta} = 26.29 \text{ A}; \quad i_c = \frac{N_c}{\Delta} = 20.04 \text{ A}$$

$$v_1 = 9.2(i_a - i_c) = 112.35 \text{ V}$$

$$v_2 = 19.2(i_b - i_c) = 120.09 \text{ V}$$

$$v_c = 11.6i_c = 232.44 \text{ V}$$

$$[b] \quad p_1 = (i_a - i_c)^2(9.2) = 1371.93 \text{ W}$$

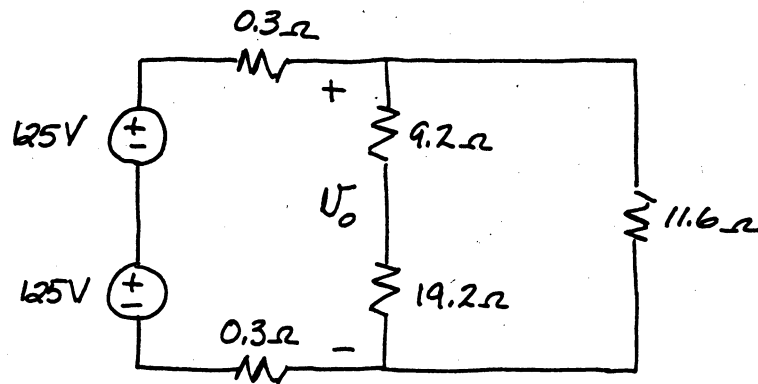
$$p_2 = (i_b - i_c)^2(19.2) = 751.13 \text{ W}$$

$$p_3 = i_c^2(11.6) = 4657.52 \text{ W}$$

$$[c] \quad \sum P_{\text{dev}} = 125(32.25) + 125(26.29) = 4031.16 + 3286.55 = 7317.72 \text{ W}$$

$$\% \text{ delivered} = \left(\frac{p_1 + p_2 + p_3}{\sum P_{\text{dev}}} \right) 100 = \frac{6780.58}{7317.72} \times 100 = 92.66\%$$

[d]



$$\frac{v_o - 250}{0.6} + \frac{v_o}{28.4} + \frac{v_o}{11.6} = 0$$

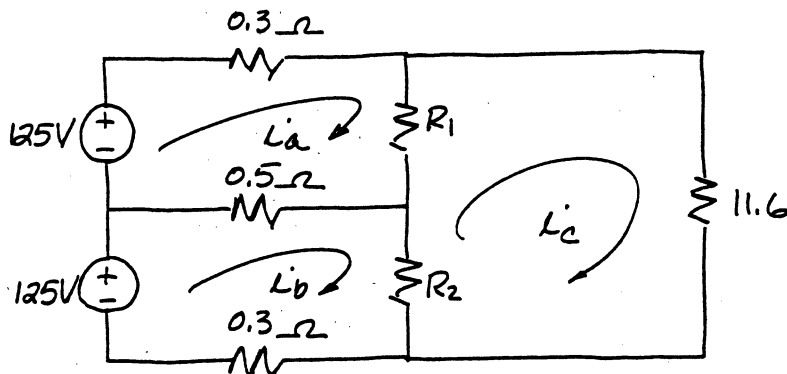
$$\therefore v_o = 233.02 \text{ V}$$

$$\therefore v_1 = \frac{233.02}{28.4}(9.2) = 75.49 \text{ V}$$

$$v_2 = \frac{233.02}{28.4}(19.2) = 157.54 \text{ V}$$

Voltage across load R_2 is excessive and could cause damage to the appliance.

P4.46



$$125 = (R_1 + 0.8)i_a - 0.5i_b - R_1i_c$$

$$125 = -0.5i_a + (R_2 + 0.8)i_b - R_2i_c$$

$$0 = -R_1i_a - R_2i_b + (R_1 + R_2 + 11.6)i_c$$

$$\Delta = \begin{vmatrix} (R_1 + 0.8) & 0.5 & -R_1 \\ -0.5 & (R_2 + 0.8) & -R_2 \\ -R_1 & -R_2 & (R_1 + R_2 + 11.6) \end{vmatrix}$$

$$\text{When } R_1 = R_2, \Delta \text{ reduces to } \Delta = 12.2R_1^2 + 19.34R_1 + 4.524.$$

$$N_a = \begin{vmatrix} 125 & -0.5 & -R_1 \\ 125 & (R_2 + 0.8) & -R_2 \\ 0 & -R_2 & (R_1 + R_2 + 11.6) \end{vmatrix}$$

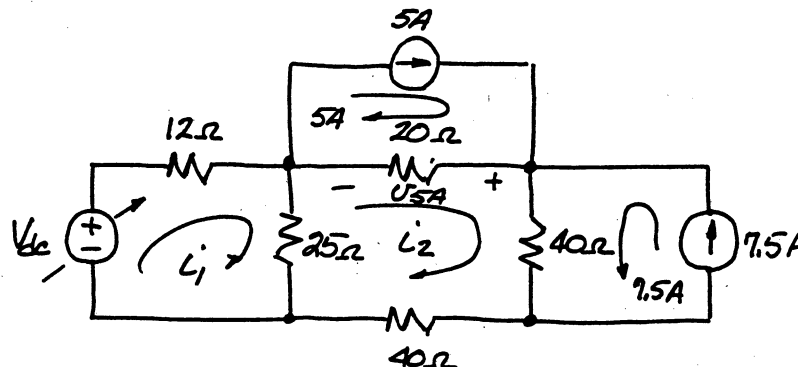
$$= 125 [(R_2 + 1.3)(R_1 + R_2 + 11.6) + R_1R_2 - R_2^2]$$

$$\begin{aligned}
 N_b &= \begin{vmatrix} (R_1 + 0.8) & 125 & -R_1 \\ -0.5 & 125 & -R_2 \\ -R_1 & 0 & (R_1 + R_2 + 11.6) \end{vmatrix} \\
 &= 125 [(R_1 + 1.3)(R_1 + R_2 + 11.6) + R_1 R_2 - R_1^2] \\
 i_a &= \frac{N_a}{\Delta}, \quad i_b = \frac{N_b}{\Delta} \\
 i_{\text{neutral}} &= i_a - i_b = \frac{N_a - N_b}{\Delta} = \frac{125[(R_1 + R_2 + 11.6)(R_2 - R_1) + R_1^2 - R_2^2]}{\Delta}
 \end{aligned}$$

Now note that when $R_1 = R_2$, i_{neutral} reduces to

$$i_{\text{neutral}} = \frac{0}{12.2R_1^2 + 19.34R_1 + 4.524} = 0$$

P4.47 The power developed by the 5-A source is zero when the voltage across the source is zero. Only two mesh-current equations are needed to find the voltage across the 5-A source, whereas the node-voltage approach requires three equations.



$$V_{dc} = 37i_1 - 25i_2$$

$$0 = -25i_1 + 125i_2 - 100 + 300$$

$$-200 = -25i_1 + 125i_2$$

$$\Delta = \begin{vmatrix} 37 & -25 \\ -25 & 125 \end{vmatrix} = 4000$$

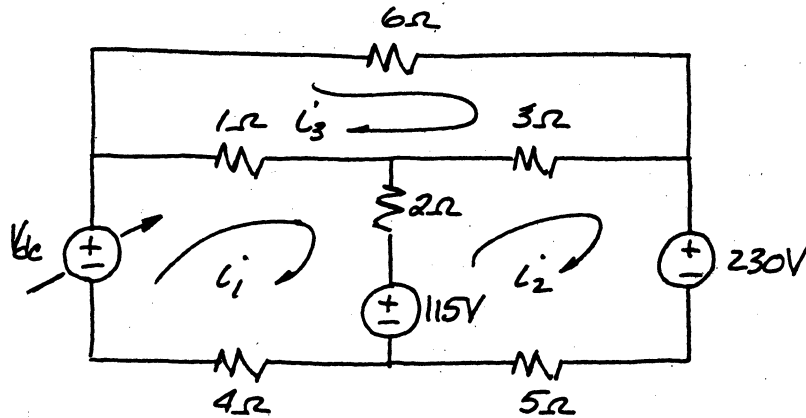
$$N_2 = \begin{vmatrix} 37 & V_{dc} \\ -25 & -200 \end{vmatrix} = 25V_{dc} - 7400$$

$$i_2 = \frac{N_2}{\Delta} = \frac{25V_{dc} - 7400}{4000}$$

$$\begin{aligned}
 v_{5A} &= (5 - i_2)20 = 100 - 20i_2 = 100 - \frac{(25V_{dc} - 7400)}{200} \\
 &= \frac{20,000 - 25V_{dc} + 7400}{200} = \frac{27,400 - 25V_{dc}}{200}
 \end{aligned}$$

$$v_{5A} = 0 \quad \text{when} \quad 25V_{dc} = 27,400 \quad \text{or} \quad V_{dc} = 1096 \text{ V}$$

P 4.48 Using the mesh-current method we have



$$V_{dc} - 115 = 7i_1 - 2i_2 - i_3$$

$$-115 = -2i_1 + 10i_2 - 3i_3$$

$$0 = -i_1 - 3i_2 + 10i_3$$

By hypothesis $i_2 = 0$, therefore we find V_{dc} such that $N_2 = 0$.

$$N_2 = \begin{vmatrix} 7 & V_{dc} - 115 & -1 \\ -2 & -115 & -3 \\ -1 & 0 & 10 \end{vmatrix} = -(V_{dc} - 115)(-20 - 3) - 115(70 - 1)$$

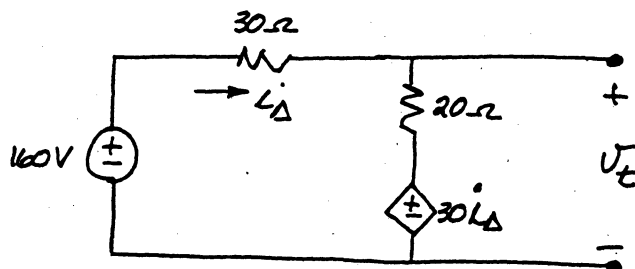
$$= 23(V_{dc} - 115) - 69(115)$$

$$\therefore 23(V_{dc} - 115) - 69(115) = 0$$

$$V_{dc} - 115 - 345 = 0$$

$$V_{dc} = 460 \text{ V}$$

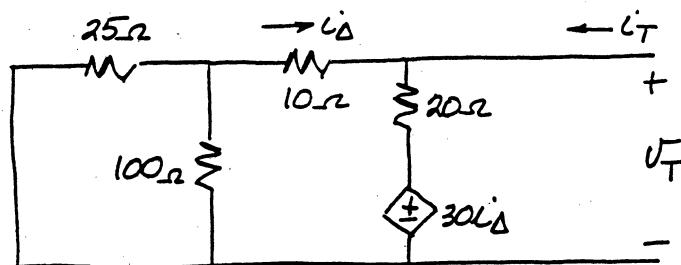
P 4.49 We begin by finding the Thévenin equivalent with respect to R_o . After making a couple of source transformations the circuit simplifies to



$$i_{\Delta} = \frac{160 - 30i_{\Delta}}{50}; \quad i_{\Delta} = 2 \text{ A}$$

$$v_{Th} = 20i_{\Delta} + 30i_{\Delta} = 50i_{\Delta} = 100 \text{ V}$$

Using the test-source method to find the Thévenin resistance gives

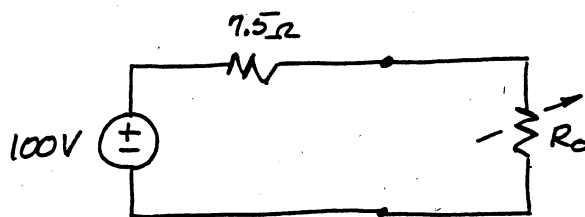


$$i_T = \frac{v_T}{30} + \frac{v_T - 30(-v_T/30)}{20}$$

$$\frac{i_T}{v_T} = \frac{1}{30} + \frac{1}{10} = \frac{4}{30} = \frac{2}{15}$$

$$R_{Th} = \frac{v_T}{i_T} = \frac{15}{2} = 7.5 \Omega$$

Thus our problem is reduced to analyzing the circuit shown below.



$$p = \left(\frac{100}{7.5 + R_o} \right)^2 R_o = 250$$

$$\frac{10^4}{R_o^2 + 15R_o + 56.25} R_o = 250$$

$$\frac{10^4 R_o}{250} = R_o^2 + 15R_o + 56.25$$

$$40R_o = R_o^2 + 15R_o + 56.25$$

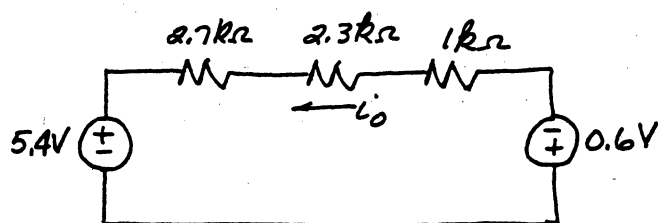
$$R_o^2 - 25R_o + 56.25 = 0$$

$$R_o = 12.5 \pm \sqrt{156.25 - 56.25} = 12.5 \pm 10$$

$$R_o = 22.5 \Omega$$

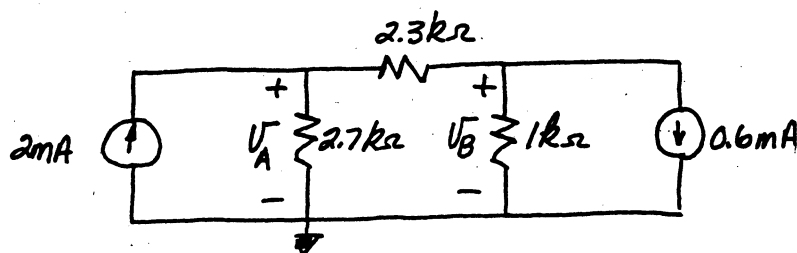
$$R_o = 2.5 \Omega$$

P4.50 [a] Apply source transformations to both current sources to get



$$i_o = \frac{-6}{6} = -1 \text{ mA}$$

[b]



$$-2 \times 10^{-3} + \frac{v_A}{2700} + \frac{v_A - v_B}{2300} = 0$$

$$\frac{v_B - v_A}{2300} + \frac{v_B}{1000} + 0.6 \times 10^{-3} = 0$$

$$\text{or } 2.3v_A + 2.7v_A - 2.7v_B = (2)(2.7)(2.3)$$

$$\boxed{5v_A - 2.7v_B = 12.42}$$

$$v_B - v_A + 2.3v_B = -1.38$$

$$\boxed{-v_A + 3.3v_B = -1.38}$$

$$\Delta = \begin{vmatrix} 5 & -2.7 \\ -1 & 3.3 \end{vmatrix} = 13.8$$

$$N_A = \begin{vmatrix} 12.42 & -2.7 \\ -1.38 & 3.3 \end{vmatrix} = 37.26$$

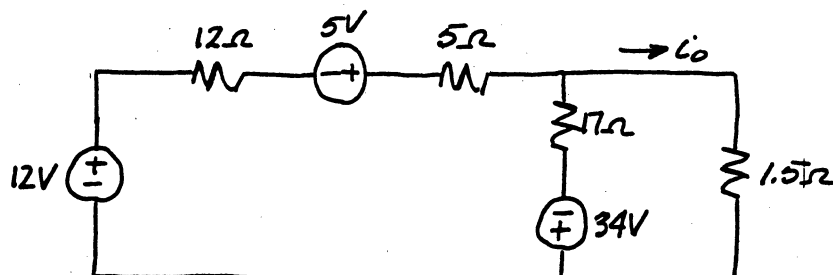
$$N_B = \begin{vmatrix} 5 & 12.42 \\ -1 & -1.38 \end{vmatrix} = 5.52$$

$$\therefore v_A = \frac{N_A}{\Delta} = 2.7 \text{ V}$$

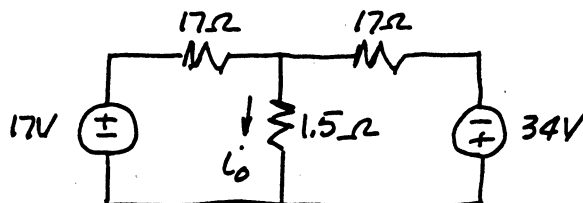
$$\therefore v_B = \frac{N_B}{\Delta} = \frac{5.52}{13.8} = 0.4 \text{ V}$$

$$\therefore i_o = \frac{v_B - v_A}{2.3} = \frac{-2.3}{2.3} = -1 \text{ mA}$$

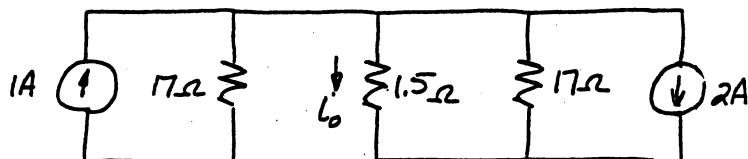
P 4.51 [a] Applying a source transformation to each current source yields



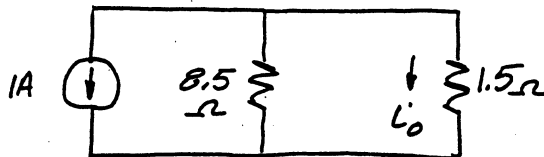
Now combine the 12-V and 5-V sources into a single voltage source and the 12-Ω and 5-Ω resistors into a single resistor, to get



Now use a source transformation on each voltage source, thus

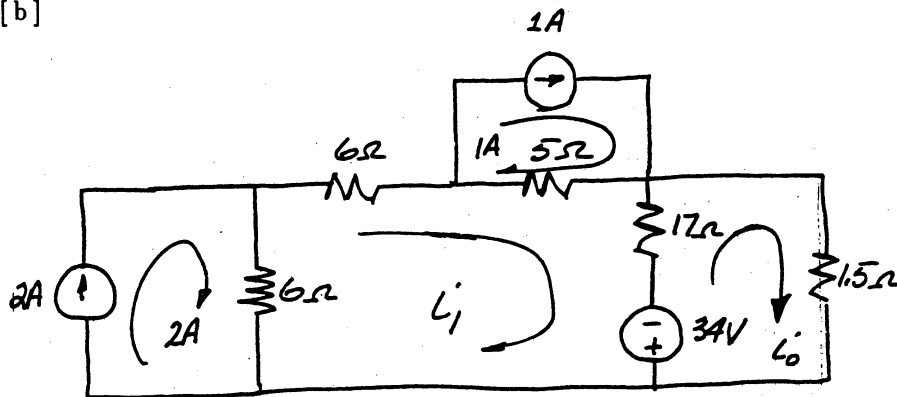


which can be reduced to



$$\therefore i_o = \frac{-1(8.5)}{10} = -0.85 \text{ A}$$

[b]



$$6(i_1 - 2) + 6i_1 + 5(i_1 - 1) + 17(i_1 - i_o) - 34 = 0$$

$$34i_1 - 17i_o = 51 \quad \text{or} \quad \boxed{2i_1 - i_o = 3}$$

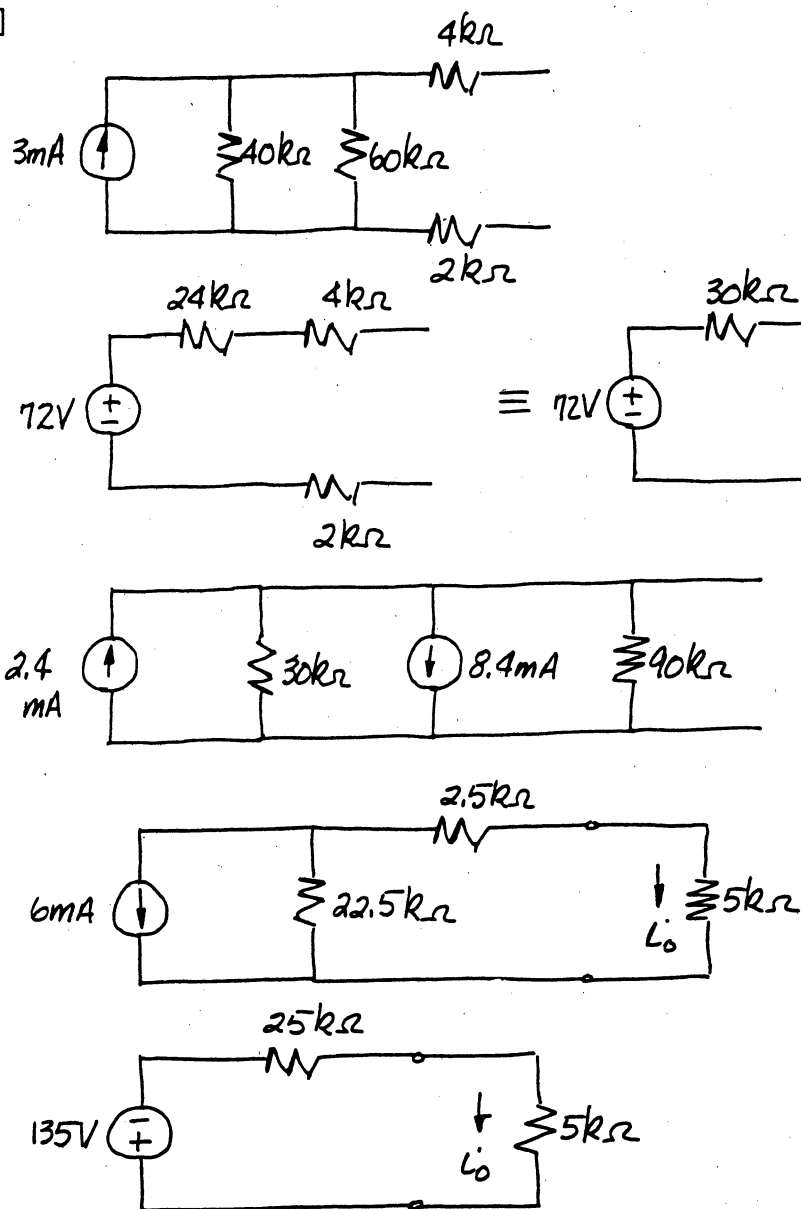
$$\text{or } 34 + 17(i_o - i_1) + 1.5i_o = 0 \quad \text{or} \quad \boxed{-17i_1 + 18.5i_o = -34}$$

$$\Delta = \begin{vmatrix} 2 & -1 \\ -17 & 18.5 \end{vmatrix} = 37 - 17 = 20$$

$$N_o = \begin{vmatrix} 2 & 3 \\ -17 & -34 \end{vmatrix} = -68 + 51 = -17$$

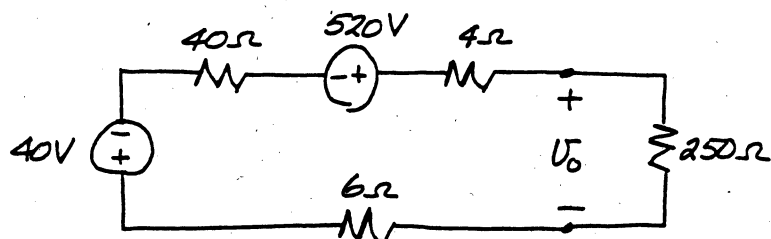
$$i_o = \frac{N_o}{\Delta} = \frac{-17}{20} = -0.85 \text{ A}$$

P4.52 [a]

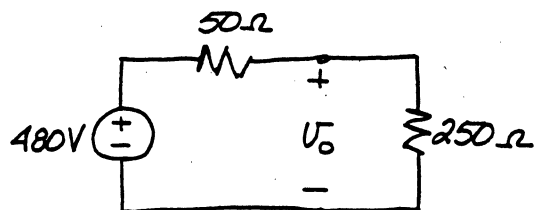


$$i_o = \frac{-135}{30} = -4.5\text{mA}$$

Next use a source transformation to convert the 1-A current source and 40- Ω resistor

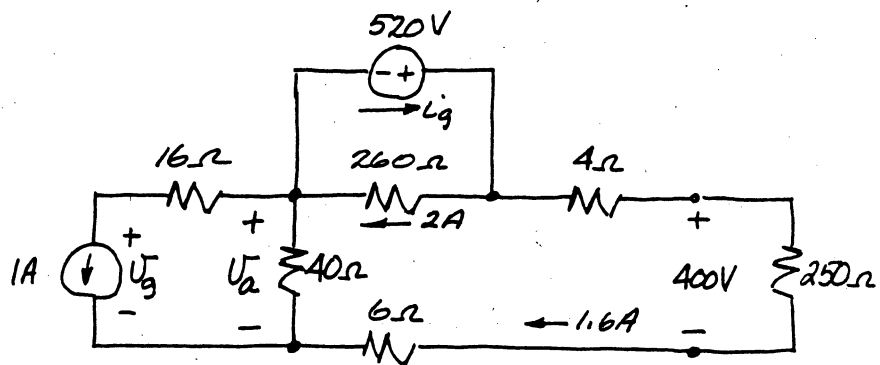


which simplifies to



It follows that $v_o = \frac{480}{300}(250) = 400 \text{ V}$

[b] Return to the original circuit with $v_o = 400 \text{ V}$



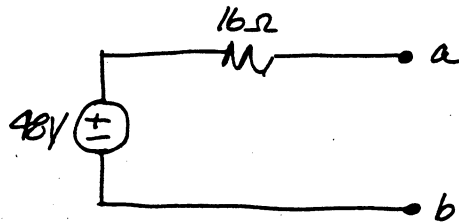
$$i_g = \frac{520}{260} + 1.6 = 3.6 \text{ A}$$

$$p_{520\text{V}}(\text{developed}) = (520)(3.6) = 1872 \text{ W}$$

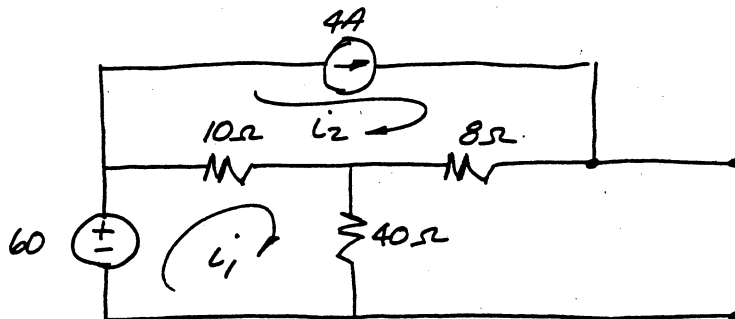
$$\begin{aligned}
 [c] \quad & v_a + 520 - 1.6(250 + 4 + 6) = 0 \\
 & v_a = -104 \text{ V} \\
 & 16(1) + v_g = -104 \\
 & v_g = -120 \text{ V} \\
 & p_{1A}(\text{developed}) = (120)(1) = 120 \text{ W} \\
 [d] \quad & \sum p_{\text{dev}} = 1872 + 120 = 1992 \text{ W} \\
 & p_{16\Omega} = 16 \text{ W} \\
 & p_{40\Omega} = \frac{(104)^2}{40} = 270.40 \text{ W} \\
 & p_{260\Omega} = (2)^2(260) = 1040 \text{ W} \\
 & p_{4\Omega} = (1.6)^2(4) = 10.24 \text{ W} \\
 & p_{250\Omega} = \frac{(400)^2}{250} = 640 \text{ W} \\
 & p_{6\Omega} = (1.6)^2(6) = 15.36 \text{ W} \\
 & \sum p_{\text{diss}} = 1992 \text{ W} \\
 & \therefore \sum p_{\text{dev}} = \sum p_{\text{diss}} = 1992 \text{ W}
 \end{aligned}$$

P 4.54 $v_{\text{Th}} = \frac{60}{50} \times 40 = 48 \text{ V}$

$$R_{\text{Th}} = 8 + \frac{(40)(10)}{50} = 16 \Omega$$



P 4.55



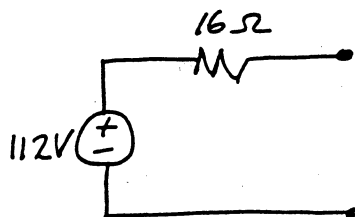
$$60 = 10(i_1 - 4) + 40i_1$$

$$100 = 50i_1$$

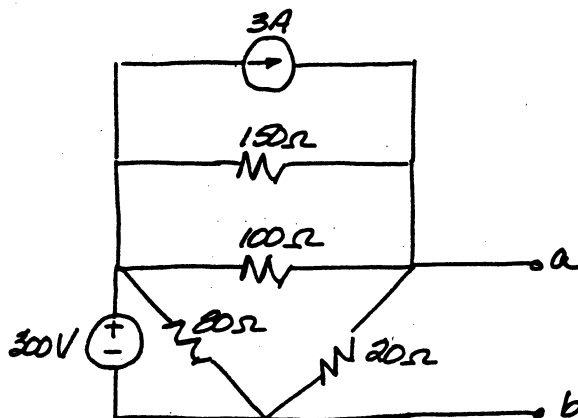
$$i_1 = 2 \text{ A}$$

$$v_{Th} = 8i_2 + 40i_1 = 32 + 80 = 112 \text{ V}$$

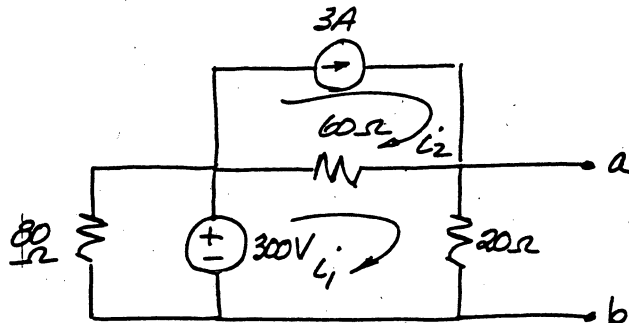
$$R_{Th} = 8 + \frac{(10)(40)}{50} = 16 \Omega$$



P4.56 After replacing the 40Ω - 10Ω - 8Ω wye with an equivalent delta the circuit becomes



Now the circuit can be further simplified to

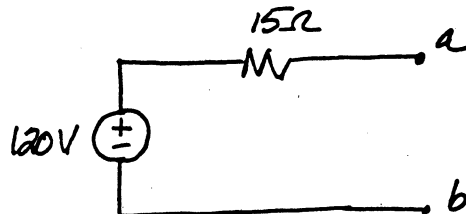


$$300 = 60(i_1 - 3) + 20i_1$$

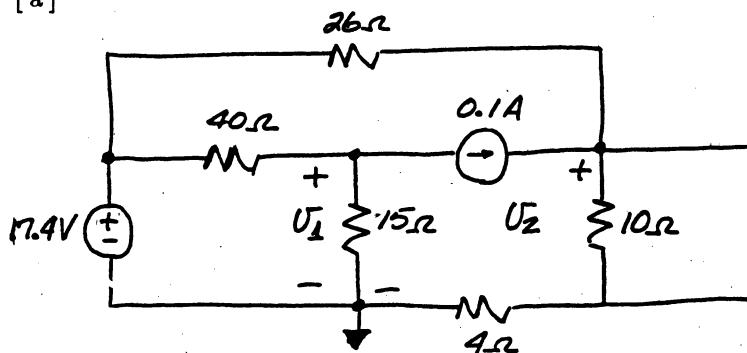
$$300 = 80i_1 - 180$$

$$i_1 = \frac{480}{80} = 6 \text{ A}$$

$$v_{Th} = (6)(20) = 120 \text{ V}; \quad R_{Th} = \frac{(60)(20)}{80} = 15 \Omega$$



P4.57 [a]

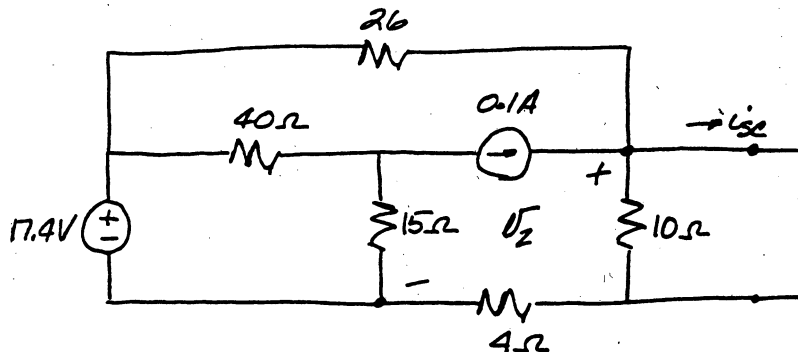


$$\frac{v_2 - 17.4}{26} + \frac{v_2}{14} - 0.1 = 0$$

$$14v_2 - 243.6 + 26v_2 = 36.4$$

$$40v_2 = 280; \quad v_2 = 7 \text{ V}$$

$$v_{Th} = \frac{v_2}{14}(10) = 5 \text{ V}$$



$$\frac{v_2 - 17.4}{26} - 0.1 + \frac{v_2}{4} = 0$$

$$4v_2 - 69.6 + 26v_2 - 10.4 = 0$$

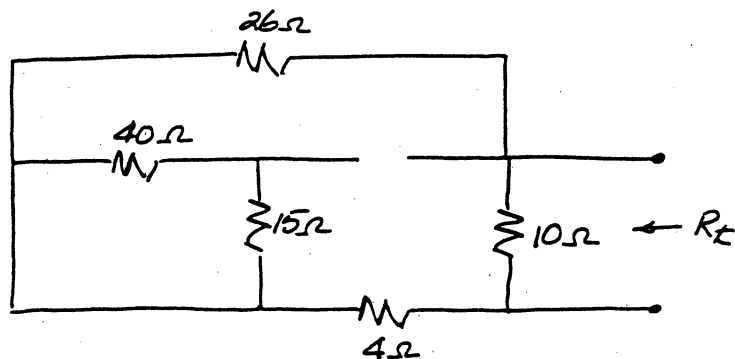
$$30v_2 = 80$$

$$v_2 = \frac{8}{3} \text{ V}$$

$$i_{sc} = \frac{v_2}{4} = \frac{2}{3} \text{ A}$$

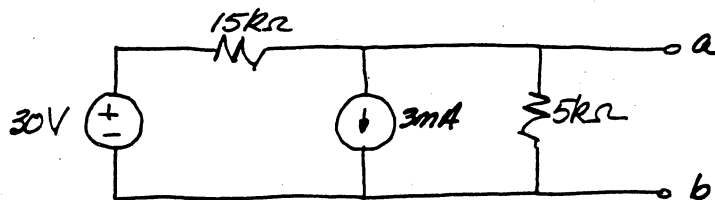
$$R_{Th} = \frac{5}{(2/3)} = 7.5 \Omega$$

[b]

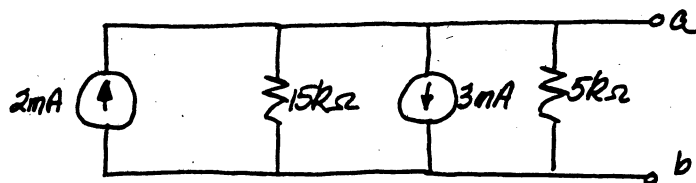


$$R_{Th} = 30 // 10 = 7.5 \Omega$$

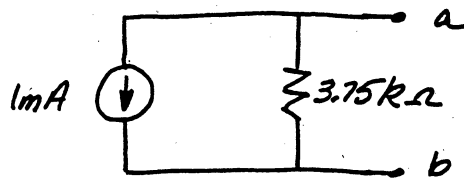
P 4.58 First we make the observation that the 10-mA current source and the 10-k Ω resistor will have no influence on the behavior of the circuit with respect to the terminals a,b. This follows because they are in parallel with an ideal voltage source. Hence our circuit can be simplified to



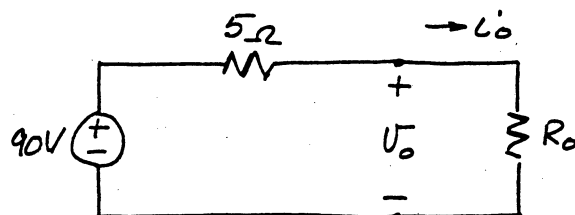
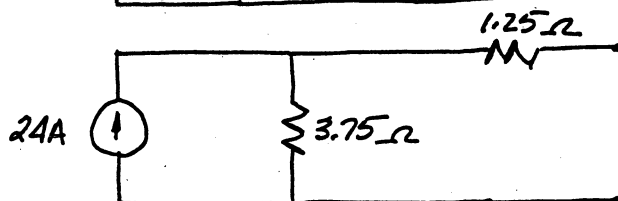
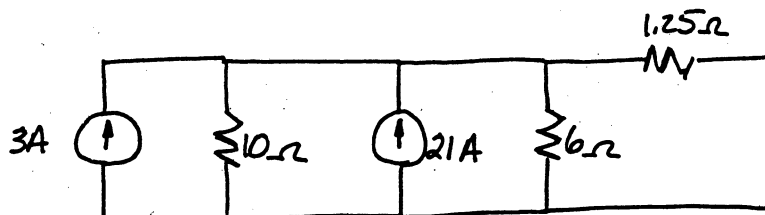
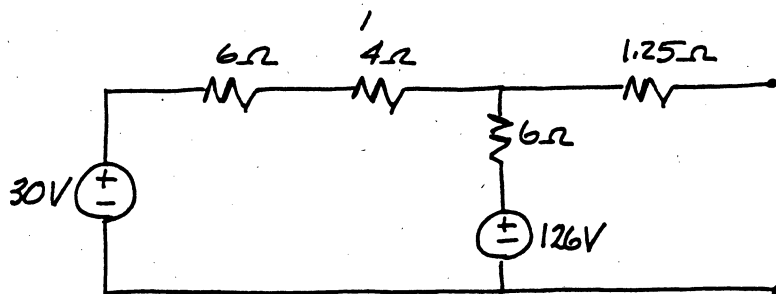
or



Therefore the Norton equivalent is

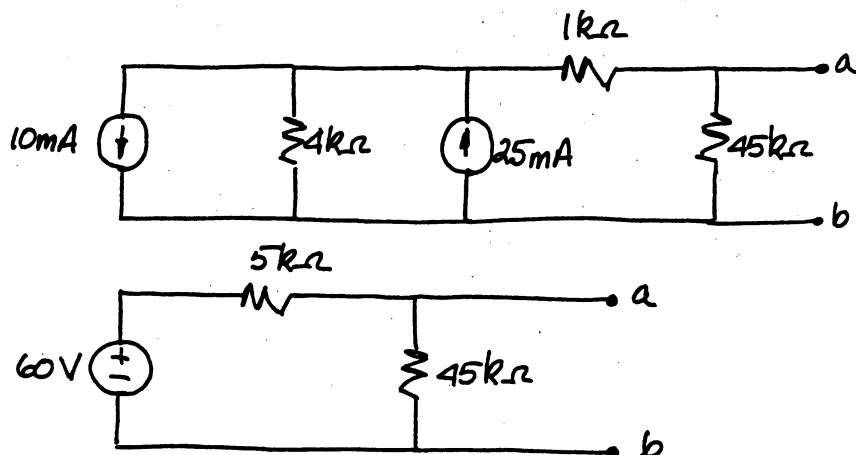


P 4.59 First, find the Thévenin equivalent with respect to R_o .
 $15//10 = 6\Omega$

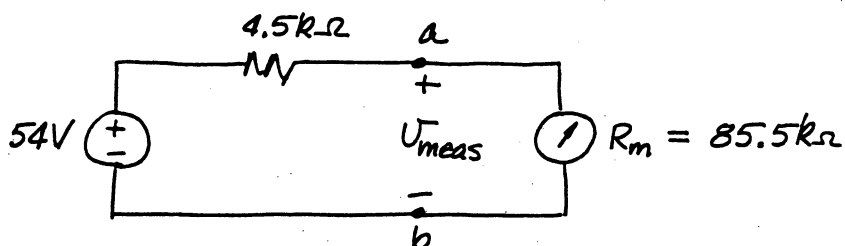


R_o	i_o	v_o	R_o	i_o	v_o
0	18	0	25	3	75
1	15	15.00	40	2	80
3	11.25	33.75	55	1.5	82.50
5	9.00	45.00	70	1.2	84.00
10	6.00	60.00	85	1.0	85.00
15	4.50	67.50	95	0.9	85.50

P4.60 [a] First, find the Thévenin equivalent with respect to a,b using a succession of source transformations.



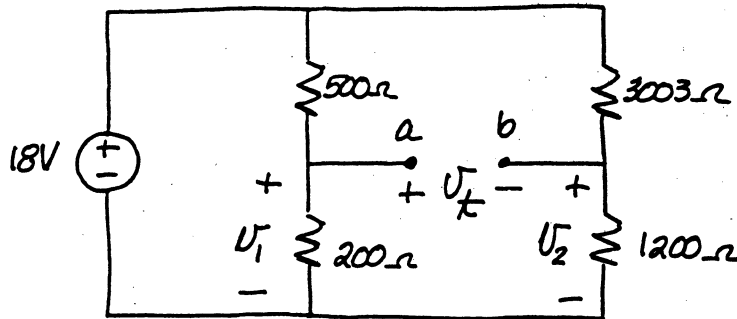
$$\therefore v_{Th} = \frac{45}{50}(60) = 54 \text{ V}; \quad R_{Th} = \frac{(5)(45)}{50} = 4.5 \text{ k}\Omega$$



$$v_{meas} = \frac{54}{90}(85.5) = 51.30 \text{ V}$$

[b] % error = $\left(\frac{51.30 - 54}{54} \right) \times 100 = -5.00\%$

P 4.61

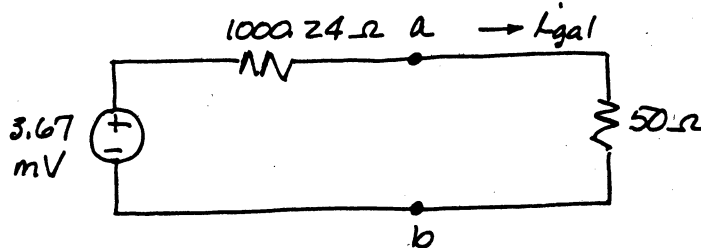


$$v_1 = \frac{18}{700}(200) = \frac{36}{7} \text{ V}$$

$$v_2 = \frac{18}{4203}(1200) \text{ V}$$

$$v_{Th} = v_1 - v_2 = \frac{36}{7} - \frac{21,600}{4203} = \frac{108}{29,421} = 3.67 \text{ mV}$$

$$R_{Th} = \frac{(500)(200)}{700} + \frac{(3003)(1200)}{4203} = \frac{29,428,200}{29,421} = 1000.24 \Omega$$



$$i_{gal} = \frac{3.67 \times 10^{-3}}{1.05024 \times 10^3} = 3.50 \mu\text{A}$$

P 4.62

$$v_{Th} = -80i_b(50 \times 10^3) = -40 \times 10^5 i_b$$

$$(500 \times 10^{-6})(100) = 1410i_b + (4 \times 10^{-5})(-40 \times 10^5 i_b)$$

$$0.05 = (1410 - 160)i_b = 1250i_b$$

$$i_b = 40 \mu\text{A}$$

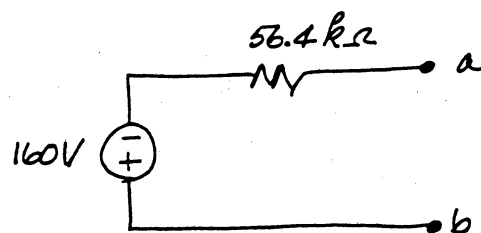
$$\therefore v_{Th} = (-40 \times 10^5)(40 \times 10^{-6}) = -160 \text{ V}$$

$$i_{sc} = -80i_b$$

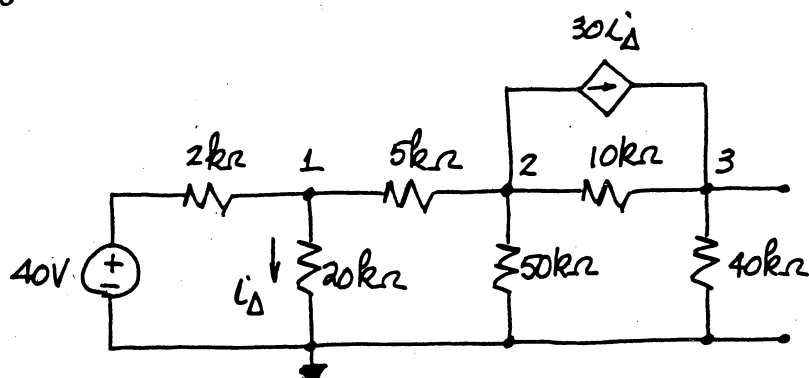
$$i_b = \frac{(500)(100)}{1410} = \frac{5000}{141} \mu\text{A}$$

$$i_{sc} = \frac{-80(5000)}{141} \times 10^{-6}$$

$$R_{Th} = \frac{-160(141)}{-80(5000) \times 10^{-6}} = 56.40 \text{ k}\Omega$$



P4.63



$$\frac{v_1 - 40}{2} + \frac{v_1}{20} + \frac{v_1 - v_2}{5} = 0$$

$$15v_1 - 4v_2 + 0v_3 = 400$$

$$\frac{v_2}{50} + \frac{v_2 - v_1}{5} + \frac{v_2 - v_3}{10} + 30\left(\frac{v_1}{20}\right) = 0$$

$$130v_1 + 32v_2 - 10v_3 = 0$$

$$\frac{v_3}{40} + \frac{v_3 - v_2}{10} - 30\left(\frac{v_1}{20}\right) = 0$$

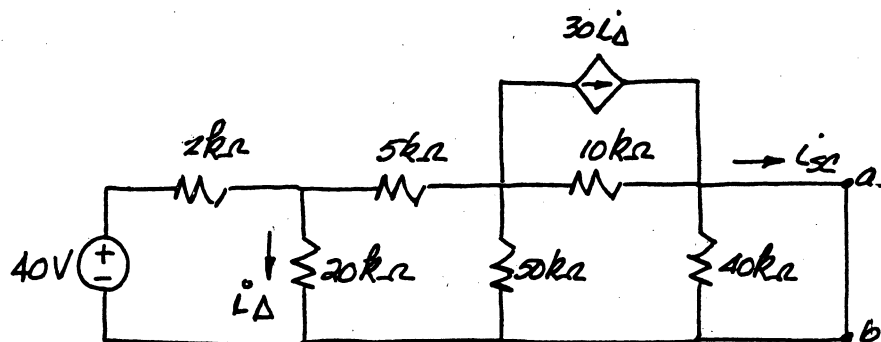
$$-60v_1 - 4v_2 + 5v_3 = 0$$

$$\Delta = \begin{vmatrix} 15 & -4 & 0 \\ 130 & 32 & -10 \\ -60 & -4 & 5 \end{vmatrix} = 10(-60 - 240) + 5(480 + 520) = 2000$$

$$N_3 = \begin{vmatrix} 15 & -4 & 400 \\ 130 & 32 & 0 \\ -60 & -4 & 0 \end{vmatrix} = 400(-520 + 1920) = 560,000$$

$$v_3 = \frac{N_3}{\Delta} = 280 \text{ V}$$

$$\therefore v_{Th} = 280 \text{ V}$$



$$\frac{v_1}{20} + \frac{v_1 - 40}{2} + \frac{v_1 - v_2}{5} = 0$$

$$15v_1 - 4v_2 = 400$$

$$\frac{v_2}{50} + \frac{v_2 - v_1}{5} + \frac{v_2}{10} + 30 \left(\frac{v_1}{20} \right) = 0$$

$$130v_1 + 32v_2 = 0$$

$$\therefore \Delta = \begin{vmatrix} 15 & -4 \\ 130 & 32 \end{vmatrix} = 1000$$

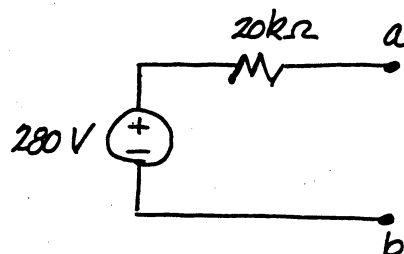
$$N_1 = \begin{vmatrix} 400 & -4 \\ 0 & 32 \end{vmatrix} = 12,800$$

$$N_2 = \begin{vmatrix} 15 & 400 \\ 130 & 0 \end{vmatrix} = -52,000$$

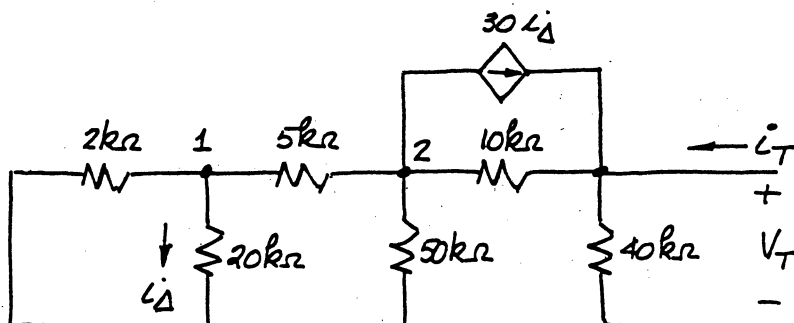
$$\therefore v_1 = \frac{N_1}{\Delta} = 12.8 \text{ V}; \quad v_2 = \frac{N_2}{\Delta} = -52 \text{ V}$$

$$i_{sc} = 30i_{\Delta} + \frac{v_2}{10} = 30 \left(\frac{12.8}{20} \right) - \frac{52}{10} = 14 \text{ mA}$$

$$R_{Th} = \frac{v_{Th}}{i_{sc}} = \left(\frac{280}{14} \right) 10^3 = 20 \text{ k}\Omega$$



Alternate calculation of R_{Th} :



$$i_T = \frac{v_T}{40} + \frac{v_T - v_2}{10} - 30 \left(\frac{v_1}{20} \right)$$

$$\frac{v_2 - v_1}{5} + \frac{v_2}{50} + \frac{v_2 - v_T}{10} + 30 \left(\frac{v_1}{20} \right) = 0$$

$$130v_1 + 32v_2 = 10v_T$$

$$\frac{v_1}{20} + \frac{v_1}{2} + \frac{v_1 - v_2}{5} = 0$$

$$15v_1 - 4v_2 = 0$$

$$\Delta = \begin{vmatrix} 130 & 32 \\ 15 & -4 \end{vmatrix} = -1000$$

$$N_1 = \begin{vmatrix} 10v_T & 32 \\ 0 & -4 \end{vmatrix} = -40v_T$$

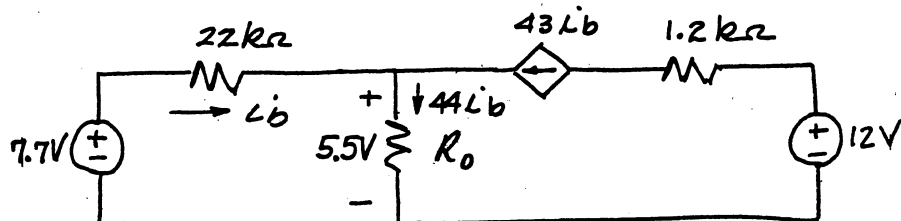
$$N_2 = \begin{vmatrix} 130 & 10v_T \\ 15 & 0 \end{vmatrix} = -150v_T$$

$$\therefore v_1 = 0.04v_T \quad \text{and} \quad v_2 = 0.15v_T$$

$$\therefore i_T = \frac{v_T}{40} + \frac{v_T - 0.15v_T}{10} - 1.5(0.04)v_T$$

$$\frac{i_T}{v_T} = 0.05 \text{ mS}; \quad R_{Th} = \frac{v_T}{i_T} = 20 \text{ k}\Omega$$

P 4.64 [a] Use source transformations to simplify the left side of the circuit.



$$i_b - \frac{7.7 - 5.5}{22} = 0.10 \text{ mA}$$

$$\text{Let } R_o = R_{\text{meter}} // 1.3 \text{ k}\Omega$$

$$R_o = \frac{5.5}{4.4} = 1.25 \text{ k}\Omega$$

$$\therefore \frac{(R_{\text{meter}})(1.3)}{R_{\text{meter}} + 1.3} = 1.25; \quad R_{\text{meter}} = \frac{(1.3)(1.25)}{0.05} = 32.50 \text{ k}\Omega$$

[b] Actual value of v_e :

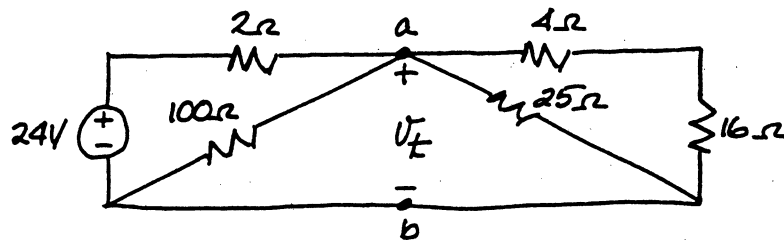
$$i_b = \frac{7.7}{22 + 44(1.3)} \cong 0.09722 \text{ mA}$$

$$v_e = 44i_b(1.3) \cong 5.56 \text{ V}$$

$$\% \text{ error} = \left(\frac{5.5 - 5.56}{5.56} \right) 100 = -1.10\%$$

P 4.65 [a] Find the Thévenin equivalent with respect to the terminals of the ammeter. This is most easily done by first finding the Thévenin with respect to the terminals of the 4.8 resistor.

Thévenin voltage: note i_ϕ is zero.

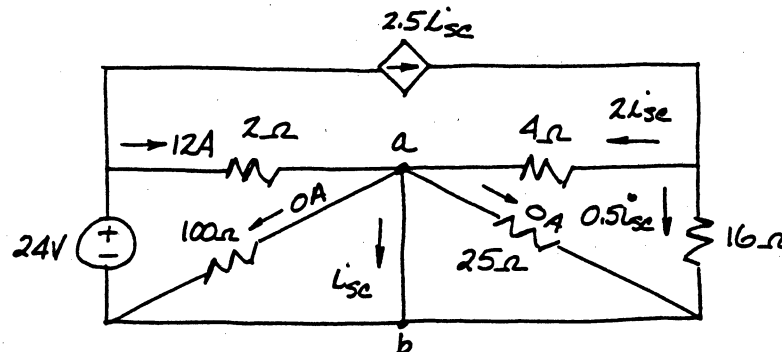


$$\frac{v_{Th}}{100} + \frac{v_{Th}}{25} + \frac{v_{Th}}{20} + \frac{v_{Th} - 24}{2} = 0$$

$$v_{Th} + 4v_{Th} + 5v_{Th} + 50v_{Th} - 1200 = 0$$

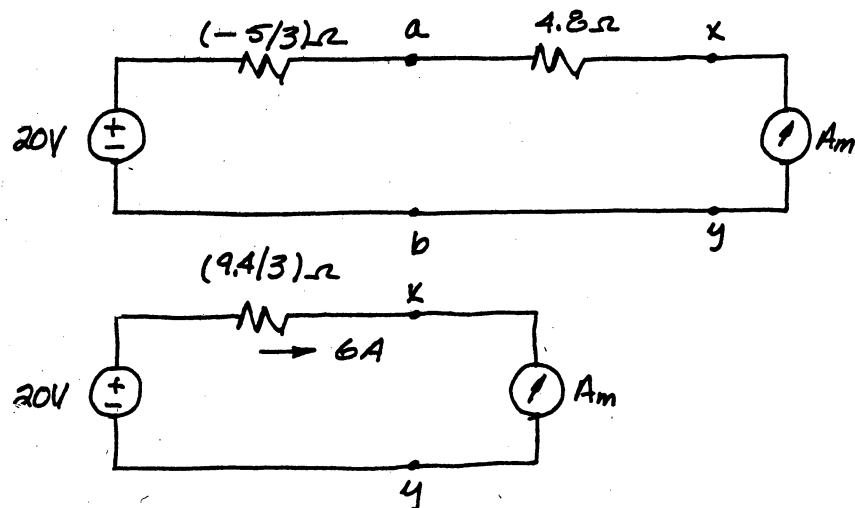
$$60v_{Th} = 1200; \quad v_{Th} = 20 \text{ V}$$

Short-circuit current:



$$i_{sc} = 12 + 2i_{sc}, \quad \therefore i_{sc} = -12 \text{ A}$$

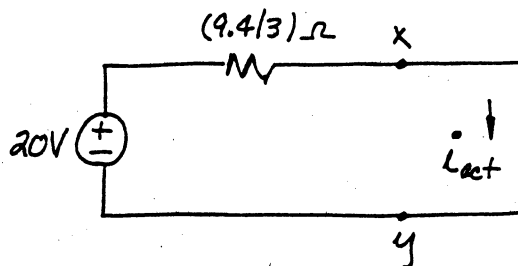
$$R_{Th} = \frac{20}{-12} = -\frac{5}{3} \Omega$$



$$R_{total} = \frac{20}{6} = \frac{10}{3} \Omega$$

$$R_{meter} = \frac{10}{3} - \frac{9.4}{3} = \frac{0.6}{3} = 0.20 \Omega$$

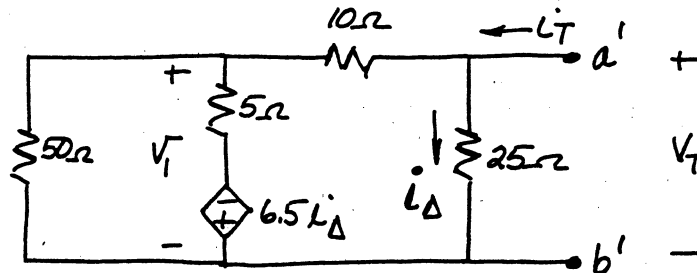
[b] Actual current:



$$i_{actual} = \frac{20}{9.4}(3) = \frac{60}{9.4} = \frac{600}{94} \approx 6.38 \text{ A}$$

$$\% \text{ error} = \frac{(6 - 30/4.7)}{30/4.7} \times 100 = \left(\frac{28.2 - 30}{30} \right) \times 100 = -6\%$$

P4.66 V_{Th} , since there are no independent sources in the circuit. To find R_{Th} we first find $R_{a'b'}$.



$$i_T = \frac{V_T}{25} + \frac{V_T - v_1}{10} = \frac{V_T}{25} + \frac{V_T}{10} - \frac{1}{10}v_1$$

$$\frac{v_1}{50} + \frac{v_1 + 6.5(V_T/25)}{5} + \frac{v_1 - V_T}{10} = 0$$

$$v_1 + 10v_1 + \frac{65}{25}V_T + 5v_1 - 5V_T = 0$$

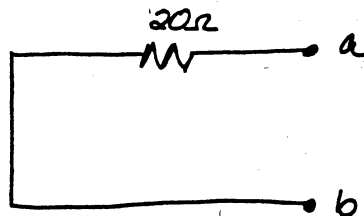
$$16v_1 = 5V_T - \frac{13}{5}V_T$$

$$v_1 = \frac{5}{16}V_T - \frac{13}{80}V_T$$

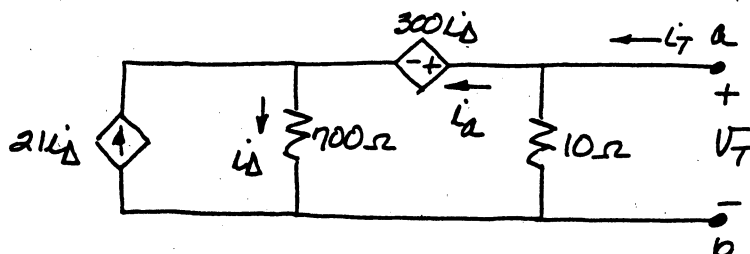
$$\therefore i_T = \frac{V_T}{25} + \frac{V_T}{10} - \frac{5}{160}V_T + \frac{13}{800}V_T$$

$$\frac{i_T}{V_T} = \frac{32 + 80 - 25 + 13}{800} = \frac{100}{800} = \frac{1}{8}$$

$$R_{a'b'} = \frac{V_T}{i_T} = 8\Omega; \quad R_{ab} = R_{a'b'} + 12 = 20\Omega; \quad R_{Th} = 20\Omega$$

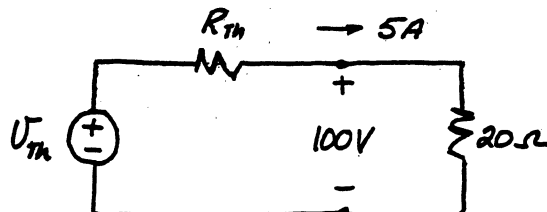


P 4.67 $V_{Th} = 0$, since circuit contains no independent sources.

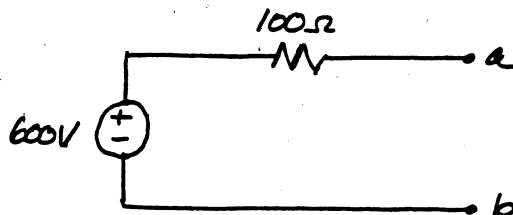


$$\begin{aligned}
 i_T &= \frac{V_T}{10} + i_a \\
 i_a &= i_\Delta - 21i_\Delta = -20i_\Delta \\
 i_\Delta &= \frac{v_T - 300i_\Delta}{700}, \quad 1000i_\Delta = v_T \\
 \therefore i_T &= \frac{V_T}{10} - 20 \left(\frac{v_T}{1000} \right) = \frac{v_T}{10} - \frac{v_T}{50} \\
 \frac{i_T}{V_T} &= \frac{1}{10} - \frac{1}{50} = \frac{4}{50} \\
 R_{Th} &= \frac{V_T}{i_T} = \frac{50}{4} = 12.5 \Omega
 \end{aligned}$$

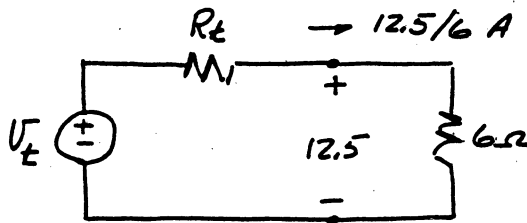
P 4.68



$$\begin{aligned}
 100 &= v_{Th} - 5R_{Th} \quad \text{and} \quad 200 = v_{Th} - 4R_{Th} \\
 \therefore 100 &= 1R_{Th}, \quad R_{Th} = 100 \Omega \\
 \therefore v_{Th} &= 100 + 5(100) = 600 \text{ V} \quad \text{or} \quad v_{Th} = 200 + 4(100) = 600 \text{ V} \\
 v_{Th} &= 600 \text{ V}, \quad R_{Th} = 100 \Omega
 \end{aligned}$$



P4.69



$$12.5 = v_{Th} - \frac{12.5}{6} R_{Th}; \quad 11.8 = v_{Th} - \frac{11.8}{0.75} R_{Th}; \quad 0.7 = \left(\frac{11.8}{0.75} - \frac{12.5}{6} \right) R_{Th}$$

$$R_{Th} = 51.28 \text{ m}\Omega$$

$$v_{Th} = 12.5 + \frac{12.5}{6} (51.28) \times 10^{-3} = 12.61 \text{ V}$$

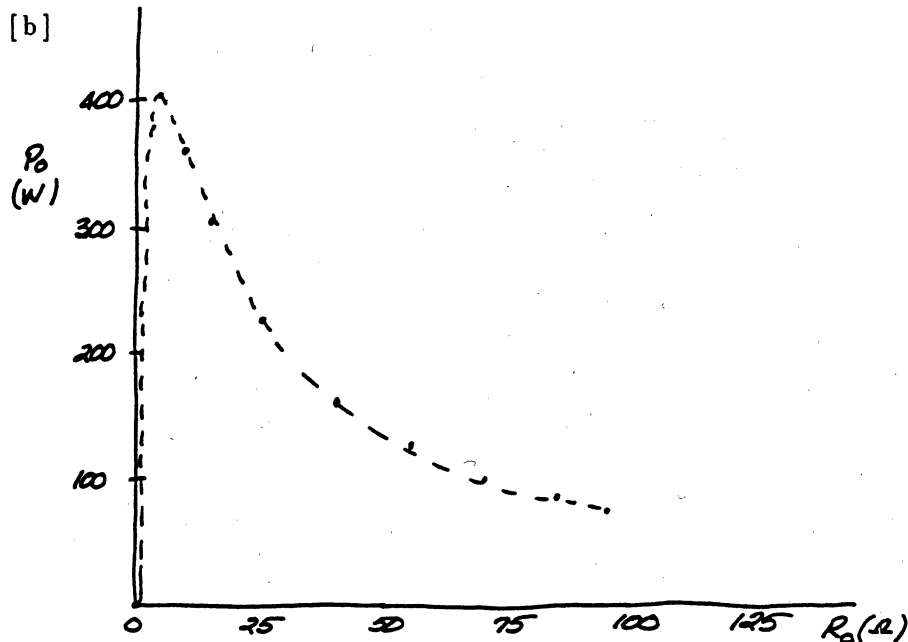
$$i_N = \frac{12.61}{0.05128} = 245.83 \text{ A}$$

$$R_N = R_{Th} = 51.28 \text{ m}\Omega$$

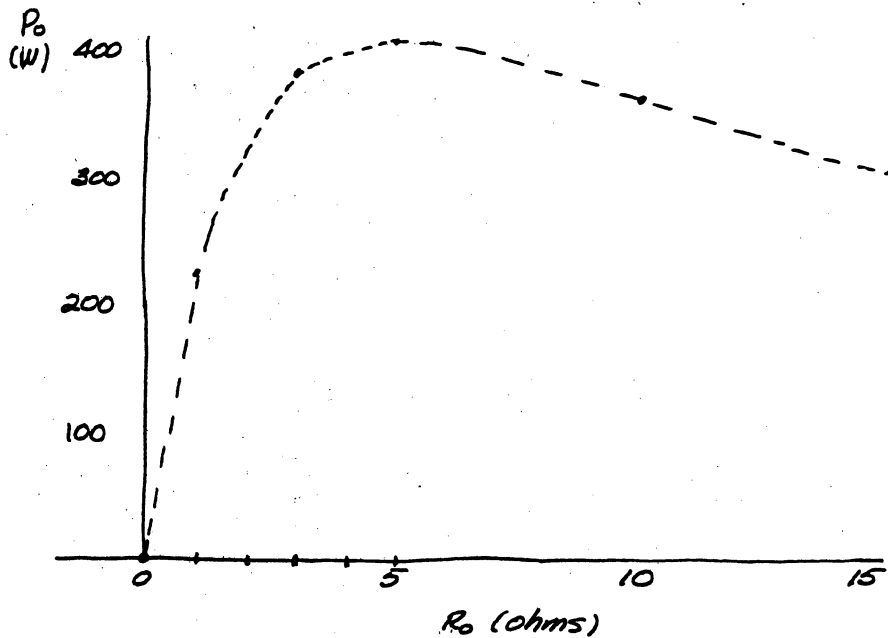
P4.70 [a]

$R_o(\Omega)$	$P_o(\text{W})$	$R_o(\Omega)$	$P_o(\text{W})$
0	0	25	225.00
1	225.00	40	160.00
3	379.69	55	123.75
5	405.00	70	100.80
10	360.00	85	85.00
15	303.75	95	76.95

[b]



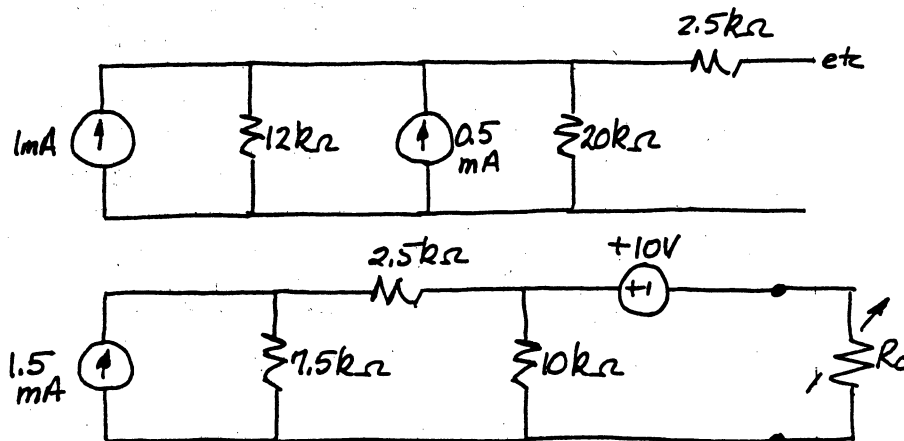
Magnify lower range of R_o scale.



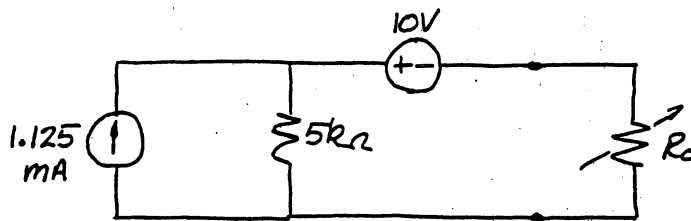
[c] $R_o = 5 \Omega$, $P_o(\max) = 405 \text{ W}$

P4.71 [a] First find the Thévenin equivalent with respect to the terminals of R_o .

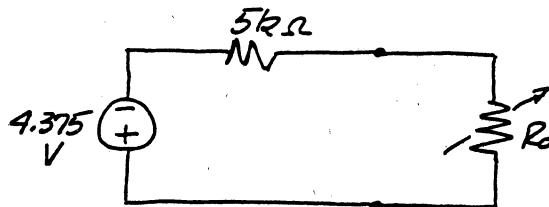
After a series of source transformations we have



Continuing with source transformations leads to



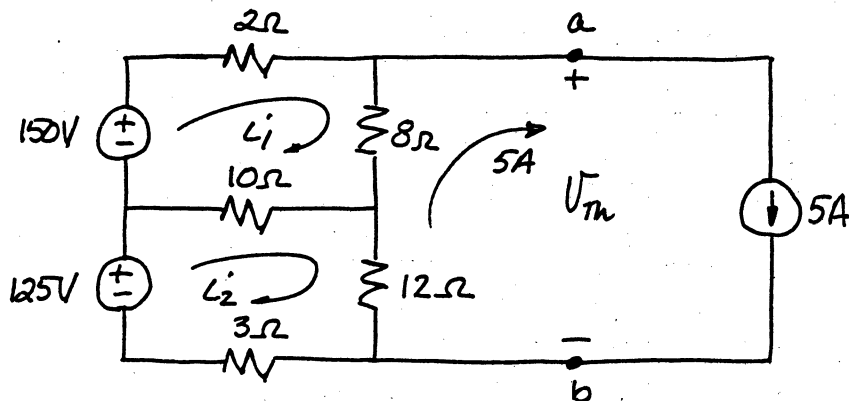
Finally we get



$$\therefore R_o = R_{Th} = 5 \text{ k}\Omega$$

$$[b] \quad P = \left(\frac{4.375}{10^4} \right)^2 (5000) = 957.03 \mu\text{W}$$

P4.72 First find the Thévenin equivalent with respect to the terminals of R_o .



$$150 = 20i_1 - 10i_2 - 40$$

$$190 = 20i_1 - 10i_2$$

$$19 = 2i_1 - i_2$$

$$125 = -10i_1 + 25i_2 - 60$$

$$185 = -10i_1 + 25i_2$$

$$\Delta = \begin{vmatrix} 2 & -1 \\ -10 & 25 \end{vmatrix} = 40$$

$$N_1 = \begin{vmatrix} 19 & -1 \\ 185 & 25 \end{vmatrix} = 660$$

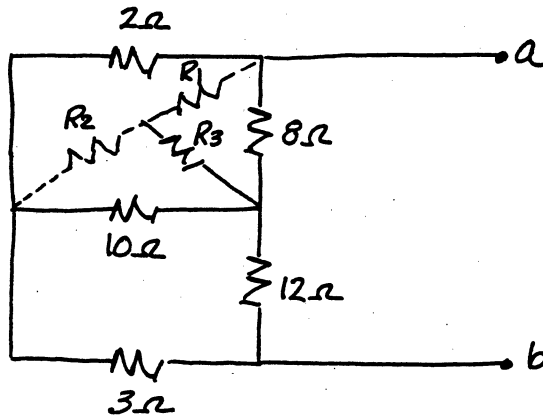
$$N_2 = \begin{vmatrix} 2 & 19 \\ -10 & 185 \end{vmatrix} = 560$$

$$i_1 = \frac{N_1}{\Delta} = \frac{660}{40} = 16.5 \text{ A}$$

$$i_2 = \frac{N_2}{\Delta} = \frac{560}{40} = 14 \text{ A}$$

$$v_{Th} = 8(i_1 - 5) + 12(i_2 - 5) = 8(11.5) + 12(9) = 200 \text{ V}$$

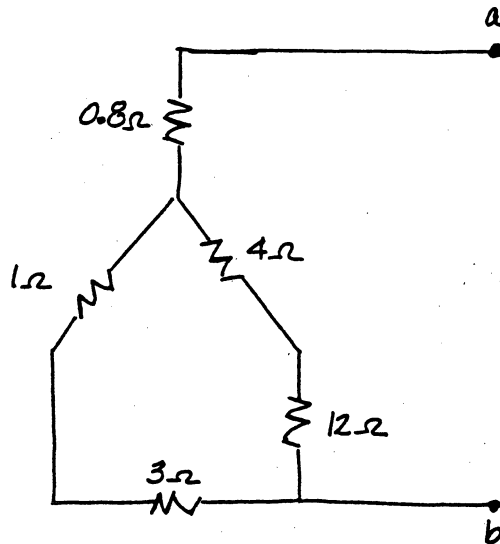
Thévenin resistance:



$$R_1 = \frac{16}{20} = 0.8 \Omega$$

$$R_2 = \frac{20}{20} = 1.0 \Omega$$

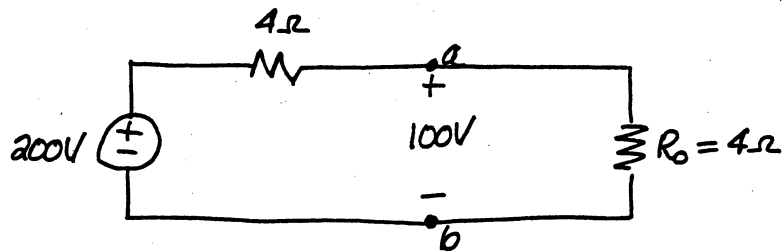
$$R_3 = \frac{80}{20} = 4.0 \Omega$$



$$R_{Th} = 0.8 + \frac{(16)(4)}{20} = 0.8 + 3.2$$

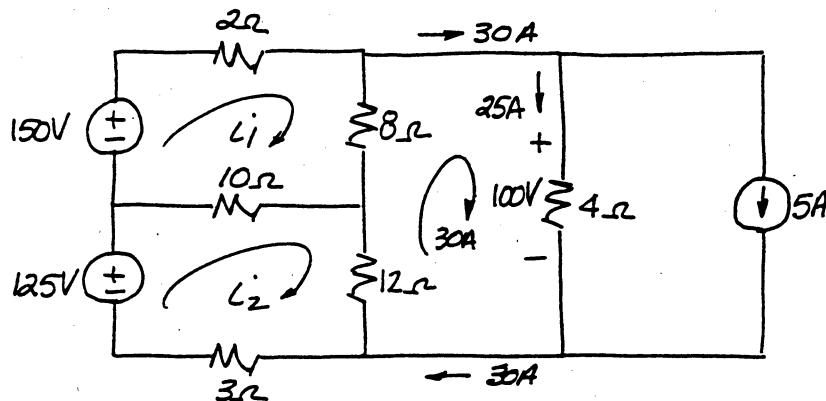
$$R_{Th} = 4 \Omega$$

Thévenin equivalent:



$$P_{\max} = \frac{(100)^2}{4} = 2500 \text{ W}$$

Now we return to the original circuit and set $R_o = 4 \Omega$. We also use the fact that when $R_o = 4 \Omega$, $v_{ab} = 100 \text{ V}$. Therefore we get the circuit shown below. After studying this circuit we note the current source is absorbing power. Hence we must find i_1 and i_2 to see if both voltage sources are developing power.



$$150 = 20i_1 - 10i_2 - 240$$

$$390 = 20i_1 - 10i_2$$

$$39 = 2i_1 - i_2$$

$$125 = -10i_1 + 25i_2 - 360$$

$$485 = -10i_1 + 25i_2$$

As before $\Delta = 40$

$$N_1 = \begin{vmatrix} 39 & -1 \\ 485 & 25 \end{vmatrix} = 1460$$

$$N_2 = \begin{vmatrix} 2 & 39 \\ -10 & 485 \end{vmatrix} = 1360$$

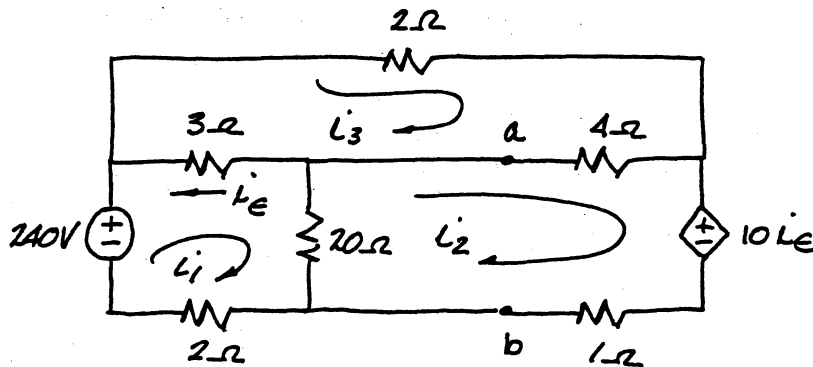
$$i_1 = \frac{N_1}{\Delta} = 36.5 \text{ A}; \quad i_2 = \frac{N_2}{\Delta} = 34 \text{ A}$$

Thus both voltage sources are developing power.

$$\sum p_{\text{dev}} = 150(36.5) + 125(34) = 9725 \text{ W}$$

$$\% \text{ delivered to } R_o = \frac{2500}{9725} \times 100 = 25.71\%$$

P 4.73 [a] Find the Thévenin equivalent with respect to the terminals of R_L .



$$240 = 25i_1 - 20i_2 - 3i_3$$

$$0 = -20i_1 + 25i_2 + 10(i_3 - i_1) - 4i_3$$

$$0 = -3i_1 - 4i_2 + 9i_3$$

$$240 = 25i_1 - 20i_2 - 3i_3$$

$$0 = -30i_1 + 25i_2 + 6i_3$$

$$0 = -3i_1 - 4i_2 + 9i_3$$

$$\Delta = \begin{vmatrix} 25 & -20 & -3 \\ -30 & 25 & 6 \\ -3 & -4 & 9 \end{vmatrix} = 25(249) + 30(-192) - 3(-45) = 600$$

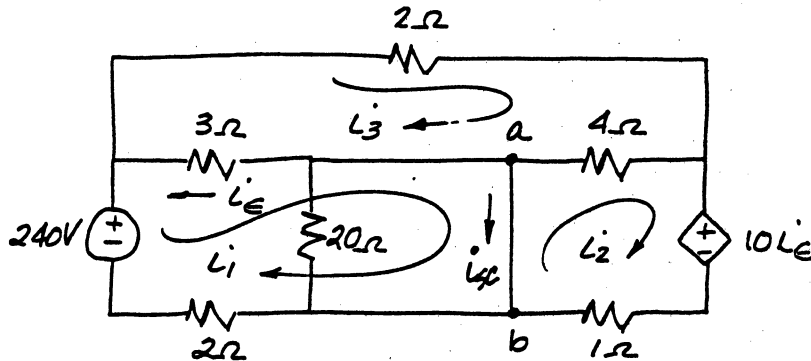
$$N_1 = \begin{vmatrix} 240 & -20 & -3 \\ 0 & 25 & 6 \\ 0 & -4 & 9 \end{vmatrix} = 240(249) = 59,760$$

$$N_2 = \begin{vmatrix} 25 & 240 & -3 \\ -30 & 0 & 6 \\ -3 & 0 & 9 \end{vmatrix} = -240(-252) = 60,480$$

$$i_1 = \frac{N_1}{\Delta} = 99.60 \text{ A}; \quad i_2 = \frac{N_2}{\Delta} = 100.80 \text{ A}$$

$$v_{\text{Th}} = v_{\text{ab}} = 20(i_1 - i_2) = -24 \text{ V}$$

Short-circuit current:



$$240 = 5i_1 - 0i_2 - 3i_3$$

$$0 = 0i_1 + 5i_2 - 4i_3 + 10(i_3 - i_1)$$

$$0 = -3i_1 - 4i_2 + 9i_3$$

$$240 = 5i_1 - 0i_2 - 3i_3$$

$$0 = -10i_1 + 5i_2 + 6i_3$$

$$0 = -3i_1 - 4i_2 + 9i_3$$

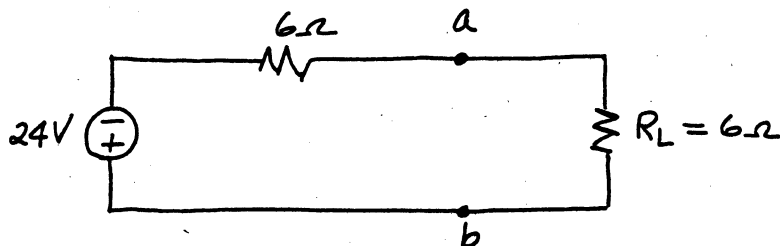
$$\Delta = \begin{vmatrix} 5 & 0 & -3 \\ -10 & 5 & 6 \\ -3 & -4 & 9 \end{vmatrix} = 5(45 - 9) + 4(30 - 30) = 180$$

$$N_1 = \begin{vmatrix} 240 & 0 & -3 \\ 0 & 5 & 6 \\ 0 & -4 & 9 \end{vmatrix} = 240(69) = 16,560$$

$$N_2 = \begin{vmatrix} 5 & 240 & -3 \\ -10 & 0 & 6 \\ -3 & 0 & 9 \end{vmatrix} = -240(-72) = 17,280$$

$$i_1 = \frac{N_1}{\Delta} = \frac{16,560}{180} = 92 \text{ A}; \quad i_2 = \frac{N_2}{\Delta} = \frac{17,280}{180} = 96 \text{ A}$$

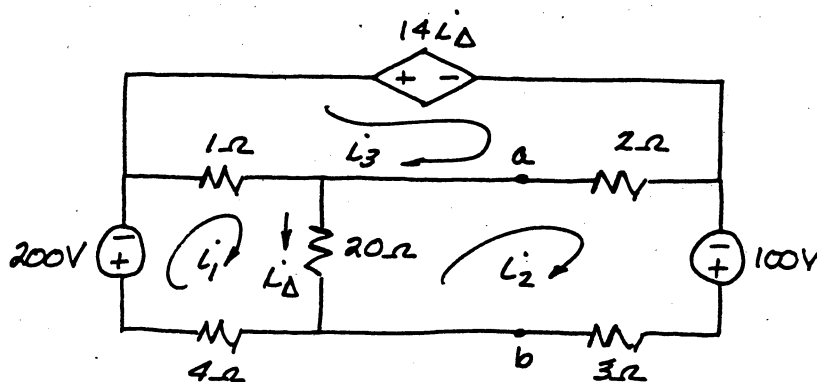
$$i_{sc} = i_1 - i_2 = -4 \text{ A}; \quad R_{Th} = \frac{v_{Th}}{i_{sc}} = \frac{-24}{-4} = 6 \Omega$$



$$R_L = R_{Th} = 6 \Omega$$

$$[b] \quad P_{\max} = \left(\frac{24}{12}\right)^2 (16) = 24 \text{ W}$$

P 4.74 [a] We begin by finding the Thévenin equivalent with respect to the terminals of R_o .



$$\begin{aligned} 200 + 25i_1 - 20i_2 - i_3 &= 0 \\ -20i_1 + 25i_2 - 2i_3 - 100 &= 0 \\ -i_1 - 2i_2 + 3i_3 + 14(i_1 - i_2) &= 0 \\ \therefore 25i_1 - 20i_2 - i_3 &= -200 \\ -20i_1 + 25i_2 - 2i_3 &= 100 \\ 13i_1 - 16i_2 + 3i_3 &= 0 \end{aligned}$$

$$\Delta = \begin{vmatrix} 25 & -20 & -1 \\ -20 & 25 & -2 \\ 13 & -16 & 3 \end{vmatrix} = 25(75 - 32) + 20(-60 - 16) + 13(40 + 25) = 400$$

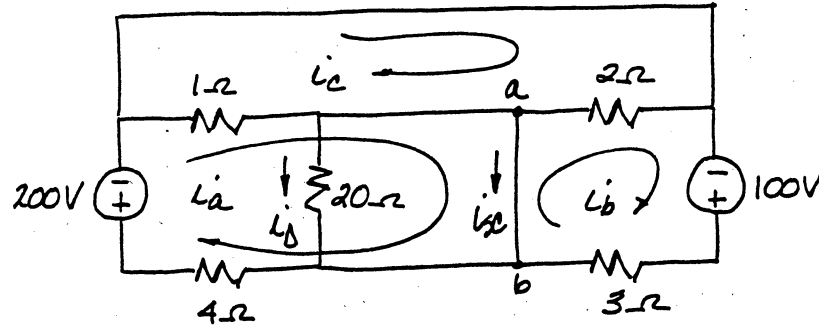
$$N_1 = \begin{vmatrix} -200 & -20 & -1 \\ 100 & 25 & -2 \\ 0 & -16 & 3 \end{vmatrix} = -200(75 - 32) - 100(-60 - 16) = -1000$$

$$N_2 = \begin{vmatrix} 25 & -200 & -1 \\ -20 & 100 & -2 \\ 13 & 0 & 3 \end{vmatrix} = 200(-60 + 26) + 100(75 + 13) = 2000$$

$$i_1 = \frac{N_1}{\Delta} = \frac{-1000}{400} = -2.5 \text{ A}; \quad i_2 = \frac{N_2}{\Delta} = \frac{2000}{400} = 5 \text{ A}$$

$$\therefore i_{\Delta} = i_1 - i_2 = -7.5 \text{ A}; \quad v_{Th} = 20i_{\Delta} = -150 \text{ V}$$

Now find the short-circuit current.



Note with the short circuit from a to b that i_{Δ} is zero, hence $14i_{\Delta}$ is also zero.

$$-200 = 5i_a + 0i_b - i_c$$

$$100 = 0i_a + 5i_b - 2i_c$$

$$0 = -i_a - 2i_b + 3i_c$$

$$\Delta = \begin{vmatrix} 5 & 0 & -1 \\ 0 & 5 & -2 \\ -1 & -2 & 3 \end{vmatrix} = 5(15 - 4) - 1(5) = 55 - 5 = 50$$

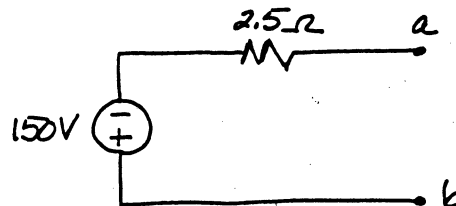
$$\Delta = 50$$

$$N_a = \begin{vmatrix} -200 & 0 & -1 \\ 100 & 5 & -2 \\ 0 & -2 & 3 \end{vmatrix} = -200(15 - 4) - 100(-2) = -2200 + 200 = -2000$$

$$N_b = \begin{vmatrix} 5 & -200 & -1 \\ 0 & 100 & -2 \\ -1 & 0 & 3 \end{vmatrix} = 200(-2) + 100(15 - 1) = -400 + 1400 = 1000$$

$$i_a = \frac{N_a}{\Delta} = \frac{-2000}{50} = -40 \text{ A}; \quad i_b = \frac{N_b}{\Delta} = \frac{1000}{50} = 20 \text{ A}$$

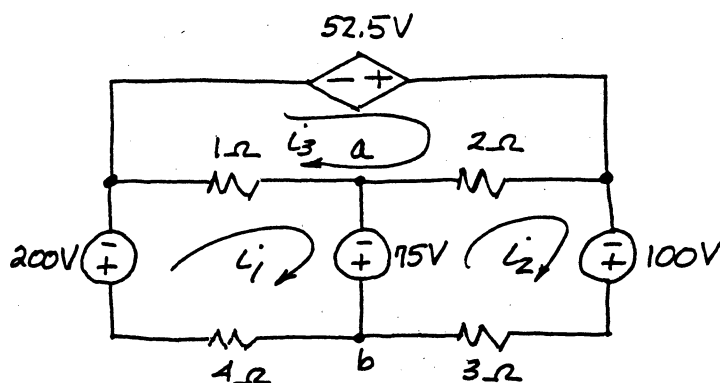
$$i_{sc} = i_a - i_b = -60 \text{ A}; \quad R_{Th} = \frac{V_{Th}}{i_{sc}} = \frac{-150}{-60} = 2.5 \Omega$$



For maximum power transfer $R_o = R_{Th} = 2.5 \Omega$

$$[b] \quad P_{max} = \left(\frac{150}{5} \right)^2 (2.5) = 2,250 \text{ W}$$

P4.75 From the solution of Problem 4.74 we know that when R_o is $2.5\ \Omega$, the voltage across R_o is 75 V , positive at the lower terminal. Therefore our problem reduces to the analysis of the following circuit. In constructing the circuit we have used the fact that i_Δ is $-75/20$, or -3.75 A , and hence $14i_\Delta$ is -52.50 V .



$$200 + 5i_1 - 0i_2 - i_3 - 75 = 0$$

$$0i_1 + 5i_2 - 2i_3 - 100 + 75 = 0$$

$$-i_1 - 2i_2 + 3i_3 - 52.5 = 0$$

$$5i_1 - 0i_2 - i_3 = -125$$

$$0i_1 + 5i_2 - 2i_3 = 25$$

$$-i_1 - 2i_2 + 3i_3 = 52.5$$

$$\Delta = \begin{vmatrix} 5 & 0 & -1 \\ 0 & 5 & -2 \\ -1 & -2 & 3 \end{vmatrix} = 50$$

$$N_1 = \begin{vmatrix} -125 & 0 & -1 \\ 25 & 5 & -2 \\ 52.5 & -2 & 3 \end{vmatrix} = -1062.50$$

$$N_2 = \begin{vmatrix} 5 & -125 & -1 \\ 0 & 25 & -2 \\ -1 & 52.5 & 3 \end{vmatrix} = 625$$

$$N_3 = \begin{vmatrix} 5 & 0 & -125 \\ 0 & 5 & 25 \\ -1 & -2 & 52.5 \end{vmatrix} = 937.50$$

$$i_1 = \frac{N_1}{\Delta} = \frac{-1062.50}{50} = -21.25\text{ A}$$

$$i_2 = \frac{N_2}{\Delta} = \frac{625}{50} = 12.5\text{ A}$$

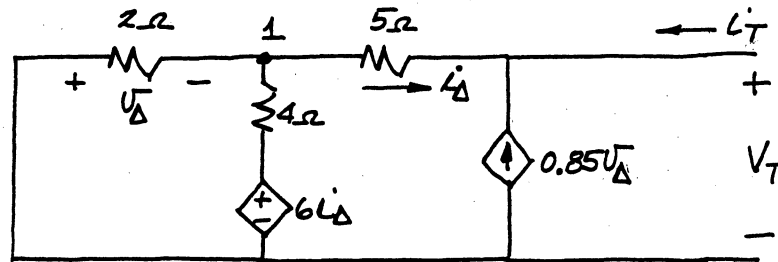
$$i_3 = \frac{N_3}{\Delta} = \frac{937.50}{50} = 18.75\text{ A}$$

Note that all three sources are developing power. Therefore

$$\sum p_{\text{dev}} = 200(21.25) + 100(12.5) + 52.5(18.75) = 6484.375 \text{ W}$$

$$\% \text{ delivered} = \frac{2250}{6484.375} \times 100 = 34.70\%$$

P 4.76 [a] Find the Thévenin resistance



$$i_T = -0.85v_\Delta + \frac{V_T - v_1}{5}, \quad v_\Delta = -v_1$$

$$i_T = 0.85v_1 + 0.2V_T - 0.2v_1 = 0.65v_1 + 0.2V_T$$

$$\frac{v_1}{2} + \frac{v_1 - 6i_\Delta}{4} + \frac{v_1 - V_T}{5} = 0$$

$$10v_1 + 5v_1 - 30i_\Delta + 4v_1 - 4V_T = 0$$

$$19v_1 - 30\left(\frac{v_1 - V_T}{5}\right) - 4V_T = 0$$

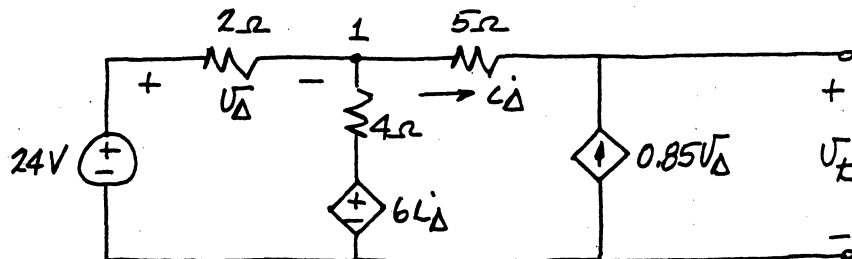
$$13v_1 + 2V_T = 0; \quad \therefore v_1 = \frac{-V_T}{6.5}$$

$$\therefore i_T = 0.65\left(\frac{-V_T}{6.5}\right) + 0.2V_T$$

$$\frac{i_T}{V_T} = \frac{1}{R_{\text{Th}}} = 0.1$$

$$\therefore R_{\text{Th}} = 10 \Omega = R_o$$

[b] Find the Thévenin voltage.



$$\frac{v_1 - 24}{2} + \frac{v_1 - 6i_\Delta}{4} + \frac{v_1 - v_{Th}}{5} = 0$$

$$10v_1 - 240 + 5v_1 - 30i_\Delta + 4v_1 - 4v_{Th} = 0$$

$$19v_1 - 30\left(\frac{v_1 - v_{Th}}{5}\right) - 4v_{Th} = 240$$

$$\boxed{13v_1 + 2v_{Th} = 240}$$

$$\frac{v_{Th} - v_1}{5} - 0.85v_\Delta = 0$$

$$v_\Delta = 24 - v_1; \quad 0.85v_\Delta = 20.4 - 0.85v_1$$

$$\frac{v_{Th} - v_1}{5} - 20.4 + 0.85v_1 = 0$$

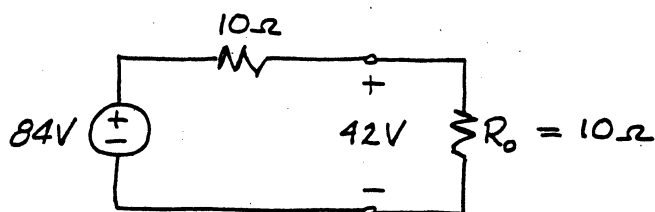
$$\boxed{3.25v_1 + v_{Th} = 102}$$

$$\Delta = \begin{vmatrix} 13 & 2 \\ 3.25 & 1 \end{vmatrix} = 6.5$$

$$N_{Th} = \begin{vmatrix} 13 & 240 \\ 3.25 & 102 \end{vmatrix} = 1326 - 780 = 546$$

$$v_{Th} = \frac{N_{Th}}{\Delta} = \frac{546}{6.5} = 84 \text{ V}$$

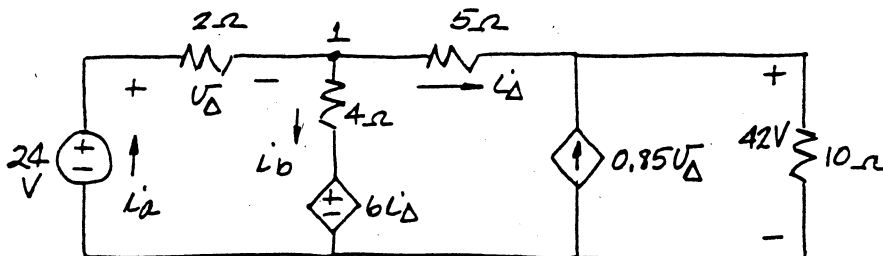
Therefore the Thévenin equivalent is



The maximum power delivered to R_o is

$$P_{\max} = \frac{(42)^2}{10} = 176.40 \text{ W}$$

When $R_o = 10\Omega$ the original circuit becomes



$$\frac{v_1 - 24}{2} + \frac{v_1 - 6i_\Delta}{4} + \frac{v_1 - 42}{5} = 0$$

$$10v_1 - 240 + 5v_1 - 30i_\Delta + 4v_1 - 168 = 0$$

$$19v_1 - 30\left(\frac{v_1 - 42}{5}\right) = 408$$

$$13v_1 = 156, \quad v_1 = 12 \text{ V}$$

$$i_\Delta = \frac{12 - 42}{5} = -6 \text{ A}$$

$$i_b = \frac{12 - 6(-6)}{4} = 12 \text{ A}$$

$$i_a = \frac{24 - 12}{2} = 6 \text{ A}$$

$$v_\Delta = 24 - 12 = 12 \text{ V}, \quad 0.85v_\Delta = 10.20 \text{ A}$$

$$p_{24\text{V}} = -24i_a = -144 \text{ W (dev)}$$

$$p_{6i_\Delta} = (6i_\Delta)(i_b) = -36(12) = -432 \text{ W (dev)}$$

$$p_{0.85v_\Delta} = -42(10.20) = -428.4 \text{ W (dev)}$$

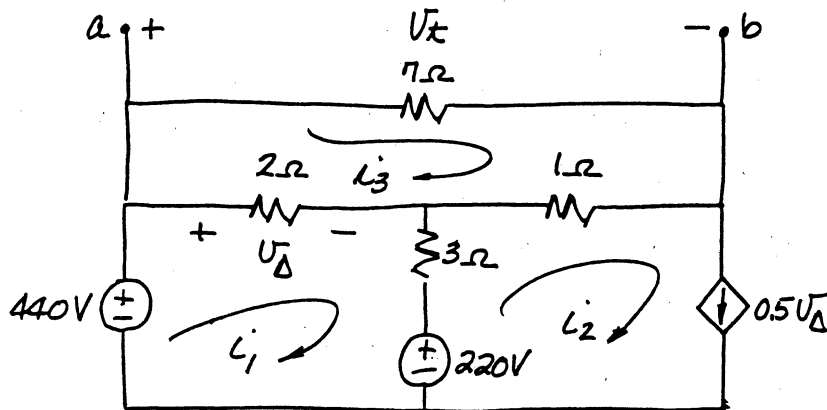
$\therefore$ All three sources are developing power.

$$\therefore \sum p_{\text{dev}} = 144 + 432 + 428.40 = 1004.40 \text{ W}$$

$\therefore$ Percent delivered to R_o is

$$\% \text{ delivered} = \frac{176.40}{1004.40} \times 100 \cong 17.56\%$$

P4.77 Find the Thévenin equivalent with respect to the terminals of R_o .



$$440 = 5i_1 - 3(0.5)(2)(i_1 - i_3) + 220 - 2i_3$$

$$0 = -2i_1 - 0.5(2)(i_1 - i_3) + 10i_3$$

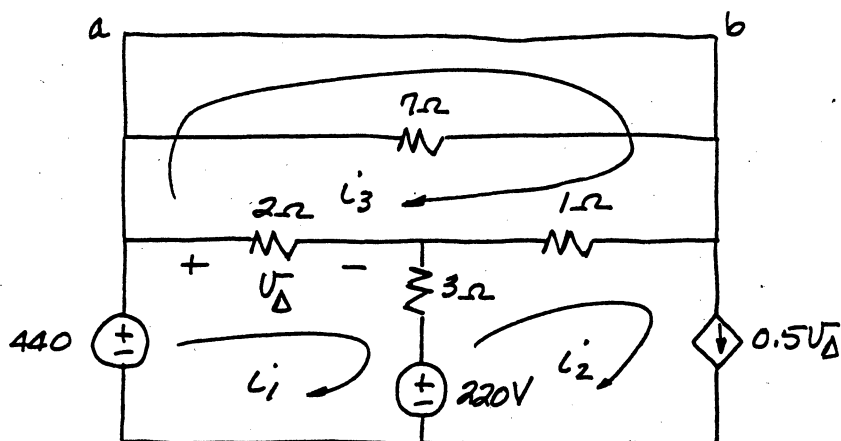
$$220 = 2i_1 + i_3$$

$$0 = -3i_1 + 11i_3$$

$$\Delta = \begin{vmatrix} 2 & 1 \\ -3 & 11 \end{vmatrix} = 25$$

$$N_3 = \begin{vmatrix} 2 & 220 \\ -3 & 0 \end{vmatrix} = 660$$

$$i_3 = \frac{N_3}{\Delta} = 26.4 \text{ A}; \quad v_{Th} = v_{ab} = 7i_3 = 184.80 \text{ V}$$



$$220 = 5i_1 - 3(0.5)(2)(i_1 - i_3) - 2i_3$$

$$0 = -2i_1 - 0.5(2)(i_1 - i_3) + 3i_3$$

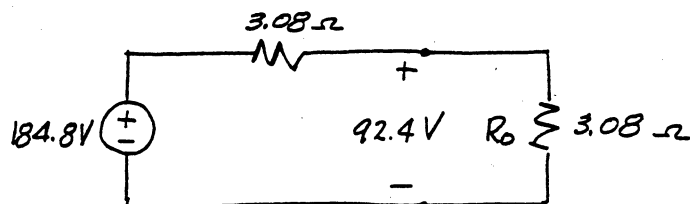
$$220 = 2i_1 + i_3$$

$$0 = i_1 + 4i_3$$

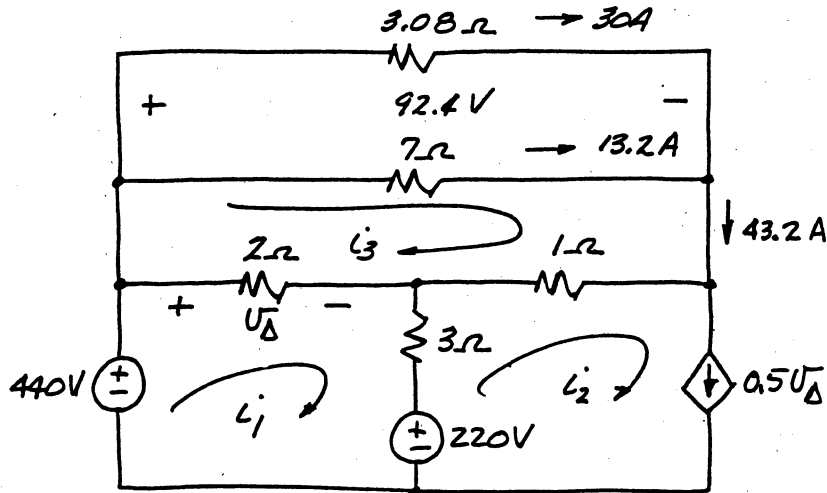
$$\Delta = \begin{vmatrix} 2 & 1 \\ -3 & 4 \end{vmatrix} = 11$$

$$N_3 = \begin{vmatrix} 2 & 220 \\ -3 & 0 \end{vmatrix} = 660$$

$$i_3 = \frac{N_3}{\Delta} = \frac{660}{11} = 60 \text{ A} = i_{sc}; \quad R_{Th} = \frac{v_{Th}}{i_{sc}} = \frac{184.80}{60} = 3.08 \Omega$$



$$P_{max} = \frac{(92.4)^2}{3.08} = 2772 \text{ W}$$



$$220 = 5i_1 - 3(0.5)(2)(i_1 - i_3) - 2i_3$$

$$220 = 2i_1 + i_3$$

$$\therefore 2i_1 = 220 - i_3 = 220 - 43.2$$

$$i_1 = 88.40 \text{ A}$$

$$v_\Delta = 2(i_1 - i_3) = 90.40 \text{ V}$$

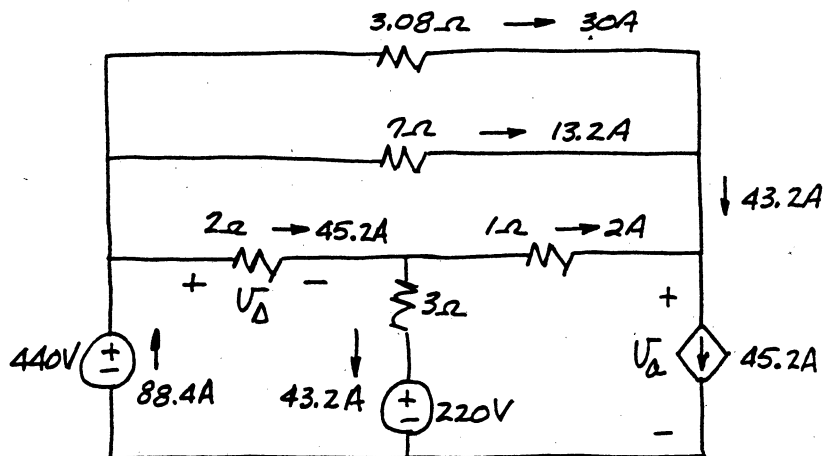
$$i_2 = 45.2 \text{ A}$$

$$\therefore i_1 - i_2 = 88.4 - 45.2 = 43.2 \text{ A}$$

$$i_1 - i_3 = 45.2 \text{ A}$$

$$i_2 - i_3 = 2 \text{ A}$$

Thus the circuit becomes



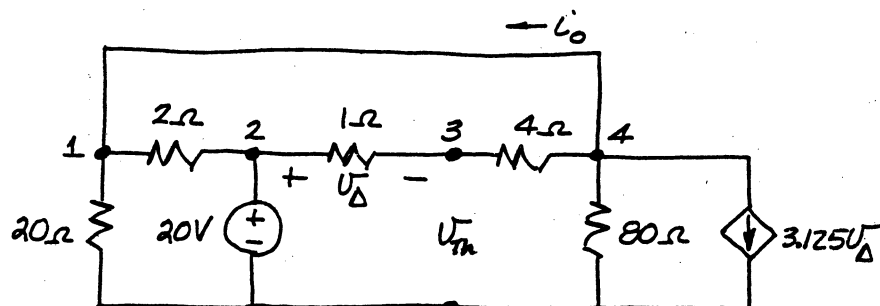
$$v_a = 220 + 3(43.2) - 2 = 347.6 \text{ V}$$

Therefore the only source developing power is the 440-V source.

$$p_{\text{dev}} = 440(88.4) = 38,896 \text{ W}$$

$$\% \text{ delivered to } R_o = \frac{2772}{38,896} \times 100 = 7.13\%$$

P4.78 [a] Find the Thévenin equivalent. With the $40\text{-}\Omega$ resistor removed $i_o = 0$ and the circuit becomes



$$\frac{v_{\text{Th}} - 20}{1} + \frac{v_{\text{Th}} - v_4}{4} = 0$$

$$\frac{v_4}{80} + 3.125v_{\Delta} + \frac{v_4 - 20}{5} + i_o = 0$$

$$\frac{v_4}{20} + \frac{v_4 - 20}{2} - i_o = 0$$

$$v_{\Delta} = 20 - v_{\text{Th}}$$

$$5v_{\text{Th}} - v_4 = 80$$

$$\frac{v_4}{80} + 3.125(20 - v_{\text{Th}}) + \frac{v_4 - 20}{5} + \frac{v_4}{20} + \frac{v_4 - 20}{2} = 0$$

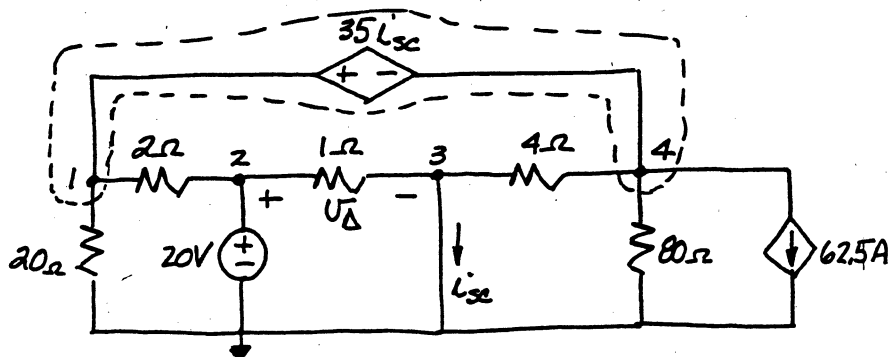
$$-250v_{\text{Th}} + 61v_4 = -3880$$

$$\Delta = \begin{vmatrix} 5 & -1 \\ -250 & 61 \end{vmatrix} = 55$$

$$N_{\text{Th}} = \begin{vmatrix} 80 & -1 \\ -3880 & 61 \end{vmatrix} = 1000$$

$$v_{\text{Th}} = \frac{N_{\text{Th}}}{\Delta} = \frac{1000}{55} = \frac{200}{11} \text{ V} \approx 18.18 \text{ V}$$

Short-circuit current:



$$v_{\Delta} = 20 \text{ V}, \quad 3.125v_{\Delta} = 62.5 \text{ A}$$

$$\frac{v_1}{20} + \frac{v_1 - 20}{2} + \frac{v_4}{4} + \frac{v_4}{80} + 62.5 = 0$$

$$44v_1 + 21v_4 = -4200$$

$$v_1 = 35i_{sc} + v_4; \quad i_{sc} = 20 + \frac{v_4}{4}$$

$$v_1 = 35 \left[20 + \left(\frac{v_4}{4} \right) \right] + v_4 = 700 + 9.75v_4$$

$$44v_1 = 30,800 + 429v_4$$

$$\therefore 30,800 + 429v_4 + 21v_4 = -4200$$

$$v_4 = -\frac{700}{9} \text{ V} \approx -77.78 \text{ V}$$

$$i_{sc} = 20 - \frac{700}{36} = \frac{5}{9} \text{ A}$$

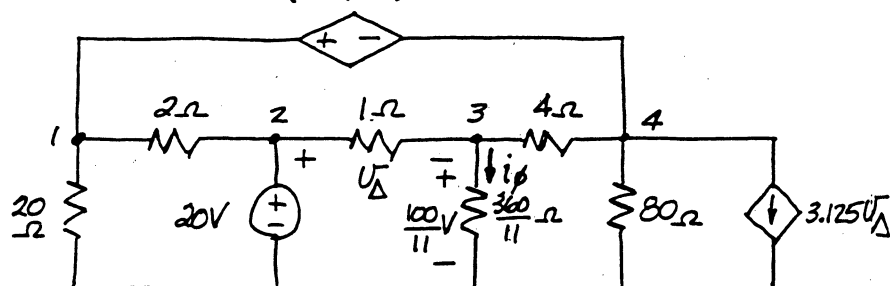
$$R_{Th} = \frac{v_{Th}}{i_{sc}} = \frac{200}{11} \cdot \frac{9}{5} = \frac{360}{11} \Omega \approx 32.73 \Omega$$

$$\therefore R_o = R_{Th} = \frac{360}{11} \Omega \approx 32.73 \Omega$$

$$[b] \quad P_{\max} = \left(\frac{200}{11} \cdot \frac{11}{720} \right)^2 \left(\frac{360}{11} \right) = \left(\frac{1}{3.6} \right)^2 \left(\frac{360}{11} \right) = \frac{100}{39.6} = \frac{250}{99} \approx 2.53 \text{ W}$$

[c] When $R_o = (360/11) \Omega$ the circuit is

$$(175/18) \text{ V}$$



$$i_\phi = \frac{100}{11} \cdot \frac{11}{360} = \frac{10}{36} = \frac{5}{18} \text{ A}$$

$$35i_\phi = \frac{175}{18} \text{ V}$$

$$\frac{(100/11) - 20}{1} + \frac{(100/11)}{(360/11)} + \frac{(100/11) - v_4}{4} = 0$$

$$\frac{-120}{11} + \frac{5}{18} + \frac{100 - 11v_4}{44} = 0$$

$$-480 + \frac{220}{18} + 100 - 11v_4 = 0$$

$$11v_4 = \frac{220}{18} - 380 = \frac{-3310}{9}$$

$$v_4 = \frac{-3310}{99} \text{ V}$$

$$v_1 = \frac{175}{18} - \frac{3310}{99} = \frac{-42,255}{1782} \text{ V}$$

$$i_{20\text{V}} = \frac{20 + (42,255/1782)}{2} + \frac{20 - (100/11)}{1} = \frac{77,895}{3564} + \frac{120}{11}$$

$$= \frac{1,284,525}{39,204} \approx 32.77 \text{ A}$$

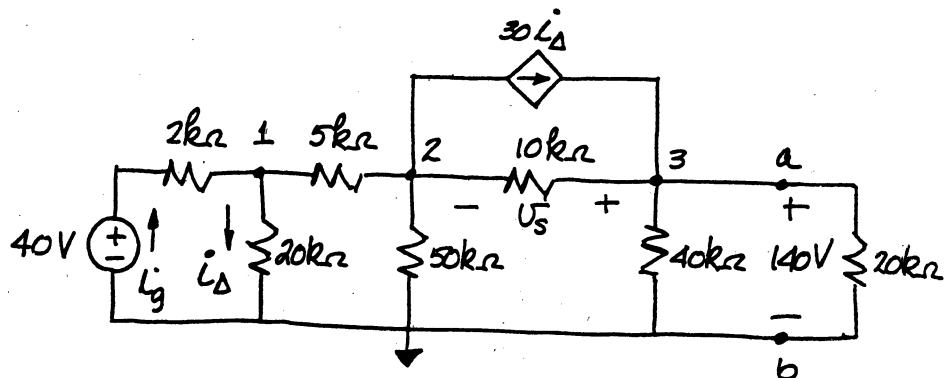
$$p_{20\text{V}} = 20(32.77) \approx 655.30 \text{ W}$$

P4.79 [a] From the solution of Problem 4.63 we have $R_{\text{Th}} = 20 \text{ k}\Omega$ and $v_{\text{Th}} = 280 \text{ V}$. Therefore

$$R_o = R_{\text{Th}} = 20 \text{ k}\Omega$$

[b] $p = \frac{(140)^2}{20} = 980 \text{ mW}$

[c]



$$\frac{v_1}{20} + \frac{v_1 - 40}{2} + \frac{v_1 - v_2}{5} = 0$$

$$15v_1 - 4v_2 = 400$$

$$\frac{v_2}{50} + \frac{v_2 - v_1}{5} + \frac{v_2 - 140}{10} + 30\left(\frac{v_1}{20}\right) = 0$$

$$130v_1 + 32v_2 = 1400$$

$$\Delta = \begin{vmatrix} 15 & -4 \\ 130 & 32 \end{vmatrix} = 1000$$

$$N_1 = \begin{vmatrix} 400 & -4 \\ 1400 & 32 \end{vmatrix} = 18,400$$

$$N_2 = \begin{vmatrix} 15 & 400 \\ 130 & 1400 \end{vmatrix} = -31,000$$

$$\therefore v_1 = 18.4 \text{ V}; \quad v_2 = -31 \text{ V}$$

$$i_g = \frac{40 - 18.4}{2} = 10.8 \text{ mA}$$

$$p_{40\text{V}}(\text{delivered}) = (40)(10.8) = 432 \text{ mW}$$

$$v_2 + v_s = 140$$

$$v_s = 140 - (-31) = 171 \text{ V}$$

$$i_{\Delta} = \frac{v_1}{20} = 0.92 \text{ mA}$$

$$30i_{\Delta} = 27.60 \text{ mA}$$

$$p_{30i_{\Delta}}(\text{delivered}) = (171)(27.6) = 4719.60 \text{ mW}$$

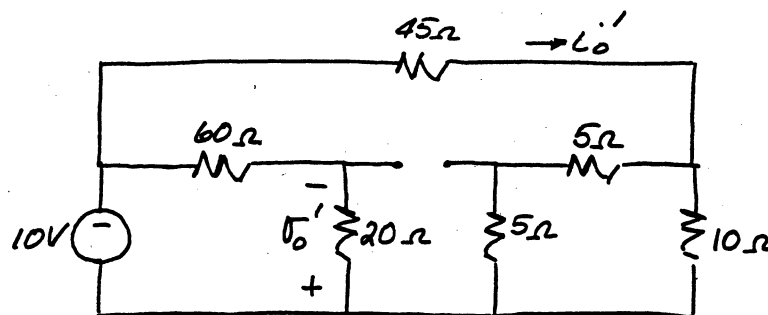
$$\sum p_{\text{dev}} = (432 + 4719.6) = 5151.60 \text{ mW}$$

$$\% \text{ delivered} = \frac{980}{5151.60} \times 100 = 19.02\%$$

P4.80 [a] Since $0 \leq R_o \leq \infty$ maximum power will be delivered to the $8\text{-}\Omega$ resistor when $R_o = 0$.

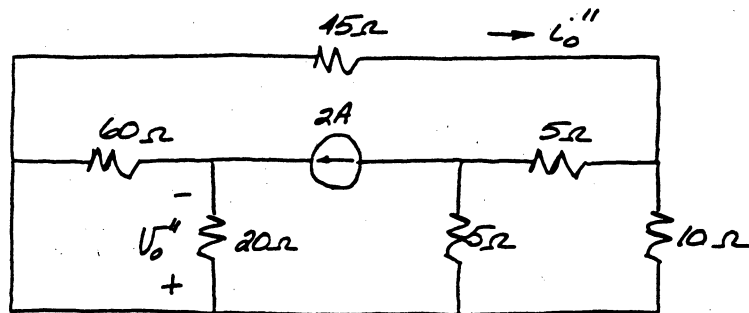
[b] $P = \frac{24^2}{8} = 72 \text{ W}$

P4.81 Voltage source acting alone

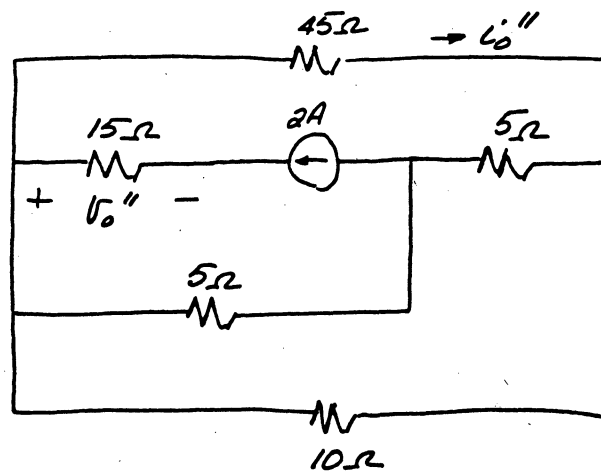


$$v_o' = \frac{-10}{80}(20) = -2.5 \text{ V}; \quad i_o' = \frac{+10}{45 + 5} = +0.20 \text{ A}$$

Current source acting alone:



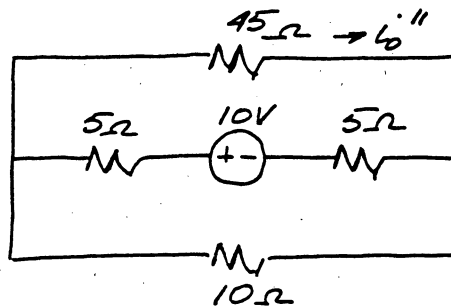
Now the circuit can be redrawn as



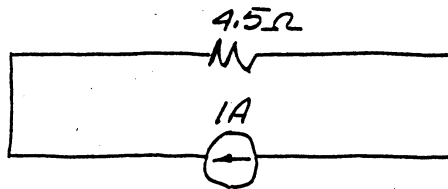
The $15\text{-}\Omega$ resistor will have no effect on i_o'' since it is in series with a 2-A source.

$$v_o'' = -15(2) = -30\text{ V}$$

To find i_o'' we simplify the circuit as follows:



Now the circuit reduces to

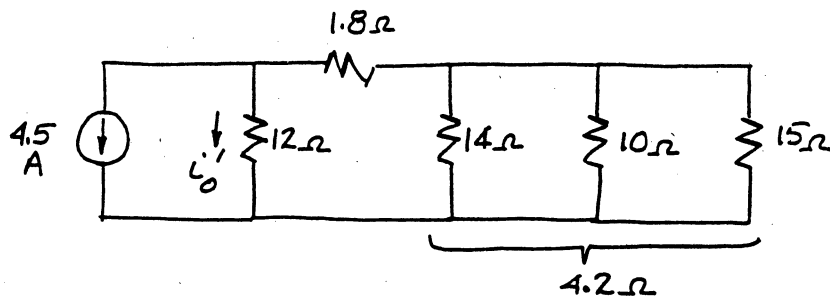


Therefore the voltage across the $45\text{-}\Omega$ resistor is 4.5 V , hence $i_o'' = \frac{4.5}{45} = 0.10\text{ A}$

$$\therefore v_o = v_o' + v_o'' = -2.5 - 30 = -32.5\text{ V}$$

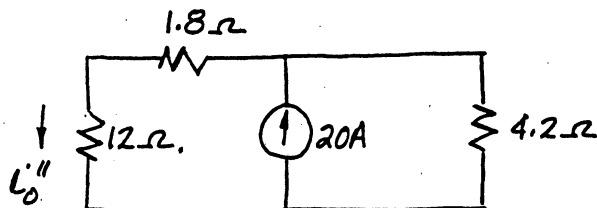
$$i_o = i_o' + i_o'' = 0.20 + 0.10 = 0.30\text{ A}$$

P 4.82 4.5-A source:



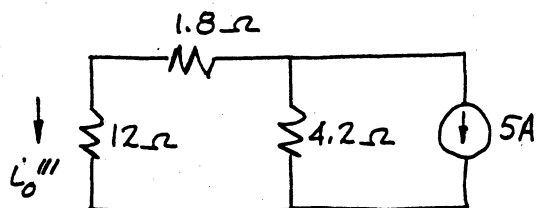
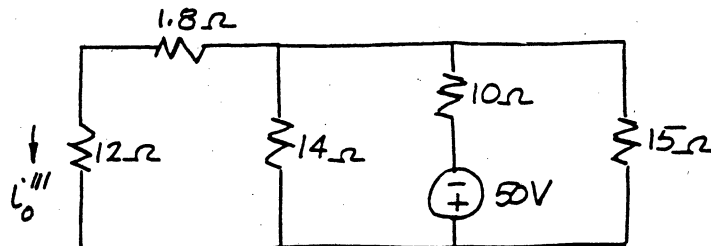
$$i_o' = \frac{(-4.5)(6)}{18} = -\frac{27}{18} = -1.5\text{ A}$$

20-A source:



$$i_o'' = \frac{(20)(4.2)}{18} = \frac{84}{18} = \frac{42}{9}\text{ A}$$

50-V source:

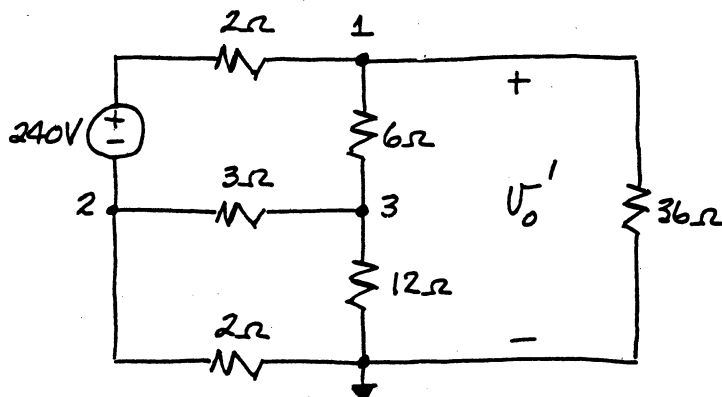


$$i_o''' = \frac{-5(4.2)}{18} = -\frac{21}{18} = -\frac{7}{6} \text{ A}$$

$$i_o = i_o' + i_o'' + i_o''' = -1.5 + \frac{42}{9} - \frac{7}{6} = \frac{-27 + 84 - 21}{18}$$

$$i_o = \frac{36}{18} = 2 \text{ A}$$

P 4.83



$$\frac{v_1 - (v_2 + 240)}{2} + \frac{v_1 - v_3}{6} + \frac{v_1}{36} = 0$$

$$18v_1 - 18v_2 - 4320 + 6v_1 - 6v_3 + v_1 = 0$$

$$25v_1 - 18v_2 - 6v_3 = 4320$$

$$\frac{v_2}{2} + \frac{v_2 - v_3}{3} + \frac{v_2 - (v_1 - 240)}{2} = 0$$

$$3v_2 + 2v_2 - 2v_3 + 3v_2 - 3v_1 + 720 = 0$$

$$-3v_1 + 8v_2 - 2v_3 = -720$$

$$\frac{v_3}{12} + \frac{v_3 - v_2}{3} + \frac{v_3 - v_1}{6} = 0$$

$$v_3 + 4v_3 - 4v_2 + 2v_3 - 2v_1 = 0$$

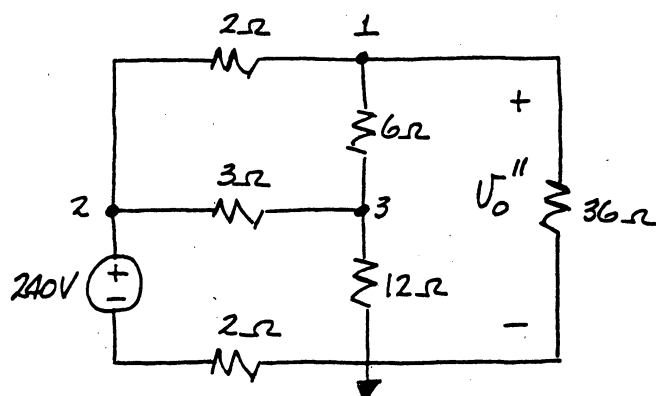
$$\boxed{-2v_1 - 4v_2 + 7v_3 = 0}$$

$$\Delta = \begin{vmatrix} 25 & -18 & -6 \\ -3 & 8 & -2 \\ -2 & -4 & 7 \end{vmatrix} = 25(56 - 8) + 3(-126 - 24) - 2(36 + 48)$$

$$\boxed{\Delta = 582}$$

$$N_1 = \begin{vmatrix} 4320 & -18 & -6 \\ -720 & 8 & -2 \\ 0 & -4 & 7 \end{vmatrix} = 4320(48) + 720(-150) = 99,360$$

$$v'_o = \frac{N_1}{\Delta} = \frac{99,360}{582} = 170.72 \text{ V}$$



$$\frac{v_1 - v_2}{2} + \frac{v_1 - v_3}{6} + \frac{v_1}{36} = 0$$

$$18v_1 - 18v_2 + 6v_1 - 6v_3 + v_1 = 0$$

$$\boxed{25v_1 - 18v_2 - 6v_3 = 0}$$

$$\frac{v_2 - v_1}{2} + \frac{v_2 - v_3}{3} + \frac{v_2 - 240}{2} = 0$$

$$3v_2 - 3v_1 + 2v_2 - 2v_3 + 3v_2 - 720 = 0$$

$$\boxed{-3v_1 + 8v_2 - 2v_3 = 720}$$

$$\frac{v_3 - v_2}{3} + \frac{v_3 - v_1}{6} + \frac{v_3}{12} = 0$$

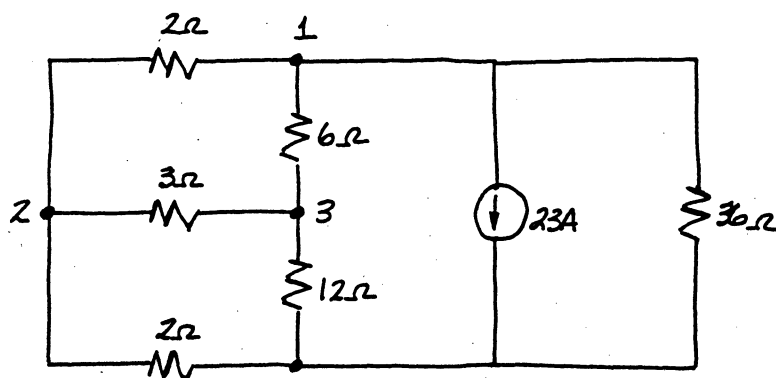
$$4v_3 - 4v_2 + 2v_3 - 2v_1 + v_3 = 0$$

$$\boxed{-2v_1 - 4v_2 + 7v_3 = 0}$$

$$\Delta = \begin{vmatrix} 25 & -18 & -6 \\ -3 & 8 & -2 \\ -2 & -4 & 7 \end{vmatrix} = 582$$

$$N_1 = \begin{vmatrix} 0 & -18 & -6 \\ 720 & 8 & -2 \\ 0 & -4 & 7 \end{vmatrix} = -720(-150) = 108,000$$

$$v_o'' = \frac{N_1}{\Delta} = \frac{108,000}{582} = 185.57 \text{ V}$$



$$\frac{v_1 - v_3}{2} + \frac{v_1 - v_3}{6} + \frac{v_1}{36} + 23 = 0$$

$$18v_1 - 18v_2 + 6v_1 - 6v_3 + v_1 = -828$$

$$25v_1 - 18v_2 - 6v_3 = -828$$

$$\frac{v_2 - v_1}{2} + \frac{v_2 - v_3}{3} + \frac{v_2}{2} = 0$$

$$3v_2 - 3v_1 + 2v_2 - 2v_3 + 3v_2 = 0$$

$$-3v_1 + 8v_2 - 2v_3 = 0$$

$$\frac{v_3}{12} + \frac{v_3 - v_2}{3} + \frac{v_3 - v_1}{6} = 0$$

$$v_3 + 4v_3 - 4v_2 + 2v_3 - 2v_1 = 0$$

$$-2v_1 - 4v_2 + 7v_3 = 0$$

As before $\Delta = 582$

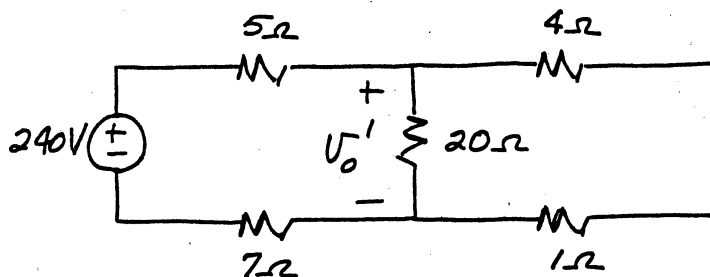
$$N_1 = \begin{vmatrix} -828 & -18 & -6 \\ 0 & 8 & -2 \\ 0 & -4 & 7 \end{vmatrix} = -828(48) = -39,744$$

$$v_o'' = \frac{N_1}{\Delta} = \frac{-39,744}{582} = -68.29$$

$$v_o = v_o' + v_o'' + v_o''' = 170.72 + 185.57 - 68.29$$

$$v_o = 288 \text{ V}$$

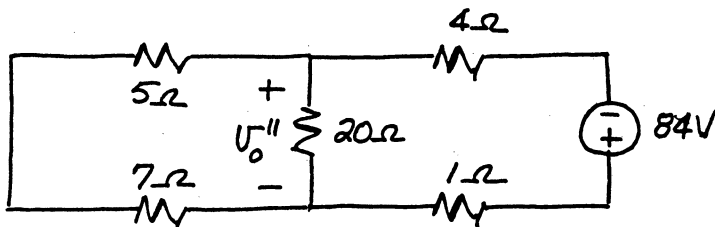
P 4.84 240-V source:



$$20\Omega // 5\Omega = 4\Omega$$

$$\therefore v_o' = \left(\frac{240}{5+7+4} \right) (4) = 60 \text{ V}$$

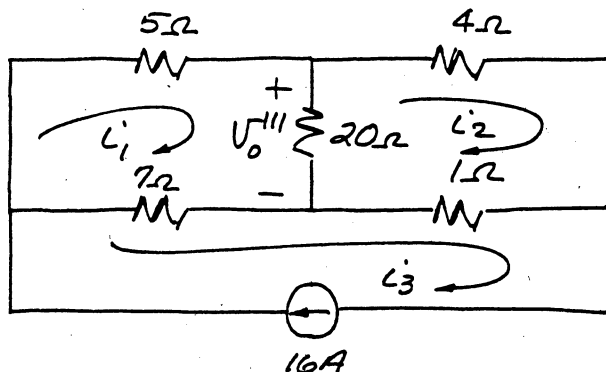
84-V source:



$$12\Omega // 20\Omega = 7.5\Omega$$

$$\therefore v_o'' = \left(\frac{-84}{4+1+7.5} \right) (7.5) = -50.4 \text{ V}$$

16-A source:



$$\begin{aligned} 0 &= 32i_1 - 20i_2 - 112 & 112 &= 32i_1 - 20i_2 \\ 0 &= -20i_1 + 25i_2 - 16 & 16 &= -20i_1 + 25i_2 \end{aligned}$$

$$\Delta = \begin{vmatrix} 32 & -20 \\ -20 & 25 \end{vmatrix} = 400$$

$$N_1 = \begin{vmatrix} 112 & -20 \\ 16 & 25 \end{vmatrix} = 3120$$

$$N_2 = \begin{vmatrix} 32 & 112 \\ -20 & 16 \end{vmatrix} = 2752$$

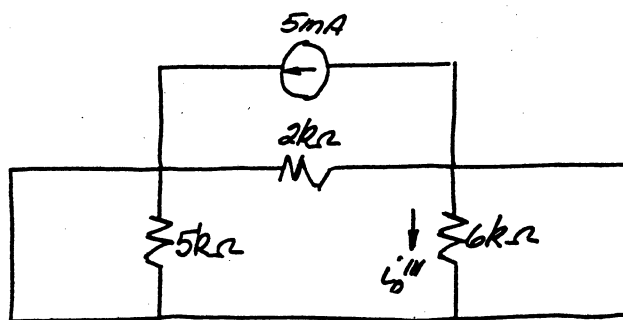
$$i_1 = \frac{N_1}{\Delta} = 7.80 \text{ A}; \quad i_2 = \frac{N_2}{\Delta} = 6.88 \text{ A}$$

$$i_1 - i_2 = 7.80 - 6.88 = 0.92 \text{ A}$$

$$v_o''' = 20(i_1 - i_2) = 18.4 \text{ V}$$

$$v_o = v_o' + v_o'' + v_o''' = 60 - 50.4 + 18.40 = 28 \text{ V}$$

P 4.85 [a] By hypothesis $i_o' + i_o'' = 3.5 \text{ mA}$.



$$i_o''' = -5 \frac{(2)}{(8)} = -1.25 \text{ mA}; \quad \therefore i_o = 3.5 - 1.25 = 2.25 \text{ mA}$$

[b] With all three sources in the circuit write a single node-voltage equation.

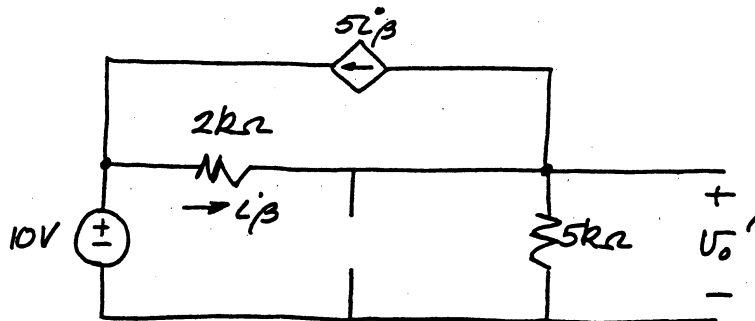
$$\frac{v_b}{6} + \frac{v_b - 8}{2} + 5 - 10 = 0$$

$$v_b + 3v_b - 24 - 30 = 0$$

$$v_b = \frac{54}{4} = 13.5 \text{ V}$$

$$i_o = \frac{v_b}{6} = 2.25 \text{ mA}$$

P 4.86 10-V source acting alone:



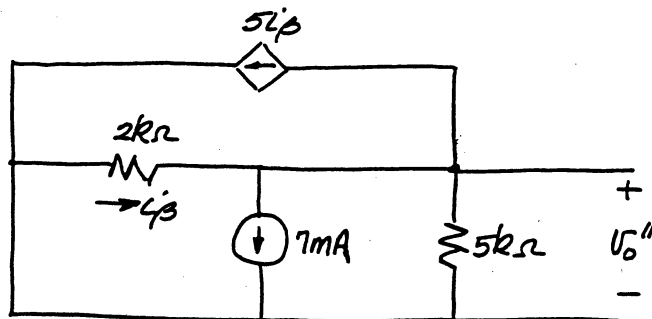
$$\frac{v_o'}{5} + \frac{v_o' - 10}{2} + 5 \left(\frac{10 - v_o'}{2} \right) = 0$$

$$2v_o' + 5v_o' - 50 + 250 - 25v_o' = 0$$

$$18v_o' = 200$$

$$v_o' = \frac{100}{9} \text{ V}$$

7-mA source acting alone:



$$\frac{v_o''}{5} + 7 + \frac{v_o''}{2} + 5 \left(\frac{-v_o''}{2} \right) = 0$$

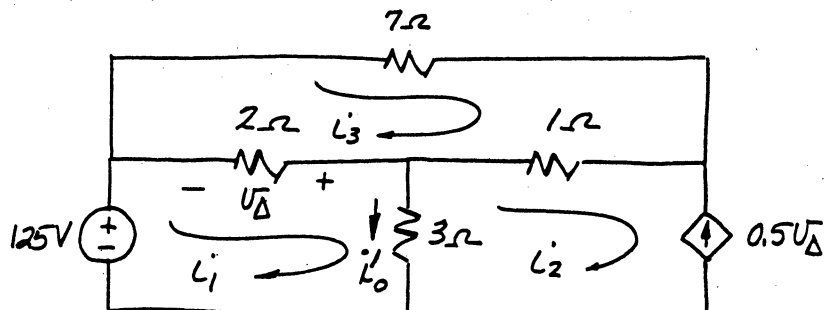
$$2v_o'' + 70 + 5v_o'' - 25v_o'' = 0$$

$$18v_o'' = 70$$

$$v_o'' = \frac{35}{9} \text{ V}$$

$$v_o = v_o' + v_o'' = \frac{135}{9} = 15 \text{ V}$$

P4.87 125-V source acting alone:



$$125 = 5i_1 - 3(-0.5)(2)(i_3 - i_1) - 2i_3$$

$$125 = 2i_1 + i_3$$

$$0 = -2i_1 - 0.5(2)(i_3 - i_1) + 10i_3$$

$$0 = -3i_1 + 11i_3$$

$$\Delta = \begin{vmatrix} 2 & 1 \\ -3 & 11 \end{vmatrix} = 25$$

$$N_1 = \begin{vmatrix} 125 & 1 \\ 0 & 11 \end{vmatrix} = 125(11)$$

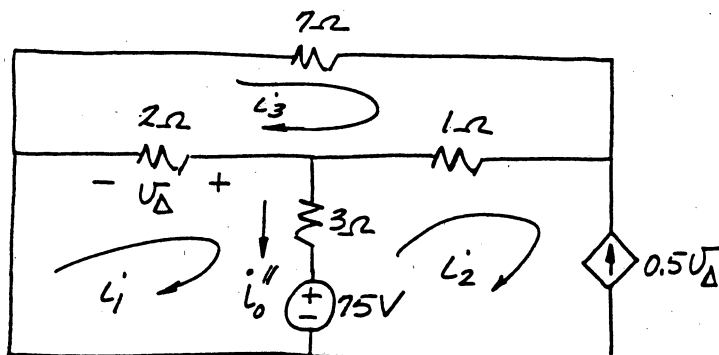
$$N_3 = \begin{vmatrix} 2 & 125 \\ -3 & 0 \end{vmatrix} = 125(3)$$

$$i_1 = \frac{N_1}{\Delta} = 55 \text{ A}; \quad i_3 = \frac{N_3}{\Delta} = 15 \text{ A}$$

$$i_2 = -0.5(2)(15 - 55) = 40 \text{ A}$$

$$i'_0 = i_1 - i_2 = 55 - 40 = 15 \text{ A}$$

75-V source acting alone:



$$-75 = 2i_1 + 3i_3$$

$$0 = -3i_1 + 11i_3$$

$$\Delta = 25; \quad N_1 = -11(75); \quad N_3 = -3(75)$$

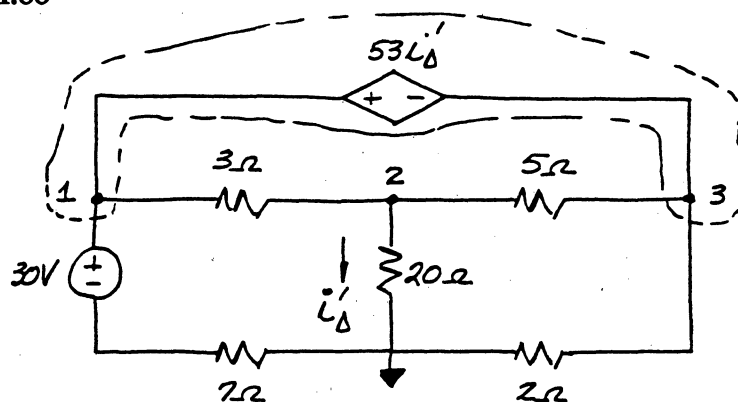
$$i_1 = -33 \text{ A}; \quad i_3 = -9 \text{ A}$$

$$i_2 = -0.5(2)(-9 + 33) = -24 \text{ A}$$

$$i_o'' = i_1 - i_2 = -33 + 24 = -9 \text{ A}$$

$$i_o = i_o'' + i_o' = -9 + 15 = 6 \text{ A}$$

P 4.88



$$\frac{v_1 - 30}{7} + \frac{v_1 - v_2}{3} + \frac{v_3 - v_2}{5} + \frac{v_3}{2} = 0$$

$$30v_1 - 900 + 70v_1 - 70v_2 + 42v_3 - 42v_2 + 105v_3 = 0$$

$$100v_1 - 112v_2 + 147v_3 = 900$$

$$v_1 = v_3 + 53 \left(\frac{v_2}{20} \right)$$

$$\therefore 100v_1 = 100v_3 + 265v_2$$

$$100v_3 + 256v_2 - 112v_2 + 147v_3 = 900$$

$$153v_2 + 247v_3 = 900$$

$$\frac{v_2}{20} + \frac{v_2 - v_1}{3} + \frac{v_2 - v_3}{5} = 0$$

$$3v_2 + 20v_2 - 20v_1 + 12v_2 - 12v_3 = 0$$

$$-20v_1 + 35v_2 - 12v_3 = 0$$

$$\text{But } 20v_1 = 20v_3 + 53v_2$$

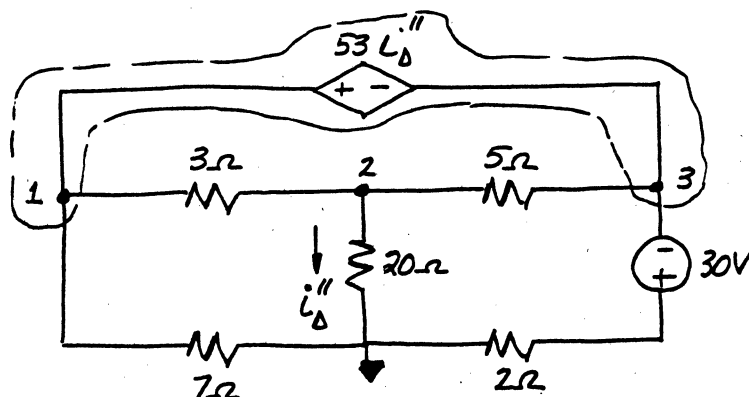
$$\therefore -20v_3 - 53v_2 + 35v_2 - 12v_3 = 0$$

$$18v_2 + 32v_3 = 0$$

$$\Delta = \begin{vmatrix} 153 & 247 \\ 18 & 32 \end{vmatrix} = 450$$

$$N_2 = \begin{vmatrix} 900 & 247 \\ 0 & 32 \end{vmatrix} = 32(900)$$

$$v_2 = \frac{N_2}{\Delta} = \frac{32(900)}{450} = 64 \text{ V}; \quad i'_\Delta = \frac{v_2}{20} = 3.2 \text{ A}$$



$$\frac{v_1}{7} + \frac{v_1 - v_2}{3} + \frac{v_3 - v_2}{5} + \frac{v_3 + 30}{2} = 0$$

$$30v_1 + 70v_1 - 70v_2 + 42v_3 - 42v_2 + 105v_3 + 3150 = 0$$

$$100v_1 - 112v_2 + 147v_3 = -3150$$

$$v_1 = v_3 + 53 \left(\frac{v_2}{20} \right)$$

$$100v_1 = 100v_3 + 265v_2$$

$$100v_3 + 265v_2 - 112v_2 + 147v_3 = -3150$$

$$153v_2 + 247v_3 = -3150$$

$$\frac{v_2 - v_1}{3} + \frac{v_2}{20} + \frac{v_2 - v_3}{5} = 0$$

$$20v_2 - 20v_1 + 3v_2 + 12v_2 - 12v_3 = 0$$

$$-20v_1 + 35v_2 - 12v_3 = 0$$

$$-20v_3 - 53v_2 + 35v_2 - 12v_3 = 0$$

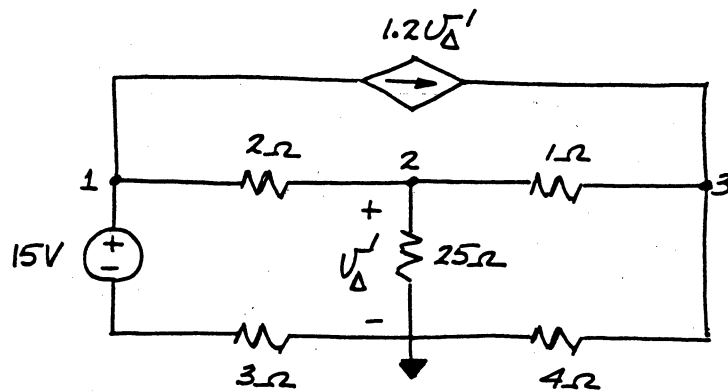
$$-18v_2 - 32v_3 = 0$$

$$18v_2 + 32v_3 = 0$$

$$\Delta = 450; \quad N_2 = -3150(32); \quad v_2 = -224 \text{ V}$$

$$i''_\Delta = \frac{-224}{20} = -11.2 \text{ A}; \quad i_\Delta = i'_\Delta + i''_\Delta = 3.2 - 11.2 = -8 \text{ A}$$

P 4.89



$$\frac{v_1 - 15}{3} + \frac{v_1 - v_2}{2} + 1.2v_2 = 0$$

$$2v_1 - 30 + 3v_1 - 3v_2 + 7.2v_2 = 0;$$

$$5v_1 + 4.2v_2 + 0v_3 = 30$$

$$\frac{v_2}{25} + \frac{v_2 - v_1}{2} + \frac{v_2 - v_3}{1} = 0$$

$$2v_2 + 25v_2 - 25v_1 + 50v_2 - 50v_3 = 0;$$

$$-25v_1 + 77v_2 - 50v_3 = 0$$

$$\frac{v_3}{4} + \frac{v_3 - v_2}{1} - 1.2v_2 = 0$$

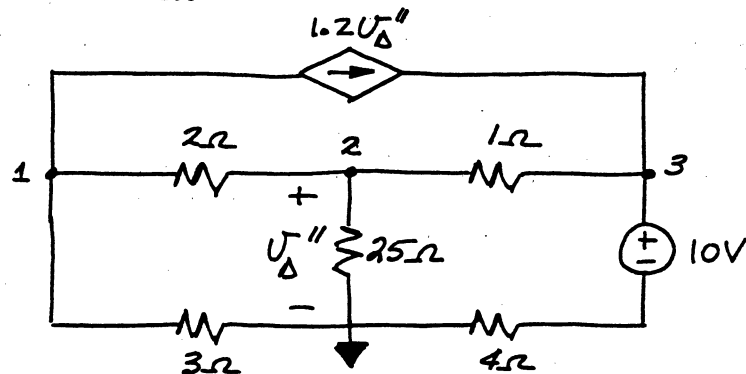
$$v_3 + 4v_3 - 4v_2 - 4.8v_2 = 0;$$

$$0v_1 - 8.8v_2 + 5v_3 = 0$$

$$\Delta = \begin{vmatrix} 5 & 4.2 & 0 \\ -25 & 77 & -50 \\ 0 & -8.8 & 5 \end{vmatrix} = 5(-55) + 25(21) = 250$$

$$N_2 = \begin{vmatrix} 5 & 30 & 0 \\ -25 & 0 & -50 \\ 0 & 0 & 5 \end{vmatrix} = -30(-125) = 3750$$

$$v_2 = v'_\Delta = \frac{N_2}{\Delta} = \frac{3750}{250} = 15 \text{ V}$$



$$\frac{v_1}{3} + \frac{v_1 - v_2}{2} + 1.2v_2 = 0;$$

$$5v_1 + 4.2v_2 + 0v_3 = 0$$

$$\frac{v_2}{25} + \frac{v_2 - v_1}{2} + \frac{v_2 - v_3}{1} = 0;$$

$$-25v_1 + 77v_2 - 50v_3 = 0$$

$$\frac{v_3 - 10}{4} + \frac{v_3 - v_2}{1} - 1.2v_2 = 0;$$

$$0v_1 - 8.8v_2 + 5v_3 = 10$$

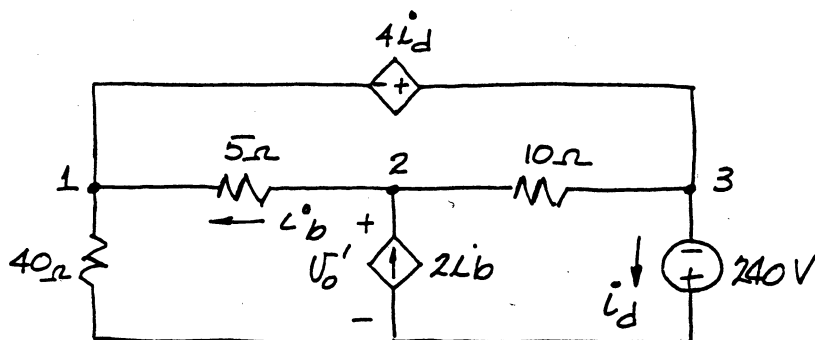
$$\Delta = \begin{vmatrix} 5 & 4.2 & 0 \\ -25 & 77 & -50 \\ 0 & -8.8 & 5 \end{vmatrix} = 250$$

$$N_2 = \begin{vmatrix} 5 & 0 & 0 \\ -25 & 0 & -50 \\ 0 & 10 & 5 \end{vmatrix} = -10(-250)$$

$$v_2 = v''_{\Delta} = \frac{N_2}{\Delta} = \frac{2500}{250} = 10 \text{ V}$$

$$v_{\Delta} = v'_{\Delta} + v''_{\Delta} = 15 + 10 = 25 \text{ V}$$

P 4.90



$$-2i_b + \frac{v_2 + 240}{10} + \frac{v_2 - v_1}{5} = 0$$

$$-2\left(\frac{v_2 - v_1}{5}\right) + \frac{v_2 + 240}{10} + \frac{v_2 - v_1}{5} = 0$$

$$\therefore \boxed{2v_1 - v_2 = -240}$$

$$v_1 + 4i_d = -240$$

$$v_1 + 4\left(2i_b - \frac{v_1}{40}\right) = -240$$

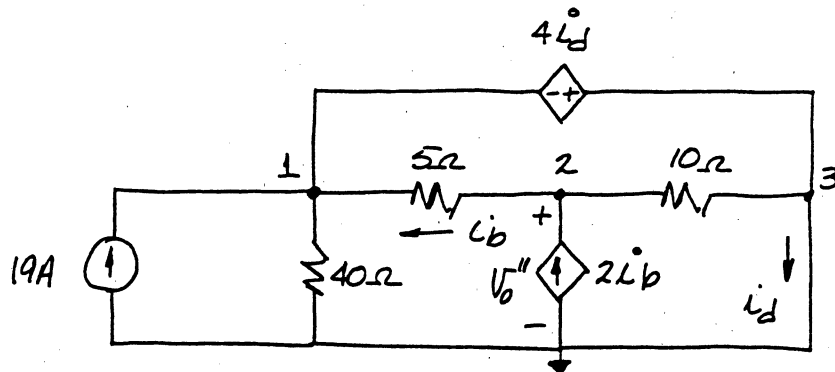
$$v_1 - \frac{v_1}{10} + 8\left(\frac{v_2 - v_1}{5}\right) = -240$$

$$\therefore \boxed{-7v_1 + 16v_2 = -2400}$$

$$\Delta = \begin{vmatrix} 2 & -1 \\ -7 & 16 \end{vmatrix} = 32 - 7 = 25$$

$$N_2 = \begin{vmatrix} 2 & -240 \\ -7 & -2400 \end{vmatrix} = -4800 - 1680 = -6480$$

$$v_2 = \frac{N_2}{\Delta} = \frac{-6480}{25} = -259.20 \text{ V} = v'_o$$



$$\frac{v_2 - v_1}{5} - 2 \left(\frac{v_2 - v_1}{5} \right) + \frac{v_2}{10} = 0; \quad \therefore \boxed{2v_1 - v_2 = 0}$$

$$v_1 + 4i_d = 0$$

$$v_1 + 4 \left(2i_b - \frac{v_1}{40} + 19 \right) = 0$$

$$v_1 + 8\left(\frac{v_2 - v_1}{5}\right) - \frac{v_1}{10} = -76; \quad \therefore \boxed{-7v_1 + 16v_2 = -760}$$

$$-7\left(\frac{v_2}{2}\right) + 16v_2 = -760$$

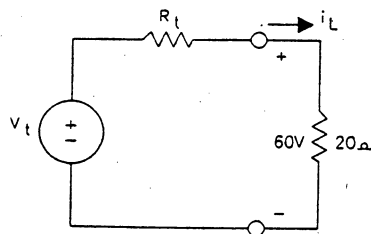
$$12.5v_2 = -760$$

$$v_2 = -60.80 \text{ V} = v_o''$$

$$\therefore v_o = v'_o + v''_o = -259.2 - 60.80$$

$$v_o = -320 \text{ V}$$

P 4.91 [a]



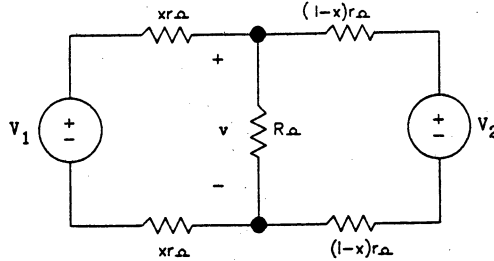
$$V_{oc} = V_{Th} = 75 \text{ V}; \quad i_L = \frac{60}{20} = 3 \text{ A}; \quad i_L = \frac{75 - 60}{R_{Th}} = \frac{15}{R_{Th}}$$

Therefore $R_{Th} = \frac{15}{3} = 5 \Omega$

$$[b] \quad i_L = \frac{V_o}{R_L} = \frac{V_{Th} - v_o}{R_{Th}}$$

$$\text{Therefore } R_{Th} = \frac{V_{Th} - V_o}{V_o/R_L} = \left(\frac{V_{Th}}{V_o} - 1 \right) R_L$$

P4.92 [a]



$$\frac{v - V_1}{2xr} + \frac{v}{R} + \frac{v - V_2}{2r(\ell - x)} = 0$$

$$v \left[\frac{1}{2xr} + \frac{1}{R} + \frac{1}{2r(\ell - x)} \right] = \frac{V_1}{2xr} + \frac{V_2}{2r(\ell - x)}$$

$$v = \frac{V_1 R \ell + x R (V_2 - V_1)}{R \ell + 2r \ell x - 2r x^2}$$

$$[b] \quad \text{Let } D = R \ell + 2r \ell x - 2r x^2$$

$$\frac{dv}{dx} = \frac{(R \ell + 2r \ell x - 2r x^2) R (V_2 - V_1) - [V_1 R \ell + x R (V_2 - V_1)] 2r(\ell - 2x)}{D^2}$$

$$\frac{dv}{dx} = 0 \quad \text{when numerator is zero.}$$

$$\text{The numerator simplifies to } x^2 + \frac{2\ell V_1}{(V_2 - V_1)} x + \frac{R \ell (V_2 - V_1) - 2r V_1 \ell^2}{2r(V_2 - V_1)} = 0$$

Solving for the roots of the quadratic yields

$$x = \frac{\ell}{V_2 - V_1} \left\{ -V_1 \pm \sqrt{V_1 V_2 - \frac{R}{2r \ell} (V_2 - V_1)^2} \right\}$$

$$[c] \quad x = \frac{\ell}{V_2 - V_1} \left\{ -V_1 \pm \sqrt{V_1 V_2 - \frac{R}{2r \ell} (V_1 - V_2)^2} \right\}$$

$$V_2 = 1200 \text{ V}, \quad V_1 = 1000 \text{ V}, \quad \ell = 16 \text{ km}$$

$$r = 5 \times 10^{-5} \Omega/\text{m}; \quad R = 3.9 \Omega$$

$$\frac{\ell}{V_2 - V_1} = \frac{16,000}{1200 - 1000} = 80; \quad V_1 V_2 = 1.2 \times 10^6$$

$$\frac{R}{2r \ell} (V_1 - V_2)^2 = \frac{3.9(-200)^2}{(10 \times 10^{-5})(16 \times 10^3)} = 0.975 \times 10^5$$

$$x = 80 \{-1000 \pm \sqrt{1.2 \times 10^6 - 0.975 \times 10^6}\} = 80 \{-1000 \pm 1050\} = 80(50)$$

$$x = 4000 \text{ m}$$

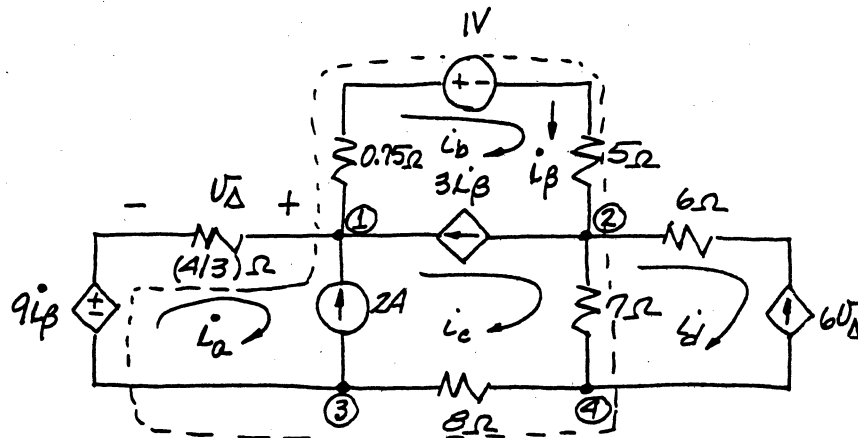
$$\begin{aligned}
 \text{[d]} \quad v_{\min} &= \frac{V_1 R l + R(V_2 - V_1)x}{Rl + 2rlx - 2rx^2} \\
 &= \frac{(1000)(3.9)(16 \times 10^3) + 3.9(200)(4000)}{(3.9)(16,000) + 10 \times 10^{-5}(16,000)(4000) - 10 \times 10^{-5}(16 \times 10^6)} \\
 &= 975 \text{ V}
 \end{aligned}$$

- P4.93 [a]** In studying the circuit in Fig. P4.93 we note it contains six meshes and six essential nodes. Further study shows that by replacing the parallel resistors with their equivalent values the circuit reduces to four meshes and four essential nodes as shown in the following diagram.

The node-voltage approach will require solving three node-voltage equations along with equations involving v_{Δ} and i_{β} .

The mesh-current approach will require writing one supermesh equation plus three constraint equations involving the three current sources. Thus at the outset we know the supermesh equation can be reduced to a single unknown current. Since we are interested in the power developed by the 1-V source, we will retain the mesh current i_b and eliminate the mesh currents i_a , i_c , and i_d .

The supermesh is denoted by the dashed line in the following figure.



- [b]** Summing the voltages around the supermesh yields

$$-9i_{\beta} + \frac{4}{3}i_a + 0.75i_b + 1 + 5i_b + 7(i_c - i_d) + 8i_c = 0$$

Note that $i_{\beta} = i_b$, and multiply the equation by 12:

$$-108i_b + 16i_a + 9i_b + 12 + 60i_b + 84(i_c - i_d) + 96i_c = 0$$

$$\text{or } 16i_a - 39i_b + 180i_c - 84i_d = -12$$

Now note: $i_b - i_c = 3i_{\beta} = 3i_b$; $\therefore i_c = -2i_b$

$$\text{whence } 16i_a - 39i_b - 360i_b - 84i_d = -12$$

Now write the constraint equations

$$v_A = 3v_x; \quad v_x = v_E - v_C - 0.9; \quad v_\Delta = v_B - v_E$$

$$i_\sigma = \frac{v_A - v_B}{4} = 0.25v_A - 0.25v_B$$

$$5i_\sigma = v_B - v_C$$

Now use the constraint equations to eliminate v_A , v_B , and v_Δ , reducing the number of equations to three.

$$v_A = 3v_E - 3v_C - 2.7$$

$$v_B = \frac{15}{9}v_E - \frac{11}{9}v_C - 1.5$$

$$v_\Delta = \frac{6}{9}v_E - \frac{11}{9}v_C - 1.5$$

We get

$$68v_C + 0v_D - 60v_E = 3.6$$

$$-286v_C + 45v_D + 156v_E = 615.60$$

$$292.80v_C + 0v_D - 124.2v_E = -2175.12$$

or

$$\begin{bmatrix} 68 & 0 & -60 \\ -286 & 45 & 156 \\ 292.8 & 0 & -124.2 \end{bmatrix} \begin{bmatrix} v_C \\ v_D \\ v_E \end{bmatrix} = \begin{bmatrix} 3.6 \\ 615.60 \\ -2175.12 \end{bmatrix}$$

Solving yields

$$v_C \approx -14.3552 \text{ V}; \quad v_D \approx -20.9474 \text{ V}; \quad v_E \approx 16.3293 \text{ V}$$

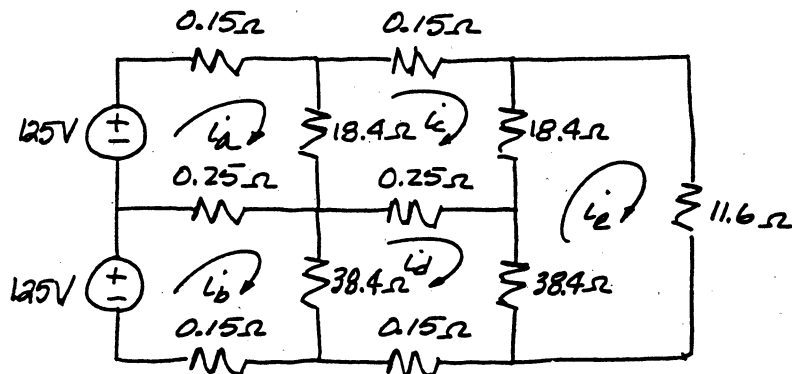
From the circuit diagram

$$p_{5A} = 5v_{5A}$$

$$5v_{5A} = 5(v_E - v_D) \approx 23.09 \text{ W}$$

$$\therefore p_{5A} = 23.09 \text{ W (absorbing)}$$

P4.95



$$125 = 18.8i_a - 0.25i_b - 18.4i_c + 0i_d + 0i_e$$

$$125 = -0.25i_a + 38.8i_b + 0i_c - 38.4i_d + 0i_e$$

$$0 = -18.4i_a + 0i_b + 37.2i_c - 0.25i_d - 18.4i_e$$

$$0 = 0i_a - 38.4i_b - 0.25i_c + 77.2i_d - 38.4i_e$$

$$0 = 0i_a + 0i_b - 18.4i_c - 38.4i_d + 68.4i_e$$

$$\begin{bmatrix} 18.8 & -0.25 & -18.4 & 0 & 0 \\ -0.25 & 38.8 & 0 & -38.4 & 0 \\ -18.4 & 0 & 37.2 & -0.25 & -18.4 \\ 0 & -38.4 & -0.25 & 77.2 & -38.4 \\ 0 & 0 & -18.4 & -38.4 & 68.4 \end{bmatrix} \begin{bmatrix} i_a \\ i_b \\ i_c \\ i_d \\ i_e \end{bmatrix} = \begin{bmatrix} 125 \\ 125 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

A computer solution yields

$$i_a = 32.77 = 32.76947 \text{ A}$$

$$i_d = 23.26650 \text{ A}$$

$$i_b = 26.45943 \text{ A}$$

$$i_e = 20.14451 \text{ A}$$

$$i_c = 26.32887 \text{ A}$$

Test:

$$i_c - i_e = 6.18436 \text{ A}$$

$$v_2 = 119.88442 \text{ V}$$

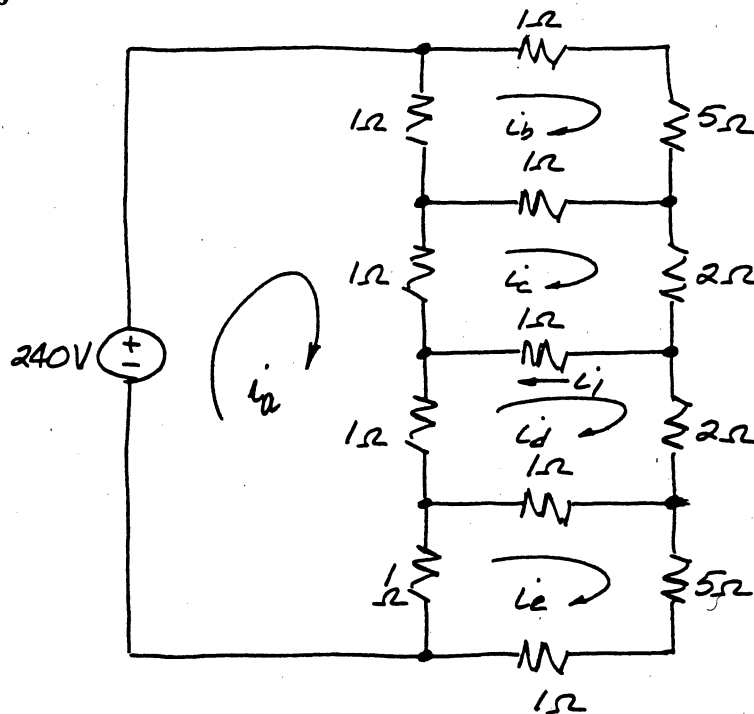
$$v_1 = 113.79222 \text{ V}$$

$$v_3 = 233.67632 \text{ V}$$

$$i_d - i_e = 3.12199 \text{ A}$$

$$v_1 + v_2 = 233.67664 \text{ V}$$

P4.96



$$240 = 4i_a - i_b - i_c - i_d - i_e$$

$$0 = -i_a + 8i_b - i_c + 0i_d + 0i_e$$

$$0 = -i_a - i_b + 5i_c - i_d + 0i_e$$

$$0 = -i_a + 0i_b - i_c + 5i_d - i_e$$

$$0 = -i_a + 0i_b + 0i_c - i_d + 8i_e$$

$$\begin{bmatrix} 4 & -1 & -1 & -1 & -1 \\ -1 & 8 & -1 & 0 & 0 \\ -1 & -1 & 5 & -1 & 0 \\ -1 & 0 & -1 & 5 & -1 \\ -1 & 0 & 0 & -1 & 8 \end{bmatrix} \begin{bmatrix} i_a \\ i_b \\ i_c \\ i_d \\ i_e \end{bmatrix} = \begin{bmatrix} 240 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

A computer solution yields

$$\begin{aligned} i_a &= 77.50 & i_d &= 22.50 \\ i_b &= 12.50 & i_e &= 12.50 \\ i_c &= 22.50 & i_1 &= i_c - i_d = 0 \text{ A} \end{aligned}$$

Check:

$$p_{240} = 240i_a = 18,600 \text{ W}$$

$$i_a - i_b = 77.50 - 12.50 = 65 \text{ A}$$

$$p_{1\Omega} = (65)^2 1 = 4225 \text{ W}$$

$$i_a - i_c = 77.50 - 22.50 = 55 \text{ A}$$

$$p_{1\Omega} = (55)^2 = 3025 \text{ W}$$

$$i_a - i_d = 55 \text{ A}$$

$$p_{1\Omega} = (55)^2 = 3025 \text{ W}$$

$$i_a - i_e = 77.50 - 12.50 = 65 \text{ A}$$

$$p_{1\Omega} = (65)^2 = 4225 \text{ W}$$

$$p_{6\Omega} = (12.5)^2 (6) = 937.50 \text{ W}$$

$$p_{6\Omega} = 937.50 \text{ W}$$

$$p_{2\Omega} = (22.50)^2 (2) = 1012.50 \text{ W}$$

$$p_{2\Omega} = 1012.50 \text{ W}$$

$$i_b - i_c = -10 \text{ A}$$

$$p_{1\Omega} = 100 \text{ W}$$

$$p_{1\Omega} = 0 \text{ W}$$

$$p_{1\Omega} = 100 \text{ W}$$

$$\begin{aligned} \sum p_{\text{abs}} &= 4225 + 3025 + 3025 + 4225 + 937.50 + 937.50 + 1012.50 \\ &\quad + 1012.50 + 100 + 0 + 100 \\ &= 18,600 \text{ W} \end{aligned}$$

The Operational Amplifier

Drill Exercises

DE 6.1 [a] $v_o = (-100/8)v_s$, $v_s = -12.5v_o$

$v_s(\text{V})$	0.40	0.72	2.00	-0.60	-0.80	-2.00
$v_o(\text{V})$	-5.0	-9.0	-10.00	7.5	10.0	15.0

[b] $-10 = -12.5v_s$, $v_s = 0.8 \text{ V}$; $15 = -12.5v_s$, $v_s = -1.2 \text{ V}$

Therefore $-1.2 \leq v_s \leq 0.8 \text{ V}$

DE 6.2 $v_o = (-4_x/8)v_s = (0.64R_x/8) = 15 \text{ V}$

Therefore $R_x = \frac{120}{0.64} = 187.50 \text{ k}\Omega$, $0 \leq R_x \leq 187.50 \text{ k}\Omega$

DE 6.3 [a] $v_o = -\frac{250}{5}v_a - \frac{250}{25}v_b = -50(0.1) - 10(0.25) = -5 - 2.5 = -7.5 \text{ V}$

[b] $v_o = -50v_a - 2.5 = -10 \text{ V}$; therefore $50v_a = 7.5$, $v_a = 0.15 \text{ V}$

[c] $v_o = -5 - 10v_b = -10 \text{ V}$; $10v_b = 5$, $v_b = 0.5 \text{ V}$

[d] $v_o = -50v_a + 10v_b = -5 + 2.5 = -2.5 \text{ V}$

$v_o = -50v_a + 2.5 = -10 \text{ V}$;

$50v_a = 12.5$, $v_a = 0.25 \text{ V}$

$-50v_a + 2.5 = 15$, $50v_a = -12.5$, $v_a = -0.25 \text{ V}$

$v_o = -5 + 10v_b = -10 \text{ V}$; $10v_b = -5$; $v_b = -0.5 \text{ V}$

$-5 + 10v_b = 15$; $10v_b = 20$; $v_b = 2.0 \text{ V}$

DE 6.4 [a] $\frac{v_1}{3.3} + \frac{v_1 - v_o}{46.2} = 0$, therefore $v_o = 15v_1$, $v_1 = v_2$

Therefore $v_o = 15v_2$, $v_2 = \frac{0.75R_x}{20 + R_x}$

Therefore when $R_x = 80 \text{ k}\Omega$, $v_2 = 0.6 \text{ V}$, $v_o = 9 \text{ V}$

[b] $\frac{15(0.75R_x)}{20 + R_x} = 10$, $R_x = 160 \text{ k}\Omega$

DE 6.5 [a] Assume v_a is acting along. Replacing v_b with a short circuit yields $v_2 = 0$, therefore $v_1 = 0$ and we have

$$\frac{0 - v_a}{R_a} + \frac{0 - v'_o}{R_b} + i_1 = 0, \quad i_1 = 0$$

Therefore $\frac{v'_o}{R_b} = -\frac{v_a}{R_a}$, $v'_o = \frac{R_b}{R_a}v_a$

Assume v_b is acting alone. Replace v_a with a short circuit. Now

$$v_2 = v_1 = \frac{v_b R_d}{R_c + R_d}$$

$$\frac{v_1}{R_a} + \frac{v_1 - v''_o}{R_b} + i_1 = 0, \quad i_1 = 0$$

$$\left(\frac{1}{R_a} + \frac{1}{R_b}\right) \left(\frac{R_d}{R_c + R_d}\right) v_b - \frac{v''_o}{R_b} = 0$$

$$v''_o = \left(\frac{R_b}{R_a} + 1\right) \left(\frac{R_d}{R_c + R_d}\right) v_b = \frac{R_d}{R_a} \left(\frac{R_a + R_b}{R_c + R_d}\right) v_b$$

$$v_o = v'_o + v''_o = \frac{R_d}{R_a} \left(\frac{R_a + R_b}{R_c + R_d}\right) v_b - \frac{R_b}{R_a} v_a$$

[b] $\frac{R_d}{R_a} \left(\frac{R_a + R_b}{R_c + R_d}\right) = \frac{R_b}{R_a}$, therefore $R_d(R_a + R_b) = R_b(R_c + R_d)$

$$R_d R_a = R_b R_c, \quad \text{therefore} \quad \frac{R_a}{R_b} = \frac{R_c}{R_d}$$

When $\frac{R_d}{R_a} \left(\frac{R_a + R_b}{R_c + R_d}\right) = \frac{R_b}{R_a}$

Eq. (6.21) reduces to $v_o = \frac{R_b}{R_a} v_b - \frac{R_b}{R_a} v_a = \frac{R_b}{R_a} (v_b - v_a)$.

DE 6.6 [a] $v_o = \frac{20(50)}{10(25)} v_b - \frac{40}{10} v_a = 4(v_b - v_a) = 24 - 4v_a$

$$24 - 4v_a = \pm 10 \text{ V}$$

$$4v_a = 24 \mp 10, \quad v_a = 3.5 \text{ V}, \quad v_a = 8.5 \text{ V}$$

Therefore $3.5 \leq v_a \leq 8.5 \text{ V}$

$$\begin{aligned}
 \text{[b]} \quad v_o &= \frac{5(50)}{10(10)} v_b - 4v_a = 2.5v_b - 4v_a \\
 2.5v_b - 4v_a &= 15 - 4v_a = \pm 10 \text{ V} \\
 15 \mp 10 &= 4v_a, \quad v_a = 1.25 \text{ V}, \quad v_a = 6.25 \text{ V} \\
 \text{Therefore} \quad 1.25 &\leq v_a \leq 6.25 \text{ V}
 \end{aligned}$$

$$\text{DE 6.7 [a]} \quad R_x \text{ (balance value)} = 20 \text{ k}\Omega$$

$$\text{Therefore} \quad 20,001 = \left[10(2) \times \frac{10^3}{1} \right] (i + \epsilon), \quad \epsilon = 5 \times 10^{-5}$$

$$\text{Therefore} \quad (v_1 - v_2) \cong (1.5 \times 10^4)(10^3) \frac{5 \times 10^{-5}}{(11,000)^2} = 6.2 \mu\text{V}$$

$$\text{[b]} \quad |\epsilon| \leq \frac{20(11,000)^2}{(1.5 \times 10^7)(2 \times 10^6)} = \left(\frac{2420}{3} \right) 10^{-7}$$

$$\text{Therefore} \quad R_x = 20,000 \left[1 \pm \left(\frac{2420}{3} \right) 10^{-7} \right]$$

$$\begin{aligned}
 \text{Thus } R_x &\text{ must lie in the range } 20,001.613 \text{ to } 19,998.387 \\
 \text{or } 19,998.387 &\leq R_x \leq 20,001.613 \Omega
 \end{aligned}$$

$$\begin{aligned}
 \text{DE 6.8 [a]} \quad v_c &= 0.5(v_1 + v_2) = 0.5(15.6 + 4.4) = 10 \mu\text{V} \\
 v_d &= (v_2 - v_1) = 4.4 - 15.6 = -11.2 \mu\text{V}
 \end{aligned}$$

$$\text{[b]} \quad \text{CMRR} = 20 \log_{10} |A_d/A_c| = 20 \log_{10} 1000 = 60 \text{ dB}$$

$$\text{[c]} \quad A_1 + A_2 = 1000, \quad -0.5A_1 + 0.5A_2 = 10^6$$

$$\text{Therefore} \quad A_1 = -999,500 \quad \text{and} \quad A_2 = 1,000,500$$

$$\begin{aligned}
 \text{[d]} \quad v_o &= A_c v_c + A_d v_d = 1000(10) \times 10^{-6} + 10^6(-11.2 \times 10^{-6}) \\
 &= 0.01 - 11.20 = -11.19 \text{ V}
 \end{aligned}$$

$$\text{[e]} \quad v_1 = v_2 = 15.6 \mu\text{V}$$

Problems

$$\text{P 6.1} \quad \frac{v_b - v_a}{20} + \frac{v_b - v_o}{160} = 0, \quad \text{therefore} \quad v_o = 9v_b - 8v_a$$

$$\text{[a]} \quad v_a = 1.5 \text{ V}, \quad v_b = 0 \text{ V}, \quad v_o = -12 \text{ V}$$

$$\text{[b]} \quad v_a = 3.0 \text{ V}, \quad v_b = 0 \text{ V}, \quad v_o = -18 \text{ V (sat)}$$

$$\text{[c]} \quad v_a = 1.0 \text{ V}, \quad v_b = 2 \text{ V}, \quad v_o = 10 \text{ V}$$

$$\text{[d]} \quad v_a = 4.0 \text{ V}, \quad v_b = 2 \text{ V}, \quad v_o = -14 \text{ V}$$

[e] $v_a = 6.0 \text{ V}, \quad v_b = 8 \text{ V}, \quad v_o = 18 \text{ V} \quad (\text{sat})$

[f] If $v_a = 4.5 \text{ V}, \quad v_o = 9v_b - 36 = \pm 18$
 $\therefore 9v_b = 36 \pm 18; \quad v_b = 54/9 = 6 \text{ V}; \quad v_b = 18/9 = 2 \text{ V}$
 $\therefore 2 \leq v_b \leq 6 \text{ V}$

P 6.2 $\frac{0-2}{5} + \frac{0-v_o}{40} = 0; \quad v_o = -16 \text{ V}$

$$i_o + \frac{v_o - 0}{40 \times 10^3} + \frac{v_o}{3.2 \times 10^3} = 0$$

$$i_o - 0.4 - 5 = 0$$

$$i_o = 5.4 \text{ mA}$$

P 6.3 Since the current into the inverting input terminal of an ideal op-amp is zero, the voltage across the $2.2 \text{ M}\Omega$ resistor is $(3.5)(2.2)$ or 7.7 V . Therefore the voltmeter reads 7.7 V .

P 6.4 $v_o = -(10)(0.5) = -5 \text{ V}; \quad i_b = \frac{v_o}{5} \times 10^{-3} = -1 \text{ mA}$

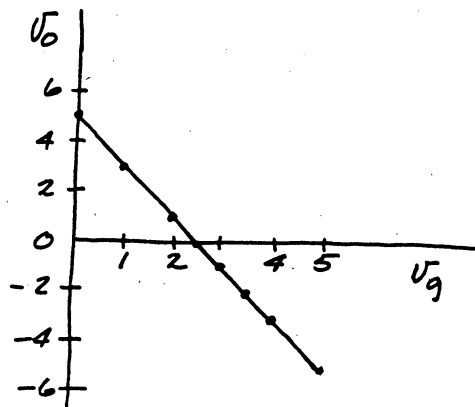
P 6.5 [a] First, note that $v_1 = v_2 = 2.5 \text{ V}$

Let v_{o1} equal the voltage output of the op-amp. Then

$$\frac{2.5 - v_g}{5} + \frac{2.5 - v_{o1}}{10} = 0, \quad \therefore v_{o1} = 7.5 - 2v_g$$

Also note that $v_{o1} - 2.5 = v_o, \quad \therefore v_o = 5 - 2v_g$

v_g	v_o
0	5
1	3
2	1
2.5	0
3	-1
4	-3
5	-5



[b] Yes, the output voltage is bipolar, i.e., $-5 \text{ V} \leq v_o \leq 5 \text{ V}$ and the input voltage is unipolar $0 \leq v_g \leq 5 \text{ V}$.

P 6.6 [a] $\frac{0 - 0.15}{2} + \frac{0 - v_1}{40} = 0, \quad \therefore v_1 = -3 \text{ V}$

[b] $\frac{v_1 - 0}{40} + \frac{v_1}{20} + \frac{v_1 - v_o}{50} = 0$
 $\therefore 19v_1 - 4v_o = 0, \quad v_o = \frac{19v_1}{4} = -14.25 \text{ V}$

[c] $i_2 = \frac{0 - v_1}{40 \times 10^3} = \frac{3}{40 \times 10^3} = 75 \mu\text{A}$

[d] $i_o + \frac{v_o}{25} + \frac{v_o - v_1}{50} = 0$
 $i_o + \left(\frac{-14.25}{25}\right) + \left(\frac{-11.25}{50}\right) = 0; \quad i_o = 795 \mu\text{A}$

P 6.7 [a] Let v_Δ be the voltage from the potentiometer contact to ground. Then

$$\frac{0 - v_g}{4} + \frac{0 - v_\Delta}{20} = 0$$

$$-5v_g - v_\Delta = 0, \quad \therefore v_\Delta = -800 \text{ mV}$$

$$\frac{v_\Delta}{\alpha R_\Delta} + \frac{v_\Delta - 0}{20} + \frac{v_\Delta - v_o}{(1 - \alpha)R_\Delta} = 0$$

$$\frac{v_\Delta}{\alpha} + 6v_\Delta + \frac{v_\Delta - v_o}{1 - \alpha} = 0$$

$$v_\Delta \left(\frac{1}{\alpha} + 6 + \frac{1}{1 - \alpha} \right) = \frac{v_o}{1 - \alpha}$$

$$\therefore v_o = -0.80 \left[1 + 6(1 - \alpha) + \frac{(1 - \alpha)}{\alpha} \right]$$

When $\alpha = 0.25$, $v_o = -0.80(1 + 4.5 + 3) = -6.8 \text{ V}$

When $\alpha = 0.80$, $v_o = -0.80(1 + 1.2 + 0.25) = -1.96 \text{ V}$

$$\therefore -6.8 \text{ V} \leq v_o \leq -1.96 \text{ V}$$

[b] $-0.8 \left[1 + 6(1 - \alpha) + \frac{(1 - \alpha)}{\alpha} \right] = -12$

$$\alpha + 6\alpha(1 - \alpha) + (1 - \alpha) = 15\alpha$$

$$\alpha + 6\alpha - 6\alpha^2 + 1 - \alpha = 15\alpha$$

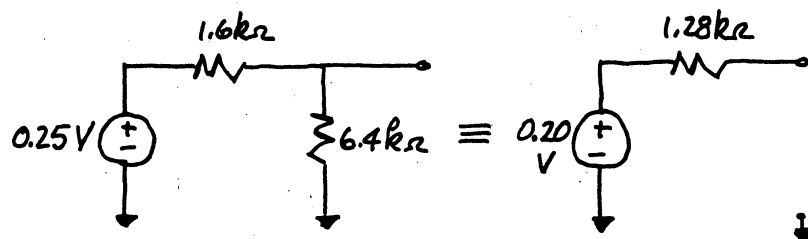
$$\therefore 6\alpha^2 + 9\alpha - 1 = 0$$

$$\alpha^2 + 1.5\alpha - \frac{1}{6} = 0$$

$$\alpha = -0.75 \pm \sqrt{0.72917}$$

$$\alpha \cong 0.1039$$

- P 6.8** [a] Replace the combination of v_g , $1.6\text{ k}\Omega$, and the $6.4\text{ k}\Omega$ resistors with its Thévenin equivalent.



$$\text{Then } v_o = \frac{-(12 + \sigma 50)}{1.28} (0.20)$$

At saturation $v_o = -5\text{ V}$; therefore

$$-\left(\frac{12 + \sigma 50}{1.28}\right) (0.2) = -5, \text{ or } \sigma = 0.4$$

Thus for $0 \leq \sigma < 0.40$ the operational amplifier will not saturate.

[b] When $\sigma = 0.272$, $v_o = \frac{-(12 + 13.6)}{1.28} (0.20) = -4\text{ V}$

$$\text{Also } \frac{v_o}{10} + \frac{v_o}{25.6} + i_o = 0$$

$$\therefore i_o = -\frac{v_o}{10} - \frac{v_o}{25.6} = \frac{4}{10} + \frac{4}{25.6} \text{ mA} = 556.25 \mu\text{A}$$

P 6.9 [a] $v_o = -\frac{220}{44}v_a - \frac{220}{27.5}v_b - \frac{220}{80}v_c = -5v_a - 8v_b - 2.75v_c$

$$v_o = -5(1) - 8(1.5) - 2.75(-4)$$

$$v_o = -5 - 12 + 11 = -6\text{ V}$$

[b] $v_o = 6 - 8v_b = \pm 10$

$$\therefore v_b = -0.5\text{ V when } v_o = 10\text{ V; } v_b = 2.0\text{ V when } v_o = -10\text{ V}$$

$$\therefore -0.5\text{ V} \leq v_b \leq 2.0\text{ V}$$

P 6.10 [a] $\frac{12-15}{55} + \frac{12-10}{66} + \frac{12-8}{220} + \frac{12}{600} + \frac{12-v_o}{330} = 0$

$$v_o = -18 + 10 + 6 + 6.6 + 12 = 16.6\text{ V}$$

[b] $-\frac{3}{55} + \frac{12-v_b}{66} + \frac{4}{220} + \frac{12}{600} + \frac{12}{330} = \frac{v_o}{330}$

$$v_o = 66.6 - 5v_b, \therefore v_b = 66.6 \pm 20$$

$$5v_b = 86.6, v_b = 17.32$$

$$5v_b = 46.6, v_b = 9.32$$

$$\therefore 9.32 \leq v_b \leq 17.32\text{ V}$$

$$\text{P6.11 [a]} \quad -\frac{3}{55} + \frac{2}{66} + \frac{4}{220} + \frac{12}{600} + \frac{12 - v_o}{R_f} = 0$$

$$\therefore v_o = 12 + \frac{12R_f}{600} + \frac{4R_f}{220} + \frac{2R_f}{66} - \frac{3R_f}{55}$$

$$\pm 20 = 12 + R_f \left(\frac{1}{50} + \frac{1}{55} + \frac{1}{33} - \frac{3}{55} \right)$$

Since $R_f > 0$,

$$8 = R_f \left(\frac{1}{50} + \frac{1}{33} - \frac{2}{55} \right); \quad 2640 = R_f(4.6); \quad R_f = 573.91 \text{ k}\Omega$$

$$[\text{b}] \quad \frac{20}{20} + \frac{20 - 12}{573.91} + i_o = 0; \quad i_o = -1.01394 \text{ mA}; \quad i_o = -1013.94 \mu\text{A}$$

P6.12 Let v_{o1} = output voltage of the amplifier on the left. Let v_{o2} = output voltage of the amplifier on the right. Then

$$v_{o1} = \frac{-50}{10}(2) = -10 \text{ V}; \quad v_{o2} = \frac{-250}{25}(-1) = 10 \text{ V}$$

$$i_a = \frac{v_{o2} - v_{o1}}{5} = \frac{20}{5} = 4 \text{ mA}$$

$$\text{P6.13 [a]} \quad \text{The output voltage of the first op-amp is } v_{o1} = \frac{-80}{20}v_g = -4v_g$$

$$\text{The output voltage of the second op-amp is } v_{o2} = \frac{-16}{10}(-4v_g) = 6.4v_g$$

When v_g has its largest value, i.e., 1.2 V, $v_{o1} = -4.8 \text{ V}$ and $v_{o2} = 7.68 \text{ V}$

Therefore neither op-amp saturates.

$$\text{The expression for } i_g \text{ is } i_g = \frac{v_g}{20} + \frac{v_g - 6.4v_g}{R_o} = v_g \left[\frac{1}{20} - \frac{5.4}{R_o} \right]$$

$$i_g = 0 \quad \text{when} \quad \left(\frac{1}{20} - \frac{5.4}{R_o} \right) = 0, \quad \text{or} \quad R_o = 108 \text{ k}\Omega$$

$$[\text{b}] \quad i_{R_o} = \frac{6.4 - 1.0}{108} = 0.05 \text{ mA}$$

$$p_{R_o} = (0.05 \times 10^{-3})^2 (108 \times 10^3)$$

$$p_{R_o} = 270 \times 10^{-6} = 270 \mu\text{W}$$

P6.14 [a] Assume the op-amp is operating within its linear range, then

$$i_L = \frac{9}{5} = 1.8 \text{ mA}$$

$$\text{For } R_L = 4 \text{ k}\Omega \quad v_o = (4 + 5)(1.8) = 16.2 \text{ V}$$

Now since $v_o < 18 \text{ V}$ our assumption of linear operation is correct, therefore

$$i_L = 1.8 \text{ mA}$$

[b] $i_L = 1.8(5 + R_L)$
 $5 + R_L = 10 \text{ k}\Omega, \quad R_L = 5 \text{ k}\Omega$

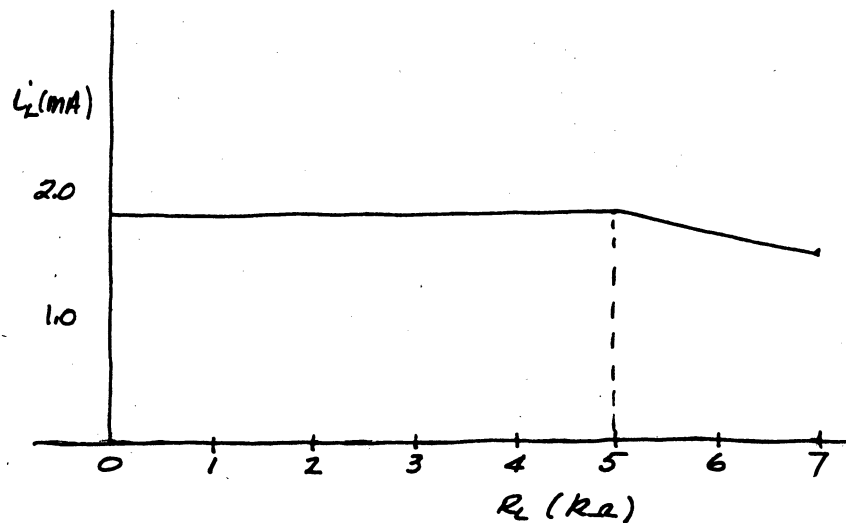
[c] Op-amp saturates for $R_L \geq 5 \text{ k}\Omega$, $\therefore i_L = \frac{18}{5+7} = 1.5 \text{ mA}$

If we assume $i_1 = i_2 \approx 0$, the voltage across the input terminals of the op-amp is

$$v_{21} \approx 9 - 5(1.5) = 1.5 \text{ V}$$

If we assume $R_{in} = 500 \text{ k}\Omega$, then $i_1 = -i_2 = -(1.5/500) = -3 \mu\text{A}$, which is small compared to i_L .

[d]



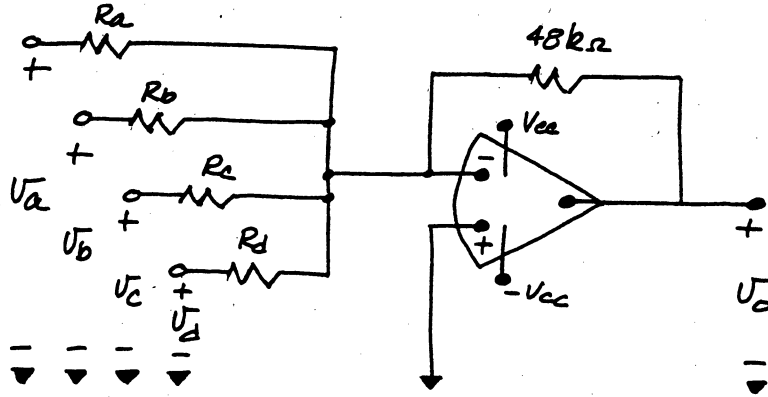
P 6.15 [a] $v_2 = v_1 = 5 \text{ V}$, therefore the current in the left $1\text{-k}\Omega$ resistor is $5/1 = 5 \text{ mA}$. This is also the current in the $1\text{-k}\Omega$ feedback resistor. Therefore the voltage across the $1\text{-k}\Omega$ right-side resistor is 10 V , i.e., $5 + 5 = 10 \text{ V}$. The current i_2 is zero, i.e., the current into the noninverting input terminal. Therefore

$$i_a = 5 + 10 + 0 = 15 \text{ mA}$$

[b] $v_o = 10 + 15R = 15; \quad R = \frac{5}{15} \times 10^3 = 333.33 \Omega$

P 6.16 $v_o = -\left[\frac{R_f}{3}(0.15) + \frac{R_f}{5}(0.10) + \frac{R_f}{25}(0.25)\right]$
 $-6 = -0.08R_f; \quad R_f = 75 \text{ k}\Omega; \quad \therefore 0 \leq R_f \leq 75 \text{ k}\Omega$

P 6.17



$$v_o = - \left[\frac{48}{R_a} v_a + \frac{48}{R_b} v_b + \frac{48}{R_c} v_c + \frac{48}{R_d} v_d \right]$$

$$\therefore R_a = 48/2 = 24 \text{ k}\Omega \quad R_c = 48/6 = 8 \text{ k}\Omega$$

$$R_b = 48/4 = 12 \text{ k}\Omega \quad R_d = 48/8 = 6 \text{ k}\Omega$$

P 6.18 [a] $v_2 = v_1 = \frac{68}{80} v_g = 0.85 v_g$
 $\therefore \frac{0.85 v_g}{30} + \frac{0.85 v_g - v_o}{63} = 0; \quad \therefore v_o = 2.635 v_g = 2.635(4), \quad v_o = 10.54 \text{ V}$

[b] $v_o = 2.635 v_g = \pm 12$
 $v_g = \pm 4.55 \text{ V}, \quad -4.55 \leq v_g \leq 4.55 \text{ V}$

[c] $\frac{0.85 v_g}{30} + \frac{0.85 v_g - v_o}{R_f} = 0$
 $\left(\frac{0.85 R_f}{30} + 0.85 \right) v_g = v_o = \pm 12$
 $\therefore 1.7 R_f + 51 = \pm 360; \quad 1.7 R_f = 360 - 51; \quad R_f = 181.76 \text{ k}\Omega$

P 6.19 [a] $v_2 = v_s, \quad v_1 = \frac{R_1 v_o}{R_1 + R_2}, \quad v_1 = v_2$
 Therefore $v_o = \left(\frac{R_1 + R_2}{R_1} \right) v_s = \left(1 + \frac{R_2}{R_1} \right) v_s$

[b] $v_o = v_s$

[c] Because $v_o = v_s$, thus the output voltage follows the signal voltage.

P 6.20 [a] $p_a = \frac{(320 \times 10^{-3})^2}{(16 \times 10^3)} = 6.4 \mu\text{W}$

$$[b] \quad v_{16k\Omega} = \left(\frac{16}{80}\right)(320) = 64 \text{ mV}$$

$$p_b = \frac{(64 \times 10^{-3})^2}{(16 \times 10^3)} = 0.256 \mu\text{W}$$

$$[c] \quad \frac{p_a}{p_b} = \frac{6.4}{0.256} = 25$$

[d] Yes, the operational amplifier serves several useful purposes:

- First, it enables the source to control 25 times as much power delivered to the load resistor. When a small amount of power controls a larger amount of power, we refer to it as *power amplification*.
- Second, it allows the full source voltage to appear across the load resistor, no matter what the source resistance. This is the *voltage follower* function of the operational amplifier.
- Third, it allows the load resistor voltage (and thus its current) to be set without drawing any current from the input voltage source. This is the *current amplification* function of the circuit.

$$\text{P 6.21} [a] \quad \frac{v_1}{11} + \frac{v_1 - v_o}{110} = 0; \quad \therefore v_o = 11v_1$$

$$\frac{v_2 - v_a}{13} + \frac{v_2 - v_b}{27} = 0$$

$$27v_2 - 27v_a + 13v_2 - 13v_b = 0$$

$$40v_2 = 27v_a + 13v_b$$

$$v_2 = 0.675v_a + 0.325v_b$$

$$v_1 = v_2$$

$$\therefore v_o = 11(0.675v_a + 0.325v_b) = 7.425v_a + 3.575v_b$$

$$v_o = 5.94 + 1.43 = 7.37 \text{ V}$$

$$[b] \quad v_2 = v_1 = \frac{v_o}{11} = 0.67 \text{ V} = 670 \text{ mV}$$

$$i_a = \frac{v_a - v_2}{13 \times 10^3} = 10 \times 10^{-6} = 10 \mu\text{A}$$

$$i_b = \frac{v_b - v_2}{27 \times 10^3} = -10 \times 10^{-6} = -10 \mu\text{A}$$

[c] The weighting factor for v_a is 7.425. The weighting factor for v_b is 3.575.

$$\text{P 6.22} [a] \quad \frac{v_1}{20} + \frac{v_1 - v_o}{100} = 0$$

$$6v_1 - v_o = 0, \quad \therefore v_o = 6v_1 = 6v_2$$

$$\frac{v_2 - v_a}{R_a} + \frac{v_2 - v_b}{R_b} + \frac{v_2 - v_c}{R_c} = 0$$

$$R_b R_c v_2 + R_a R_c v_2 + R_a R_b v_2 = v_a R_b R_c + v_b R_a R_c + v_c R_a R_b$$

$$\therefore (R_b R_c + R_a R_c + R_a R_b) v_2 = R_b R_c v_a + R_a R_c v_b + R_a R_b v_c$$

$$\text{Let } \sum PR = R_b R_c + R_a R_c + R_a R_b$$

$$\text{Then } v_o = \frac{6R_b R_c}{\sum PR} v_a + \frac{6R_a R_c}{\sum PR} v_b + \frac{6R_a R_b}{\sum PR} v_c$$

$$\text{By hypothesis } \frac{6R_b R_c}{\sum PR} = 1; \quad \frac{6R_a R_c}{\sum PR} = 2; \quad \frac{6R_a R_b}{\sum PR} = 3$$

$$\text{Therefore } \frac{R_b}{R_a} = \frac{1}{2}, \quad R_a = 2R_b = 30 \text{ k}\Omega; \quad \frac{R_c}{R_b} = \frac{2}{3}, \quad R_c = \frac{2}{3}R_b = 10 \text{ k}\Omega$$

$$[b] \quad v_o = 0.7 + 0.8 + 3.3 = 4.8 \text{ V}$$

$$\therefore v_1 = v_2 = \frac{1}{6}(4.8) = 0.8 \text{ V}$$

$$\therefore i_a = \frac{0.7 - 0.8}{30 \times 10^3} = -3.33 \mu\text{A}$$

$$i_b = \frac{0.4 - 0.8}{15 \times 10^3} = -26.67 \mu\text{A}$$

$$i_c = \frac{1.1 - 0.8}{10 \times 10^3} = 30 \mu\text{A}$$

$$\text{Check: } i_a + i_b + i_c = 0 \\ -3.33 - 26.67 + 30 = 0 \quad (\text{checks})$$

$$\text{P 6.23 [a]} \quad \frac{v_1}{R_g} + \frac{v_1 - v_o}{180} = 0$$

$$\therefore v_o = \left(1 + \frac{180}{R_g}\right) v_1 = Gv_1 = Gv_2$$

$$\frac{v_2 - v_a}{8} + \frac{v_2 - v_b}{2} + \frac{v_2 - v_c}{1} + \frac{v_2}{9} = 0$$

$$\therefore 125v_2 = 9v_a + 36v_b + 72v_c$$

$$\therefore v_o = \frac{9Gv_a}{125} + \frac{36Gv_b}{125} + \frac{72Gv_c}{125}$$

$$\text{It follows that } \frac{9G}{125} = 1.8, \quad G = 0.2(125) = 25$$

$$\therefore 1 + \frac{180}{R_g} = 25, \quad R_g = \frac{180}{24} = 7.5 \text{ k}\Omega$$

$$[b] \quad v_o = 1.8(0.5) + 7.2(0.25) + 14.4(0.15) = 4.86 \text{ V} = 194.40 \text{ mV}$$

$$V_2 = V_1 = \frac{4.86(7.5)}{187.5} = 194.4 \text{ mV}$$

$$i_a = \frac{500 - 194.4}{8} = 38.20 \mu\text{A}$$

$$i_b = \frac{250 - 194.4}{2} = 27.80 \mu\text{A}$$

$$i_c = \frac{150 - 194.4}{1} = -44.40 \mu\text{A}$$

$$i_g = \frac{194.40}{7.5} = 25.92 \mu\text{A}$$

$$i_h = \frac{194.40}{9} = 21.60 \mu\text{A}$$

$$i_o = -\frac{4860}{3.6} - 25.92$$

$$i_o = -1375.92 \mu\text{A}$$

P 6.24 $v_1 = v_2 = \alpha v_g$

$$\frac{v_1 - v_g}{R_1} + \frac{v_1 - v_o}{R_f} = 0$$

$$(v_1 - v_g) \frac{R_f}{R_1} + v_1 - v_o = 0$$

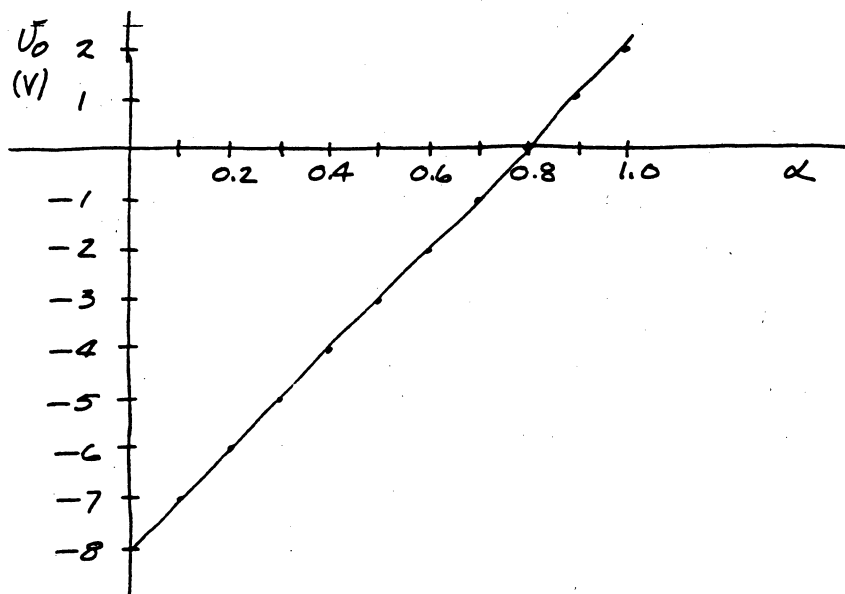
$$v_o = (\alpha v_g - v_g)4 + \alpha v_g$$

$$= [(\alpha - 1)4 + \alpha]v_g$$

$$= (5\alpha - 4)v_g$$

$$= (5\alpha - 4)(2) = 10\alpha - 8$$

α	v_o	α	v_o	α	v_o
0.0	-8 V	0.4	-4 V	0.8	0 V
0.1	-7 V	0.5	-3 V	0.9	1 V
0.2	-6 V	0.6	-2 V	1.0	2 V
0.3	-5 V	0.7	-1 V		



P 6.25 $\frac{v_1 - v_a}{4.7} + \frac{v_1 - v_o}{R_f} = 0$

$$\therefore v_o = \left(1 + \frac{R_f}{4.7}\right) v_1 - \frac{R_f}{4.7} v_a, \quad v_1 = v_2 = \left(\frac{R_b}{R_a + R_b}\right) v_b$$

$$\therefore v_o = \left(1 + \frac{R_f}{4.7}\right) \left(\frac{R_b}{R_a + R_b}\right) v_b - \frac{R_f}{4.7} v_a$$

By hypothesis $\frac{R_f}{4.7} = 10$, $R_f = 47 \text{ k}\Omega$

$$R_a + R_b = 220 \text{ k}\Omega$$

$$\text{Thus } \left(1 + \frac{47}{4.7}\right) \left(\frac{R_b}{220}\right) = 10$$

$$\therefore R_b = 200 \text{ k}\Omega; \quad \therefore R_a = 220 - 200 = 20 \text{ k}\Omega$$

P 6.26 [a] $v_o = \frac{R_d(R_a + R_b)}{R_a(R_c + R_d)}v_b - \frac{R_b}{R_a}v_a = \frac{120(24 + 75)}{24(130 + 120)} \cdot 5 - \frac{75}{24}(8)$
 $v_o = 9.9 - 25 = -15.10 \text{ V}$

[b] $\frac{v_1 - 8}{24} + \frac{v_1 + 15.10}{75} = 0$
 $3.125v_1 - 25 + v_1 + 15.10 = 0$
 $4.125v_1 = 9.9; \quad v_1 = 2.4 \text{ V}$
 $i_a = \frac{8 - 2.4}{24} = 233 \mu\text{A}; \quad R_{in a} = \frac{8}{i_a} = 34.3 \text{ k}\Omega$

[c] $R_{in b} = R_c + R_d = 250 \text{ k}\Omega$

P 6.27 $v_o = \frac{R_d(R_a + R_b)}{R_a(R_c + R_d)}v_b - \frac{R_b}{R_a}v_a$

By hypothesis: $R_b/R_a = 6$; $R_c + R_d = 450 \text{ k}\Omega$; and

$$\frac{R_d(R_a + R_b)}{R_a(R_c + R_d)} = 4.2 = \frac{R_d(7R_a)}{R_a(450)}$$

$$\therefore R_d = 0.6(450) = 270 \text{ k}\Omega, \quad R_c = 450 - 270 = 180 \text{ k}\Omega$$

Also, when $v_o = 0$ we have $\frac{v_1 - v_a}{R_a} + \frac{v_1}{R_b} = 0$

$$\therefore \frac{R_b}{R_a}(v_1 - v_a) + v_1 = 0 \quad \text{or} \quad 7v_1 = 6v_a, \quad v_1 = \left(\frac{6}{7}\right)v_a$$

$$i_a = \frac{v_a - v_1}{R_a} = \frac{v_a}{7R_a}$$

$$\therefore R_{in a} = 7R_a = 21 \text{ k}\Omega, \quad R_a = 3 \text{ k}\Omega, \quad R_b = 6R_a = 18 \text{ k}\Omega$$

P 6.28 $v_2 = 1000i_b$

$$\frac{1000i_b}{R_1} + \frac{1000i_b - v_o}{R_f} - i_a = 0$$

$$\therefore 1000i_b \left[\frac{1}{R_1} + \frac{1}{R_f} \right] - i_a = \frac{v_o}{R_f}$$

$$\therefore 1000i_b \left[1 + \frac{R_f}{R_1} \right] - R_f i_a = v_o$$

By hypothesis $v_o = 5000(i_b - i_a)$

$$\therefore R_f = 5000 \Omega$$

$$1000 \left(1 + \frac{R_f}{R_1} \right) = 5000$$

$$\therefore R_1 = 1250 \Omega$$

P 6.29 [a] $\frac{v_2}{20} + \frac{v_2 - v_c}{30} + \frac{v_2 - v_d}{20} = 0$ or $8v_2 = 2v_c + 3v_d$, $v_2 = 0.25v_c + 0.375v_d$

$$\frac{v_1 - v_a}{20} + \frac{v_1 - v_b}{18} + \frac{v_1 - v_o}{180} = 0 \text{ or } 20v_1 - 9v_a - 10v_b = v_o$$

$$v_1 = v_2 \text{ (ideal op-amp)}$$

$$\therefore 5v_c + 7.5v_d - 9v_a - 10v_b = v_o$$

$$\therefore v_o = 5(3) + 7.5(4) - 9(1) - 10(2) = 15 + 30 - 9 - 20 = 16 \text{ V}$$

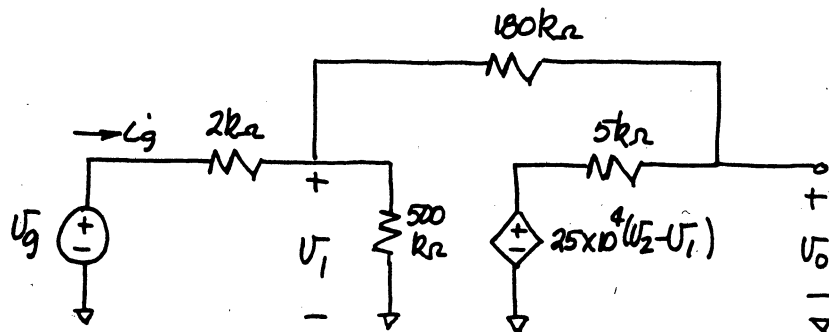
[b] $v_o = 5v_c + 30 - 9 - 20 = 5v_c + 1$

$$\therefore 5v_c + 1 = \pm 20$$

$$v_c = 3.8 \text{ V (+ saturation), } v_c = -4.2 \text{ V (- saturation)}$$

$$-4.2 \text{ V} \leq v_c \leq 3.8 \text{ V}$$

P 6.30 [a]



$$\frac{v_1}{500} + \frac{v_1 - v_g}{2} + \frac{v_1 - v_o}{180} = 0$$

$$456.8v_1 - 5v_o = 450v_g; \quad 91.36v_1 - v_o = 90v_g$$

$$\frac{v_o - 250,000(-v_1)}{5} + \frac{v_o - v_1}{180} = 0; \quad 9 \times 10^6 v_1 + 37v_o = 0$$

$$\Delta = \begin{vmatrix} 91.36 & -1 \\ 9 \times 10^6 & 37 \end{vmatrix} = 9,003,380.32$$

$$N_o = \begin{vmatrix} 91.36 & 90v_g \\ 9 \times 10^6 & 0 \end{vmatrix} = -81 \times 10^7 v_g$$

$$v_o = \frac{N_o}{\Delta} = -89.966v_g; \quad \frac{v_o}{v_g} = -89.966$$

$$[b] \quad N_1 = \begin{vmatrix} 90v_g & -1 \\ 0 & 37 \end{vmatrix} = 3330v_g$$

$$v_1 = \frac{N_1}{\Delta} = 3.7 \times 10^{-4}v_g$$

$$v_g = 100 \text{ mV}, \quad v_1 = 36.986 \mu\text{V}$$

$$[c] \quad i_g = \frac{v_g - v_1}{2} = \frac{v_g - 3.7 \times 10^{-4}v_g}{2}$$

$$R_g = \frac{v_g}{i_g} = \frac{v_g}{v_g - 3.70 \times 10^{-4}v_g} \cdot (2000)$$

$$R_g = 2000.74 \Omega$$

$$[d] \quad \frac{v_o}{v_g} = 90; \quad v_1 = 0 \text{ V}; \quad R_g = 2000 \Omega$$

P 6.31 [a] From the solution of Problem 6.30 we have

$$91.36v_1 - v_o = 90v_g$$

$$\text{At the output we now have } \frac{v_o + 25 \times 10^4 v_1}{5} + \frac{v_o - v_1}{180} + \frac{v_o}{1.6} = 0$$

$$\text{or } 9 \times 10^6 v_1 + 149.5 v_o = 0$$

$$\therefore \Delta = \begin{vmatrix} 91.36 & -1 \\ 9 \times 10^6 & 149.5 \end{vmatrix} = 9,013,658.32$$

$$N_o = \begin{vmatrix} 91.36 & 90v_g \\ 9 \times 10^6 & 0 \end{vmatrix} = -81 \times 10^7 v_g$$

$$v_o = \frac{N_o}{\Delta} = -89.86v_g; \quad \frac{v_o}{v_g} = -89.86$$

$$[b] \quad N_1 = \begin{vmatrix} 90v_g & -1 \\ 0 & 149.5 \end{vmatrix} = 13,455v_g; \quad v_1 = \frac{N_1}{\Delta} = 1.49 \times 10^{-3}v_g$$

$$\text{When } v_g = 100 \text{ mV}, \quad v_1 = 149.27 \mu\text{V}$$

$$[c] \quad R_g = \frac{v_g}{i_g}, \quad i_g = \frac{v_g - v_1}{2000} = \frac{v_g - 1.49 \times 10^{-3}v_g}{2000}$$

$$\therefore R_g = \frac{1}{1 - 1.49 \times 10^{-3}}(2000) = 2002.99 \Omega$$

$$[d] \quad \frac{v_o}{v_g} = -90; \quad v_1 = 0 \text{ V}; \quad R_g = 2000 \Omega$$

P 6.32 [a] $\frac{v_1}{16} + \frac{v_1 - v_g}{800} + \frac{v_1 - v_o}{200} = 0$ or $55v_1 - 4v_o = v_g$

$$\frac{v_o}{20} + \frac{v_o - v_1}{200} + \frac{v_o - 50,000(v_2 - v_1)}{8} = 0$$

$$36v_o - v_1 - 125 \times 10^4(v_2 - v_1) = 0$$

$$v_2 = v_g + \frac{(v_1 - v_g)(240)}{800} = 0.7v_g + 0.3v_1$$

$$36v_o - v_1 - 125 \times 10^4(0.7v_g - 0.7v_1)$$

$$36v_o + 874,999v_1 = 875,000v_g$$

$$\Delta = \begin{vmatrix} 55 & -4 \\ 874,999 & 36 \end{vmatrix} = 3,501,976$$

$$N_o = \begin{vmatrix} 55 & v_g \\ 874,999 & 875,000v_g \end{vmatrix} = 47,250,001v_g$$

$$v_o = \frac{N_o}{\Delta} = 13.49v_g; \quad \frac{v_o}{v_g} = 13.49$$

$$[b] \quad N_1 = \begin{vmatrix} v_g & -4 \\ 875,000v_g & 36 \end{vmatrix} = 3,500,036v_g$$

$$v_1 = \frac{N_1}{\Delta} = 0.999446v_g; \quad v_1 = 999.45 \text{ mV}$$

$$v_2 = 0.7(1000) + 0.3(999.45) = 999.83 \text{ mV}$$

$$[c] \quad v_2 - v_1 = 387.78 \mu\text{V}$$

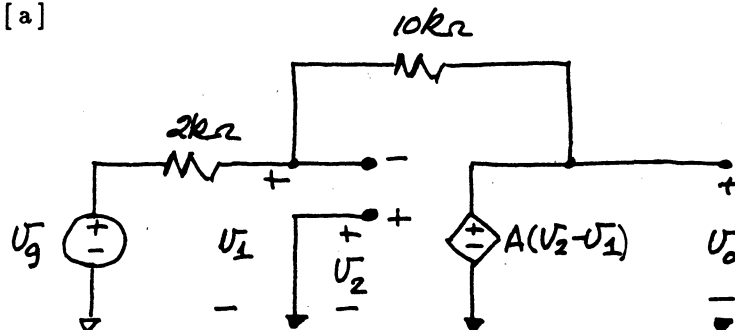
$$[d] \quad i_g = \frac{(1000 - 999.83)10^{-3}}{240 \times 10^3} = 692.47 \text{ pA}$$

$$[e] \quad \frac{v_g}{16} + \frac{v_g - v_o}{200} = 0, \quad \text{since } v_1 = v_2 = v_g$$

$$\therefore v_o = 13.5v_g, \quad \frac{v_o}{v_g} = 13.5$$

$$v_1 = v_2 = 1 \text{ V}; \quad v_2 - v_1 = 0 \text{ V}; \quad i_g = 0 \text{ A}$$

P 6.33 [a]



$$\frac{v_1 - v_g}{2} + \frac{v_1 - v_o}{10} = 0$$

$$\therefore 5v_1 - 5v_g + v_1 - v_o = 0$$

$$6v_1 - v_o = 5v_g$$

$$\text{Also } v_o = A(v_2 - v_1) = -Av_1$$

$$\therefore v_1 = \frac{-v_o}{A}$$

$$\therefore 6\left(\frac{-v_o}{A}\right) - v_o = 5v_g$$

$$v_o = \left(\frac{6}{A_1} + 1\right) = -5v_g$$

$$v_o = \frac{-5Av_g}{(A + 6)}$$

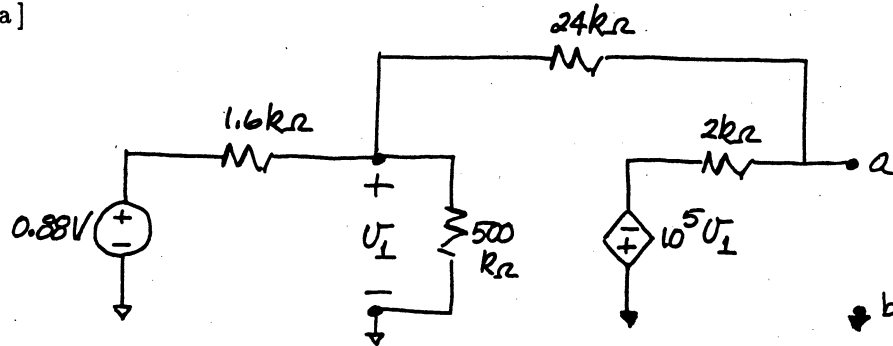
$$[b] \quad v_o = \frac{-5(194)}{200}(1) = -4.85 \text{ V}$$

$$[c] \quad v_o = \frac{-5}{(1+6/A)}(1) = -5 \text{ V}$$

$$[d] \quad \frac{-5A}{(A+6)}(1) = -0.99(5)$$

$$\therefore -5A = -4.95(A+6); \quad -0.05A = -29.70; \quad A = 594$$

P 6.34 [a]



$$\frac{v_1 - 0.88}{1.6} + \frac{v_1}{500} + \frac{v_1 - v_o}{24} = 0$$

$$300v_1 + 0.96v_1 + 20v_1 - 20v_o = 264;$$

$$320.96v_1 - 20v_o = 264$$

$$\frac{v_o + 10^5 v_1}{2} + \frac{v_o - v_1}{24} = 0;$$

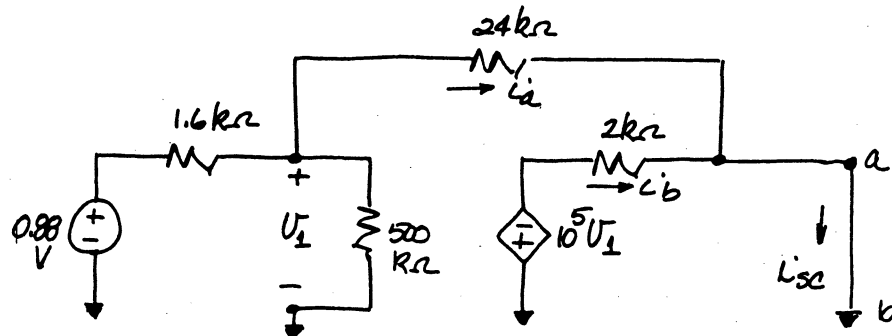
$$12 \times 10^5 v_1 + 13v_o = 0$$

$$\Delta = \begin{vmatrix} 320.96 & -20 \\ 12 \times 10^5 & 13 \end{vmatrix} = 24,004,172.48$$

$$N_o = \begin{vmatrix} 320.96 & 264 \\ 12 \times 10^5 & 0 \end{vmatrix} = -3168 \times 10^5$$

$$v_o = \frac{N_o}{\Delta} = -13.20 \text{ V} = v_{Th}$$

Short-circuit current calculation:



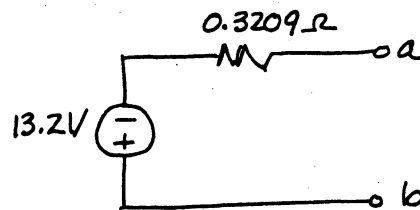
$$i_{sc} = i_a + i_b; \quad i_a = \frac{v_1}{24}; \quad i_b = \frac{-10^5 v_1}{2}$$

$$\frac{v_1 - 0.88}{1.6} + \frac{v_1}{500} + \frac{v_1}{24} = 0$$

$$320.96 v_1 = 264; \quad v_1 = 0.8225 \text{ V}$$

$$i_{sc} = \frac{0.8225}{24} + \frac{(-10^5)(0.8225)}{2} = -41,126.59 \text{ mA} = -41.13 \text{ A}$$

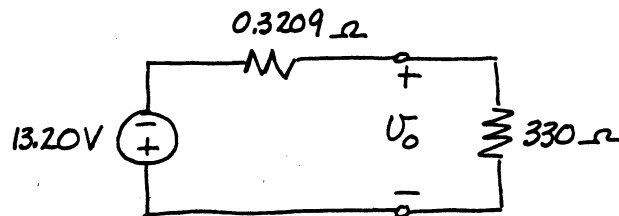
$$R_{Th} = \frac{v_{Th}}{i_{sc}} = \frac{-13.20}{-41.13} = 0.3209 \Omega$$



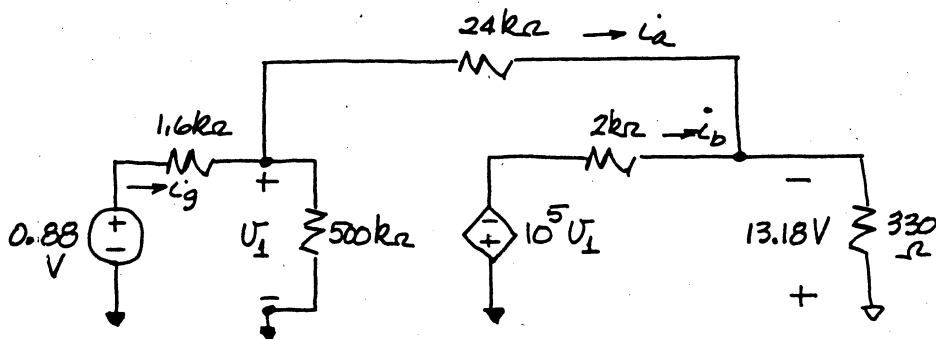
- [b] The output resistance of the inverting amplifier is the same as the Thévenin resistance, i.e.,

$$R_o = R_{Th} = 0.3209 \Omega$$

- [c]



$$v_o = \frac{-13.20}{330.3209}(330) = -13.18 \text{ V}$$



$$\frac{v_1 - 0.88}{1.6} + \frac{v_1}{500} + \frac{v_1 + 13.18}{24} = 0$$

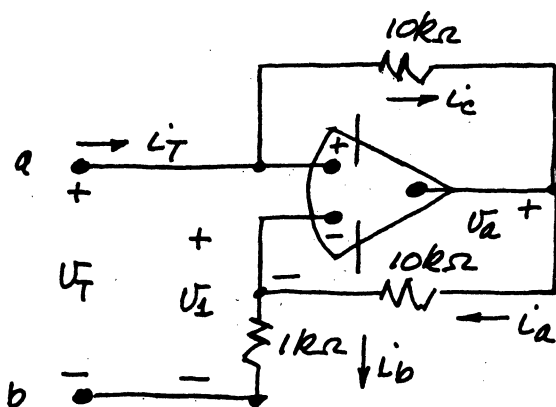
$$320.96v_1 = 0.30; \quad v_1 = 9.42 \times 10^{-4} \text{ V}$$

$$i_g = \frac{0.88 - 9.42 \times 10^{-4}}{1.6}$$

$$R_g = \frac{0.88}{0.88 - 9.42 \times 10^{-4}} (1600)$$

$$R_g = 1601.71 \Omega$$

P 6.35 Since the circuit contains no independent sources, the Thévenin voltage is zero.



Apply a test voltage across a, b and note

$$v_2 = v_T = v_1$$

$$\therefore i_b = \frac{v_T}{1}; \quad i_a = i_b = \frac{v_T}{1}$$

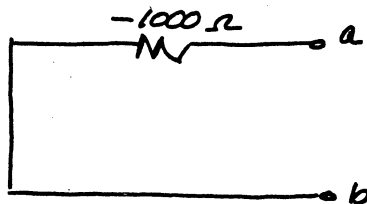
$$v_a = 10i_a = 10v_T$$

$$i_c = \frac{v_T - (v_T + 10v_T)}{10} = \frac{-10v_T}{10} = -v_T (\text{mA})$$

$$i_T = i_c = -10^{-3}v_T$$

$$R_{Th} = \frac{v_T}{i_T} = -10^3 \Omega$$

$$R_{Th} = -1000 \Omega$$



P 6.36 [a] Since the ideal op-amp draws no current, $v_1 = \frac{V_{dc}R_4}{R_1 + R_4}$ and $v_2 = \frac{V_{dc}R_2}{R_2 + R_x}$

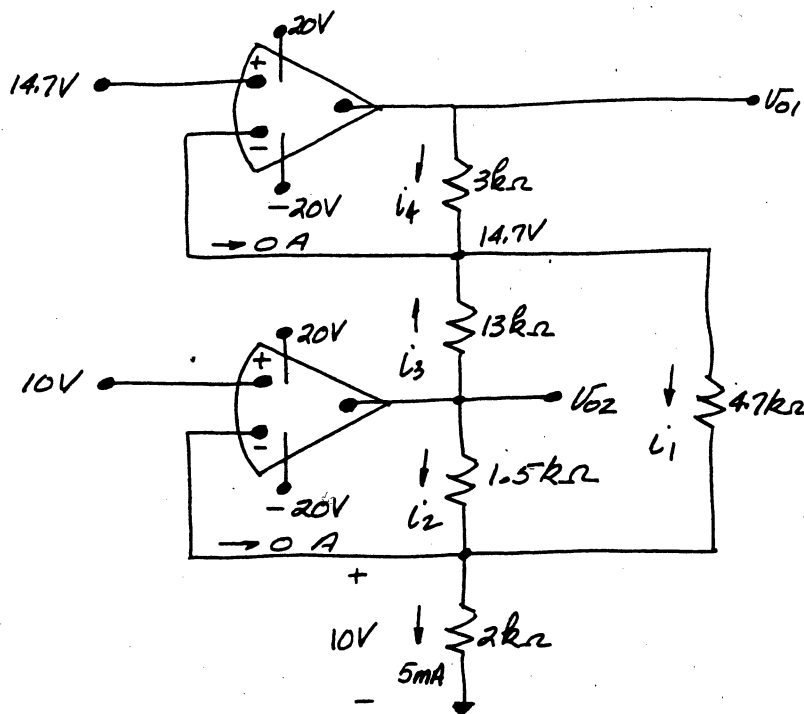
$$\text{Therefore } v_1 - v_2 = V_{dc} \left[\left(\frac{R_4}{R_1 + R_4} \right) - \left(\frac{R_2}{R_2 + R_x} \right) \right]$$

When the terms inside the braces [] are put over a common denominator and the relationship $R_4R_x = R_1R_2(1 + \epsilon)$ is used to simplify the resulting expression, the result is Eq. 6.37.

[b]
$$\frac{\epsilon}{1 + \alpha\epsilon} = \epsilon - \alpha\epsilon^2 + \alpha^2\epsilon^3 - \alpha^3\epsilon^4 \dots$$

Since $\alpha < 1$, the righthand side reduces to ϵ for small values of ϵ , and Eq. 6.37 simplifies to Eq. 6.38.

P 6.37



$$i_1 = \frac{14.7 - 10}{4.7} = 1 \text{ mA}$$

$$i_2 + i_1 + 0 = 5; \quad i_2 = 5 - 1 = 4 \text{ mA}$$

$$v_{o2} = 10 + 1.5i_2 = 16 \text{ V}$$

$$i_3 = \frac{16 - 14.7}{13} = \frac{1.3}{13} = 0.10 \text{ mA}$$

$$i_3 + i_4 - i_1 = 0; \quad i_4 = i_1 - i_3 = 1 - 0.10 = 0.9 \text{ mA}$$

$$v_{o1} = 14.7 + 3(0.9) = 17.40 \text{ V}$$

P 6.38 $v_2 = \frac{-18}{9}(1.5) = -3 \text{ V} = v_1$

$$\frac{v_1 + 18}{1.6} + \frac{v_1 - v_o}{R_f} = 0$$

$$\frac{15}{1.6} - \frac{3}{R_f} = \frac{v_o}{R_f}$$

$$\therefore v_o = \frac{15}{1.6}R_f - 3; \quad v_o = +18 \text{ V} \quad \text{or} \quad -9 \text{ V}$$

$$\therefore \frac{15}{1.6}R_f = 18 + 3 = 21; \quad R_f = 2.24 \text{ k}\Omega$$

P 6.39 Let the top op-amp be No. 1 and the lower op-amp be No. 2. Then

$$i_a = \frac{-1.32}{2.2} = -0.60 \text{ mA}$$

$$v_{o2} = (6.8 + 2.2)i_a = -5.4 \text{ V}$$

$$i_{27 \text{ k}\Omega} = \frac{v_{o2}}{27 \text{ k}\Omega} = \frac{-5.4}{27 \text{ k}\Omega} = -0.2 \text{ mA}$$

$$v_x = -(-0.2)(20) = 4 \text{ V}$$

$$i_a + i_o + i_{27 \text{ k}\Omega} = 0$$

$$i_o = -i_a - i_{27 \text{ k}\Omega} = +0.6 + 0.2 = 0.8 \text{ mA}$$

P 6.40 Let v_{o1} be the output voltage of the first op-amp. Then

$$\frac{0 - 1.1}{3} + \frac{0 - v_{o1}}{18} + \frac{0 - v_o}{24} = 0 \quad \text{or} \quad \boxed{-4v_{o1} - 3v_o = 26.4}$$

$$\frac{v_{o1}}{27} + \frac{v_{o1} - v_o}{3} = 0; \quad \boxed{10v_{o1} - 9v_o = 0}$$

$$\Delta = \begin{vmatrix} -4 & -3 \\ 10 & -9 \end{vmatrix} = 36 + 30 = 66$$

$$N_{o1} = \begin{vmatrix} 26.4 & -3 \\ 0 & -9 \end{vmatrix} = -237.6$$

$$N_o = \begin{vmatrix} -4 & 26.4 \\ 10 & 0 \end{vmatrix} = -264$$

$$v_{o1} = \frac{N_{o1}}{\Delta} = -3.6 \text{ V}; \quad v_o = \frac{N_o}{\Delta} = -4.0 \text{ V}$$

$$i_{24 \text{ k}} = \frac{v_o}{24} = \frac{-4}{24} = -\frac{1}{6} \text{ mA}$$

$$i_{1.6 \text{ k}} = \frac{v_o}{1.6} = \frac{-4}{1.6} = -2.5 \text{ mA}$$

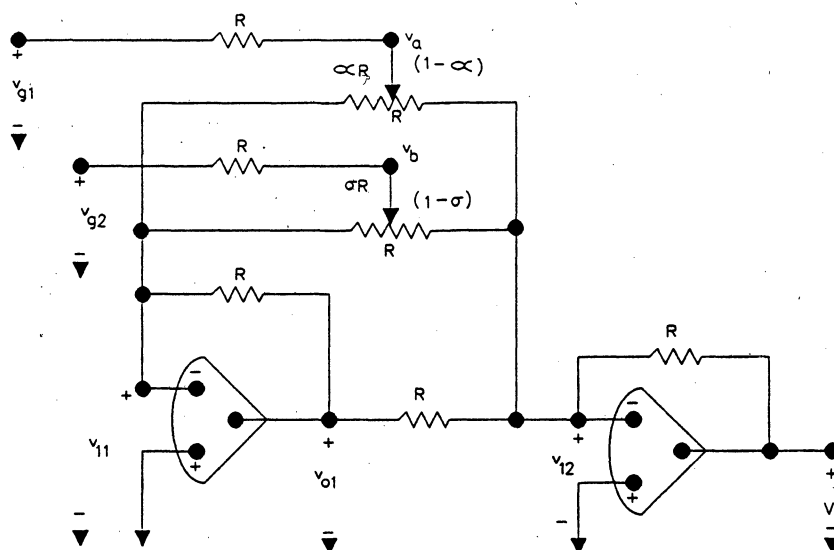
$$i_{3 \text{ k}} = \frac{v_o}{27 + 3} = \frac{-4}{30} = -\frac{2}{15} \text{ mA}$$

$$i_o + i_{24 \text{ k}} + i_{1.6 \text{ k}} + i_{3 \text{ k}} = 0$$

$$i_o - \frac{1}{6} - 2.5 - \frac{2}{15} = 0$$

$$i_o = \frac{1}{6} + 2.5 + \frac{2}{15} = 2.8 \text{ mA}$$

P 6.41 [a] The circuit of Fig. P6.41 is redrawn with intermediate voltages defined to facilitate the analysis.



$$v_{11} = v_{12} = 0$$

$$\frac{0 - v_{01}}{R} + \frac{0 - v_b}{\sigma R} + \frac{0 - v_a}{\alpha R} = 0$$

$$\text{Therefore } v_{01} = -\frac{v_a}{\alpha} - \frac{v_b}{\sigma}$$

$$\frac{0 - v_b}{(1 - \sigma)R} + \frac{0 - v_a}{(1 - \alpha)R} + \frac{0 - v_{01}}{R} + \frac{0 - v_o}{R} = 0$$

$$\text{Therefore } v_o = -v_{01} - \frac{v_a}{1 - \alpha} - \frac{v_b}{1 - \sigma}$$

$$v_o = \frac{v_a}{\alpha} + \frac{v_b}{\sigma} - \frac{v_a}{1 - \alpha} - \frac{v_b}{1 - \sigma} = \frac{v_a(1 - 2\alpha)}{\alpha(1 - \alpha)} + v_b \frac{(1 - 2\sigma)}{\sigma(1 - \sigma)}$$

$$\frac{v_a - v_{g1}}{R} + \frac{v_a - 0}{\alpha R} + \frac{v_a - 0}{(1 - \alpha)R} = 0$$

$$v_a + \frac{v_a}{\alpha} + \frac{v_a}{1 - \alpha} = v_{g1}$$

$$v_a \left(\frac{\alpha(1 - \alpha) + (1 - \alpha) + \alpha}{\alpha(1 - \alpha)} \right) = v_{g1}$$

$$v_a = \frac{v_{g1}\alpha(1 - \alpha)}{(\alpha - \alpha^2 + 1)}$$

$$\text{By symmetry } v_b = \frac{v_{g2}\sigma(1 - \sigma)}{\sigma - \sigma^2 + 1}$$

$$\text{Therefore } v_o = \frac{(1 - 2\alpha)}{(\alpha - \alpha^2 + 1)} v_{g1} + \frac{(1 - 2\sigma)}{(\sigma - \sigma^2 + 1)} v_{g2}$$

[b] $\alpha = \sigma = 1 :$

$$v_o = -v_{g1} - v_{g2} = -(v_{g1} + v_{g2}); \quad \text{inverted summing amplifier}$$

[c] $\alpha = \sigma = 0 :$

$$v_o = v_{g1} + v_{g2}; \quad \text{noninverted summing amplifier}$$

P6.42 It follows directly from the circuit that $v_o = -\frac{120}{7.5}v_g = -16v_g$

From the plot of v_g we have $v_g = 0, \quad t < 0$

$$v_g = t \quad 0 \leq t \leq 0.5$$

$$v_g = 1 - t \quad 0.5 \leq t \leq 1.5$$

$$v_g = -2 + t \quad 1.5 \leq t \leq 2.5$$

$$v_g = 3 - t \quad 2.5 \leq t \leq 3.5$$

$$v_g = -4 + t \quad 3.5 \leq t \leq 4.5, \quad \text{etc.}$$

Therefore

$$v_o = -16t \quad 0 \leq t \leq 0.5$$

$$v_o = -16 + 16t \quad 0.5 \leq t \leq 1.5$$

$$v_o = 32 - 16t \quad 1.5 \leq t \leq 2.5$$

$$v_o = -48 + 16t \quad 2.5 \leq t \leq 3.5$$

$$v_o = 64 - 16t \quad 3.5 \leq t \leq 4.5, \quad \text{etc.}$$

These expressions for v_o are valid as long as the op-amp is not saturated. To find the saturation times, we set $v_o = \pm 5 \text{ V}$.

$$-16t = -5; \quad t = 312.5 \text{ ms}$$

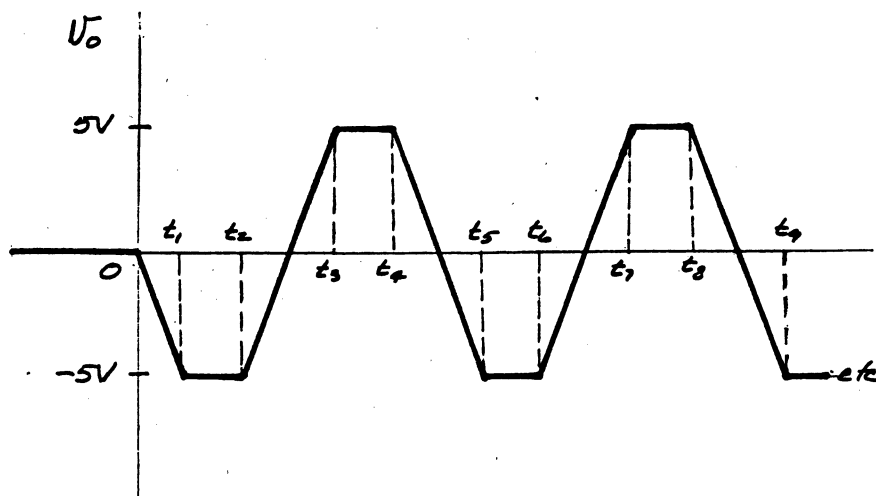
$$-16 + 16t = \pm 5; \quad t = 687.5 \text{ ms}, \quad 1312.5 \text{ ms}$$

$$32 - 16t = \pm 5; \quad t = 1687.5 \text{ ms}, \quad 2312.5 \text{ ms}$$

$$-48 + 16t = \pm 5; \quad t = 2687.5 \text{ ms}, \quad 3312.5 \text{ ms}$$

$$64 - 16t = \pm 5; \quad t = 3687.5 \text{ ms}, \quad 4312.5 \text{ ms}$$

The plot is shown below.



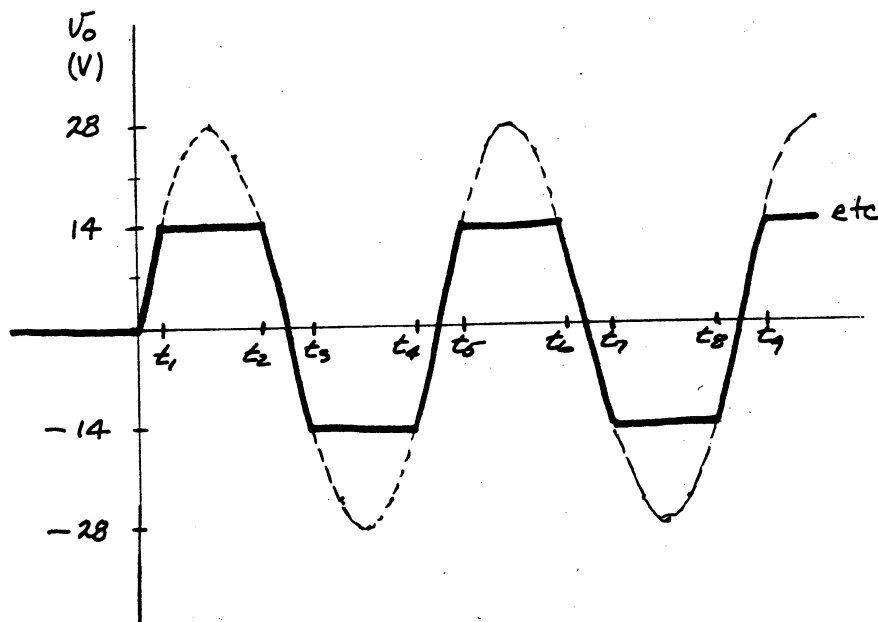
$$\begin{array}{lll}
 t_1 = 312.5 \text{ ms} & t_4 = 1687.5 \text{ ms} & t_7 = 3312.5 \text{ ms} \\
 t_2 = 687.5 \text{ ms} & t_5 = 2312.5 \text{ ms} & t_8 = 3687.5 \text{ ms} \\
 t_3 = 1312.5 \text{ ms} & t_6 = 2687.5 \text{ ms} & t_9 = 4312.5 \text{ ms, etc.}
 \end{array}$$

P 6.43

$$\begin{aligned}
 v_2 &= \frac{5.6}{8.0} v_g = 0.7 v_g \\
 \frac{0.7 v_g}{2} + \frac{0.7 v_g - v_o}{18} &= 0 \\
 6.3 v_g + 0.7 v_g &= v_o \\
 v_o &= 7 v_g = 28 \sin\left(\frac{5\pi}{3}\right) t \text{ V} \quad 0 \leq t \leq \infty \\
 v_o &= 0 \quad t \leq 0
 \end{aligned}$$

At saturation

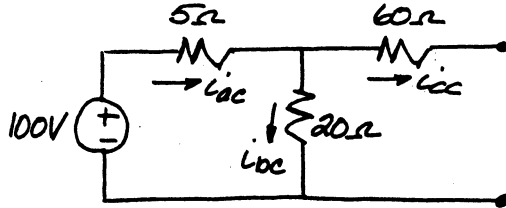
$$\begin{aligned}
 28 \sin\left(\frac{5\pi}{3}\right) t &= \pm 14; \quad \sin \frac{5\pi}{3} t = \pm 0.5 \\
 \therefore \frac{5\pi}{3} t &= \frac{\pi}{6}, \frac{5\pi}{6}, \frac{7\pi}{6}, \frac{11\pi}{6}, \text{ etc.} \\
 t &= 0.10 \text{ s}, 0.50 \text{ s}, 0.70 \text{ s}, \text{ etc.}
 \end{aligned}$$



$$\begin{array}{lll}
 t_1 = 0.10 \text{ s} & t_4 = 1.1 \text{ s} & t_7 = 1.9 \text{ s} \\
 t_2 = 0.5 \text{ s} & t_5 = 1.3 \text{ s} & t_8 = 2.3 \text{ s} \\
 t_3 = 0.70 \text{ s} & t_6 = 1.7 \text{ s} & t_9 = 2.5 \text{ s, etc.}
 \end{array}$$

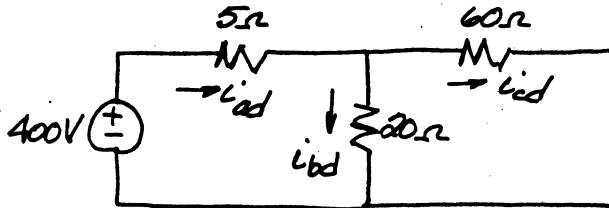
P 6.44 $v_c = \frac{300 - 100}{2} = 100 \text{ V}; \quad v_d = 300 + 100 = 400 \text{ V}$

The common-mode circuit is



$$i_{ac} = i_{bc} = \frac{100}{25} = 4 \text{ A}; \quad i_{cc} = 0$$

The differential mode circuit is



$$i_{ad} = \frac{400}{5 + 15} = 20 \text{ A}; \quad i_{bd} = 20 \left(\frac{60}{80} \right) = 15 \text{ A}; \quad i_{cd} = 20 \left(\frac{20}{80} \right) = 5 \text{ A}$$

$$\therefore i_a = i_{ac} + \frac{1}{2} i_{ad} = 4 + \frac{1}{2} (20) = 14 \text{ A}$$

$$i_b = i_{bc} + \frac{1}{2} i_{bd} = 4 + \frac{1}{2} (15) = 11.5 \text{ A}$$

$$i_c = i_{cc} + \frac{1}{2} i_{cd} = 0 + \frac{1}{2} (5) = 2.5 \text{ A}$$

$$i_d = i_{bc} - \frac{1}{2} i_{bd} = 4 - \frac{1}{2} (15) = -3.5 \text{ A}$$

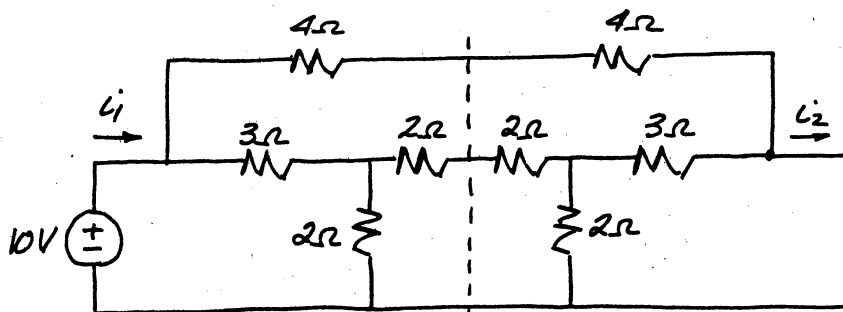
$$i_e = i_{ac} - \frac{1}{2} i_{ad} = 4 - \frac{1}{2} (20) = -6 \text{ A}$$

Check:

$$\sum p_{\text{dev}} = 300i_a - 100i_e = 4200 + 600 = 4800 \text{ W}$$

$$\begin{aligned} \sum p_{\text{diss}} &= (14)^2(5) + (11.5)^2(20) + (2.5)^2(120) + (-3.5)^2(20) + (-6)^2(5) \\ &= 4800 \text{ W} \end{aligned}$$

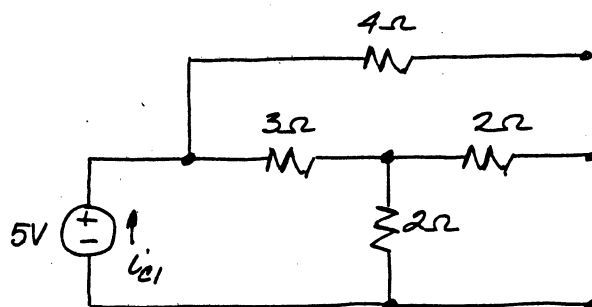
P 6.45 Redraw the circuit to highlight the symmetry.



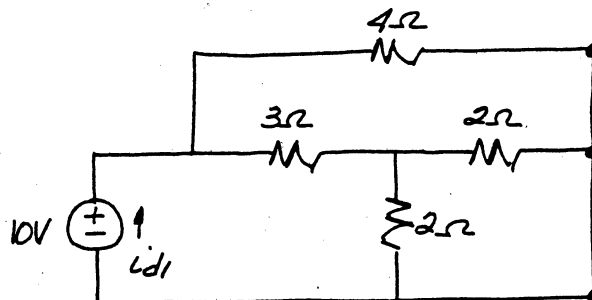
Common-mode voltage $v_c = \frac{1}{2}(10 + 0) = 5 \text{ V}$

Differential-mode voltage $v_d = 10 - 0 = 10 \text{ V}$

Common-mode circuit $i_{c1} = \frac{5}{5} = 1 \text{ A}$



Differential-mode circuit $i_{d1} = \frac{10}{2} = 5 \text{ A}$



$$i_1 = i_{c1} + \frac{1}{2}i_{d1} = 1 - \frac{1}{2}(5) = 3.5 \text{ A}$$

$$-i_2 = i_{c1} - \frac{1}{2}i_{d1} = 1 - \frac{1}{2}(5) = -1.5 \text{ A}$$

$$i_2 = 1.5 \text{ A}$$