Print engine name: PrintServer 20

Print engine version: 17

Printer firmware version: 32

Server Adobe PostScript version: 48.3

Server software version: V2.0

Server network node: crawford

Server name: crawford

Server job number:

Client software version: WRL-1.0

Client network node: util

Client name: flm

Client job name: Circuits\_acdc.ps.732464587

Submitted at: Thu Mar 18 09:39:19 199320:41 1993

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# flm@util Circuits\_acdc.ps.732464587



# ELECTRICAL CIRCUITS DC AND AC

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The section numbers refer to chapters and sections in <u>Engineering in Training Review Manual</u>, 8th <u>Edition</u> by Michael Lindeburg.

Current may be defined by a derivative, i.e. the rate at which charge is moved:

$$i = \frac{dq}{dt}$$

or in the form of an integral as the total charge moved:

$$q = \int_{0}^{t} i(t) dt$$

where i is in units of coulombs/second, or amperes.

# 47.1 Voltage

Voltage is a measure of the work required to move a unit charge through an electric field (usually inside an electrical circuit element such as a resistor). It requires one joule of energy to move one coloumb of charge through a potential difference of one volt.

$$w = \int v dq$$

where w is in joules, v is in volts and dq is in coulombs.

# 47.2 Resisitivity and Resistance

The resistance of ordinary wire can be calculated provided one knows the resistivity of the wire as

$$R = \frac{\rho l}{A}$$

where l is the length of the wire and A is its cross-sectional area. The resistivity  $\rho$  is a property of the material and a function of temperature as given by

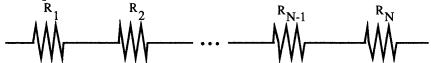
$$\rho = \rho_0 (1 + \alpha \Delta t)$$

where  $\rho_0 = 1.7241 \times 10^{-6} \ \Omega$ -cm²/cm at 20°C,  $\alpha$ =0.00382/°C for hard-drawn copper of the type most commonly used for electrical wiring, and  $\Delta T$  is the temperature difference between the temperature of the desired resistance and that at which  $\rho_0$  is specified, in this case  $\Delta T$ = $T_{specified}$ -20°C.

# Do problem 47-1.

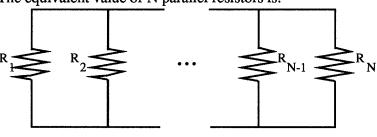
Problem 47-3 will be done as an example.

The equivalent value of N series resistors is:



$$R_{eq} = \sum_{j=1}^{N} R_j$$

The equivalent value of N parallel resistors is:

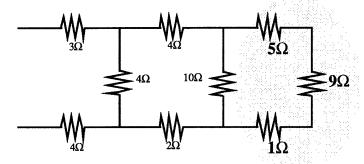


$$R_{eq} = \frac{1}{\sum_{j=1}^{N} \frac{1}{R_j}}$$

For the important case of two resistors in parallel:

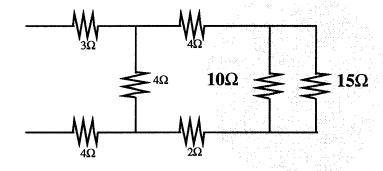
$$R_{eq} = \frac{R_1 R_2}{R_1 + R_2}$$

Equivalent resistance for a complex network:



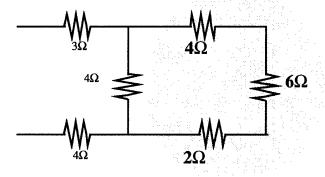
Looks like three resistors in series:

$$R_{eq} = 5\Omega + 1\Omega + 9\Omega = 15\Omega$$



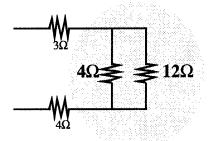
Looks like two resistors in parallel:

$$R_{eq} = \frac{(10)(15)}{(10) + (15)} = 6 \Omega$$



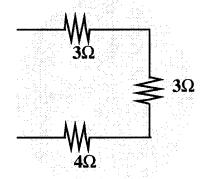
Looks like three resistors in series  $R_{eq} = 4 + 6 + 2 = 12\Omega$ 

$$R_{eq} = 4 + 6 + 2 = 12\Omega$$



Looks like two resistors in parallel:

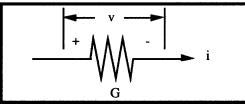
$$R_{eq} = \frac{(4)(12)}{(4) + (12)} = 3 \Omega$$



Looks like three resistors in series:  $R_{eq} = 3 + 3 + 4 = 10\Omega$ 

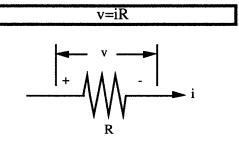
$$R_{eq} = 3 + 3 + 4 = 10\Omega$$

47.3 Conductivity and conductance Ohm's Law can also be written in terms of conductance which is simply 1/R, i.e. v=i/G where G is in mhos, the unit of conductance.



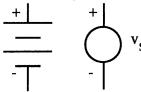
47.4 Ohm's Law Electrical resistance

where R is in units of ohms.

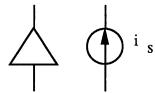


# 47.5 Energy sources

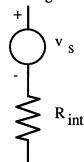
independent ideal voltage source:



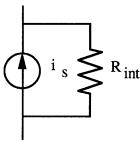
independent ideal current source:



independent real voltage source:



independent real current source:



Perfect voltage and current sources have the following characteristics:

A perfect (ideal) voltage source has R<sub>int</sub>=0.

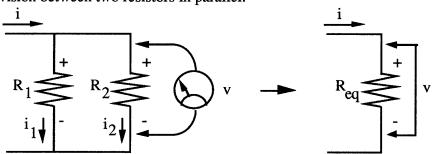
A perfect (ideal) current source has Rint=∞.

# 47.6 Voltage Sources in Series and Parallel

Voltage sources that are in series (even if there are intervening resistances) can be algebraically combined into a single equivalent resistance.

# 47.10 Voltage and Current dividers

Current division between two resistors in parallel:



Since the resistors are in parallel they MUST have the same voltage across them

$$R_{eq} = \frac{R_1 R_2}{R_1 + R_2}$$

$$v = iR_{eq} = \frac{R_1 R_2}{R_1 + R_2} i$$

$$i_1 = \frac{v}{R_1} = \frac{R_2}{R_1 + R_2} i$$

$$i_2 = \frac{v}{R_2} = \frac{R_1}{R_1 + R_2} i$$

This is known as a current divider.

Voltage division between two resistors in series (see the figure below). As the resistors are in series they MUST have the same current thru them.

$$R_{eq} = R_1 + R_2$$

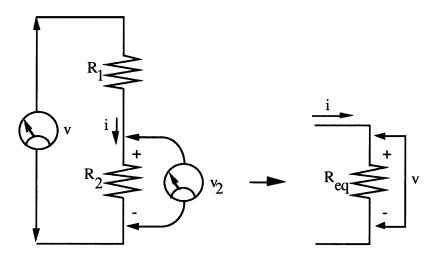
Using Ohm's Law

$$i = \frac{v}{R_{eq}} = \frac{v}{R_1 + R_2}$$

Knowing the current through each resistor we can apply Ohm's Law again to get

$$v_2 = iR_2 = \frac{v}{R_1 + R_2} R_2 = \frac{R_2}{R_1 + R_2} v$$

This result is known as a voltage divider.



Do problem 47-12.

Also look at the units in Problem 47-13 which will be assigned in section 47.15.

# 47.11 Power

Power may also be defined, using our previous relationships, as p=vi.

The unit of power is joules/second, or watts. 746 watts = 1 horsepower is a very common conversion.

# Do problem 47-7.

# 47.12 Decibels

Decibels are units used to express power ratios

$$db = 10 \log_{10} \left( \frac{P_2}{P_1} \right)$$

or voltage and current ratios

$$db = 20 \log_{10} \left( \frac{V_2}{V_1} \right)$$

$$db = 20 \log_{10} \left( \frac{I_2}{I_1} \right)$$

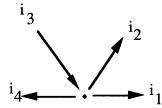
Do problem 47-14. Problem 47-15 will be done as an example.

## 47.14 Kirchoff's Laws

Kirchoff's current Law: the algebraic sum of all currents entering or leaving a node is zero. Mathematically,

$$\sum_{j=1}^{N} i_j = 0$$

For a simple example: i<sub>3</sub>-i<sub>1</sub>-i<sub>2</sub>-i<sub>4</sub>=0 where we used the negative sign to indicate current leaving the node. IMPORTANT: It does not matter whether you use the positive or negative sign to indicate current leaving the node AS LONG AS YOU ARE CONSISTENT.

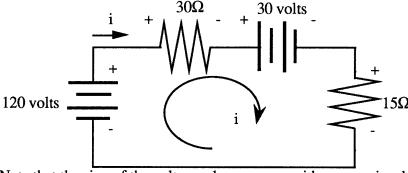


Kirchoff's voltage law states that the algebraic sum of the voltages around any closed path in a circuit is zero, i.e.

$$\sum_{j=1}^{N} v_j = 0$$

# 47.15 Simple Series Circuit

Determine the voltage drop across the resistors and the power delivered by the batteries.



Note that the sign of the voltages drops agrees with our previously defined convention. Summing the voltages around the circuit in a clockwise direction:

$$-120 + 30i + 30 + 15i = 0$$
  
 $45i = 90$   
 $i = 2$  amps

The voltage drop across the  $30\Omega$  resistor is:

$$v_{30\Omega} = iR = (2)(30) = 60 \text{ volts}$$
  
 $v_{15\Omega} = iR = (2)(15) = 30 \text{ volts}$ 

The power supplied by the batteries is:

$$P_{120V} = vi = (120)(2) = 240$$
 watts  
 $P_{30V} = vi = (30)(2) = 60$  watts

The power dissipated by the resistors is:

$$P_{30\Omega} = i2R = (2)2(30) = 120$$
 watts  
 $P_{15\Omega} = i2R = (2)2(15) = 60$  watts

where we used the following formula to calculate the power:

$$P = vi = i^2 R = \frac{v^2}{R}$$

Note that the batteries use a lot of power just canceling each other out.

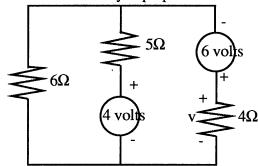
Do problem 47-13.

# 47.21 Superposition

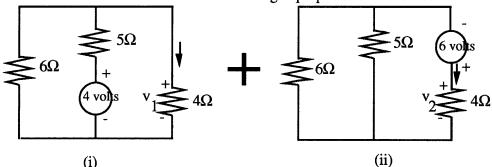
Superposition can be used to determine node voltages but is usually more complex than the loop current method discussed in the next section. To solve a problem by superposition we consider only one voltage or current source at a time (all the other voltage sources are replaced by shorts, all the other current sources are replaced by open circuits) and sum up the resulting voltages or currents. Superposition works because electrical sources are linear.

Example:

Find the voltage v across the  $4\Omega$  resistor by superposition.



To find v in this circuit we consider the following superposition of sources:



In circuit (i), the total resistance seen by the source is  $5 + 416 = 5 + 2.4 = 7.4\Omega$ . The total current is then i=4volts/7.4 $\Omega$ =0.54 ampere. This current goes through the  $5\Omega$  resistor and, then, splits with 0.54(6/(4+6)) = 0.324 amperes going through the  $4\Omega$  resistor. The voltage drop  $v_1$  is then  $v_1$ = iR = (0.324 amperes) $(4\Omega)$ = 1.3 volts.

In circuit (ii), the total resistance seen by the source is  $4 + 5||6 = 4 + 2.73 = 6.73\Omega$ . The total current is i=6volts/6.73 $\Omega$ =0.892 ampere. This current goes through the  $4\Omega$  resistor directly below the source. The voltage drop  $v_2$  across the  $4\Omega$  resistor is then  $v_2$ = iR = (0.892 amperes)( $4\Omega$ )= 3.57 volts.

Since the currents going through the  $4\Omega$  resistor are in the same direction they <u>add</u> giving, for the original circuit,  $v = v_1 + v_2 = 1.3 + 3.57 = 4.87$  volts.

Do problem 47-19.

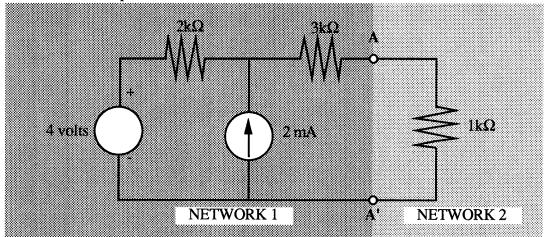
# 47.22 Norton's Theorem

Norton's Theorem (formal definition)

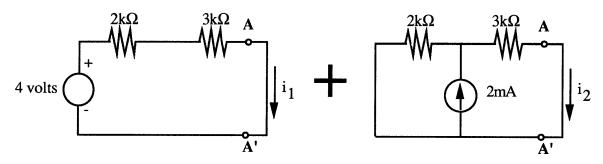
Given any linear circuit, rearrange it in the form of two networks 1 and 2 that are connected together by two zero resistance conductors. Define a current  $i_{SC}$  as the short-circuit current which would appear at the terminals A and A' of network 1 if network 2 were replaced by a short circuit. Then, all the currents and voltages in network 2 will remain unchanged if network 1 is killed (all independent voltage sources and current sources in network 1 are replaced by short circuits and open circuits, respectively) and an independent current source  $i_{SC}$  is connected, with proper polarity, in parallel with the equivalent resistance of the dead (inactive) network 1.

# Example:

Find the Norton equivalent circuit of Network 1 shown below.



Replace network 2 by a short-circuit and superimpose the 4 volt and the 2 ma sources to find  $i_{sc}$ .

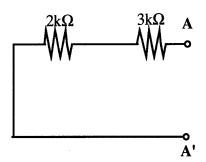


The current  $i_1 = 4$  volts/5k $\Omega = 0.8$ mA. The current  $i_2$  is found using the current divider relationship.

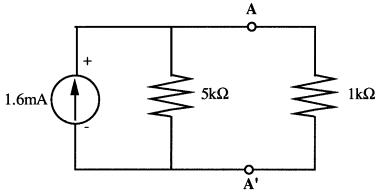
$$i_2 = 2mA \left(\frac{2k\Omega}{2k\Omega + 3k\Omega}\right) = 2mA \left(\frac{2}{5}\right) = 0.8 \text{ mA}$$

Both currents are in the same direction so  $i_{sc} = i_1 + i_2 = 0.8 \text{mA} + 0.8 \text{mA} = 1.6 \text{mA}$ . Shorting out the voltage sources and opening the current sources yields:

Shorting out the voltage sources and opening the current sources yields:



The terminal resistance  $R_T = 2k\Omega + 3k\Omega = 5k\Omega$ The final Norton equivalent circuit is then:



which is certainly easier to analyze than the original circuit with multiple sources.

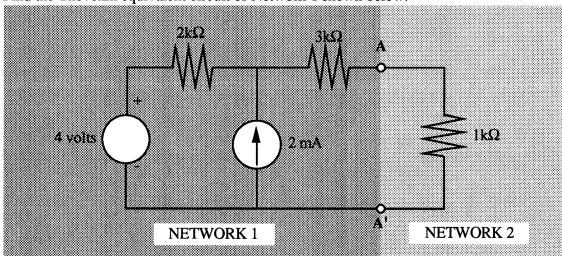
# 47.23 Thevenin's Theorem

Thevenin's Theorem (formal definition):

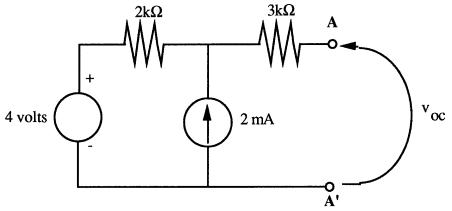
Given any linear circuit, rearrange it in the form of two networks 1 and 2 that are connected together by two zero resistance conductors at A and A'. Define a voltage  $v_{0c}$  as the open-circuit voltage which would appear between the terminals A and A' if network 2 were disconnected so that no current is drawn from network 1. Then, all the currents and voltages in network 2 will remain unchanged if network 1 is killed (i.e., all independent voltage sources and current sources in network 1 are replaced by short circuits and open circuits, respectively) and an independent voltage source  $v_{0c}$  is connected, with proper polarity, in series with the equivalent resistance of the dead (inactive) network 1.

Example:

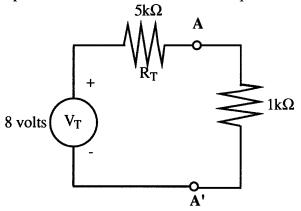
Find the Thevenin equivalent circuit of Network 1 shown below.



Disconnect network 2 at AA' and calculate the open circuit voltage from network 1.

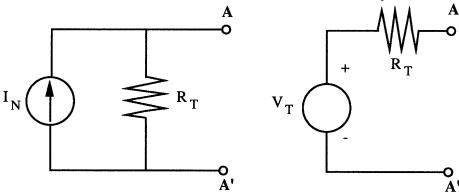


No current flows through the  $3k\Omega$  resistor. Use superposition to find  $v_{oc}$ . From the voltage source only,  $v_1=4$  volts. From the current source only  $v_2=(2k\Omega)(2mA)=4$  volts. The voltages are of the same polarity so  $v_{oc}=4+4=8$  volts. The equivalent resistance is found by replacing the 4 volt source by a short and the 2mA current source by an open and computing the resultant Thevenin resistance  $R_T=2k\Omega+3$  k $\Omega=5k\Omega$ . The Thevenin equivalent circuit to connect at AA' in place of network 1 is then:



# Equivalence of Norton and Thevenin Equivalent Circuits

If you know the Norton equivalent circuit, the Thevenin equivalent circuit is directly computable from Ohm's Law. This observation also works the other way.



Norton equivalent circuit

Thevenin equivalent circuit

Note that R<sub>T</sub> is the same in both circuits and V<sub>T</sub>=I<sub>N</sub>R<sub>T</sub>.

Perfect voltage and current sources have the following characteristics:

A perfect (ideal) voltage source has R<sub>T</sub>=0.

A perfect (ideal) current source has  $R_T = \infty$ .

For a perfect (ideal) source,

if  $V_T=0$  then the source is replaced by a short,  $R_T=0$ .

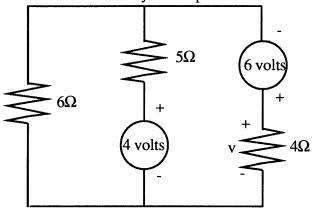
if  $I_N=0$  then the source is replaced by an open,  $R_T=\infty$ .

Do problem 47-18. HINT: Directly apply the Thevenin equivalent circuit shown above.

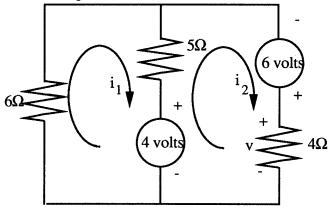
# 47.24 Loop Current Method

# Example:

Find the voltage v across the  $4\Omega$  resistor by the loop current method.



To find v in this circuit we assume current directions for the chosen loops and write Kirchoff's voltage law for each loop as shown below:



Writing the loop equations:

loop1:  $6i_1 + 5i_1 - 5i_2 + 4$ volts =0

loop2:  $-4\text{volts} + 5i_2 - 5i_1 - 6\text{volts} + 4i_2 = 0$ 

Simplifying,

loop1:  $11i_1 - 5i_2 = -4$ volts

loop2:  $-5i_1 + 9i_2 = +10$ volts

which can be solved to give

 $i_2 = +1.216$  amperes and  $i_1 = 0.19$  amperes.

The voltage v across the  $4\Omega$  resistor is then

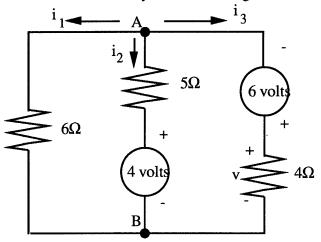
 $v = i_2(4\Omega) = (1.216)(4) = 4.864 \text{ volts}$ 

# Do problem 47-21.

# 47.25 Node Voltage Method

Example:

Find the voltage v across the  $4\Omega$  resistor by the node voltage method.



To find v in this circuit we assume that the node B is ground (0 volts). Typically, the ground is associated with the negative side of a voltage source or other voltage reference. In this case, ground is the negative side of the voltage drop v. The only other node in the circuit is A and we will define the voltage at A to be  $V_A$ . Using the node voltage method we apply Kirchoff's current law to node A.

At A: 
$$i_1 + i_2 + i_3 = 0$$
  
where  
 $V_A = i_1(6\Omega)$ , or  $i_1 = \frac{V_A}{6}$   
 $V_A = i_2(5\Omega) + 4$  volts, or  $i_2 = \frac{V_A - 4}{5}$   
 $V_A = i_3(4\Omega) - 6$  volts, or  $i_3 = \frac{V_A + 6}{4}$ 

Substituting these results into Kirchoff's current law and solving for V<sub>A</sub>:

$$\frac{V_A}{6} + \frac{V_{A}-4}{5} + \frac{V_{A}+6}{4} = 0$$

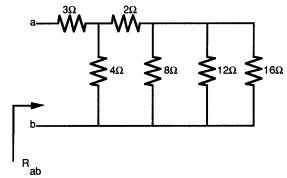
$$V_A = -1.135 \text{ volts.}$$

Then,  $i_3 = (-1.135+6)/4 = 1.216$  amperes and  $v = i_3(4\Omega) = (1.216$  amperes)(4  $\Omega$ ) = 4.864 volts

Notice that all three examples give the same answer. You may judge whether one is particularly easier or faster than the others.

The equivalent resistance Rab is closest to

- (a) 2 ohms
- (b) 4 ohms
- (c) 6 ohms
- (d) 8 ohms
- (e) 10 ohms



Solution:

 $R_{eq}$  for the  $8\Omega$ ,  $12\Omega$  and  $16\Omega$  resistors in parallel is

$$R_{eq} = \frac{1}{\frac{1}{8} + \frac{1}{12} + \frac{1}{16}} = 3.68\Omega$$

and

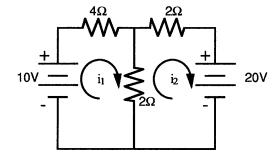
$$R_{ab} = 3 + 411(2+3.68) = 3 + \frac{4 \times (2+3.68)}{4 + (2+3.68)} = 3 + 2.35 = 5.35\Omega$$

The correct answer is (c).

# CIRCUITS 4

The power supplied by the

- 10 volt source is
- (a) 12 watts
- (b) 0 watts
- (c) -12 watts
- (d) 16 watts
- (e) -16 watts



Solution:

Call the clockwise loop currents i<sub>1</sub> and i<sub>2</sub> as shown in the drawing above. Use KCL to obtain two equations in two unknowns

$$61_1 - 21_2 = 10$$
  
 $-2i_1 + 4i_2 = -20$ 

$$-21_1 + 41_2 = -20$$

 $6i_1 - 2i_2 = 10$   $-2i_1 + 4i_2 = -20$ Multiplying the first equation by two gives

$$12i_1 - 4i_2 = 20$$

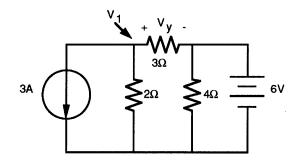
and adding the last two equations we get the solution that  $i_1=0$ .

$$P_{10 \text{ volt source}} = i_1(10 \text{ volts}) = 0$$

The correct answer is (b).

The voltage V<sub>v</sub> is closest to

- (a) 0 volts
- (b) 3.6 volts
- (c) -1.2 volts
- (d) 7.2 volts
- (e) -7.2 volts



# Solution:

Call the voltage drop (from top to bottom) across the  $2\Omega$  resistor V<sub>1</sub>. Using KCL to sum the currents at the node pointed to by V<sub>1</sub> in the above drawing gives the following expression

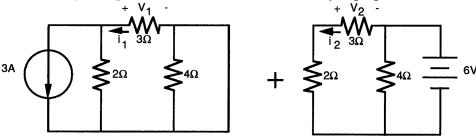
$$\frac{V_1}{2} + \frac{V_1 - 6}{3} = -3$$

Note that we used the + sign for currents coming out of the node. Solving for  $V_v$  gives V:

$$V_y = V_1 - 6 = -7.2 \text{ volts}$$

or  $V_1 = -1.2$  volts. The correct answer is (e).

Alternatively, this problem could have been solved by superposition



Since the  $4\Omega$  resistor is shorted out by the 6 volt source in the circuit on the left we can solve for

the loop current as 
$$i_1 = \frac{2}{2+3} (3A) = 1.2 A$$

The voltage across the  $3\Omega$  resistor is then

$$V_1 = -\left(\frac{6}{5}A\right)(3\Omega) = -\frac{18}{5}A$$

 $V_1 = -\left(\frac{6}{5}A\right)(3\Omega) = -\frac{18}{5}A$ Examing the right hand circuit we can solve for the current i<sub>2</sub> as

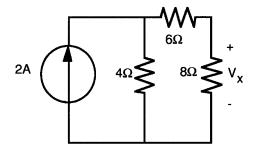
$$i_2 = \frac{6 \text{ V}}{5\Omega} = \frac{6}{5} \text{ A}$$

$$V_2 = -\left(\frac{6}{5}A\right)3\Omega = -\frac{18}{5}$$
 volts

The voltage across the 
$$3\Omega$$
 resistor is then given by  $V_2 = -\left(\frac{6}{5}A\right)3\Omega = -\frac{18}{5}$  volts  
Vy is then the sum of the voltages across the  $3\Omega$  resistor, i.e.  $V_y = V_1 + V_2 = -\frac{18}{5} - \frac{18}{5} = -\frac{36}{5} = -7.2$  volts

The voltage V<sub>x</sub> is closest to

- (a) 16 volts
- (b) 8 volts
- (c) 3.55 volts
- (d) 6.42 volts
- (e) 4.65 volts



#### Solution:

Using current division the current through the  $8\Omega$  resistor is

$$i_{8\Omega} = 2 \times \frac{4}{4 + (6+8)} = \frac{8}{18}$$
 Amps

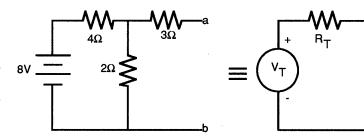
The voltage across the  $8\Omega$  resistor is then given by Ohm's Law as

$$V_x = i_{8\Omega} \times 8\Omega = \frac{8}{18} \times 8 = \frac{64}{18} = 3.55 \text{ Volts}$$
  
The correct answer is (c).

# CIRCUITS 10

The Thevenin equivalent at terminals a-b is closest to

- (a)  $V_T=5.33$  volts,  $R_T=5\Omega$
- (b)  $V_T=1.84$  volts,  $R_T=4.33\Omega$
- (c)  $V_T=1.84$  volts,  $R_T=5\Omega$
- (d)  $V_T = 5.33$  volts,  $R_T = 4.33\Omega$
- (e)  $V_T = 2.67$  volts,  $R_T = 4.33\Omega$



. h

#### Solution:

V<sub>T</sub> is the open-circuit voltage from terminals a-b. The open circuit voltage at a-b is given by the voltage divider relationship

$$V_T = 8 \times \frac{2}{2+4} = 2.67 \text{ Volts}$$

Note that the  $3\Omega$  resistor does enter this relationship since no current flows through it if terminals a-b are open. R<sub>T</sub> is the equivalent resistance with all the sources replaced by their equivalent impedances. For a voltage source this is zero, a short, placing the  $4\Omega$  and  $2\Omega$  resistors in parallel and their resultant in series with the  $3\Omega$  resistor to give

$$R_T = 3 + \frac{2\times4}{2+4} = 3 + \frac{8}{6} = 4.33 \ \Omega$$
  
The correct answer is (e).

The Thevenin equivalent at terminals a-b is closest to

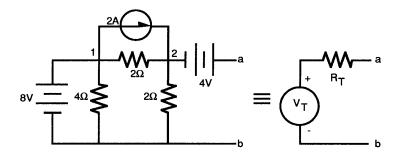
(a)  $V_T=10$  volts,  $R_T=1.5 \Omega$ 

(b)  $V_T=12$  volts,  $R_T=1.0 \Omega$ 

(c)  $V_T=12$  volts,  $R_T=1.5 \Omega$ 

(d)  $V_T=10$  volts,  $R_T=1.0 \Omega$ 

(e)  $V_T=0$  volts,  $R_T=1.0 \Omega$ 



# Solution:

Since this is a more complex circuit than the previous example we must find  $V_T$  indirectly by first finding the voltage  $V_2$  at node 2. Using KCL at node 2 gives the relationship for  $V_2$  as

$$\frac{V_2}{2} + \frac{V_2 - 8}{2} - 2 = 0$$

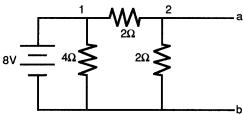
where currents leaving the node are positive. Note that  $V_2$ -8 is the voltage across the resistor between nodes 1 and 2 since the voltage at node 1 must be 8 volts. Solving for  $V_2$ ,  $V_2$ =6 volts. Using KVL across the  $2\Omega$  output resistor and the 4V voltage source we can get the voltage  $V_{ab}$  as  $V_{ab}$ = $V_2$ +4=6+4=10 Volts.

 $R_T$  is relatively easy to determine. Replacing all of the sources by their equivalent impedances, the voltage sources are replaced by shorts and the current source is replaced by an open. The  $4\Omega$  resistor is shorted out by the 8V voltage source leaving only two  $2\Omega$  resistors in parallel.  $R_T$  is

$$R_T = 2||2 = \frac{2 \times 2}{2 + 2} = 1\Omega$$
 The correct answer is (d).

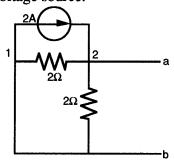
 $V_T$  could also be determined by superposition; however, there will be three components to  $V_T$  due to the fact that three sources are present. These contributions are shown below:

From the 8 volt source

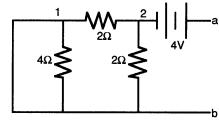


 $V_{ab}=+4$  volts

Redrawing the original circuit to explicitly show the  $2\Omega$  resistors in parallel as a result of the shorting out of the  $4\Omega$  resistor by the 8V voltage source.

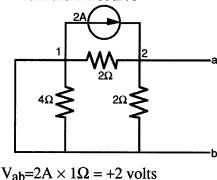


From the 4 volt source



 $V_{ab} = +4 \text{ volts}$ 

From the 2A source



The resulting  $V_{ab}$  is then the sum of all the voltage contributions, i.e.  $V_{ab}=4+4+2=10$  volts as before.

**CIRCUITS 12** This is the Wheatstone Bridge circuit and often appears on the exam.

The Norton equivalent at terminals a-b is closest to

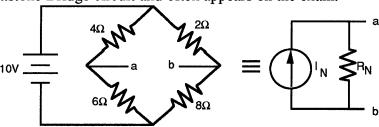
(a)  $I_N=0.2$  amps,  $R_N=4$   $\Omega$ 

(b)  $I_N=0.2$  amps,  $R_N=5$   $\Omega$ 

(c)  $I_N=-0.5$  amps,  $R_N=4$   $\Omega$ 

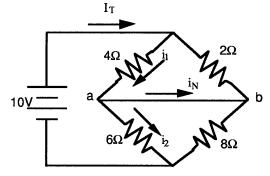
(d)  $I_N=0.5$  amps,  $R_N=5$   $\Omega$ 

(e)  $I_N=-0.5$  amps,  $R_N=2$   $\Omega$ 



## Solution:

The Norton current  $I_N$  is defined as the current between terminals a and b when terminals a and b are shorted together. The resulting circuit looks like a series combination of  $4\Omega || 2\Omega$  and  $6\Omega || 8\Omega$ .



The total current I<sub>T</sub> supplied by the 10 volt source is then

$$I_T = \frac{10 \text{ volts}}{\frac{4 \times 2}{4 + 2} + \frac{8 \times 6}{8 + 6}} = \frac{10 \text{ volts}}{\frac{8}{6}\Omega + \frac{48}{14}\Omega} = 2.1 \text{Amps}$$

Using the current divider relationship the current  $i_1$  through the  $4\Omega$  resistor and the current  $i_2$  through the  $6\Omega$  resistor can be calculated as

$$i_1 = 2.1 \text{ Amps} \times \frac{2}{4+2} = 0.7 \text{ Amps}$$

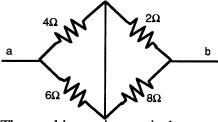
and

$$i_2 = 2.1 \text{ Amps} \times \frac{8}{6+8} = 1.2 \text{ Amps}$$

The Norton current IN can then be found by applying KCL to node a

$$i_N = i_1 - i_2 = 0.7 \text{ Amps} - 1.2 \text{ Amps} = -0.5 \text{ Amps}$$

 $R_N$  is relatively easy to determine. Replacing the voltage source by a short we are now facing the circuit shown below with a  $4\Omega || 6\Omega$  combination in series with the  $2\Omega || 8\Omega$  combination.



The resulting resistance is then

$$R_N = \frac{4 \times 6}{4 + 6} + \frac{8 \times 2}{8 + 2} = 4.0\Omega$$

The correct answer is (c).

 $I_N$  could also be determined by finding the Thevenin equivalent and converting it to a Norton equivalent. The  $4\Omega$  and  $6\Omega$  resistors form a voltage divider at terminal a. The voltage at terminal a is then

$$V_a = \frac{6}{4+6} (10 \text{ volts}) = 6 \text{ volts}$$

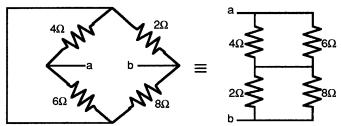
 $V_a = \frac{6}{4+6} (10 \text{ volts}) = 6 \text{ volts}$ The voltage at terminal b can be found in a similar manner

$$V_b = \frac{8}{2+8} (10 \text{ volts}) = 8 \text{ volts}$$

The Thevenin voltage is the voltage difference between a and b.

$$V_T = V_a - V_b = 6 - 8 = -2 \text{ volts}$$

 $V_T = V_a - V_b = 6 - 8 = -2$  volts The Thevenin resistance  $R_T$  is found by shorting the voltage source and computing the resistance between terminals a and b as shown below

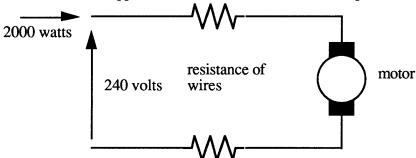


$$R_T = \frac{4 \times 6}{4 + 6} + \frac{2 \times 8}{2 + 8} = 2.4 + 1.6 = 4.0\Omega$$

Note that  $R_T = R_N$  and that  $V_T$  and  $I_N$  satisfy Ohm's Law

$$I_N = \frac{V_T}{R_T} = \frac{-2 \text{ volts}}{4\Omega} = -0.5 \text{ Amps}$$

**Problem 47-3** A 240 volt motor requiring 2000 watts is located 1 km from a power source. What minimum copper wire diameter is to be used if the power loss is to be kept less than 5%?



Several assumptions are used in this problem: (1) the voltage at the line input is 240 volts, not at the motor; (2) that the 2000 watts are required by the motor, not at the input.

The power loss due to the resistors is 0.05×2000=100 watts. The total power consumed by the circuit is then

$$P = VI = (240 \text{ volts}) I = 2100 \text{ watts}$$

Solving for I gives I=8.75 amps. We can now use this current to find the wire resistance.

$$P = I^2R = (8.75)^2R = 100$$
 watts

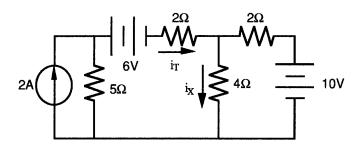
or  $R=1.30\dot{6}\Omega$ . Kemember that this is the total resistance of the wire. Calculating the wire resistance using the total wire distance of 2km we can solve for the diameter of the wire.

$$R = \frac{\rho l}{A} = \frac{\rho l}{\pi \left(\frac{D}{2}\right)^{2}} = \frac{\left(0.6788 \times 10^{-6} \frac{\Omega - in^{2}}{in}\right) \left(2km \times 3281 \frac{ft}{km} \times 12 \frac{in}{ft}\right)}{\pi \left(\frac{D}{2}\right)^{2}} = 1.306\Omega$$

or D=0.228 inches

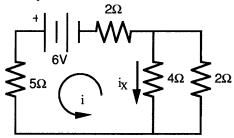
When solving for ix using superposition, the contribution due to the 6V source is

- (a) -0.24 amps
- (b) 0.24 amps
- (c) 0 amps
- (d) 0.72 amps
- (e) -0.72 amps



## Solution:

To find the contribution from the 6V source, we replace the 2 amp source by an open circuit and the 10 volt source by a short. Redrawing the circuit to show the 6V source circuit a little more clearly



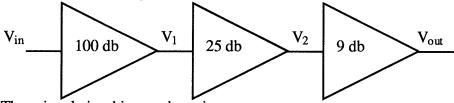
The total current i due to the 6V source is given as

$$i = \frac{6 \text{ volts}}{5 + 4||2 + 2} = \frac{6 \text{ volts}}{5 + \frac{4 \times 2}{4 + 2} + 2} = \frac{18}{25} = 0.72 \text{ amps}$$

The fraction of this current flowing through the  $4\Omega$  resistor is given by a current divider  $i_X = -\frac{2}{2+4} (0.72 \text{ amps}) = -0.24 \text{ amps}$ 

Note the use of the minus sign since I defined i to be in the opposite direction to  $i_X$ . The correct answer is (a).

**Problem 47-15** Three cascaded amplifier stages have amplifications of 100 db, 25db and 9db. What is the overall amplification?



The gain relationships can be written as

100 db = 20 log 
$$\left(\frac{V_1}{V_{in}}\right)$$
 = 20 log  $V_1$  - 20 log  $V_{in}$ 

25 db = 20 log 
$$\left(\frac{V_2}{V_1}\right)^{11}$$
 = 20 log V<sub>2</sub> - 20 log V<sub>1</sub>

9 db = 
$$20 \log \left( \frac{V_{\text{out}}^{(V_1)}}{V_2} \right) = 20 \log V_{\text{out}} - 20 \log V_2$$

and can be combined by adding the right and left hand sides of the above expressions

134 db = 
$$20 \log \left( \frac{V_{out}}{V_{in}} \right) = 20 \log V_{out} - 20 \log V_{in}$$

# 47.28 Transient analysis

# **Initial Conditions**

Before we can solve transient problems involving inductors and capacitors we must understand the initial conditions that apply to the differential equations:

Because no circuit can supply infinite power:

- (1) the <u>current</u> through an <u>inductor</u> cannot change instantaneously
- (2) the voltage across a capacitor cannot change instantaneously

These rules are the boundary conditions which apply to inductors and capacitors and, for purposes of writing time dependent expressions for voltage and current, can be written as:

For an inductor

i(0-)=i(0+)

where it is assumed that a switch has been opened or closed in the network at

For a capacitor

v(0-)=v(0+)

where it is assumed that a switch has been opened or closed in the network at

Basically, this means that for inductors the current is continuous, whereas for capacitors the voltage is continuous.

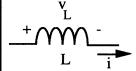
Preview (This material is in 48.11 and 48.12):

The voltage current relationship for a capacitor cannot be written without using integrals or derivatives.

Using the above definitions we can write "Ohm's Law" for a capacitor as

$$i_C = \frac{dq}{dt} = C\frac{dv}{dt}$$
or, in integral form, as

$$v(t) = v(t_0) + \frac{1}{C} \int_0^t i_C(t) dt$$



For the inductor, "Ohm's Law" is

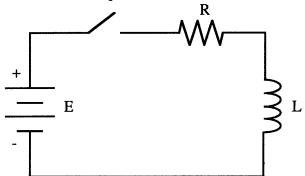
$$v_L = L \frac{di}{dt}$$

or, in integral form,

$$i(t) = i(t_0) + \frac{1}{L} \int_{0}^{t} v_L(t) dt$$

A transient is what occurs whenever you open or close a switch in an electrical network. The voltages and currents must quickly re-adjust themselves to the new network. The presence of capacitors and inductors in the network means that that the voltage and current readjustments occur according to the differential equations describing these circuit components.

Consider the simple series circuit shown below:



The question is what is the current in the circuit as a function of time for t≥0, the switch closes at t=0. This requires the use of differential equations. To describe this circuit begin with Kirchoff's voltage law

$$\sum_{} V_n \\ E - iR - L\frac{di}{dt} = 0$$
 This is a differential equation in i

$$L\frac{di}{dt} + iR = E$$

The homogeneous (or transient) solution comes from solving the equation with the right hand side of the equation set to zero.

$$L\frac{di}{dt} + iR = 0$$

 $\frac{dt}{dt} + Rt = 0$ The solution to this equation is an exponential of the form

$$i(t) = Ae^{kt}$$

where A and k are constants to be determined. Substituting this solution into the above differential equation we can find k

$$LAke^{kt} + Ae^{kt}R = 0$$

Dividing through by Aekt

$$Lk+R=0$$

or

$$k=-R/L$$

The constant A must come from the steady-state solution of the original differential equation. In the steady-state all derivatives are zero since nothing is changing. Therefore, the differential equation for this solution reduces to

or

$$i = \frac{E}{R}$$

 $i = \frac{E}{R}$  The resulting total solution is the sum of the steady-state and transient solutions

or

$$i(t) = \frac{E}{R} + Ae^{-\frac{R}{L}t}$$

To find A we must apply the boundary conditions on i, i.e. that

$$i(0-)=i(0+)$$
. Let  $i(0-)=i_0$ . At  $t=0+$ 

$$i_0 \approx \frac{E}{R} + A$$

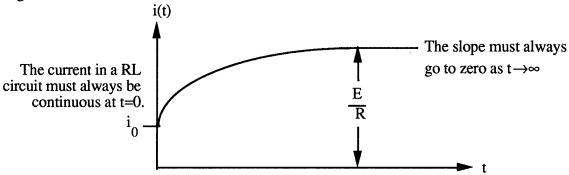
$$A = i_0 \cdot E$$

$$A = I_0 - \frac{L}{R}$$

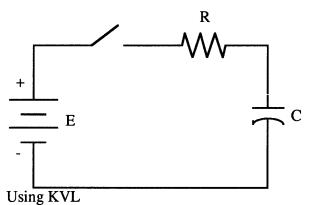
Therefore, the final time dependent expression for i(t) is

$$i(t) = \frac{E}{R} + \left(i_0 - \frac{E}{R}\right)e^{-\frac{R}{L}t}$$

 $i(t) = \frac{E}{R} + \left(i_0 - \frac{E}{R}\right)e^{-\frac{R}{L}t}$  The factor L/R is called the time constant of the circuit since it determines how rapidly the current changes in the circuit.



For a similar series RC circuit, the objective is to predict the voltage across the capacitor as a function of time given that the capacitor has a voltage  $v_0$  across it at time t=0.



$$E - iR - \frac{1}{C} \int_{0}^{t} i(t') dt' = 0$$

We cannot use i as the variable for capacitors - we must use voltage.

$$v_c(t) = \frac{1}{C} \int_{t_0}^t i(t') dt'$$

which is the integral form of

$$i = C \frac{dv_c}{dt}$$

The differential equation is then

$$E - R\left(C\frac{dv_c}{dt}\right) - v_c = 0$$

or, rewriting the equation in a more standard form,

$$RC\frac{dv_c}{dt} + v_c = E$$

As before this equation has a homogeneous and a steady-state solution.

For the homogeneous solution:

$$RC\frac{dv_c}{dt} + v_c = 0$$

Letting  $v_c(t)=Ae^{kt}$ 

$$RCAke^{kt} + Ae^{kt} = 0$$

or, solving for k,

$$k = \frac{-1}{RC}$$

The steady-state solution comes from setting all time derivatives to zero to give

$$v_c = E$$

The total solution is then

$$v_c(t) = v_{steady-state} + v_{transient}$$

$$v_c(t) = E + Ae^{-\frac{t}{RC}}$$

At 
$$t=0$$
,  $v_c(t)=v_O$  so

$$v_c(0) = v_0 = E + A$$

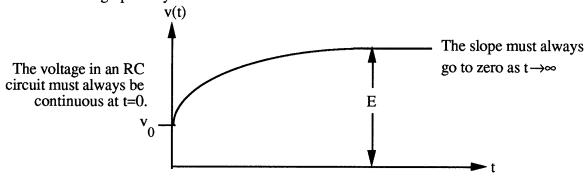
and

$$A = v_O - E$$

The final solution is then

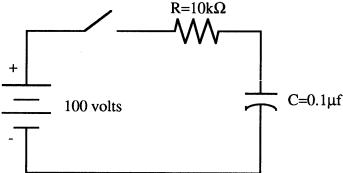
$$v_c(t) = (v_0 - E)e^{-\frac{t}{RC}} + E$$

which is shown graphically below



# Example:

Most of the time you do not need any fancy math as shown above to solve the problem. Simply remember the boundary conditions and the general form of the solutions.



Consider the above circuit. The time constant is simply computed as

$$\tau = RC = (10 \times 10^{-3})(0.1 \times 10^{-6}) = 10^{-3} \text{ seconds}$$

Assume  $v_0=0$  since it was not given. The problem is to determine v across the capacitor at  $t=5\times10^{-4}$  seconds. The general form of the solution was shown graphically above. Expressing this general solution mathematically

$$v(t) = E + (v_0-E)e^{-\frac{t}{RC}}$$
  
which for the given constants becomes

$$v(t) = 100 + (0-100)e^{-\frac{t}{10^{-3}}}$$

and, at t=5×10<sup>-4</sup> seconds, is  

$$v(5×10^{-4}) = 100 \left(1 - e^{-\frac{5×10^{-4}}{10^{-3}}}\right) = 100 \left(1 - e^{-\frac{1}{2}}\right)$$

$$v(5×10^{-4}) \approx 39.35 \text{ volts}$$

# Summary of important relationships for solving transient problems.

Component	Initial condition	<u>t=0</u> +	t=∞	τ	Ohm's Law
Capacitor	V(0-)=V(0+)	short	open	RC	$I = C \frac{dV}{dt}$
					or $V = \frac{1}{C} \int I dt$
Inductor	I(0-)=I(0+)	open	short	L/R	$V = L \frac{dI}{dt}$

The differential equation

$$A\frac{dI}{dt} + BI = C$$

has two solutions. One solution is the d.c. (also called steady state solution) which occurs when all the derivatives go to zero. This solution is simply I=C/B. The other solution is the transient solution (also called the homogeneous solution) and requires that C=0, i.e. solve

$$A\frac{dI}{dt} + BI = 0$$

This solution is always of the form  $I(t) = Ae^{mt}$  and can be solved for by simply substituting this expression for I(t) into

$$A\frac{dI}{dt} + BI = 0$$

Do problems 47-28, 47-29 (initial conditions)

The switch S closes at T=0. The complete response for i(t) for t>0

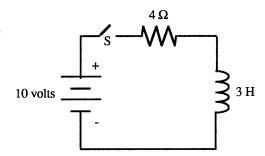
is

(a) 
$$2.5 + Ae^{-0.75t}$$

(c) 
$$2.5 + 2.5e^{-1.33t}$$

(d) 0

(e) 
$$2.5 - 2.5e^{-1.33t}$$



We use KVL to write the differential equation for the circuit using the correct expression for the impedance of the inductor.

$$-10 + 4i + 3\frac{di}{dt} = 0$$

Re-writing this in conventional form with the sources on the right hand side of the equation

$$3\frac{di}{dt} + 4i = 10$$

dt dt (or homogeneous) solution is obtained by setting the derivatives equal to zero or, in this case

$$4i = 10$$

The transient solution is always an exponential in form. Substituting i(t)=Aekt into the differential equation and setting the source (the right hand side of the equation) equal to zero we obtain

$$3\frac{di}{dt} + 4i = 0$$

$$3kAe^{kt} + 4Ae^{kt} = 0$$
  
 $3k+4=0$ 

$$3k+4=0$$

$$k = -4/3$$

The total solution is then  $i(t) = i_{transient} + i_{homogeneous} = Ae^{-1.33t} + 2.5$ 

The coefficient A is solved for by using the boundary condition that  $i(0^+)=i(0^-)=0$ .

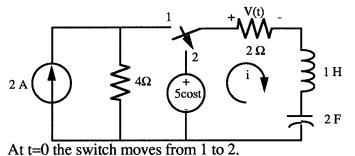
This requires that  $i(0^+) = A + 2.5 = 0$ , or that A=-2.5.

Then  $i(t) = 2.5 - 2.5e^{-1.33t}$  and the correct answer is (e).

# Circuits 32

The form of the transient part of V(t)for t>0 is

- (a)  $(A_1+A_2)e^{-0.5t}$
- (b)  $A_1\cos(0.5t) + A_2\sin(0.5t)$
- (c)  $A_1e^{-t}\cos(0.5t) + A_2e^{-t}\sin(0.5t)$
- (d)  $A_1e^{-1.71}t + A_2e^{-0.29}t$
- (e) 0



## Solution:

For t>0 the equation of the circuit is

$$\frac{di}{dt} + 2i + \frac{1}{2} \int_0^t i(\alpha) d\alpha + V_C(0^+) = 5\cos(t)$$

where  $V_c(0^+)$ , the initial voltage on the capacitor, is zero. Differentiating the above equation to remove the integral

$$\frac{d^2i}{dt^2} + 2\frac{di}{dt} + \frac{1}{2}i(t) = -5\sin(t)$$

 $\frac{d^2i}{dt^2} + 2\frac{di}{dt} + \frac{1}{2}i(t) = -5\sin(t)$ The left hand side of this equation describes the transient response. For the transient

$$\frac{\mathrm{d}^2 \mathrm{i}}{\mathrm{d}t^2} + 2\frac{\mathrm{d}\mathrm{i}}{\mathrm{d}t} + \frac{1}{2}\mathrm{i}(t) = 0$$

If we let i(t)=Aemt we get

$$m^2 A e^{mt} + 2m A e^{mt} + \frac{1}{2} A e^{mt} = 0$$

which reduces to the characteristic equation

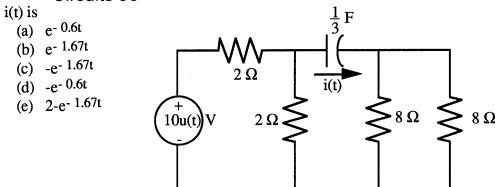
$$m^2 + 2m + 0.5 = 0$$

 $m^2 + 2m + 0.5 = 0$ This equation can be solved using the quadratic formula

$$m = \frac{-2 \pm \sqrt{(2)^2 - 4(1)(0.5)}}{2} = -1.71 \text{ and } -0.29$$

The only answer with these exponents is (d).

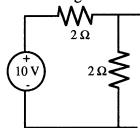
# Circuits 36



# Solution:

There are many ways to solve this problem but, perhaps, the easiest way is to Thevenize the left hand side of the circuit (the voltage source and the two  $2\Omega$  resistors) and replace the right hand side of the circuit (the two  $8\Omega$  resistors in parallel) by its equivalent resistance.

Thevenizing the left hand side of the circuit

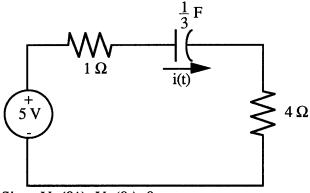


$$V_T = \frac{2}{2+2} \cdot 10 = 5 \text{ volts}$$
 and

$$R_{\rm T} = \frac{2 \times 2}{2+2} = 1 \Omega$$

NOTE: This is a good technique to use to get rid of current sources in problems.

The 8  $\Omega$  resistors in parallel can be replaced by a 4  $\Omega$  resistor. Redrawing the original circuit and replaceing the left hand side by its Thevenin equivalent and replacing the two  $8\Omega$  resistors by a single  $4\Omega$  resistance, we get the following circuit



Since 
$$V_C(0^+)=V_C(0^-)=0$$
  
 $i_C(0^+)=\frac{5 \text{ volts}}{1\Omega + 4\Omega}=1 \text{ amp}$ 

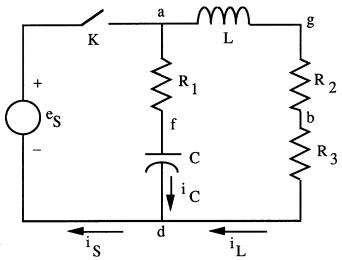
The time constant for the circuit can be directly computed as

$$\tau = RC = (5 \Omega)(\frac{1}{3} F) = 1.67$$
 seconds  
The solutions should be of the form

$$Ae^{-\frac{1}{1.67}} = Ae^{0.6t}$$

The correct answer is (a).

Example afternoon problem (this is actually tougher than most afternoon problems):



You are given that  $e_S(t)=E+E_1\sin(500t)+E_2\sin(1000t)$ , L=10 millihenries, C=200 microfarads,  $R_1$ =10 ohms,  $R_2$ =5.0 ohms and  $R_3$ =5.0 ohms in the above circuit.

For questions 11-14 assume that switch K is closed at t=0 and answer the questions for the instant immediately after the switch is closed, i.e. for time  $t=0^+$ .

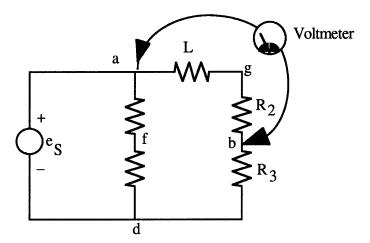
- 11. If E=30V,  $E_1=40V$  and  $E_2=20V$ , the current i<sub>C</sub> is most nearly
- (A) 0.0 amperes
- (B) 1.5 amperes
- (C) 2.8 amperes
- (D) 3.0 amperes
- (E) 6.0 amperes

This problem is most easily solved by recalling the initial conditions for capacitors which require that V(0-) = V(0+). The initial voltage on the capacitor is 0 volts so the voltage across the capacitor immediately after the switch is closed must also be 0 volts. The applied voltage  $e_S(t=0+) \approx 30$  since  $e_S(t=0+)$ 

The correct answer is (D).

- 12. If E=30V,  $E_1$ =40V and  $E_2$ =20V, the magnitude of the voltage between points a and b is most nearly
- (A) 5.0 volts
- (B) 7.5 volts
- (C) 15 volts
- (D) 22 volts
- (E) 30 volts

The voltage being referred to is across the series combination of the inductor and  $R_2$  as shown in the diagram below.



As in question #11 the voltage  $e_S(0^+) \approx 30$  volts,  $i_L(0^+) = i_L(0^-)$  since the current through inductors is continuous, and  $V_C(0^+) = V_C(0^-)$  since the voltage across capacitors is continuous. Since there is no current flow through L at  $t=0^+$  the inductor represents an open circuit. The potential at a is +30 volts; the potential at b is zero since it is connected to ground through  $R_3$  and no current is flowing through  $R_3$ . The potential  $v_{ab}$  is then 30 volts. The correct answer is (E)

13. If E,  $E_1$  and  $E_2$  are magnitudes such that  $i_C$  at  $t=0^+$  is 2.0 amperes, the rate of change of the voltage between points f and d is most nearly

- (A) 0.0 volts/second
- (B) 20 volts/second
- (C)  $5 \times 10^2$  volts/second
- (D)  $5 \times 10^3$  volts/second
- (E)  $1.0 \times 10^4$  volts/second

This question is a lot simpler than it sounds and is a direct application of of the definition of capcitance. By definition,

$$i_C = C \frac{dv}{dt}$$

dt which includes a direct expression of the rate of change of voltage. Evaluating this expression for  $t=0^+$ ,

$$i_{C}(0^{+}) = C \frac{dv}{dt} \Big|_{0^{+}}$$

which can be solved for the time rate of change of voltage at t=0+

$$\frac{d\mathbf{v}}{dt}\Big|_{t=0^+} = \frac{i_C(0^+)}{C} = \frac{2 \text{ Amperes}}{200 \times 10^{-6} \text{ Farads}} = 10^4 \frac{\text{volts}}{\text{second}}$$

The closest answer is (E).

14. If E,  $E_1$  and  $E_2$  are magnitudes such that the voltages between points a and g is 40 volts at  $t=0^+$ , the rate of change of  $i_L$  is most nearly

- (A) 0.0 amps/second
- (B) 4×10<sup>-2</sup> amps/second
- (C)  $4\times10^3$  amps/second
- (D) 2×10<sup>4</sup> amps/second
- (E) 4×10<sup>4</sup> amps/second

The solution of this problem is almost identical to that of problem #13 with the exception that the voltage expression must be that for an inductor, i.e.

$$V_L = L \frac{di}{dt}$$

Evaluating this expression at t=0+

$$\frac{di}{dt}\Big|_{t=0^+} = \frac{V_L(0^+)}{L} = \frac{40 \text{ volts}}{10 \times 10^{-3} \text{ Henrys}} = 4000 \frac{\text{amps}}{\text{second}}$$

The answer is (C).

- 15. If E=30V,  $E_1$ =40V and  $E_2$ =20V, the magnitude of the current i<sub>C</sub> is most nearly
- (A) 0.0 amperes
- (B) 1.5 amperes
- (C) 2.8 amperes
- (D) 3.0 amperes
- (E) 6.0 amperes
- $e_S(t)=E+E_1\sin(500t)+E_2\sin(1000t)$
- $i_C(0^-)=0$  and  $i_L(0^-)=0$  since there are no voltage sources for t<0. Using our rules for boundary conditions on inductors and capacitors  $i_L(0^+)=i_L(0^-)$  but  $i_C(0^+)\ne i_C(0^-)$ . At t=0+  $e_S(0^+)=30+40\sin(500\times0^+)+20\sin(1000\times0^+)\approx 30$  volts since the sine of a small number is approximately zero. Since  $V_C(0^+)=V_C(0^-)$  (remember that the voltage across a capacitor is continuous) the current  $i_C$  through  $R_1$  at t=0+ must then be given by  $i_C=30$ volts/10ohms = 3 amperes. The answer is (D).